

Core to earth's sustainable development



GEOTECHNICAL INVESTIGATION

Magatle Filling station Development

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Executive Summary

Nkhophele Holdings conducted a geotechnical investigation in June 2019 for the development of a filling station and a shopping centre at Magatle, Zebediela. The site investigation was aimed at evaluating engineering characteristics of near surface soils underlying the site.

Test pitting and laboratory testing were used to conduct the investigation. Nine (9) test pits were excavated which indicated that the surficial soils comprise residual material occurring as gravelly sand.

The investigation findings suggest that the soils encountered on the site may exhibit low potential expansiveness. The investigation findings further suggest that the site be classified as soil site class 2/C according to NHBRC Loading conditions. Overall the geotechnical investigation indicates that the site is developable albeit with precautionary measures.



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1. INTRODUCTION

Nkhophele Holdings was appointed in June 2019 by Executive Petroleum to conduct a geotechnical investigation for the development of a filling station and a shopping centre. Building plans, layout and structural loads for the proposed structures were not provided. This report presents the findings of a geotechnical investigation carried out on the site.

2. TERMS OF REFERENCE AND SCOPE OF WORK

The project entails the development of a filling station and shopping centre at Magatle, Zebediela in Limpopo. The site investigation was carried out in accordance with SAIEG, GFSH-2, TRH14 guidelines, and all NHBRC Home Building Manuals and included the following:

- Trial pitting, in-situ soil profiling and sampling;
- Laboratory testing;
- Site classification according to GFSH-2 Document and;
- Foundation Recommendations

3. SITE DESCRIPTION

3.1. LOCATION

The site is situated at Magatle, Zebediela, Limpopo, approximately 18 km south west of Lebowakgomo and directly opposite the Magatle Police Station (Figure 1). The site is rectangular in shape and covers an area of approximately 5 Ha. The centre coordinates of the site are 24°27'33.32"S, 29°24'49.65"E. The site is currently undeveloped and occasionally used as a show ground facility. Redundant electrical concrete poles and remnants on old building structures where observed on site.





Figure 1. Site Locality

3.2. CLIMATE

The average daily maximum and minimum temperatures of Zebediela are characterised by moderate fluctuations in seasonal temperature, with a high of 30°C in summer and a low of 6°C in winter. Precipitation in the study area occurs mainly in the summer, with the maximum rainfall experienced during November - January. The site is located in an area designated a weinert value less than 5 which suggests that chemical weathering is the dominant form of weathering.

3.3. TOPOGRAPHY AND DRAINAGE

The site was relatively flat with the elevation ranging between 903 m amsl (above mean sea level) and 908 m amsl. Erosional features such as dongas, and furrows were not observed on site. No watercourses traverse the site; however, the Nkumpi River is situated 200 m east of the site.

3.4. **G**EOLOGY

According to the 1:250 000 geological map sheet 2428 Nylstroom Geological Map Series (Figure 2), the investigated area is underlain by sedimentary rocks of the Karoo Sequence. The Karoo sequence in the Nylstroom area is made up of the volcanic rocks and sandstones of the Letaba Formation; red sandstone of the Clarens Formation; sandstone, mudstone, siltstone and shale of the Irrigasie Formation and shale, sandstone, conglomerate and coal beds of the Ecca Group. The development site is underlain by the red sandstone of the Clarens Formation.



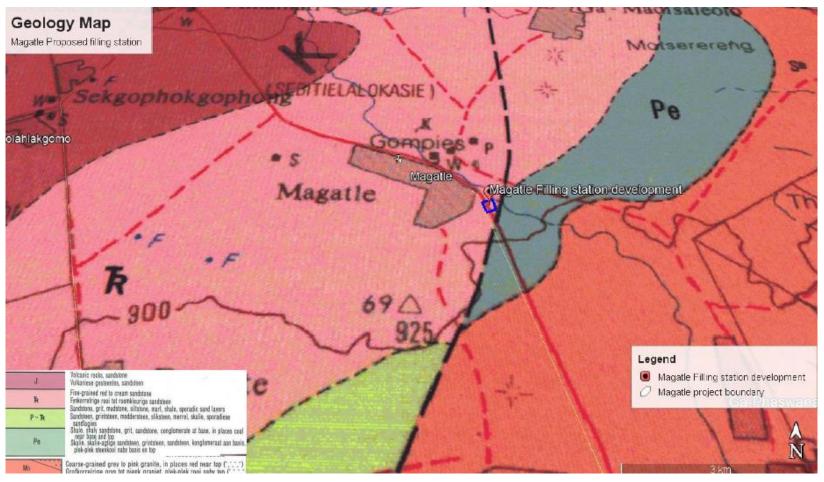


Figure 2. Site Geology

4. INVESTIGATION METHODOLOGY

The approach to this geotechnical investigation utilizes of a combination of literature review (Desktop Study) and field investigation. The literature review was conducted to assess the current state of the environment according to available literature resources.

4.1. AVAILABLE INFORMATION

- Topographic map of the Director of Surveys at a scale of 1: 50 000: Sheet 2429AD Zebediela (East);
- Geological Map of the GSO: Scale 1: 250 000 Sheet Geological series 2428 Nylstroom;
- Expansive Roadbed Treatment for Southern Africa: D J Weston (1980) 4th Int. Conf. on Expansive Soils, Vol. 1, Denver pp 339-360
- National Home Builders Registration Council: Home Builders Manual: Parts 1 and 2, Revision 1, February 1999;
- Technical Recommendations for Highways TRH14 Guidelines for Road Construction Materials by the National Institute for Transport and road research of the Council for Scientific and Industrial Research, (1985);
- SAICE's Guidelines for Urban Engineering Geological Investigations;
- Schwartz, K. (1985). Collapsible soils. The Civil Engineer in South Africa, July, p379-393 and;
- New, M., Lister, D., Hulme, M. and Makin, I., 2002: A high-resolution data set of surface climate over global land areas. Climate Research 21:1-25

4.2. FIELD INVESTIGATION

The following methodology was adopted for the field investigation:

Test pitting was conducted using a Tractor-Loader-Backhoe (TLB) and test pits were excavated to the maximum depth of 2.76 m. The test pits were logged by a registered engineering geologist according to MCCSSO method prescribed by Jennings et al. (1973). The trial pits were loosely backfilled after





profiling. The location of the test pits is indicated on the test pit locality plan available in Appendix A. Detailed soil profiles are attached in Appendix B.

5. FIELD INVESTIGATION RESULTS

5.1. TEST PITTING AND PROFILING

The field investigation was carried out by a Nkhophele holdings engineering geologist on the 27 June 2019. A total of nine (9) test pits were excavated across the site. The test pitting indicates that the site is underlain by a cover of transported colluvial material occurring as sand with sparse to abundant fragments of gravel. The material encountered in the test pits is described below and detailed test pit logs are available in Appendix B.

- **Transported** The transported horizon was encountered at depths between ground level and 1.02 m. the transported material is comprised of slightly moist, reddish-brown sandy-silt.
- **Pebble Marker** The transported horizon is underlain by a pebble marker comprising sandy-gravel with round gravel. The pebble marker was encountered at depths between 0.73 m and 1.60 m. The pebble marker is however absent in test pits ZBM 03, ZBM 04, and ZBM 09.
- Residual Sandstone The site is underlain chiefly by Slightly moist, Light brown to reddish-brown gravelly-sand from weathered residual sandstone. The residual sandstone was encountered at depths between 0.88 m and 2.76 m, however at ZBM 09, the sandstone was unweathered when excavated and the trial pit could only be excavated till 0.98 m. Trial pit ZBM 01, ZBM 04 and ZBM05 residual sandstone had cobbles.

5.2. LABORATORY TESTING

Representative soil samples were taken at specific positions from material encountered in the test pits. Ten (10) samples were collected and submitted to Civilab Civil Engineering Testing Laboratory for Foundation Indicator and California Bearing (CBR) testing to determine basic engineering characteristics including:

- Atterberg Limits (plastic limit, liquid limit and plasticity index);
- Potential Expansiveness;



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- Grading analysis and;
- MOD and CBR.

The laboratory tests were conducted to assist with the classification, description, and delineation of homogenous zones. The results of the foundation indicator, MOD and CBR tests are presented in Appendix C and are summarized in Table 1 and Table 2. The samples were taken from the test pit position denoted in the same manner.

Foundation Indicator – A total of six (6) foundation indicator samples were collected. Two (2) from the transported horizon, one (1) from the pebble marker horizon and three (3) from the residual sandstone horizon.

