

EXXARO COAL CENTRAL

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KALABASFONTEIN PROJECT, FORZANDO COMPLEX: GEOTECHNICAL RISK ASSESSMENT

1. Introduction.

Exxaro Coal Central (ECC) holds a prospecting right to the Kalabasfontein area. As part of the Mining Right Application an Environmental Impact Assessment (EIA) must be conducted / completed. The assessment must consider the impact mining activities will have on the integrity of the environment or surface structures.

Several features occur on the surface area within the Kalabasfontein Reserve Area that needs to be protected. The features include dwellings, provincial roads, wetlands, streams and farmhouses. These features will either be undermined, or mining will occur within 100 m of them.

ECC plans to exploit the No.4 Seam reserves in this area. The reserves will be exploited through underground mining methods with mining heights (total seam extraction) expected to range from 2.1 m – 2.7. Mining heights more than 2.7 m may be encountered in localized zones. The depth of mining in the reserve area will range between 29.0 m and 117.0 m below ground surface.

This report details the geotechnical methodology that will be followed in the Mine Design Process to ensure that mining has no impact on the stability or integrity of the surface

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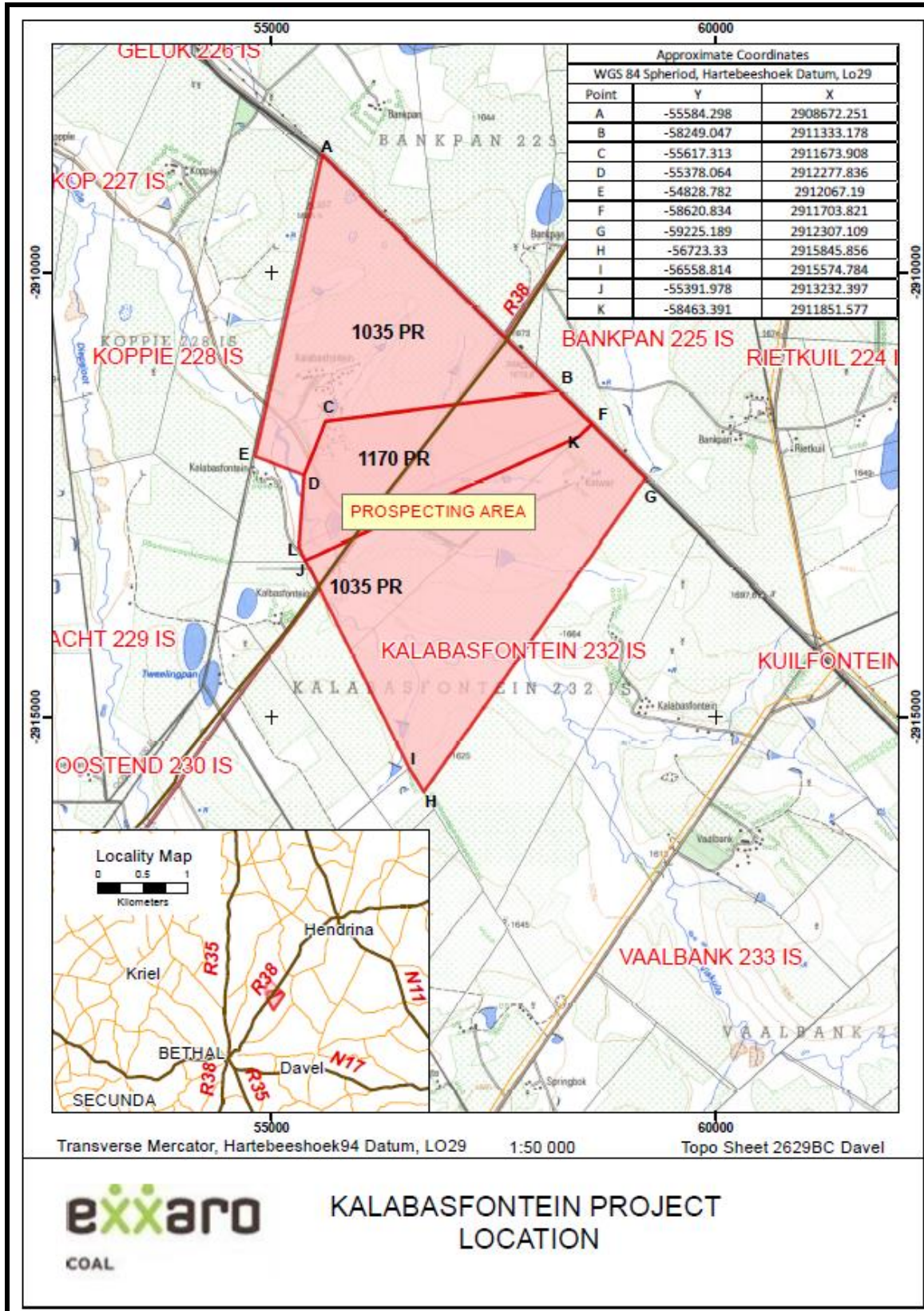


Figure 1: Plan showing Kalabasfontein Project location.

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2. Information provided.

The following information was provided for use in this investigation:

- Locality plans (Figure 1).
- Geological boreholes logs (Appendix 1 & Indicated in Figure 2).

3. Methodology

The following investigation methodology was used in the risk assessment:

- Analysis of geological borehole log information for pillar designs, sinkhole and subsidence analysis.

4. Pillar Design.

Two risks can be expected when undermining surface structures:

- Pillars can collapse, usually over the entire panel,
- Roof failure can occur resulting in sinkhole formation.

a. Pillar Stability.

1) Pillar Strength

The pillar's strength is calculated using the van der Merwe and Mathey (2013) equation which is based on the review of 85 panel pillar cases as compared to the widely used Salamon and Munro (1967) formula which was based on 27 failed panel pillar cases. The van der Merwe and Mathey (2013) formula is given by:

$$\sigma_s = 5.47 \frac{w_s^{0.8}}{h} \text{ (MPa)} \quad (1)$$

Where:

σ_s - is the pillar strength.

h - is the pillar height.

w - is the pillar width or effective pillar width for rectangular pillars.

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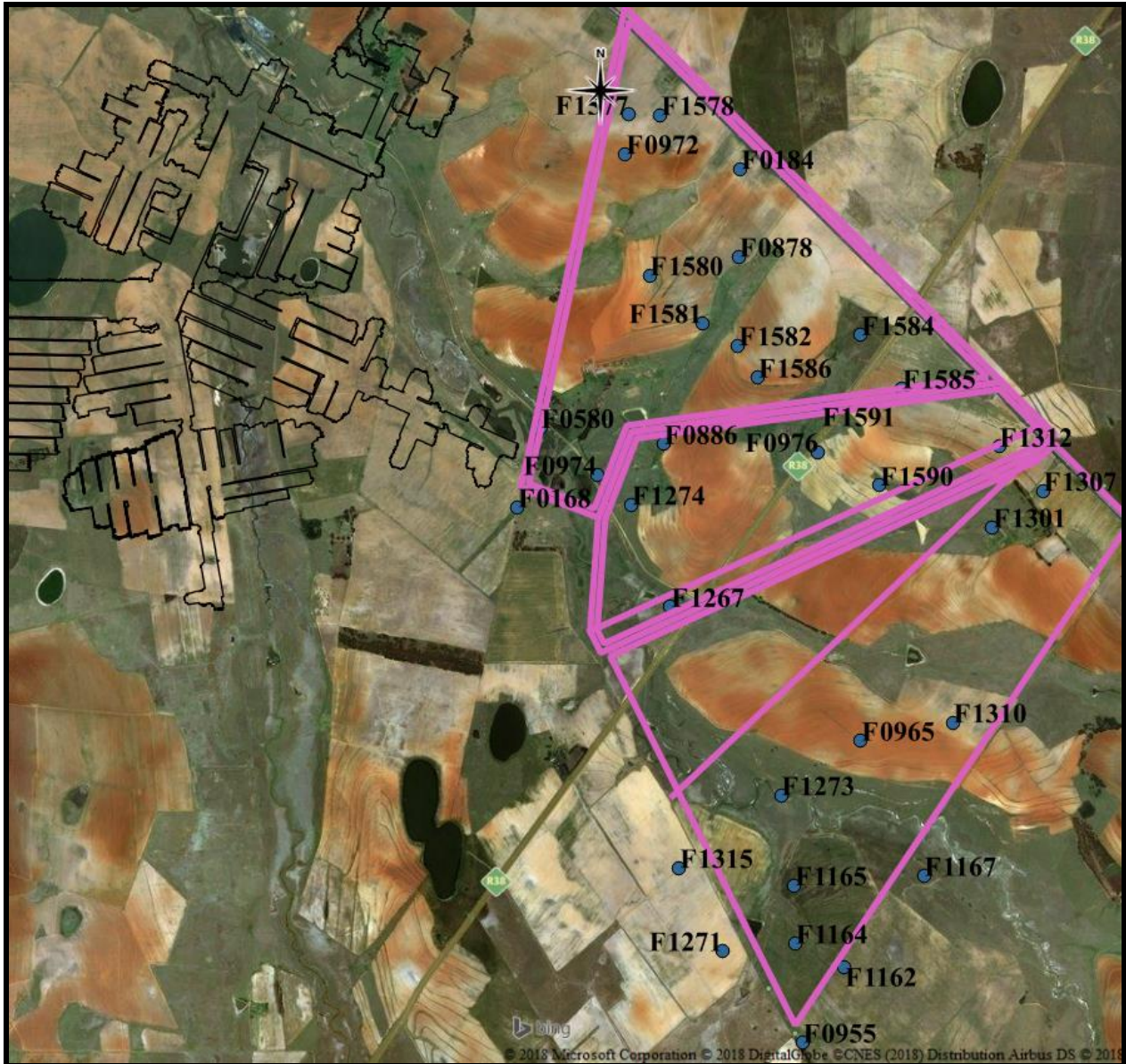


