

Flood Frequency Analysis: Rational Method Department of Water Affairs application

Flood Frequency Analysis: Rational Method

Project = BOKAMOSO ENEGY PV DEVELOPMENT
 Analysed by = CAS COETZER
 Name of river = BOKAMOSO ENEGY PV DEVELOPMENT
 Description of site = MATJESSPRUIT 145: LEEUDORINGSTAD
 Date = 5/30/2016
 Area of catchment = 3.622 km²
 Dolomitic area = 0.0 %
 Mean annual rainfall (MAR) = 520.00 mm
 Length of longest watercourse = 3.12 km
 Flow of water = Overland flow
 Height difference = 30.0 m
 Value of r for over land flow = Sparse grass (r=0,3)
 Rainfall region = Coastal
 Area distribution = Rural: 50 %, Urban: 50 %, Lakes: 0 %

Catchment description - Urban area (%)

Lawns		Residential and industry	Business		
Sandy, flat (<2%)	1	Houses	0	City centre	0
Sandy, steep (>7%)	9	Flats	0	Suburban	0
Heavy soil, flat (<2%)	1	Light industry	0	Streets	80
Heavy soil, steep (>7%)	9	Heavy industry	0	Maximum flood	0

Catchment description - Rural area (%)

Surface slopes	Permeability	Vegetation
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Lakes and pans	0	Very permeable	0	Thick bush & forests	0
Flat area	100	Permeable	0	Light bush & cultivated land	0
Hilly	0	Semi-permeable	55	Grasslands	55
Steep areas	0	Impermeable	45	Bare	45

Average slope	= 0.00962 m/m
Time of concentration	= 1.73 h
Run-off factor	
Rural - C1	= 0.431
Urban - C2	= 0.812
Lakes - C3	= 0.000
Combined - C	= 0.622

The HRU, Report 2/78, Depth-Duration-Frequency diagram was used to determine the point rainfall.

Return Period (years)	Time of concentration (hours)	Point rainfall (mm)	ARF (%)	Average intensity (mm/h)	Factor Ft	Runoff coefficient (%)	Peak flow (m ³ /s)
1:2	1.73	20.8	99.9	12.0	0.75	56.8	6.840
1:5	1.73	28.3	99.8	16.3	0.80	57.9	9.487
1:10	1.73	35.8	99.8	20.6	0.85	58.9	12.22
1:20	1.73	44.2	99.7	25.4	0.90	60.0	15.36
1:50	1.73	57.4	99.7	33.1	0.95	61.1	20.31
1:100	1.73	70.7	99.6	40.6	1.00	62.2	25.42

Run-off coefficient percentage includes adjustment saturation factors (Ft) for steep and impermeable catchments

Flood Frequency Analysis: Alternative Rational Method

Project = BOKAMOSO ENEGY PV DEVELOPMENT
Analysed by = CAS COETZER
Name of river = BOKAMOSO ENEGY PV DEVELOPMENT
Description of site = MATJESSPRUIT 145: LEEUDORINGSTAD
Date = 5/30/2016
Area of catchment = 3.622 km²
Dolomitic area = 0.0 %
Length of longest watercourse = 3.12 km
Flow of water = Overland flow
Height difference = 30.0 m
Value of r for over land flow = Sparse grass (r=0,3)
Area distribution = Rural: 50 %, Urban: 50 %, Lakes: 0 %

Catchment description - Urban area (%)

Lawns	Residential and industry	Business
Sandy, flat (<2%)	1 Houses	0 City centre
Sandy, steep (>7%)	9 Flats	0 Suburban
Heavy soil, flat (<2%)	1 Light industry	0 Streets
Heavy soil, steep (>7%)	9 Heavy industry	0 Maximum flood

Catchment description - Rural area (%)

Surface slopes	Permeability	Vegetation
Lakes and pans	0 Very permeable	0 Thick bush & forests
Flat area	100 Permeable	0 Light bush & cultivated land
Hilly	0 Semi-permeable	55 Grasslands
Steep areas	0 Impermeable	45 Bare

Days on which thunder was heard = 60 days/year
Weather Services station number = 399241
Weather Services station location = LEEUKOP

Mean annual precipitation (MAP)	= 520 mm						
Duration	2	5	10	20	50	100	200
1 day	54	73	88	103	125	143	163
2 days	67	95	116	138	170	198	228
3 days	74	105	128	153	190	220	253
7 days	95	139	173	210	263	308	358

The modified recalibrated Hershfield relationship was used to determine point rainfall.