- Transported The samples collected indicate a Liquid Limit ranging from 21% to 23% with the Linear Shrinkage ranging between 4% and 5.5%. The samples indicate low to medium plasticity with the overall Plasticity Index ranging between 7% and 8%. Based on the clay content and plasticity, the soils underlying the site will exhibit low potential expansiveness.
- Pebble Marker The sample collected indicate a Liquid Limit of 26% with the Linear Shrinkage ranging between 4.5%. The samples indicate low plasticity with the overall Plasticity Index of 4%. Based on the clay content and plasticity, the soils underlying the site will exhibit low potential expansiveness.
- Residual Sandstone The samples collected indicate a Liquid Limit ranging from non-plastic to 31% with the Linear Shrinkage ranging between non-plastic and 5.5%. The samples indicate low to medium plasticity with the overall Plasticity Index ranging between non-plastic and 6%. Based on the clay content and plasticity, the soils underlying the site will exhibit low potential expansiveness.

Road Indicators and CBR - Four (4) sample were collected, one (1) transported and three (3) residual sandstone and submitted for California Bearing Ration (CBR) Testing.

Transported – The grading modulus of the sample was 0.9 with a Plasticity Index of 21%. The samples collected indicate a fair CBR with the value of 12% at 95% MOD AASHTO. The sample



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indicate a maximum swell of 0.1%. Based on the grading modulus, Atterberg limits and CBR soils underlying the site may be classified as G8.

Residual Sandstone – The grading modulus of the samples ranges between 1.5 and 2.1 with
the Plasticity Index ranging between non-plastic and 12%. The samples collected indicate a
good CBR with the values ranging between 43% and 82% at 95% MOD AASHTO. The sample
indicates a maximum swell ranging between 0.1% and 1.1%. Based on the grading modulus,
Atterberg limits and CBR soils underlying the site may be classified as ranging between G5 and
G6.



Table 1: Foundation Indicator Test Results

Sample	Description	Depth (m)	At	terberg L	imit	GM	Grading a		analysi	s (%)	USC	Potential
No.	Description	Depth (iii)	LL %	LS %	Overall Pl %	GIVI	Clay	Silt	Sand	Gravel	0	expansiveness
ZBM01	Transported	0.00-1.73	21	4	7	0.89	16	16	63	5	SC	Low
ZBM01	Residual sandstone	1.00-1.27	NP	NP	NP	1.98	3	7	44	46	SM	Low
ZBM02	Pebble marker	1.02-1.60	26	4.5	4	1.63	4	15	47	34	SC	Low
ZBM04	Residual sandstone	0.88- 2.50	31	5.5	6	1.52	6	16	52	26	SC	Low
ZBM08	Transported	0.00-0.85	23	5.5	8	0.99	17	14	67	2	SC	Low
ZBM08	Residual sandstone	1.01-2.40	30	5.5	4	2.11	3	11	26	60	GC	Low
LL :Liquid	Limit PI :Plasticity	Index LS :Lir	near Shrinka	age GM :	Grading Modul	us NP :N	Non-				USC	Unified Soil Classificat

NP :Non-Plastic

Table 2: CBR and MOD Test Results

			CBR @						Max.	0110	Max Dry	TRH14	
Sample No.	Description	Depth (m)	90%	93%	95%	98%	100%	GM	PI (%)	Swell (%)	OMC (%)	Densit y (kg/m³)	Classificatio n
ZBM01	Transported	0.00-1.73	11	12	12	13	14	0.9	21	0.1	9.2	2059	G8
ZBM01	Residual sandstone	1.00-1.27	38	60	82	131	179	2.0	NP	0.1	9.2	2028	G5
ZBM04	Residual sandstone	0.88- 2.50	26	36	45	63	79	1.5	12	0.4	13.2	1898	G6
ZBM08	Residual sandstone	1.01-2.40	131	38	43	51	58	2.1	12	1.1	11.4	1935	G6

PI :Plasticity Index

GM: Grading Modulus

OMC:Optimum Moisture Content

CBR :California Bearing Ratio

NP: Non- Plastic

6. **GEOTECHNICAL EVALUATION**

The objective of the investigation was to assess geotechnical properties of the surficial soils. The following geotechnical characteristics relevant to the development were assessed:

- **Expansive Potential**
- Collapse Potential
- Compressibility
- Groundwater
- Drainage & Erodibility
- Excavatability
- Slope Instability
- Subsidence
- Problematic soils

Table 3 gives the basis of the soil site classification that was applied during the investigation and Table 4 gives the geotechnical classification for urban development.

Table 3: Soil Site Classification (NHBRC Building Manual)

Geotechnical category and site class designation	Geotechnical characteristics					
Active soils (heave/shrink) - (H)	Expected range of total movement at surface:					
H	< 5 mm					
H1	5 – 15 mm					
H2	15 – 30 mm					
H3	> 30mm					
Compressible soils (S)	Expected range of total movement at surface:					
S	< 5 mm					
S1	5 – 15 mm					
S2	> 15 mm					
Collapsible Soils (C)	Expected range of total movement at surface:					
C	< 5 mm					
C1	5 – 10 mm					





C2	> 10 mm
Excavation – (R) r1 r2 r3	sub outcrop scattered outcrop and sub-outcrop outcrop, scattered outcrop and sub-outcrop
P – Problem soils	Dolomitic Areas, marshy areas, contaminated areas, abandoned borrow areas, land fill, mining subsidence and mine waste fill, shallow undermined areas, exploration pits or adits.
Inundation and seepage – (W)	Wet area, drainage line, seepage zone

Table 4: Geotechnical Classification for Urban Development (GFSH-2 Document)

Geotechnical Sub-Area	Definition
1	Areas recommended or favourable for development
2	Areas where development can be considered with certain precautionary measures.
3	Areas that are not recommended for development

6.1. EXPANSIVE SOILS

Active/expansive soils are defined as fine grained soils (generally with high clay content) that change in volume in response to the change in moisture content. These soils may increase in volume (heave/swell) upon wetting and decrease in volume (shrink) upon drying out. These soils are classified as (H) according to the SAICE site classes. Depending on the severity of the predicted movement, expansive soils can be classified as H, H1, H2 or H3 (Table 3).

The site is mainly underlain by sand and gravely sand and the laboratory results of all the samples analysed indicate low plasticity. Therefore, problems associated with heaving soils are not anticipated to occur on the site.



6.2. **COLLAPSIBLE SOILS**

Collapsible soils are defined as soils that have a potential for collapse and are commonly open-textured (e.g. honey comb and pinhole) with a high void ratio (Brink, 1985). These soils are typically silty sands, sands, sandy and gravelly soils commonly found in colluvial and aeolian sands. Soils which exhibit potentially collapsible characteristics are classified with the soil site class 'C' according to the SAICE site classification system (Table 3).

The soils encountered on the site typically sand and gravely sand with no visual open-textured structures such as voids and pinholes, which indicate collapse potential. The laboratory results indicate that the site is underlain by moderate sands with a moderate content of gravelly sands. From the site observations and laboratory testing the site is therefore classified with the soil site class C according to the SAICE site classification system.

6.3. **COMPRESSIBLE SOILS**

Compressible soils are soils in which the bulk volume of the soil may gradually decrease with time when subjected to an applied load. These soils typically comprise fine-grained soils such as clay, clayey sand and clayey silt with low plasticity, gravelly and sandy soil. According to the SAICE soil site class these soils are denoted as class 'S' and may vary (S, S1, S2) depending on the severity of the bulk volume change.

The site is generally underlain by silty and sandy gravel. The laboratory results indicate that the samples comprise low silt and clay content with low plasticity. Therefore, problems associated with compressible soils are not anticipated to occur on the site.

6.4. **G**ROUNDWATER

Groundwater may negatively affect structures founded on non-cohesive soil (sands and silt). When non-cohesive soils become saturated, the stiffness, vertical stress and effective confining stress are reduced resulting in lower bearing pressures of the soil. Furthermore, a shallow/perched groundwater table normally presents a problem of rising damp on structures. Therefore, appropriate remedial



Director: Ndivhuwo Ratshikhopha | Registration Number: 2015/432441/07 NK-0108 measures such as damp proofing needs to be incorporated in the construction of structures in areas where a shallow/ perched water table is anticipated. Various Pedogenic soils (ferricrete/calcrete and signs of ferruginisation/calcification) may indicate fluctuating or seasonally perched water table commonly caused by retarded vertical infiltration and percolation rates.