Figure 2: Satellite image showing Kalabasfontein boundaries (Purple) and the boreholes used in the assessment.

2) Pillar Load.

The pillar load is calculated using the tributary area theory which states that individual pillars carry an equal proportion of the of overburden load. This assumption applies where the pillars are of uniform size and the panel width is greater than the depth to the seam. The pillar load for square pillars is given by:

$$Load = \frac{0.025HC_1C_2}{w_1w_2} MPa \quad (2)$$

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Where:

H – is the depth to floor of the seam.

$C1$ – is the pillar center distance in the split direction.

$C2$ – is the pillar center distance in the advance direction.

w_1 – pillar width in the split direction.

w_2 – is the pillar width in the advance direction.

3) Safety Factor

The pillar safety factor is the ratio between the pillar strength and the pillar load.

$$\text{Safety Factor} = \frac{\text{Pillar Strength}}{\text{Pillar load}} \quad (3)$$

b. Probability of Survival (POS)

A study undertaken by van der Merwe and Mathey (2013a) found that safety factor on its own is only a subjective evaluation of pillar stability. This is due to the fact that the survival of the pillar cannot be quantified through a safety factor calculation although a higher safety factor implies a higher rate of survival.

The concept of probability of survival was introduced to overcome the safety factor limitations. The following probability of survival formula was derived from the study:

$$POS_{OR} = 100 - 100Exp[-2.5FS_{OR}^{1.8}] (\%) \quad (4)$$

Where FS is safety factor calculated with equation 3.

van der Merwe and Mathey (2013a) further proposed acceptable POS norms which are given in the table below:

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Table 1: Recommended POS

Category	Minimum POS (%)	Remarks
Production panel	99.0	Short term, limited access, low traffic
Secondary development	99.5	Medium term, general access, medium traffic
Main development	99.9	Long term, general access, high traffic
Surface structure (1)	99.99	Low sensitivity to subsidence
Surface structure (2)	99.995	High sensitivity to subsidence, public access

c. Pillar Life Index

Van der Merwe (2003) undertook a study of failed pillar cases in both the Vaal and Witbank Coalfields in an effort to predict the life of pillars before failure. A recent review or update of the rate scaling was conducted by van der Merwe (2016) taking into account the concept of Probability of Survival

The amount a pillar has to scale in order to reach a Probability of Survival of 50%, is given by:

$$d_c = w - [0.002285HhC^2]^{0.3571} \text{ (m)} \quad (5)$$

Where H = mining depth (m)
 C = pillar centre distance (m)
 h = mining height (m)

The predicted life of the pillar is then given by:

$$PLI = \left[\frac{d_c}{mh^x} \right]^{\frac{1}{1-x}} \text{ (Years)} \quad (6)$$

Where m = dimensionless constant, 0.1799 for the No, 1, 2 and 4 Seams
 x = dimensionless constant, 0.7549 for the No, 1, 2 and 4 Seams
 h = mining height (m).

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d_c = amount of scaling for POS of 50%

Table 2: Recommended minimum pillar life index

Category	Minimum PLI (Years)	Remarks
Production panel	500 years	Short term, limited access, low traffic
Secondary development	800 years	Medium term, general access, medium traffic
Main development	1 000 years	Long term, general access, high traffic
Surface structure (1)	2 000 years	Low sensitivity to subsidence
Surface structure (2)	2 000 years	High sensitivity to subsidence, public access

The calculated pillar life index was found to be in excess of 2 000 years. Cognisance must be given to the fact that no pillar failure has been reported at Forzando South Coal Mine.

5. Sinkholes

Bulking factor analysis determines the height at which roof failure will progress to before being arrested by fallen material or by the effect of wedging. Bulking factor is defined as the ratio of total volume (solid plus void) to solid volume. Bulking factor is an important factor in determining the amount of material that will spill into the workings and the height of the goaf (z). A suggested bulking factor for caved sedimentary roof strata of 1, 3 was used. It should be noted that this approach assumes failure on the immediate roof of an intersection.

The caving height z is given by:

$$12 \frac{(hD_B^2 + 2h^2 D_B \cot \alpha)}{(K - 1)\pi} = \left[\frac{(fD_B)^3}{2 \tan \phi} - (fD_B - 2z \tan \phi)^2 \left(\frac{fD_B}{2 \tan \phi} - z \right) \right] \text{ (m)} \quad (7)$$

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Where D_B = bord width
 f = ratio of bottom of collapse cavity to bord width (i.e. if the bottom of the collapse is the intersection width, $f = 1.414$)
 K = bulking factor
 α = angle of repose of collapsed rock
 ϕ = inclination of collapse cavity sidewall, measured off the vertical. (20°)

The second termination mechanism, wedging out, occurs when the cavity height is given by:

$$z_m = \frac{f D_B}{2 \tan \phi} \text{ (m)} \quad (8)$$

The maximum height of the cavity is then the smallest of z or z_m . If the collapse cavity reaches the bottom of the weathered rock zone, it is assumed that a sinkhole can occur.

6. Subsidence

The act of mining will ultimately result in some sort of surface subsidence. Whether the subsidence is visible or not is dependent on the following factors:

- Depth of mining.
- Percentage extraction.
- The time at which the subsidence occurs.