Average slope	= 0.00962 m/m
Time of concentration	= 1.73 h
Run-off factor	
Rural - C1	= 0.431
Urban - C2	= 0.812
Lakes - C3	= 0.000
Combined - C	= 0.622

Return period (years)	Time of concentration (hours)	Point rainfall (mm)	ARF (%)	Average intensity (mm/h)	Factor Ft	Runoff coefficient (%)	Peak flow (m ³ /s)
1:2	1.73	31.00	100.0	17.89	0.75	56.8	10.22
1:5	1.73	52.29	100.0	30.19	0.80	57.9	17.57
1:10	1.73	68.40	100.0	39.49	0.85	58.9	23.41
1:20	1.73	84.51	100.0	48.79	0.90	60.0	29.45
1:50	1.73	105.80	100.0	61.08	0.95	61.1	37.54
1:100	1.73	121.91	100.0	70.38	1.00	62.2	44.01
1:200	1.73	138.02	100.0	79.68	1.00	62.2	49.83

Run-off coefficient percentage includes adjustment saturation factors (Ft) for steep and impermeable catchments

Flood frequency analysis: Standard Design Flood method

Project name	= BOKAMOSO ENEGY PV DEVELOPMENT
Analysed by	= CAS COETZER
Name of river	= BOKAMOSO ENEGY PV DEVELOPMENT
Description of site	= MATJESSPRUIT 145: LEEUDORINGSTAD
Date	= 5/30/2016
Catchment characteristics:	
Area of catchment	= 3.622 km ²
Length of longest watercourse	= 3.12 km
1085 height difference	= 30 m
Average slope	= 0.0128 m/m
Drainage basin characteristics:	
Drainage basin number	= 7
Mean annual daily max rain	= 49 mm
Days on which thunder was heard	= 39 days
Runoff coefficient C2	= 15 %
Runoff coefficient C100	= 60 %
Basin mean annual precipitation	= 510 mm
Basin mean annual evaporation	= 1700 mm
Basin evaporation index MAE/MAP	= 3.33

RAINFALL DATA

The rainfall data in the table below are derived from two sources. The daily rainfall is from the Department of Water Affairs's publication TR102 for the representative site. The modified Hershfield equation is used for durations up to four hours. Linear interpolation is used for values between 4 hours and one day.

Weather Services station ex TR102 = 328726 @ OLIVINE

Point mean annual precipitation = 510 mm

Dur:	RP =2	5	10	20	50	100	200
.25 h	14	24	32	39	49	57	64
.50 h	19	32	41	51	64	74	84
1 h	23	39	51	63	79	91	103
2 h	27	46	61	75	94	108	122
4 h	32	54	70	87	109	125	142
1 day	49	68	82	96	118	137	157
2 days	62	87	107	128	158	184	213
3 days	68	94	115	136	167	193	221
7 days	84	118	144	172	211	243	279

CAUTION. The time of concentration is less than one hour.

Runoff coefficients C2 = 15 % C100 = 60 %

Return period (years)	Time of concentration (hours)	Point precipitation (mm)	ARF (%)	Catchment precipitation (mm)	Runoff coefficient (%)	Peak flow (m ³ /s)
1:2	0.85	22.1	100.0	22.1	15.0	3.923
1:5	0.85	37.4	100.0	37.4	31.2	13.78
1:10	0.85	48.9	100.0	48.9	39.7	22.92
1:20	0.85	60.4	100.0	60.4	46.7	33.28
1:50	0.85	75.6	100.0	75.6	54.6	48.74
1:100	0.85	87.1	100.0	87.1	60.0	61.72
1:200	0.85	98.6	100.0	98.6	64.8	75.50

Empirical methods Midgley and Pitman as well as Kovács Method

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 Description of site = MATJESSPRUIT 145: LEEUDORINGSTAD
 Date = 5/30/2016

 Area of catchment = 3.622 km²
 Length of longest watercourse = 3.12 km
 Height difference along equal-area slope = 25.0 m
 Distance to catchment centroid = 1.6 km
 Dolomitic area = 0.0 %
 Mean annual rainfall = 520.0 mm
 Veld type = 1
 Kovács region = K4 (K = 4.6)
 Catchment parameter with regard to
 reaction time = 0.065

 Peak discharges by means of an empirical method developed by Midgley and Pitman

Return period (years)	KT constant	Peak flow (m ³ /s)
1:10	0.17	4.175
1:20	0.23	5.649
1:50	0.32	7.859
1:100	0.40	9.824

This RMF calculation includes a transition zone adjustment in the case of small catchments.