The fieldwork was conducted during the dry season and no groundwater or groundwater seepage was encountered during the field investigation.

6.5. DRAINAGE AND ERODIBILITY

The site is relatively flat and may promote the ponding of water and a river is located to the east of the site. Therefore, the site must be shaped to improve stormwater runoff and extensive stormwater management must be considered. All drainage boundaries near wet areas or drainage lines and floodlines must be confirmed by the relevant Competent Person (floodline specialist).

6.6. EXCAVATABILITY

Excavatability may be defined as the degree of difficulty at which the ground can be excavated. The test pits were excavated to depths ranging between 0.98m and 2.76m with no refusal. Excavatability problems may be anticipated within the vicinity of trial pit ZBM09 where shallow sandstone bedrock was encountered. Excavations for the proposed development are expected to utilise soft to intermediate excavation techniques for the removal of the soils underlying the site.

6.7. SLOPE INSTABILITY

The site slopes towards the east with a gradient of less than 6%. Therefore, slope related instability is not anticipated on the site.

6.8. SUBSIDENCE

No subsidence related problems are anticipated on the site

6.9. PROBLEMATIC SOILS

No problematic soils including dolomite or uncontrolled fill was encountered on the site.



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7. RECOMMENDATIONS

7.1. SOIL SITE CLASSIFICATION

The investigation findings indicate that soils with gravelly sand with low expansive potential underlie the site. Furthermore, based on field observations (geological, hydrogeological, and geomorphological) and laboratory soil testing of soil samples, the site can be classified as: **2/C**

7.2. FOUNDATION RECOMMENDATIONS

Founding conditions are favourable for the proposed development and conventional construction methods can be implemented. Depending on the design and loads to be applied, the following foundation recommendations are made:

Strip Footing

- The width of the strip footings must be at least 600 mm in the case of a foundation to a loadbearing or free-standing masonry wall or to a timber framed wall supporting a roof.
- Where any strip foundation is laid at more than one level, the higher portion of the foundation shall extend over the lower portion for a distance at least equal to the thickness of the foundation.

7.3. PRECAUTIONS

The following precautions may be considered during construction on the site:

- The site is relatively flat therefore extensive site drainage and plumbing/service precautions must be considered.
- · Structures to have damp proofing.
- The site must be graded to prevent ponding of storm water.
- 1.5 m apron around the structures to prevent water ingress under the immediate area or the foundation.
- Walkways and drive ways must be paved to allow easy access to the property during wet seasons.



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- Planting of grass/lawn on the stands may be considered to prevent erosion.
- Roads must be paved or tarred. Specialist advice must be sought for the installation of the roads.
- Care must be taken with foundation designs where foundations straddle different soil mediums such as rock and soil.

7.4. **PAVEMENT LAYERS**

The soils underlying the site exhibit good compaction characteristics for road building and pavement construction. According to the TRH14 guidelines, the residual sandstone soils underlying the site are classified as G5 and G6, therefore are suitable for subbase, selected layer and subgrade construction.

CONCLUSION 8.

This report documents the findings of a near surface geotechnical investigation conducted for the development of Magatle filling station and shopping centre. The investigation was carried out by means of test pitting and laboratory testing of collected samples. Based on the field investigation and laboratory testing the following conclusions can be drawn:

- The site is typically underlain by transported material, pebble marker and residual sandstone. The bedrock encountered on the site is dominantly red sandstone.
- Laboratory testing of the collected samples indicates that the underlying soil exhibits low potential expansiveness.
- The residual sandstone soils underlying the site are classified as G5 and G6, therefore are suitable for subbase, selected layer and subgrade construction.
- Groundwater seepage was not encountered in all of the test pits excavated.
- The investigated site is relatively flat lying which may lead to poor stormwater drainage. The site must be shaped to improve stormwater runoff and extensive management must be considered.



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Overall the geotechnical investigation findings suggest that the site is developable albeit with precautionary measures



Appendix A: Test Pit Location





Appendix B: Soil Logs



LEGEND Sheet 1 of 1

JOB NUMBER: NK108

· · ·		
000	GRAVEL	{SA02}
	SANDY	{SA05}
	SILT	{SA06}
	SILTY	{SA07}
	SANDSTONE	{SA11}
	DISTURBED SAMPLE	{SA38}

Name 🌘

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PROFILED BY: DATE:

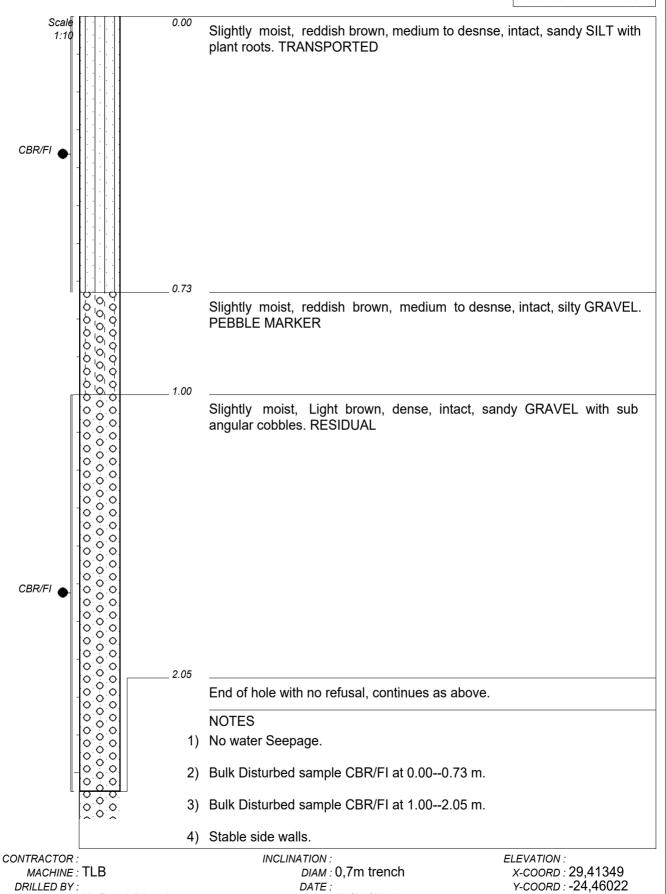
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JOB NUMBER: NK108

HOLE No: ZBM01



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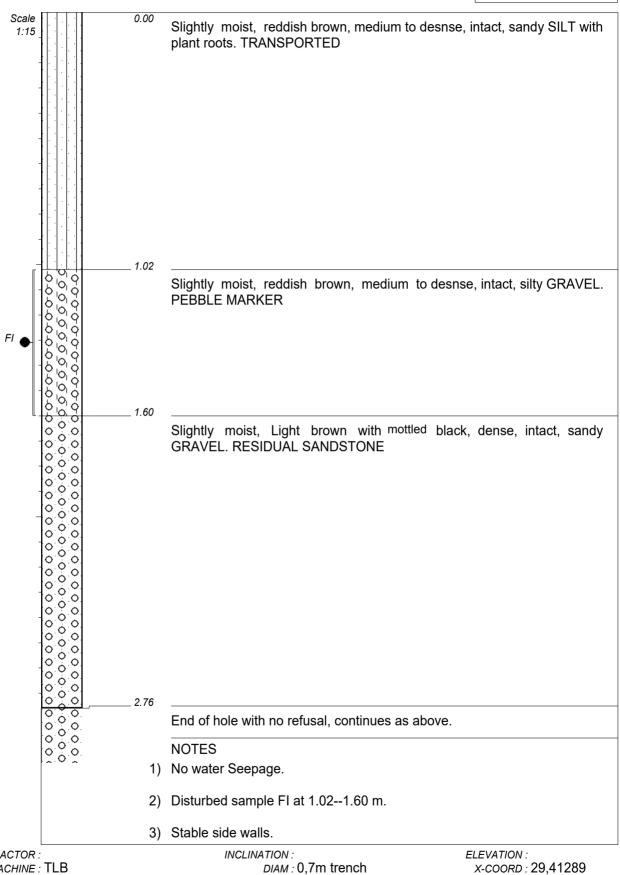
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HOLE No: ZBM02 Sheet 1 of 1

JOB NUMBER: NK108

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HOLE No: ZBM02



CONTRACTOR:

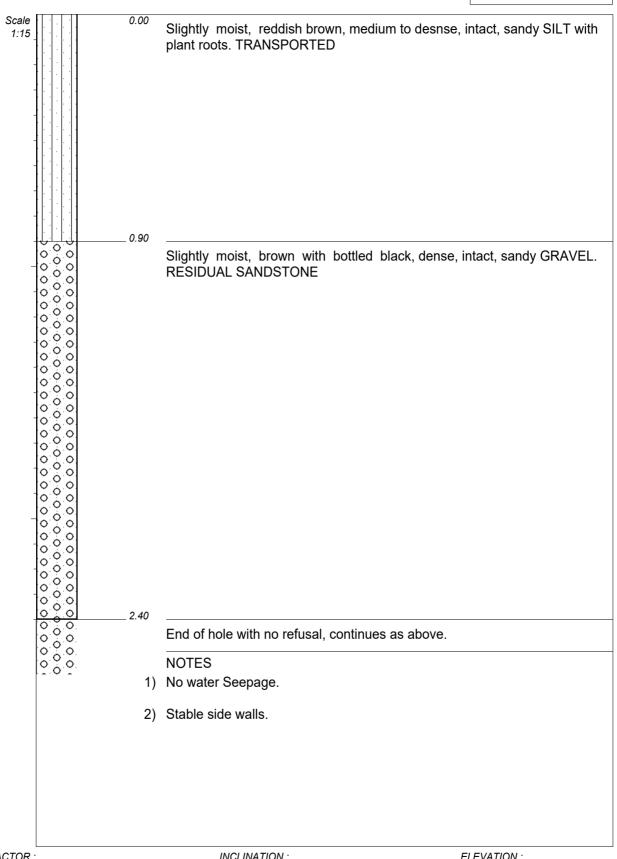
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HOLE No: ZBM03 Sheet 1 of 1

JOB NUMBER: NK108



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DATE: 27/06/2019

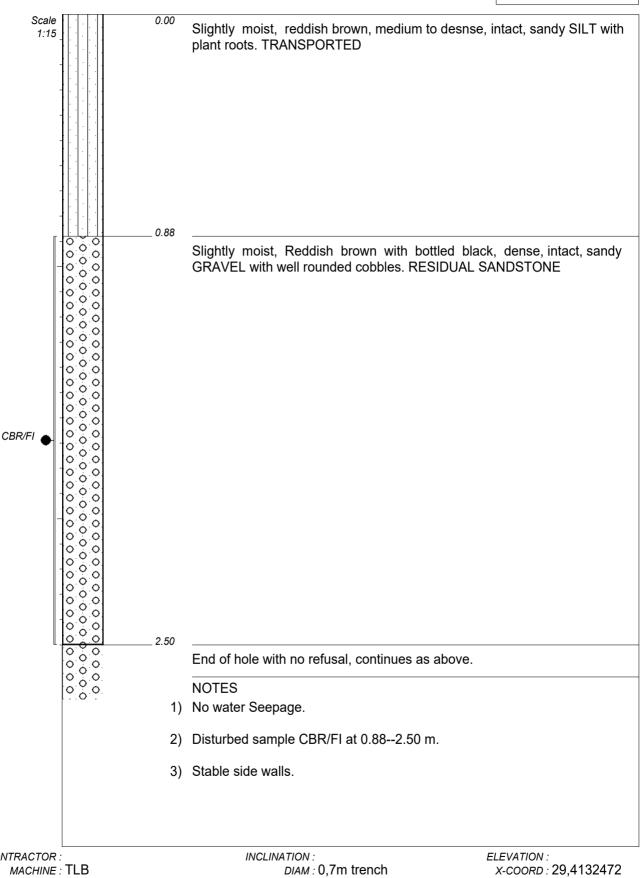
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HOLE No: ZBM04 Sheet 1 of 1

JOB NUMBER: NK108



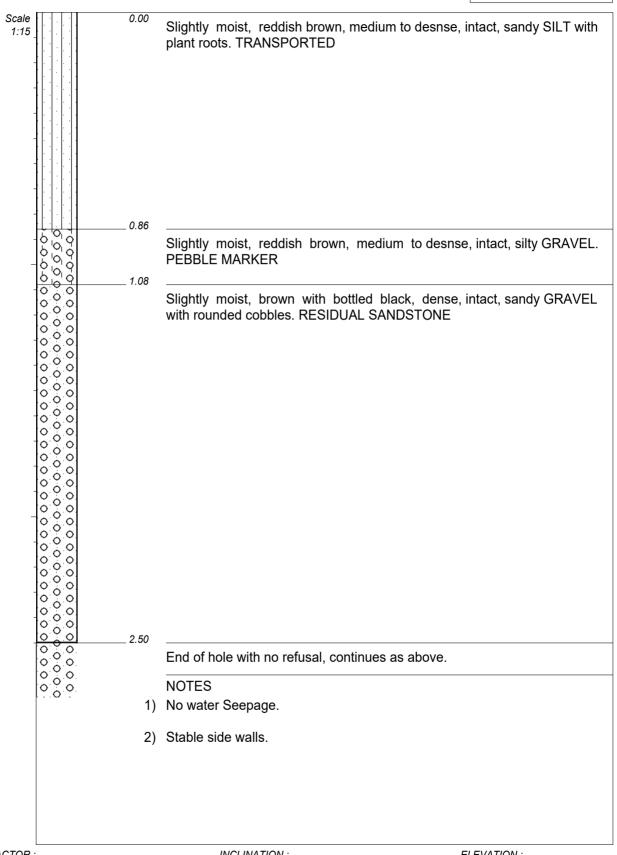
CONTRACTOR:

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HOLE No: ZBM05 Sheet 1 of 1

JOB NUMBER: NK108



CONTRACTOR:

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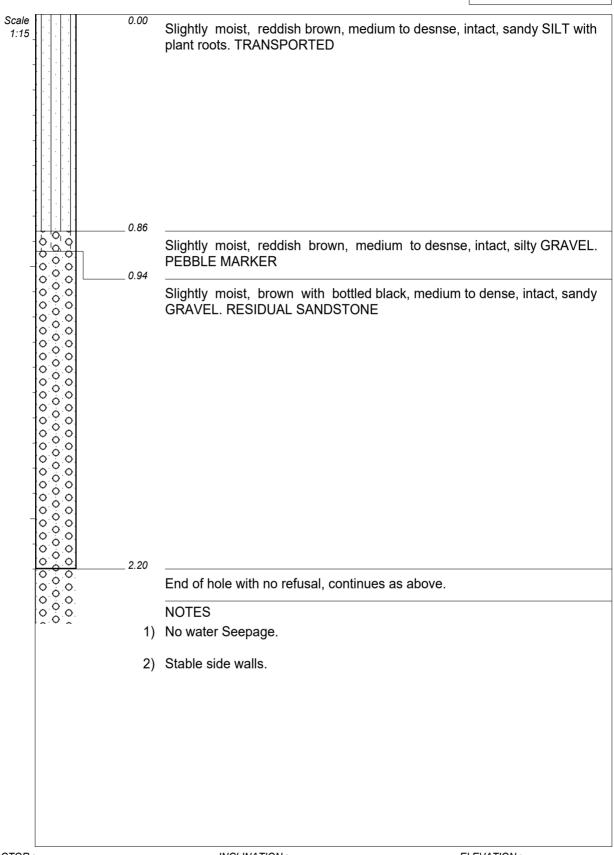
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HOLE No: ZBM06 Sheet 1 of 1

JOB NUMBER: NK108



CONTRACTOR:

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DIAM: 0,7m trench

DATE:

DATE: 27/06/2019

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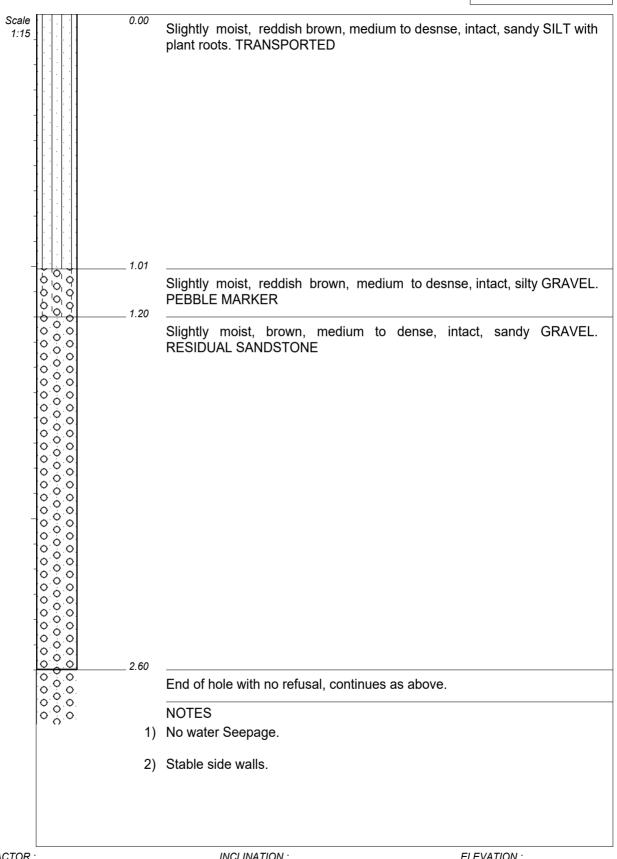
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ELEVATION:

X-COORD: 29,414081 *Y-COORD*: -24,460023

HOLE No: ZBM07 Sheet 1 of 1

JOB NUMBER: NK108



CONTRACTOR:

MACHINE: TLB

DRILLED BY:

PROFILED BY: N. Ratshikhopha

TYPE SET BY: N. Ratshikhopha SETUP FILE: STANDARD.SET INCLINATION:

DIAM: 0,7m trench

DATE:

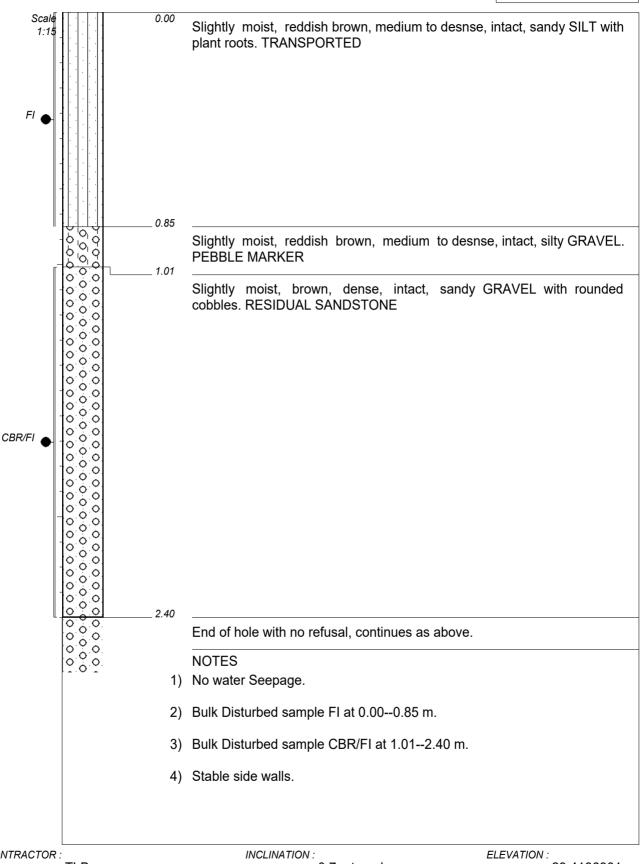
DATE: 27/06/2019

DATE: 11/07/2019 12:21 TEXT: ..ofile\ZBProfilesCopy.txt **ELEVATION**:

x-coord : 29,414565 Y-COORD: -24,459817

HOLE No: ZBM08 Sheet 1 of 1

JOB NUMBER: NK108



CONTRACTOR:

MACHINE: TLB DRILLED BY:

PROFILED BY: N. Ratshikhopha TYPE SET BY: N. Ratshikhopha SETUP FILE: STANDARD.SET

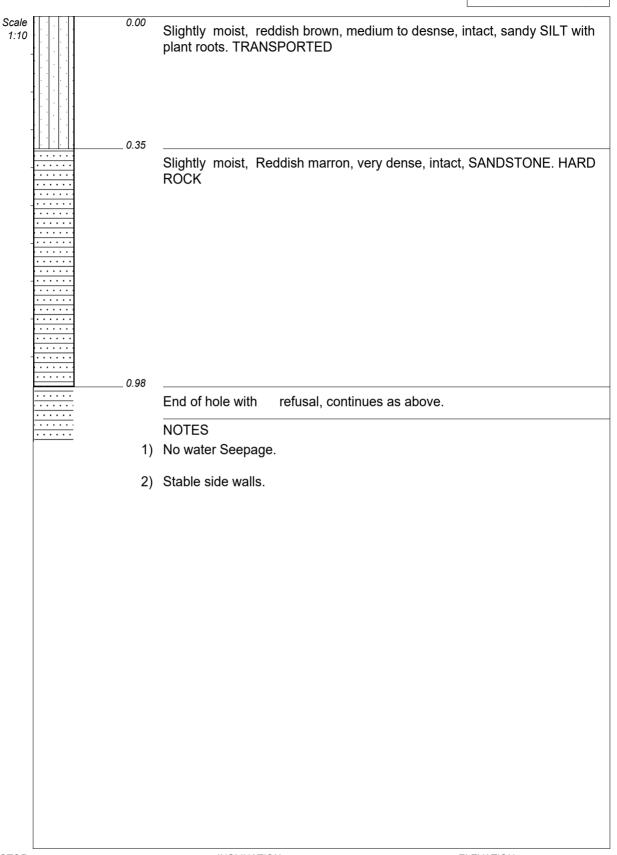
DIAM: 0,7m trench DATE: DATE: 27/06/2019

DATE: 11/07/2019 12:21 TEXT: ..ofile\ZBProfilesCopy.txt X-COORD: 29,4136301 Y-COORD: -24,4592438

Executive Petroleum Zebediela Magatle filling station and shops development

HOLE No: ZBM09 Sheet 1 of 1

JOB NUMBER: NK108



CONTRACTOR:

MACHINE : TLB DRILLED BY :

PROFILED BY: N. Ratshikhopha

TYPE SET BY: N. Ratshikhopha SETUP FILE: STANDARD.SET INCLINATION:

DIAM: 0,7m trench

DATE:

DATE: 27/06/2019

DATE: 11/07/2019 12:21 TEXT: ..ofile\ZBProfilesCopy.txt **ELEVATION**:

X-COORD: 29,4132472 Y-COORD: -24,458164

HOLE No: ZBM09

Appendix C: Laboratory Test Results





36 Fourth Street, Booysens Reserve, Johannesburg 2091 PO Box 82223, Southdale 2135

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Civil Engineering Testing Laboratories

Client : NKHOPHELE HOLDINGS (COO)

Address : UNIT 3, OXFORD OFFICE PARK

3 BAUHINIA STREET

HIGHVELD TECHNO PARK

Client Reference : Order No.

Order No. : Ndivhuwo

Attention :

E-mail

Facsimile : 086 565 5359

000 000 0009

ndivhuwo@nkhopheleh.co.za

Date Received : 01/07/2019 **Date Tested** : 01/07/2019

Date Tested : 01/07/2019 - 22/07/2019 **Date Reported** : 01/08/2019

Project : Zebedial Geotech

Project No.: 2019-B-968

Report Status

Final

Page : 1 of 10

Herewith please find the test report(s) pertaining to the above project. All tests were conducted in accordance with prescribed test method(s). Information herein consists of the following:

Test(s) conducted / Item(s) measured	Qty.	Test Method(s)	Authorized By**	Page(s
Moisture Density Relationship	4.000	SANS 3001 GR30	S Pullen	5-8
Atterberg Limits <0.425mm	6.000	SANS 3001 GR10	S Pullen/C Petersen	2-4, 9-10
Sieve Analysis 0.075mm	6.000	SANS 3001 GR1	S Pullen/B Mvubu	2-4, 9-10
California Bearing Ratio (CBR)	4.000	SANS 3001 GR40	S Pullen	9-10
Hydrometer Analysis	6.000	SANS 3001 GR3	S Pullen/B Mvubu	2-4
		us.		

Any test results contained in this report and marked with * in the table above are "not SANAS accredited" and are not included in the schedule of accreditation for this laboratory.

Any information contained in this test report pertain only to the areas and/or samples tested. Documents may only be reproduced or published in their full context.

While every care is taken to ensure that all tests are carried out in accordance with recognised standards, neither Civilab (Proprietary) Limited nor its employess shall be liable in any way whatsoever for any error made in the execution or reporting of tests or any erroneous conclusions drawn therefrom or for any consequences thereof.