The magnitude of subsidence in a stable pillar system is negligible. Cognisance must be given to the fact that although highly unlikely, pillar failure might occur resulting in the subsidence. The maximum subsidence in that unlikely event is given by:

$$S_{m,pf} = 2.986 \left\{ 1 - \frac{1}{2\lambda} \right\} \text{ (m)} \quad (9)$$

$$\lambda = \frac{h_e/H}{0.027} \quad (10)$$

Where H = mining depth

h_e = equivalent mining height, *mining height x extraction ratio.*

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Van der Merwe and Madden (2010) further classifies the expected subsidence profile into the following classes based on the panel width and magnitude of subsidence:

Table 3: Classification of subsidence profiles (Van der Merwe et al, 2010)

Class	S_m/H	Description
A	<0.001	Barely noticeable, smooth, continuous profile, hairline cracks
B	0.001 - 0.005	Difficult to notice, smooth profile, cracks 1 to 2 cm wide
C	0.005 – 0.02	Noticeable in flat terrain, smooth, cracks 2 to 10 cm wide, compression ridges 1 to 5 cm high
D	0.02 – 0.05	Noticeable in most terrains, visible vertical displacements across cracks, cracks 10 to 50 cm wide, compression ridges 5 to 50 cm high
E	>0.05	Severe profile, almost vertical sides, cracks wider than 50 cm, compression ridges higher than 50 cm

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7. Results

Table 4: Summary of assessment Borehole number	Base of Weathering	Depth to Floor (H) (m)	Mining Height (m)	Centre Distance (m)	Centre Distance 2 (m)	Effective Width (m)	Pillar Strength (MPa)	Load (MPa)	Corrected Safety Factor	Pillar Width to Height Ratio	Percentage Areal Extraction	PoS
F0168	16.00	100.56	2.45	18.00	18.00	10.80	14.98	6.98	2.45	4.41	64.00	99.99965
F0184	14.00	90.16	2.10	15.00	18.00	9.06	15.18	7.22	2.40	5.14	68.80	99.99944
F0580	3.90	71.23	2.10	15.00	15.00	7.80	13.47	6.59	2.45	3.71	72.96	99.99966
F0878	16.18	103.78	2.10	18.00	18.00	10.80	17.48	7.21	2.77	5.14	64.00	99.99998
F0886	10.72	40.63	2.10	15.00	15.00	7.80	13.47	3.76	4.30	3.71	72.96	100
F0955	15.77	42.84	2.10	15.00	15.00	7.80	13.47	3.96	4.08	3.71	72.96	100
F0965	17.50	61.45	2.10	15.00	15.00	7.80	13.47	5.68	2.85	3.71	72.96	99.99999
F0972	36.96	117.03	2.10	18.00	18.00	10.80	17.48	8.13	2.46	5.14	64.00	99.99966
F0974	6.22	42.21	2.10	15.00	15.00	7.80	13.47	3.90	4.14	3.71	72.96	100
F0976	19.50	70.12	2.10	15.00	15.00	7.80	13.47	6.48	2.49	3.71	72.96	99.99976
F1162	12.67	38.11	2.10	15.00	15.00	7.80	13.47	3.52	4.59	3.71	72.96	100
F1164	9.35	47.47	2.10	15.00	15.00	7.80	13.47	4.39	3.68	3.71	72.96	100
F1165	6.59	30.82	2.10	15.00	15.00	7.80	13.47	2.85	5.67	3.71	72.96	100
F1167	9.57	26.99	2.10	15.00	15.00	7.80	13.47	2.50	6.48	3.71	72.96	100
F1267	12.43	69.54	2.10	15.00	15.00	7.80	13.47	6.43	2.51	3.71	72.96	99.99998
F1271	12.54	49.78	2.10	15.00	15.00	7.80	13.47	4.60	3.51	3.71	72.96	100
F1273	6.37	67.28	2.10	15.00	15.00	7.80	13.47	6.22	2.60	3.71	72.96	99.99991

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Borehole number	Base of Weathering	Depth to Floor (H) (m)	Mining Height (m)	Center Distance (m)	Center Distance 2 (m)	Effective Width (m)	Pillar Strength (MPa)	Load (MPa)	Corrected Safety Factor	Pillar Width to Height Ratio	Percentage Areal Extraction	PoS
F1274	9.87	53.59	2.10	15.00	15.00	7.80	13.47	4.95	3.26	3.71	72.96	100
F1301	12.22	93.48	2.10	15.00	18.00	9.06	15.18	7.49	2.32	5.14	68.80	99.9988
F1305	13.98	108.76	2.67	18.00	18.00	10.80	13.75	7.55	2.08	4.04	64.00	99.99117
F1307	25.07	110.09	2.34	18.00	18.00	10.80	15.69	7.65	2.34	4.62	64.00	99.99907
F1310	12.23	49.34	2.10	15.00	15.00	7.80	13.47	4.56	3.54	3.71	72.96	100
F1312	12.90	117.48	2.10	18.00	18.00	10.80	17.48	8.16	2.45	5.14	64.00	99.99963
F1315	8.20	46.88	2.29	15.00	16.00	8.27	12.95	4.10	3.72	3.84	71.40	100
F1577	21.00	112.70	2.10	18.00	18.00	10.80	17.48	7.83	2.55	5.14	64.00	99.99986
F1578	30.00	118.65	2.10	18.00	18.00	10.80	17.48	8.24	2.42	5.14	64.00	99.99954
F1580	8.30	95.18	2.10	15.00	18.00	9.06	15.18	7.63	2.27	5.14	68.80	99.99828
F1581	15.10	106.25	2.10	18.00	18.00	10.80	17.48	7.38	2.71	5.14	64.00	99.99997
F1582	12.70	103.76	2.46	18.00	18.00	10.80	14.92	7.21	2.37	4.39	64.00	99.99923
F1584	21.00	112.08	2.10	18.00	18.00	10.80	17.48	7.78	2.57	5.14	64.00	99.99988
F1585	21.20	112.09	2.19	18.00	18.00	10.80	16.76	7.78	2.46	4.93	64.00	99.99967
F1586	17.80	108.96	2.16	18.00	18.00	10.80	16.99	7.57	2.57	5.00	64.00	99.99988
F1590	9.80	91.25	2.10	15.00	18.00	9.06	15.18	7.31	2.37	5.14	68.80	99.99928
F1591	11.40	95.70	2.10	15.00	18.00	9.06	15.18	7.67	2.26	5.14	68.80	99.99809

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Borehole number	Depth to Floor (H) (m)	Base of Weathering	Mining Height (m)	Bord Width (m)	Effective Width (m)	Percentage Areal Extraction	Pillar Life (yr)	max Subsidence	Subsidence Ratio	Subsidence Class
F0168	100.56	16.00	2.45	7.20	10.80	64.00	28758.33	0.98501901	0.0097953	C
F0184	90.16	14.00	2.10	7.20	9.06	68.80	20365.72	1.00709631	0.0111701	C
F0580	71.23	3.90	2.10	7.20	7.80	72.96	11046.44	1.26702794	0.0177878	C
F0878	103.78	16.18	2.10	7.20	10.80	64.00	59266.64	0.84458109	0.0081382	C
F0886	40.63	10.72	2.10	7.20	7.80	72.96	30015.93	1.85190222	0.0455797	D
F0955	42.84	15.77	2.10	7.20	7.80	72.96	27792	1.79382549	0.0418727	D
F0965	61.45	17.50	2.10	7.20	7.80	72.96	15036.6	1.41165322	0.0229724	D
F0972	117.03	36.96	2.10	7.20	10.80	64.00	46478.15	0.76243877	0.0065149	C
F0974	42.21	6.22	2.10	7.20	7.80	72.96	28405.27	1.8100514	0.0428821	D
F0976	70.12	19.50	2.10	7.20	7.80	72.96	11436.78	1.28198878	0.0182828	C
F1162	38.11	12.67	2.10	7.20	7.80	72.96	32819.64	1.92222638	0.0504389	E
F1164	47.47	9.35	2.10	7.20	7.80	72.96	23734.14	1.68213681	0.0354358	D
F1165	30.82	6.59	2.10	7.20	7.80	72.96	42980.86	2.15265515	0.069846	E
F1167	26.99	9.57	2.10	7.20	7.80	72.96	49964.12	2.29070021	0.0848722	E
F1267	69.54	12.43	2.10	7.20	7.80	72.96	11646.45	1.28994257	0.0185496	C
F1271	49.78	12.54	2.10	7.20	7.80	72.96	21969.57	1.63102611	0.0327647	D
F1273	67.28	6.37	2.10	7.20	7.80	72.96	12502.85	1.32186345	0.0196472	C