Regional maximum flood: 163.1 m³/s

Kovács Method

Q50 (RMF) : 67.84 m³/s (based on QT/QRMF relationship for **Kovács** regions)
Q100 (RMF) : 85.45 m³/s (based on QT/QRMF relationship for Kovács regions)
Q200 (RMF) : 102.58 m³/s (based on QT/QRMF relationship for Kovács regions)

The following equivalent maxima make no transition zone adjustments for small catchments.

Equivalent southern African maximum

K-factor 5.6: 532 m³/s

Equivalent world maxima

K-factor 6.0: 1056 m³/s

K-factor 6.3: 1765 m³/s

HERBST ALGORITHM DEVELOPED AT THE DEPARTMENT OF WATER AFFAIRS

$$Q_T = C_{\text{HERBST}} A^{0.46} P^{0.93} (1 + (K_T * C_V) / 100)$$

With:

C_{HERBST} = Coefficient of variation

A = Catchment area in km²

P = Mean annual precipitation

K_T = Frequency factor

For this situation:

Coefficient of variation	=	170.1
Catchment area	=	3.62 km ²
Mean annual precipitatio	=	520 mm
Frequency factor	=	4.3
Recurrence interval	=	100 year

Q_T : 67 m³/s

**HRU ALGORITHM DEVELOPED AT THE
THE WITS UNIVERSITY**

$$Q_T = 0,0377 K_T P A^{0,8} (S^{0,5} / (L L_c))^{0,2}$$

With:

K_T = Constant dependant on veld zone and T

A = Catchment area in km^2

P = Mean annual precipitation mm

S = Slope of the longest water course in m/m

L = Length of the longest stream in km

L_c = Distance to the centroid of the catchment in km

For this situation:

$$K_T = 1.200$$

$$A = 3.62 \text{ km}^2$$

$$P = 520 \text{ mm}$$

$$S = 0.0096$$

$$L = 3.12 \text{ km}$$

$$L_c = 3.6 \text{ km}$$

$$\text{Recurrence interval} = 100 \text{ year}$$

$$Q_T = 26 \text{ m}^3/\text{s}$$

**TEN NOORT STEPHENSON ALGORITHM DEVELOPED AT
WITS UNIVERSITY**

$$Q_T = (a_3P + b_3)T^{-b_2}A^{b_1}$$

With:

T = Recurrence interval in years

A = Catchment area in km²

P = Mean annual precipitation mm

b₁ = Coefficient dependant on veld zone, region and P

b₂ = Coefficient dependant on veld zone, region and P

b₃ = Coefficient dependant on veld zone, region and P

a₃ = Coefficient dependant on veld zone, region and P

For this situation:

T = 100 year

A = 3.62 km²

P = 520 mm

a₃ = 0.0012

b₁ = 0.69

b₂ = 0.49

b₃ = -0.18

Q_T = 19 m³/s

UNIT HYDROGRAPH METHOD

$$Q = Q_p \times d_e \times F_m = \text{Peak flood in m}^3/\text{s}$$

With:

$$Q_p = \text{Peak flood of the 1 hour synthetic hydrograph} \\ = K_U \times (A / T_L)$$

$$A = \text{Catchment area in km}^2$$

$$T_L = C_T [L \times L_C / (S^{0.5})]^{0.36} = \text{Basin lag in hour}$$

$$C_T = \text{Constant depending on the sone}$$

$$L = \text{Length of the longest stream in km}$$

$$L_C = \text{Distance to catchment centroid in km}$$

$$S = \text{Average slope along longest stream}$$

$$P = \text{Mean annual precipitation}$$

$$K_U = \text{Constant depending on the sone}$$

$d_e = \text{Percentage of storm run-off} \times d_g$

$d_g = d \times a$ in mm

$d =$ Design rainfall depth in mm

$a =$ Area reduction factor

$i =$ Rainfall intensity mm/hour

and,

$F_m = \text{Highest ordinate obtained with the S-curve transformation}$

For this situation:

A	=	3.62 km ²
T _L	=	1.76 hour
C _T	=	0.32
L	=	3.12 km
L _C	=	3.6 km
S	=	0.0096 m/m
P	=	520 mm
K _U	=	0.386
d _g	=	90 mm
d	=	55.8 mm
a	=	1
i	=	94.508 mm/hour
F _m	=	1

$$T = 100 \text{ year}$$

$$Q_p = 0.7923 \text{ m}^3/\text{s}$$

$$d_e = 55.8 \text{ mm}$$

$$Q = 44.21 \text{ m}^3/\text{s}$$