All interpretations, Interpolations, Opinions and/or Classifications contained in this report falls outside our scope of accreditation.

The following parameters, where applicable, were excluded from the classification procedure: Chemical modifications, Additional fines, Fractured Faces, Soluble Salts, pH, Conductivity, Coarse Sand Ratio, Durability (COLTO: G4-G9).

The following parameters, where applicable, were assumed: Rock types were assumed to be of an Arenaceous nature with Siliceous cementing material

Unless otherwise requested or stated, all samples will be discarded after a period of 3 months.

This report is completely confidential between the parties (Civilab and Civilab's client) and shall not be disclosed to anybody else, unless agreed upon in writing or made publicly available by the client or required to make available by law.

Deviations in Test Methods:

**All results are authorized electronically by approved managers and/or technical signatories.

Technical Signatory:

S. Pollen

Signature:

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Civil Engineering Testing Laboratories

Ndivhuwo

01/07/2019

01/08/2019

01/07/2019 - 22/07/2019

Client : NKHOPHELE HOLDINGS (COO)

Address : UNIT 3, OXFORD OFFICE PARK

: 3 BAUHINIA STREET

HIGHVELD TECHNO PARK

Attention :

Facsimile : 086 565 5359

E-mail : ndivhuwo@nkhopheleh.co.za

Project : Zebedial Geotech

Project No.: 2019-B-968

Report Status : Final

Client Reference :

Order No.

Date Received

Date Reported

Date Tested

Page : 1 of 10

Herewith please find the test report(s) pertaining to the above project. All tests were conducted in accordance with prescribed test method(s). Information herein consists of the following:

Test(s) conducted / Item(s) measured	Qty.	Test Method(s)	Authorized By**	Page(s)
Moisture Density Relationship	4.000	SANS 3001 GR30	S Pullen	5-8
Atterberg Limits <0.425mm	6.000	SANS 3001 GR10	S Pullen/C Petersen	2-4, 9-10
Sieve Analysis 0.075mm	6.000	SANS 3001 GR1	S Pullen/B Mvubu	2-4, 9-10
California Bearing Ratio (CBR)	4.000	SANS 3001 GR40	S Pullen	9-10
Hydrometer Analysis	6.000	SANS 3001 GR3	S Pullen/B Mvubu	2-4

Any test results contained in this report and marked with * in the table above are "not SANAS accredited" and are not included in the schedule of accreditation for this laboratory.

Any information contained in this test report pertain only to the areas and/or samples tested. Documents may only be reproduced or published in their full context.

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All interpretations, Interpolations, Opinions and/or Classifications contained in this report falls outside our scope of accreditation.

The following parameters, where applicable, were excluded from the classification procedure: Chemical modifications, Additional fines, Fractured Faces, Soluble Salts, pH, Conductivity, Coarse Sand Ratio, Durability (COLTO: G4-G9).

The following parameters, where applicable, were assumed: Rock types were assumed to be of an Arenaceous nature with Siliceous cementing material.

Unless otherwise requested or stated, all samples will be discarded after a period of 3 months.

This report is completely confidential between the parties (Civilab and Civilab's client) and shall not be disclosed to anybody else, unless agreed upon in writing or made publicly available by the client or required to make available by law.

Deviations in	l est N	/lethods:

l echnical Signatory:	
Signature:	

^{**}All results are authorized electronically by approved managers and/or technical signatories.

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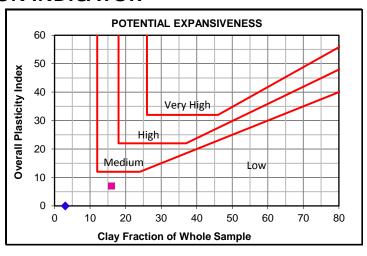


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Client NKHOPHELE HOLDINGS (COO) Date Reported: 01/08/2019 **Project** Zebedial Geotech 2019-B-968 Page No. Project No of 10

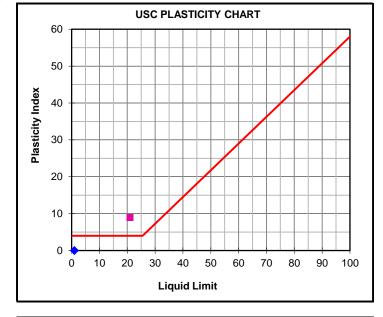
FOUNDATION INDICATOR

Laboratory Number	r	4	2 -
,	·I	7	2
Field Number		ZBM01	ZBM01
Client Reference			
Depth (m)		1.0-1.27	0.00-1.73
Position			
Coordinates	X Y		
Description			
Aditional Information	on		
Calcrete / Crushed			
Stabilizing Agent			
Maistura Contant & D.	olativa Done	itv	SANS 2001 CD20



Moisture Content & Relative Density		SANS 3001 GR	130
Moisture Content (%)			
Relative Density (S.G.)			
Sieve Analysis (Wet Prep)	SAN	IS 3001 GR1	

Sieve Analysis (Wet Prep)		SANS 3001 GR1	
	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
jii	37.5 mm	94	100
ass	28 mm	89	100
<u>a</u>	20 mm	81	100
ge	14 mm	71	100
nta	5 mm	61	99
Percentage Passing	2 mm	54	95
) er	1 mm	46	90
	0.425 mm	34	82
	0.250 mm	30	74
	0.150 mm	23	54
	0.075 mm	14	34
Grading Modulus		1.98	0.89



Hydrometer Analysis		SANS 3	001 GR3
Φ	0.060 mm	10	32
taç ng	0.040 mm	7	28
ssi	0.020 mm	6	24
Passing	0.006 mm	4	20
P –	0.002 mm	3	16
Gravel	%	46	5
Sand	%	44	63
Silt	%	7	16
Clay	%	3	16

Laboratory Number		1 🔷	2
Atterberg Limits -425µ		SANS 3001	GR10
Liquid Limit	%		21
Plasticity Index	%	NP	9
Linear Shrinkage	%		4.0
Overall PI	%		7
Classifications			

A-1-b(0)

A-2-4(0)

SC Unified (ASTM D2487) SM Weston Swell @ 1 kPa Note: An assumed S.G. may be used in Hydrometer Analysis calculations 100 80 Percentage Passing 60 40 20 0 0.001 0.01 0.1 100 Medium Medium Fine Coarse Fine Coarse Fine Medium Coarse Clay Silt Sand Gravel

HRB (AASHTO)

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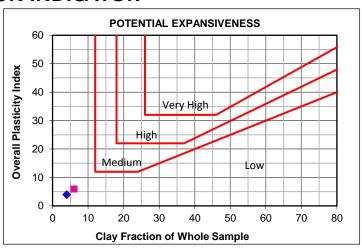


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FOUNDATION INDICATOR

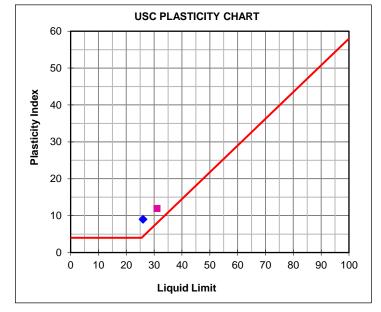
_			
Laboratory Number		3 •	4
Field Numbe	r	ZBM02	ZBM04
Client Refere	nce		
Depth (m)		1.02-1.60	0.88-2.50
Position			
Coordinates	X Y		
Description			
Aditional Information			
Calcrete / Crushed			
Stabilizing Ag	gent		
		•	



Moisture Content & Relative Density

Moisture Content (%) Relative Density (S.G.)