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Borehole number	Depth to Floor (H) (m)	Base of Weathering	Mining Height (m)	Bord Width (m)	Effective Width (m)	Percentage Areal Extraction	Pillar Life (yr)	max Subsidence	Subsidence Ratio	Subsidence Class
F1274	53.59	9.87	2.10	7.20	7.80	72.96	19376.09	1.55273027	0.0289743	D
F1301	93.48	12.22	2.10	7.20	9.06	68.80	18766.09	0.97797063	0.0104618	C
F1305	108.76	13.98	2.67	7.20	10.80	64.00	15116.38	0.9911215	0.0091129	C
F1307	110.09	25.07	2.34	7.20	10.80	64.00	30063.49	0.88017731	0.0079951	C
F1310	49.34	12.23	2.10	7.20	7.80	72.96	22293.73	1.64054017	0.0332497	D
F1312	117.48	12.90	2.10	7.20	10.80	64.00	46099.23	0.75992626	0.0064686	C
F1315	46.88	8.20	2.29	7.20	8.27	71.40	24013.54	1.76636226	0.0376784	D
F1577	112.70	21.00	2.10	7.20	10.80	64.00	50297.49	0.78748367	0.0069874	C
F1578	118.65	30.00	2.10	7.20	10.80	64.00	45129.23	0.75346996	0.0063504	C
F1580	95.18	8.30	2.10	7.20	9.06	68.80	17997.96	0.96368946	0.0101249	C
F1581	106.25	15.10	2.10	7.20	10.80	64.00	56621.78	0.82796624	0.0077926	C
F1582	103.76	12.70	2.46	7.20	10.80	64.00	26301.91	0.96336847	0.0092846	C
F1584	112.08	21.00	2.10	7.20	10.80	64.00	50871.15	0.79120384	0.0070593	C
F1585	112.09	21.20	2.19	7.20	10.80	64.00	40944.25	0.8199084	0.0073147	C
F1586	108.96	17.80	2.16	7.20	10.80	64.00	46649.21	0.83006011	0.007618	C
F1590	91.25	9.80	2.10	7.20	9.06	68.80	19825.47	0.99734773	0.0109298	C
F1591	95.70	11.40	2.10	7.20	9.06	68.80	17769.53	0.95940276	0.0100251	C

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Borehole number	Depth to Floor (H) (m)	Base of Weathering	Mining Height (m)	Bord Width (m)	Effective Width (m)	Percentage Areal Extraction	Caving Height (m)	Stable Overburden (m)	%Comp Layer	Sum Comp Layer	Max Comp Thickness (m)
F0168	100.56	16.00	2.45	7.20	10.80	64.00	14.00	68.11	39.05%	32.06	20.36
F0184	90.16	14.00	2.10	7.20	9.06	68.80	14.00	60.06	52.46%	38.85	22.04
F0580	71.23	3.90	2.10	7.20	7.80	72.96	14.00	51.23	74.23%	48.42	23.99
F0878	103.78	16.18	2.10	7.20	10.80	64.00	14.00	71.50	56.25%	48.09	19.24
F0886	40.63	10.72	2.10	7.20	7.80	72.96	14.00	13.81	97.48%	27.11	15.19
F0955	42.84	15.77	2.10	7.20	7.80	72.96	14.00	10.97	77.97%	19.47	19.47
F0965	61.45	17.50	2.10	7.20	7.80	72.96	14.00	27.85	64.44%	26.97	21.78
F0972	117.03	36.96	2.10	7.20	10.80	64.00	14.00	63.97	57.27%	44.65	22.59
F0974	42.21	6.22	2.10	7.20	7.80	72.96	14.00	19.89	83.80%	28.4	23.18
F0976	70.12	19.50	2.10	7.20	7.80	72.96	14.00	34.52	63.03%	30.58	16.61
F1162	38.11	12.67	2.10	7.20	7.80	72.96	14.00	9.34	89.37%	20.86	50.86
F1164	47.47	9.35	2.10	7.20	7.80	72.96	14.00	22.02	65.38%	23.55	23.55
F1165	30.82	6.59	2.10	7.20	7.80	72.96	14.00	8.13	93.85%	20.77	20.77
F1167	26.99	9.57	2.10	7.20	7.80	72.96	14.00	1.32	100.00%	15.32	15.32
F1267	69.54	12.43	2.10	7.20	7.80	72.96	14.00	41.01	55.34%	30.44	18.93
F1271	49.78	12.54	2.10	7.20	7.80	72.96	14.00	21.14	62.15%	21.84	21.84
F1273	67.28	6.37	2.10	7.20	7.80	72.96	14.00	44.81	65.91%	38.76	22.13

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Borehole number	Depth to Floor (H) (m)	Base of Weathering	Mining Height (m)	Bord Width (m)	Effective Width (m)	Percentage Areal Extraction	Caving Height (m)	Stable Overburden (m)	%Comp Layer	Sum Comp Layer	Max Comp Thickness (m)
F1274	53.59	9.87	2.10	7.20	7.80	72.96	14.00	27.62	74.41%	30.97	17.74
F1301	93.48	12.22	2.10	7.20	9.06	68.80	14.00	65.16	56.92%	45.06	20.39
F1305	108.76	13.98	2.67	7.20	10.80	64.00	14.00	78.11	71.54%	65.9	20.55
F1307	110.09	25.07	2.34	7.20	10.80	64.00	14.00	68.68	72.44%	59.89	18.78
F1310	49.34	12.23	2.10	7.20	7.80	72.96	14.00	21.01	65.21%	22.83	21.63
F1312	117.48	12.90	2.10	7.20	10.80	64.00	14.00	88.48	60.69%	62.2	15.53
F1315	46.88	8.20	2.29	7.20	8.27	71.40	14.00	22.39	74.00%	26.93	22.97
F1577	112.70	21.00	2.10	7.20	10.80	64.00	14.00	75.60	69.71%	62.46	22.73
F1578	118.65	30.00	2.10	7.20	10.80	64.00	14.00	72.55	54.47%	47.14	22.3
F1580	95.18	8.30	2.10	7.20	9.06	68.80	14.00	70.78	46.59%	39.5	24.59
F1581	106.25	15.10	2.10	7.20	10.80	64.00	14.00	75.05	57.77%	51.44	24.11
F1582	103.76	12.70	2.46	7.20	10.80	64.00	14.00	74.60	57.04%	50.54	24.69
F1584	112.08	21.00	2.10	7.20	10.80	64.00	14.00	74.98	55.32%	49.22	18.92
F1585	112.09	21.20	2.19	7.20	10.80	64.00	14.00	74.70	66.99%	59.42	16.56
F1586	108.96	17.80	2.16	7.20	10.80	64.00	14.00	75.00	42.34%	37.68	15.57
F1590	91.25	9.80	2.10	7.20	9.06	68.80	14.00	65.35	58.36%	46.31	16.95
F1591	95.70	11.40	2.10	7.20	9.06	68.80	14.00	68.20	58.98%	48.48	19.14

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8. Conclusions.

a. Pillar Stability.

No potential pillar instability is anticipated if the Reserves are mined with pillars laid-out on minimum 15.0m x 15.0 m center and maximum 18.0 m x 18.0 m center layout with 7.2 m bords. Pillar size variation will be a function of bord width, mining depth and mining height. Pillar sizes generally increase with increasing mining depth, mining height and bord widths. All the pillars were found to have a probability of survival more than 99.995% which is recommended for the highly sensitive surface structures. This therefore implies a probability of failure of < 0.005%.

Pillar life index calculation shows that all pillars will have a life index of at least 11 046 years before a 50% probability of failure is reached. This is far more than the recommended 2000 years for highly sensitive structures.

b. Sinkhole

A maximum caving height of 14.0 m was calculated for all areas should roof failure occur. No sinkhole is therefore expected in the reserve area as the maximum caving height does not progress to / intersect the weathered zone in any of the boreholes.

Cognisance must also be given to the fact that the overburden is comprised of at least 39% competent sandstone layers. Competent means any lithological units with a thickness of at least 1.0 m and a composition of at least 80% sandstone.

A minimum sandstone thickness of 15 m in the overburden was found during the investigation. This layer has a unsupported stable span of at least 20 m when jointed and 49 m when unjointed. Thus, pillar failure must occur before the overburden can fail. This means that sinkhole hole probabilities are low in the area.

c. Subsidence

The magnitude of maximum subsidence in a bord and pillar layout is dependent on the unlikely event that panel's pillar system fails. Cognisance must be taken to the fact that the calculated pillar life index and probability of survival are far greater than the recommended minimums, indicating a stable pillar system.

The investigation shows that a Class C, D & E subsidence profile will occur in the area in the unlikely event that pillar fails. The subsidence profile will have the following characteristics:

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- Class C: Noticeable in flat terrain, smooth, cracks 2 to 10 cm wide, compression ridges 1 to 5 cm high.
- Class D: Noticeable in most terrains, visible vertical displacements across cracks, cracks 10 to 50 cm wide, compression ridges 5 to 50 cm high.
- Class E: Severe profile, almost vertical sides, cracks wider than 50 cm, compression ridges higher than 50 cm.

Class D & E subsidence will largely be constrained to distal southern and western portion of the reserve area.

9. Recommendations


The following are recommended based on the investigation:

- The following mine design will apply when mining in the area:
 - Pillar Centers Range : Minimum 15.0 m x 15.0 m and Maximum of 18.0 m x 18.0 m
 - Bord width : 7.2 m
 - Mining Height : Total seam thickness extraction
 - Pillar design process will be such that the Probability of survival criterion for the different surface features is met or satisfied.
- Surface elevation monitoring points should be installed at positions surrounding the sensitive structures such as building and tarred road at convenient points. During mining, surveys should be conducted monthly and continued monthly for three months after mining has ceased for a period of three months. Thereafter the periods can be relaxed to quarterly for a further year and after that annual surveys should be conducted.
- Survey beacons should consist of 20 mm rebar and be anchored in concrete with the anchor at least a metre deep. The protruding end of the beacon should not protrude more than 10 cm, to avoid accidental damage.
- Similar beacons should be installed in an area with similar ground conditions, more than 200 m away from any undermining to serve as control measurements.

Should you have any further queries please feel free to contact myself at the following locations: Tel. (011) 441 6989, Cell. (084) 372 4507, or Email. rofhiwa.phadagi@exxaro.com

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Yours Sincerely



Mr. Rofhiwa Phadagi

10. References.

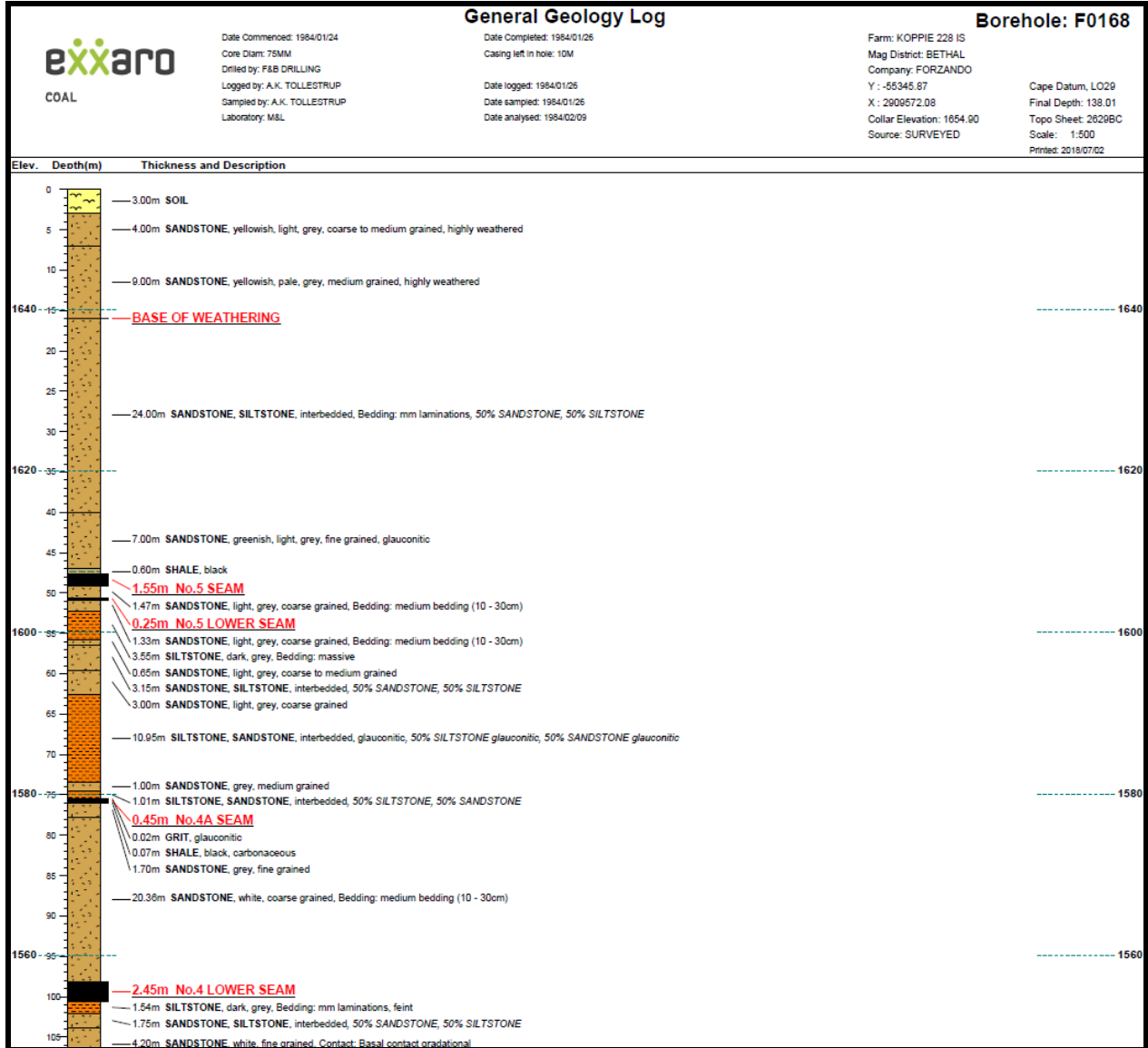
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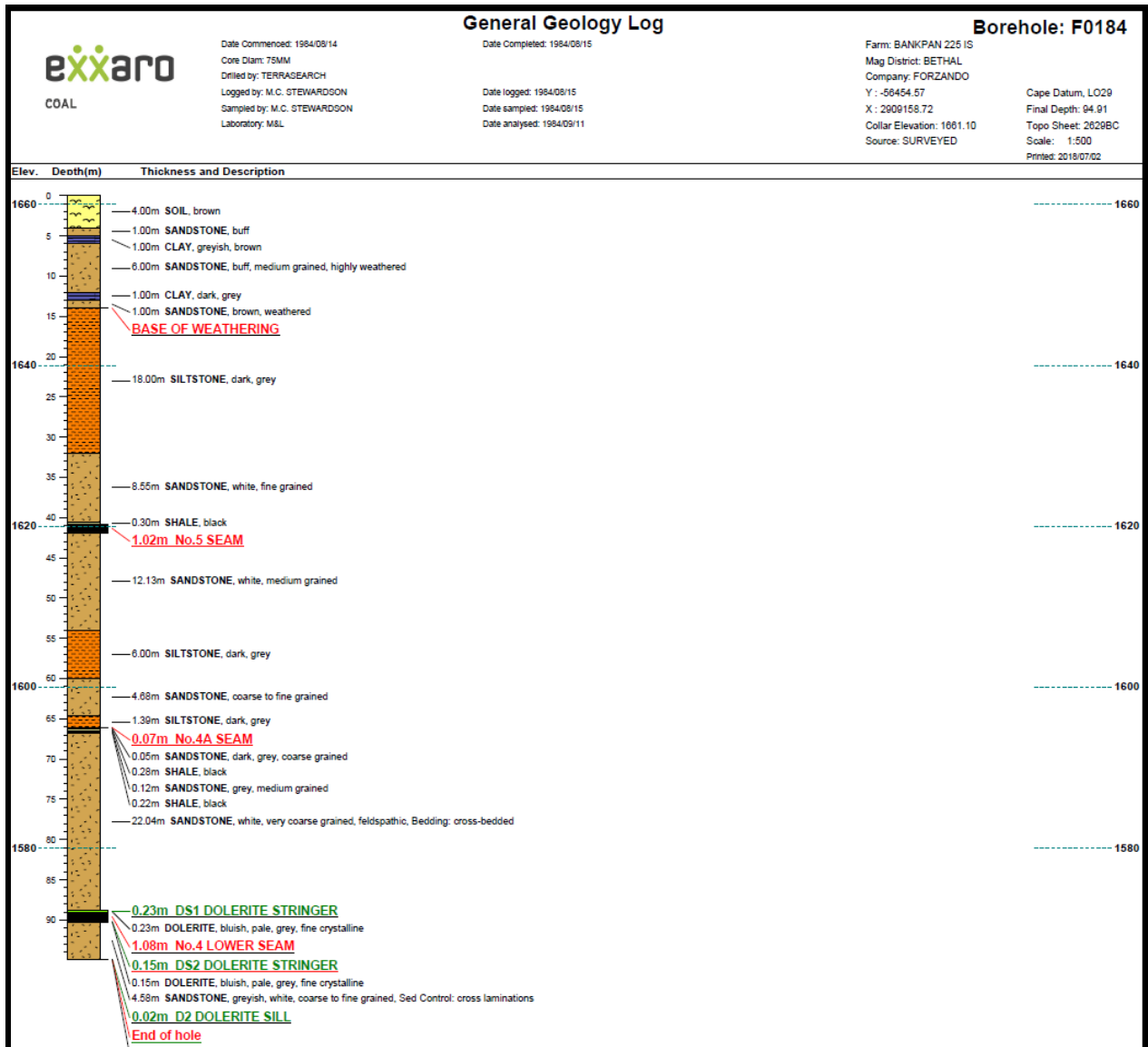
APPENDIX 1