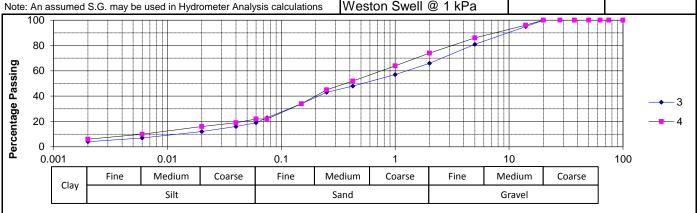
Relative Dell	, , ,		
Sieve Analysis (Wet Prep)		SANS 3	001 GR1
	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
CD.	50 mm	100	100
Passing	37.5 mm	100	100
388	28 mm	100	100
ä	20 mm	100	100
age	14 mm	95	96
nta	5 mm	81	86
Percentage	2 mm	66	74
)er	1 mm	57	64
	0.425 mm	48	52
	0.250 mm	43	45
	0.150 mm	34	34
	0.075 mm	23	22
Grading Mod	ulus	1.63	1.52



Hydrometer Analysis		001 GR3
0.060 mm	19	22
0.040 mm	16	19
0.020 mm	12	16
0.006 mm	7	10
0.002 mm	4	6
%	34	26
%	47	52
%	15	16
%	4	6
	0.060 mm 0.040 mm 0.020 mm 0.006 mm 0.002 mm % %	0.060 mm 19 0.040 mm 16 0.020 mm 12 0.006 mm 7 0.002 mm 4 % 34 % 47 % 15

Laboratory Number		3	4
Atterberg Limits -425µ		SANS 3001 C	3R10
Liquid Limit	%	26	31
Plasticity Index	%	9	12
Linear Shrinkage	%	4.5	5.5
Overall PI	%	4	6
	Class	ifications	

HRB (AASHTO) A-2-4(0) A-2-6(0) Unified (ASTM D2487) SC SC Weston Swell @ 1 kPa



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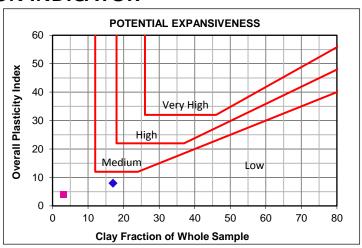


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FOUNDATION INDICATOR

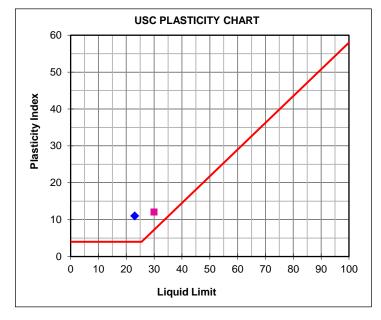
_			
Laboratory N	umber	5 🔷	6 -
Field Numbe	r	ZBM08	ZBM08
Client Refere	nce		
Depth (m)		0.00-0.85	1.01-2.40
Position			
Coordinates	X Y		
Description			
Aditional Info	rmation		
Calcrete / Cri	ushed		
Stabilizing Ag	gent		
		•	



Moisture Content & Relative Density

Moisture Content (%) Relative Density (S.G.)

Relative Deli	Sity (3.G.)		
Sieve Analysis (Wet Prep)		SANS 3	001 GR1
	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
CD.	50 mm	100	100
in	37.5 mm	100	91
Passing	28 mm	100	88
ä	20 mm	100	79
ge	14 mm	100	70
nta	5 mm	100	49
Percentage	2 mm	98	40
)eľ	1 mm	88	37
_	0.425 mm	72	34
	0.250 mm	62	30
	0.150 mm	45	24
	0.075 mm	31	15
Grading Mod	ulus	0.99	2.11



Hydrometer Ana	alysis	SANS 3	001 GR3
<u>e</u>	0.060 mm	31	14
taç ng	0.040 mm	28	11
ssi	0.020 mm	25	7
Percentage Passing	0.006 mm	19	4
	0.002 mm	17	3
Gravel	%	2	60
Sand	%	67	26
Silt	%	14	11
Clay	%	17	3

Laboratory Number		5	6			
Atterberg Limits -425µ		SANS 3001 (GR10			
Liquid Limit	%	23	30			
Plasticity Index	%	11	12			
Linear Shrinkage	%	5.5	5.5			
Overall PI	%	8	4			
Classifications						

A-2-6(0)

SC

A-2-6(0)

GC

Unified (ASTM D2487) Weston Swell @ 1 kPa Note: An assumed S.G. may be used in Hydrometer Analysis calculations 100 80 Percentage Passing 60 40 20 0 0.001 0.01 0.1 100 Medium Medium Fine Coarse Fine Coarse Fine Medium Coarse Clay Silt Sand Gravel

HRB (AASHTO)





1

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Date Reported: 01/08/2019

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Project: Zebedial Geotech Project No: 2019-B-968

MOISTURE DENSITY RELATIONSHIP

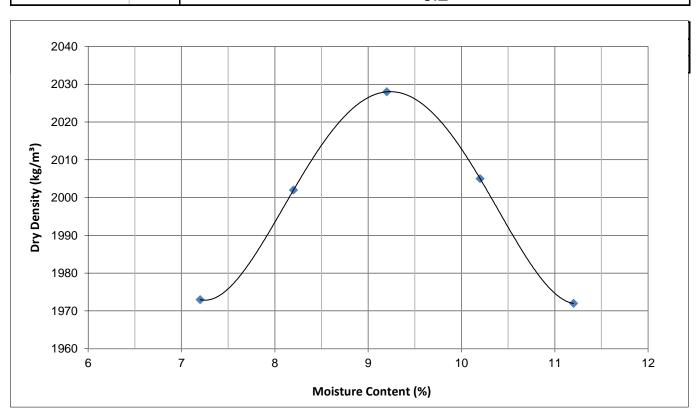
Laboratory Number		1
Field Number		ZBM01
Client Reference		
Depth (m)		1.0-1.27
Position		
Coordinates	Х	
Coordinates	Υ	
Description		
Additional Information	on	
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30

Compactive Effort: Modified AASHTO

Dry Density	kg/m³	1973	2002	2028	2005	1972	
Moisture Content	%	7.2	8.2	9.2	10.2	11.2	

Max. Dry Density	kg/m³	2028
Optimum Moisture	%	9.2



Zebedial Geotech

2019-B-968

NKHOPHELE HOLDINGS (COO)

PO Box 82223, Southdale 2135

Client : Project :

Project No:

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1

Civil Engineering Testing Laboratories

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MOISTURE DENSITY RELATIONSHIP

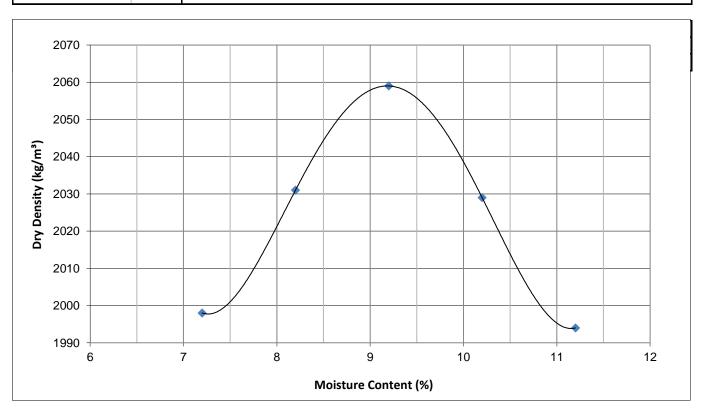
		-
Laboratory Number		2
Field Number		ZBM01
Client Reference		
Depth (m)		0.00-1.73
Position		
Coordinates	Х	
Coordinates	Υ	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30

Compactive Effort:	Modified AASHTO

Dry Density	kg/m³	1998	2031	2059	2029	1994	
Moisture Content	%	7.2	8.2	9.2	10.2	11.2	

Max. Dry Density	kg/m³	2059
Optimum Moisture	%	9.2



Client Project :

Project No:

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Zebedial Geotech

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NKHOPHELE HOLDINGS (COO)





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MOISTURE DENSITY RELATIONSHIP

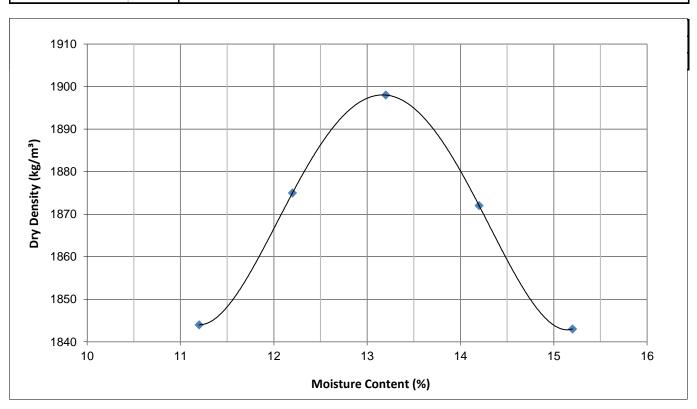
Laboratory Number		4		
Field Number		ZBM04		
Client Reference				
Depth (m)		0.88-2.50		
Position				
Coordinates	Х			
Coordinates	Y			
Description				
Additional Information				
Calcrete / Crushed				
Stabilizing Agent				