GEOLOGICAL BOREHOLES

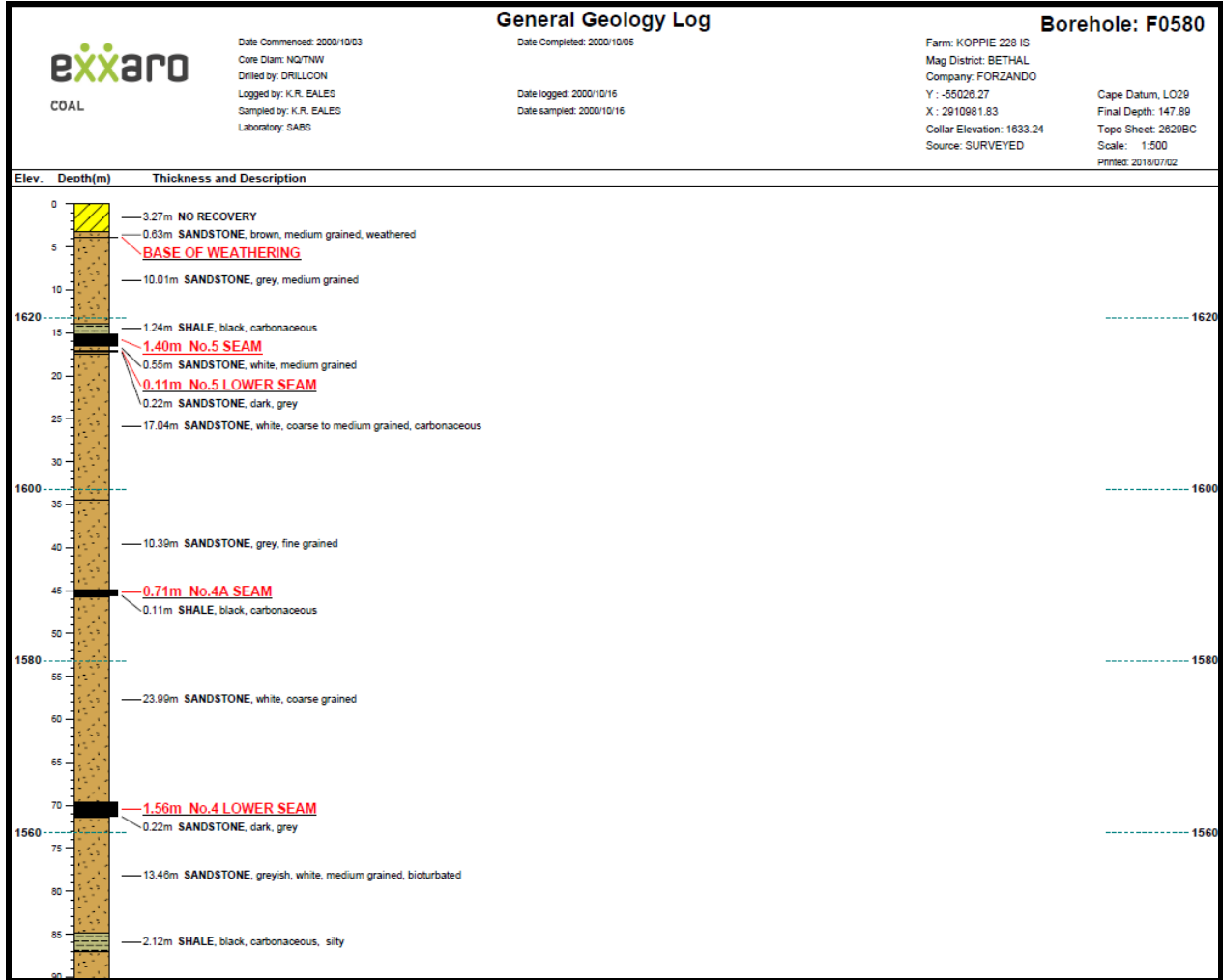
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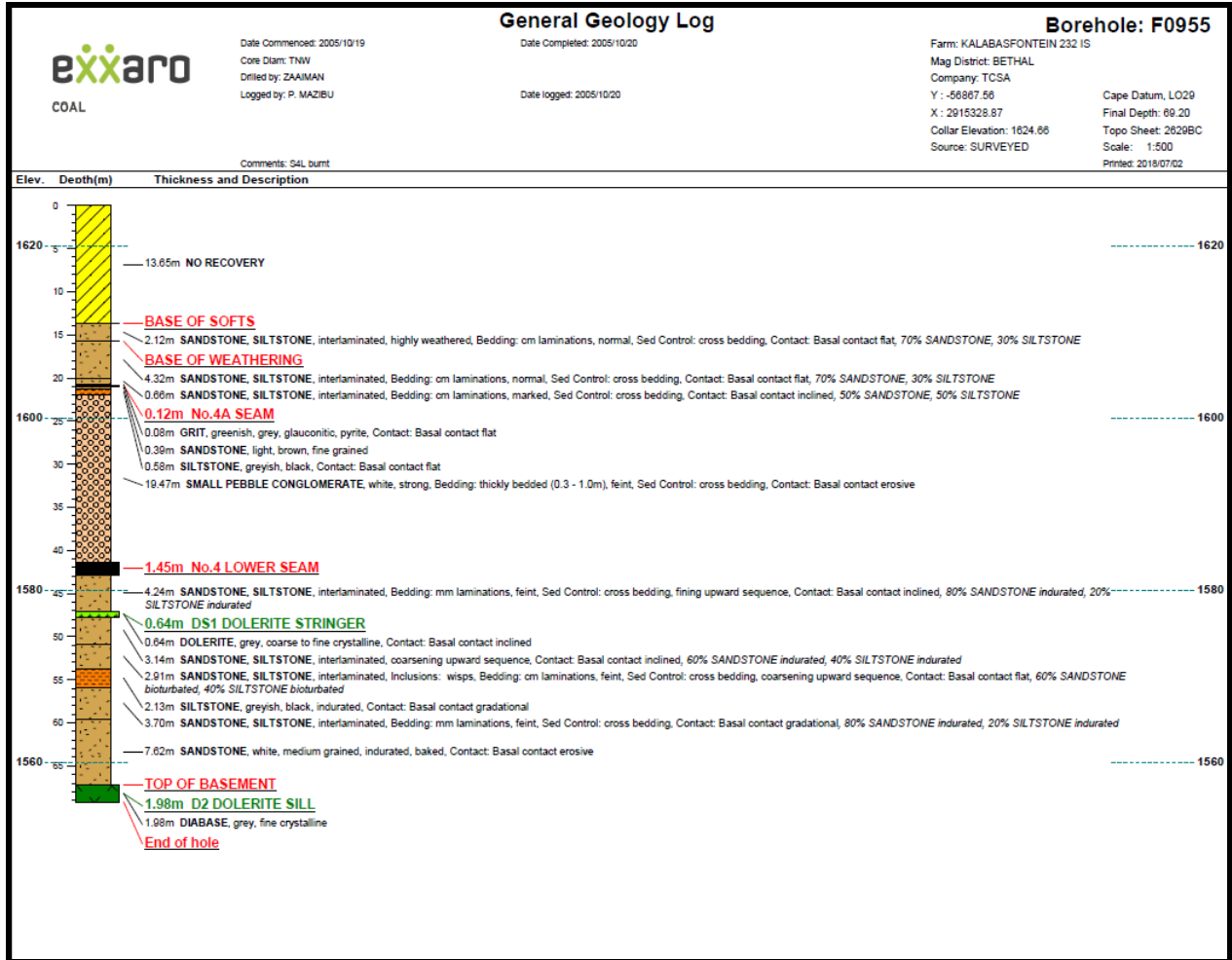
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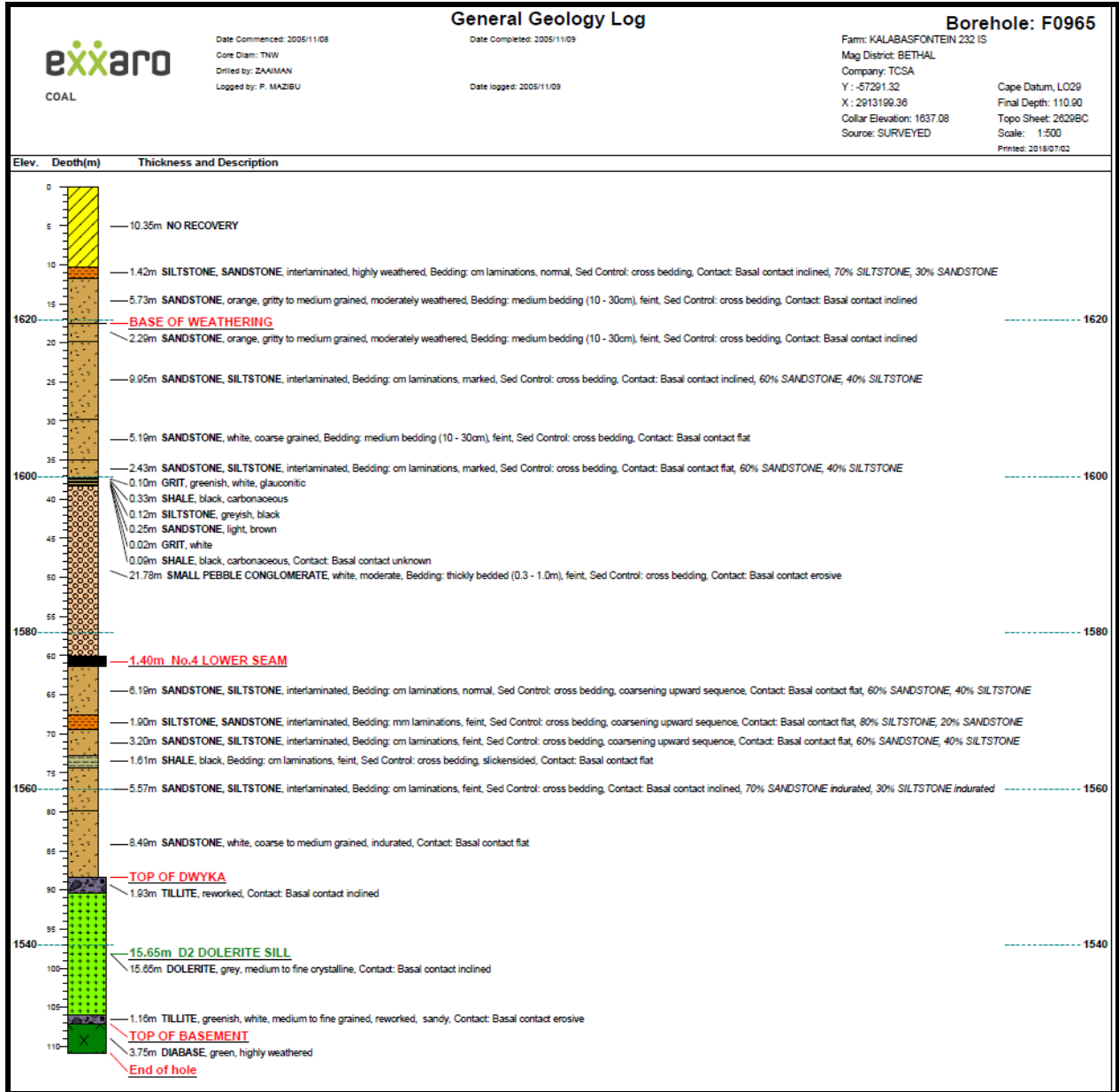
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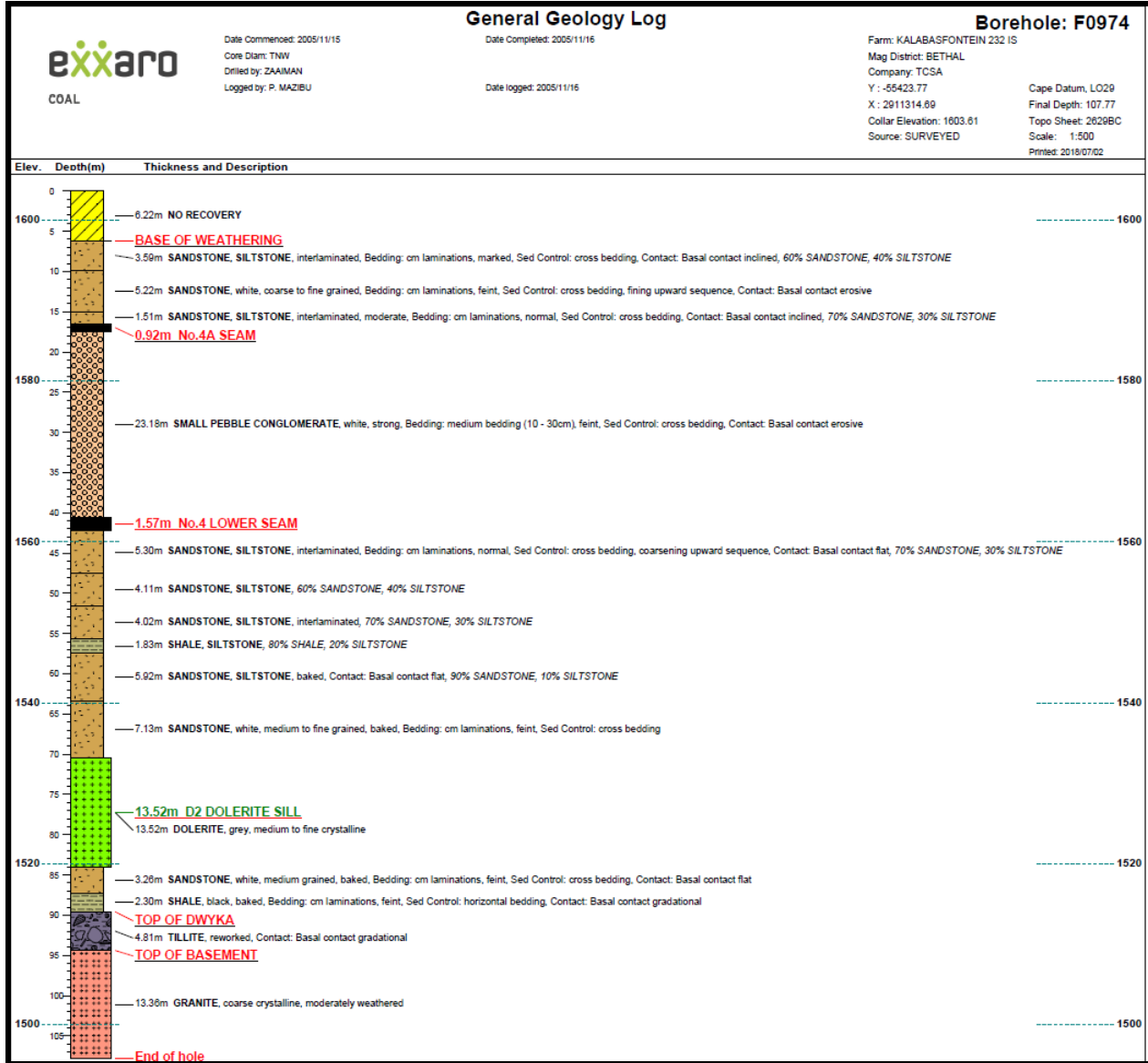
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