Maximum Dry Density & Optimum Moisture Content -**SANS 3001 GR30**

Compactive Effort:	Modified AASHTO

Dry Density	kg/m³	1844	1875	1898	1872	1843	
Moisture Content	%	11.2	12.2	13.2	14.2	15.2	

Max. Dry Density	kg/m³	1898
Optimum Moisture	%	13.2



Zebedial Geotech

2019-B-968

NKHOPHELE HOLDINGS (COO)

PO Box 82223, Southdale 2135

Client Project

Project No:

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1

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Page No. : 8 of 10

MOISTURE DENSITY RELATIONSHIP

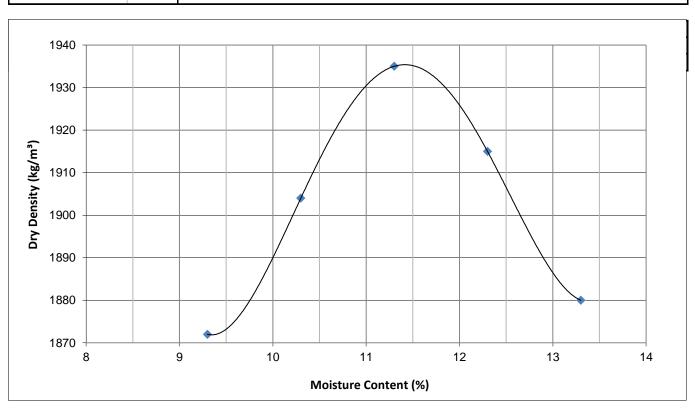
Laboratory Number		6
Field Number		ZBM08
Client Reference		
Depth (m)		1.01-2.40
Position		
0	Х	
Coordinates	Υ	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30

Compactive Effort: Modified AASHTO

Dry Density	kg/m³	1872	1904	1935	1915	1880	
Moisture Content	%	9.3	10.3	11.3	12.3	13.3	

Max. Dry Density	kg/m³	1935
Optimum Moisture	%	11.4



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Client : NKHOPHELE HOLDINGS (COO)

Project : Zebedial Geotech

Project No. : 2019-B-968

Date Received : 01/07/2019

Date Reported : 01/08/2019

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CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

O. 1211 O 1111 11 12 1111 11 11 11 11 11 11 11 11				
Laboratory No.		1 🔷	2	
Field Number		ZBM01	ZBM01	
Client Reference	е			
Depth (m)		1.0-1.27	0.00-1.73	
Position				
Coordinates	X Y			
Description				
Additional inforr	nation			
Calcrete/Crushe	ed			
Stabilizing Ager	nt			
0:			0.1110.0004.004	

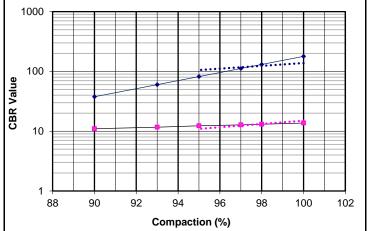
	,		
Sieve A	nalysis (Wet pr	eparation)	SANS 3001 GR1
	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
D	50 mm	100	100
Sin	37.5 mm	94	100
Passing	28 mm	89	100
	20 mm	81	100
tag	14 mm	71	100
Percentage	5 mm	61	99
erc	2 mm	54	95
₾.	1 mm	46	90
	0.425 mm	34	82
	0.250 mm	30	74
	0.150 mm	23	54
	0.075 mm	14	34
Grading M	odulus	2.0	0.9

Soil Mortar Analysis				
Coarse Sand	37	14		
Coarse Fine Sand	7	9		
Medium Fine Sand	13	21		
Fine Fine Sand	17	21		
Silt and Clay	26	36		
Attorborg Limits SANS 2001 CP10				

Atterberg Limits	SANS 3001 GR10		
Liquid Limit (%)		21	
Plasticity Index (%)	NP	9	
Linear Shrinkage (%)		4.0	

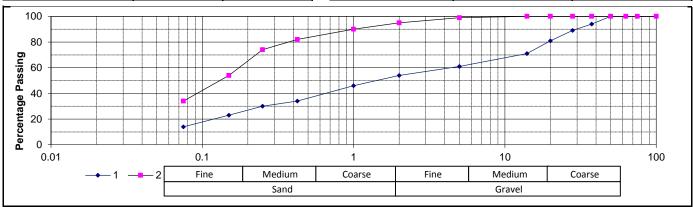
Laborator	y No.	1 🔷	2
Maximum Dry	/ Density & Op	timum Moisture Content	SANS 3001 GR30
MDD	kg/m ³	2028	2059
OMC	%	9.2	9.2
С	alifornia Bea	SANS 3001 GR40	

Camorna Bearing Ratio				OAIT	0 3001 0	71170	
		Comp	paction	Data			
Moisture %		9.3		9.3			
Dry Density	kg/m ³	2026	1926	1826	2064	1963	1859
Compaction	า %	100.0	95.1	90.1	100.0	95.1	90.1
Penetration Data							
	2.50 mm	138	106	38	15	11	11
CBR at	5.00 mm	171	118	43	16	12	10
	7.50 mm	175	115	46	16	13	9
Swell	%	0	0	0.1	0.1	0.2	0.2
Final Moisture (%)		11.0	13	14.8	10.9	12.5	16.5



Interpolated CBR Data					
	@	100%	0	179	14
	@	98%	노	131	13
l ~	@	97%	AASHT	112	13
CBR	@	95%		82	12
ľ	@	93%	Mod.	60	12
	@	90%	2	38	11
	@	SANS3001	Midpoint	121	13
Classifications					

Classifications					
HRB (AASHTO)	A-1-b(0)	A-2-4(0)			
COLTO	G5	G8			
TRH14	G5	G8			



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Client : NKHOPHELE HOLDINGS (COO)

Project : Zebedial Geotech

Project No. : 2019-B-968

Date Received : 01/07/2019

Date Reported : 01/08/2019

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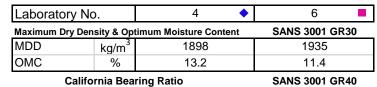
CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

Laboratory No.	4	6
Field Number	ZBM04	ZBM08
Client Reference		
Depth (m)	0.88-2.50	1.01-2.40
Position		
Coordinates X Y		
Description		
Additional information		
Calcrete/Crushed		
Stabilizing Agent		

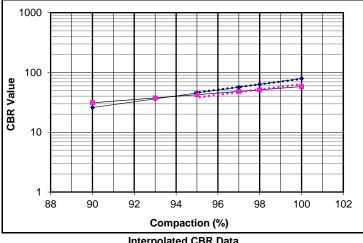
Sieve A	nalysis (Wet pr	eparation)	SANS 3001 GR1
	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
D	50 mm	100	100
Passing	37.5 mm	100	91
as	28 mm	100	88
e L	20 mm	100	79
tag	14 mm	96	70
en	5 mm	86	49
Percentage	2 mm	74	40
Δ.	1 mm	64	37
	0.425 mm	52	34
	0.250 mm	45	30
	0.150 mm	34	24
	0.075 mm	22	15
Grading M	lodulus	1.5	2.1

Soil Mortar Analysis				
Coarse Sand	30	15		
Coarse Fine Sand	10	9		
Medium Fine Sand	15	17		
Fine Fine Sand	16	22		
Silt and Clay	30	38		

Atterberg Limits	SANS 3001 GR10		
Liquid Limit (%)	31	30	
Plasticity Index (%)	12	12	
Linear Shrinkage (%)	5.5	5.5	



	Compaction Data						
Moisture	%		13.3		11.4		
Dry Density	kg/m ³	1903	1806	1712	1940	1843	1761
Compaction	า %	100.0	94.9	90.0	100.0	95.0	90.8
Penetration Data							
	2.50 mm	78	46	26	64	38	33
CBR at	5.00 mm	59	39	23	58	32	28
	7.50 mm	45	32	22	54	27	25
Swell	%	0.2	0.4	0.4	0.5	0.6	1.1
Final Moisture (%)		15.9	17.5	19.1	14.9	16.6	18.4



interpolated CBN Data					
	@	100%	0	79	58
	@	98%	4SHT(63	51
~	@	97%	AS	57	48
CBR	@	95%	₹.	45	43
	@	93%	Mod	36	38
	@	90%	2	26	31
	@	SANS3001	Midpoint	60	50

Classifications				
HRB (AASHTO)	A-2-6(0)	A-2-6(0)		
COLTO	G7	G7		
TRH14	G6	G6		