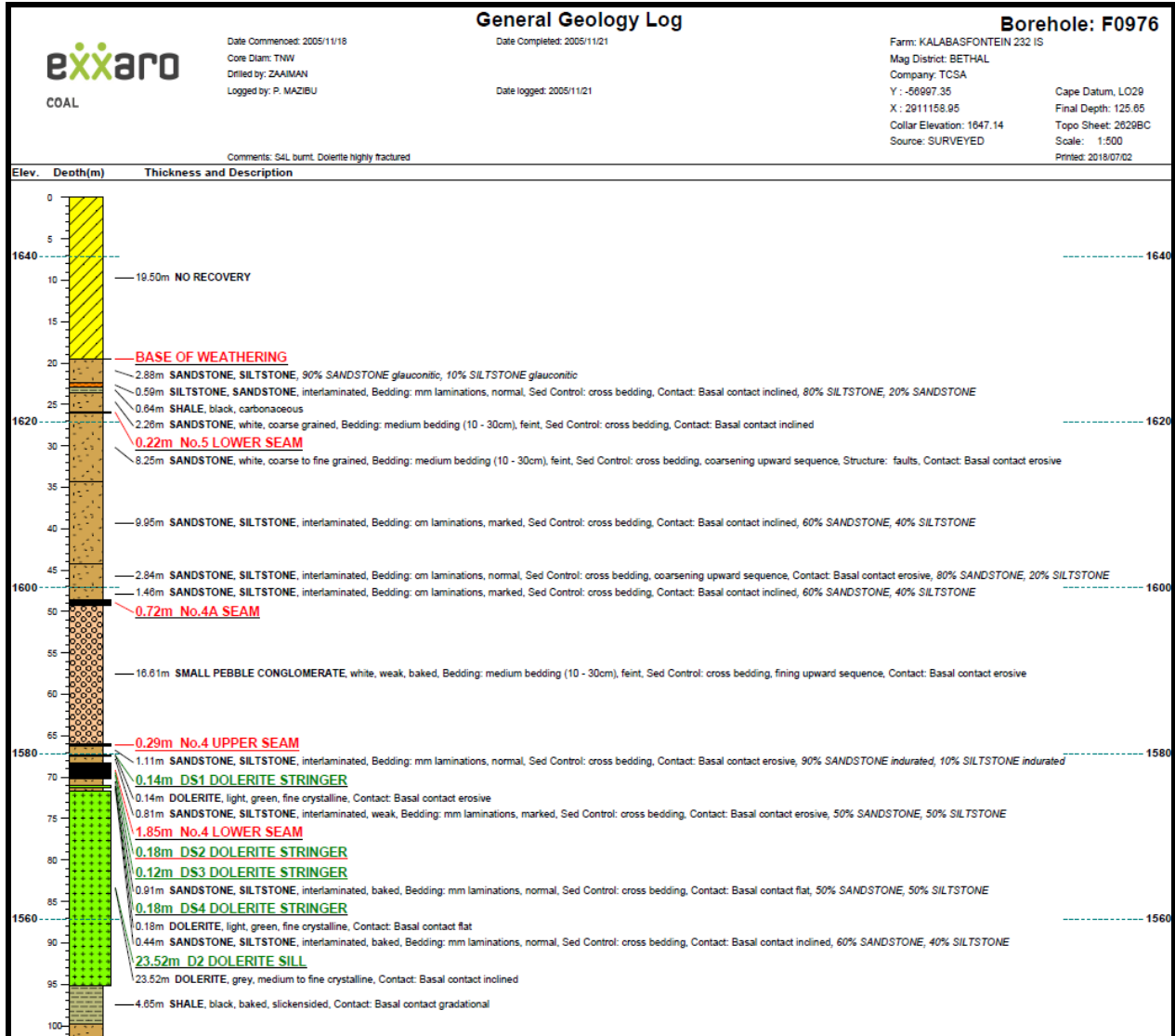
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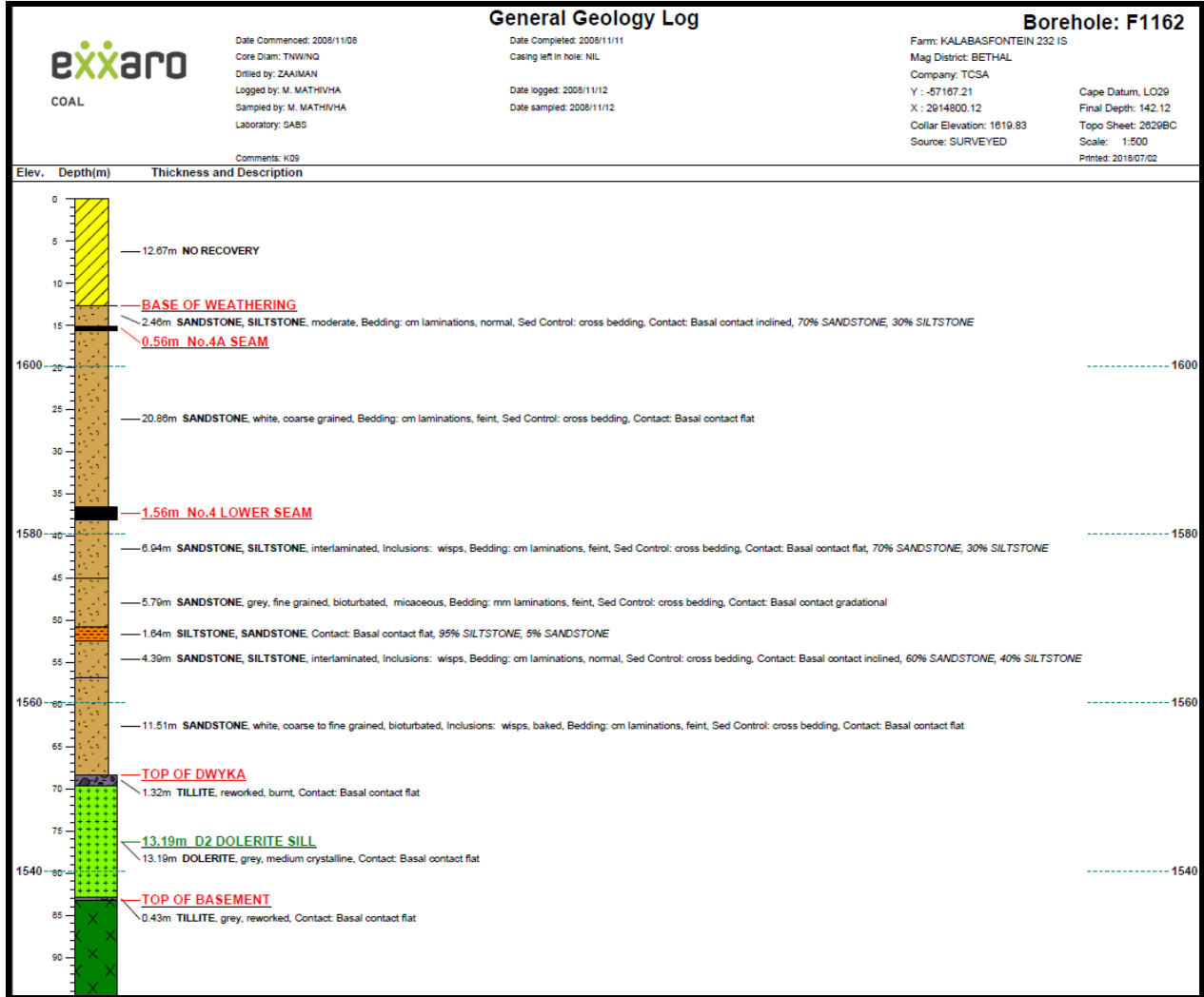
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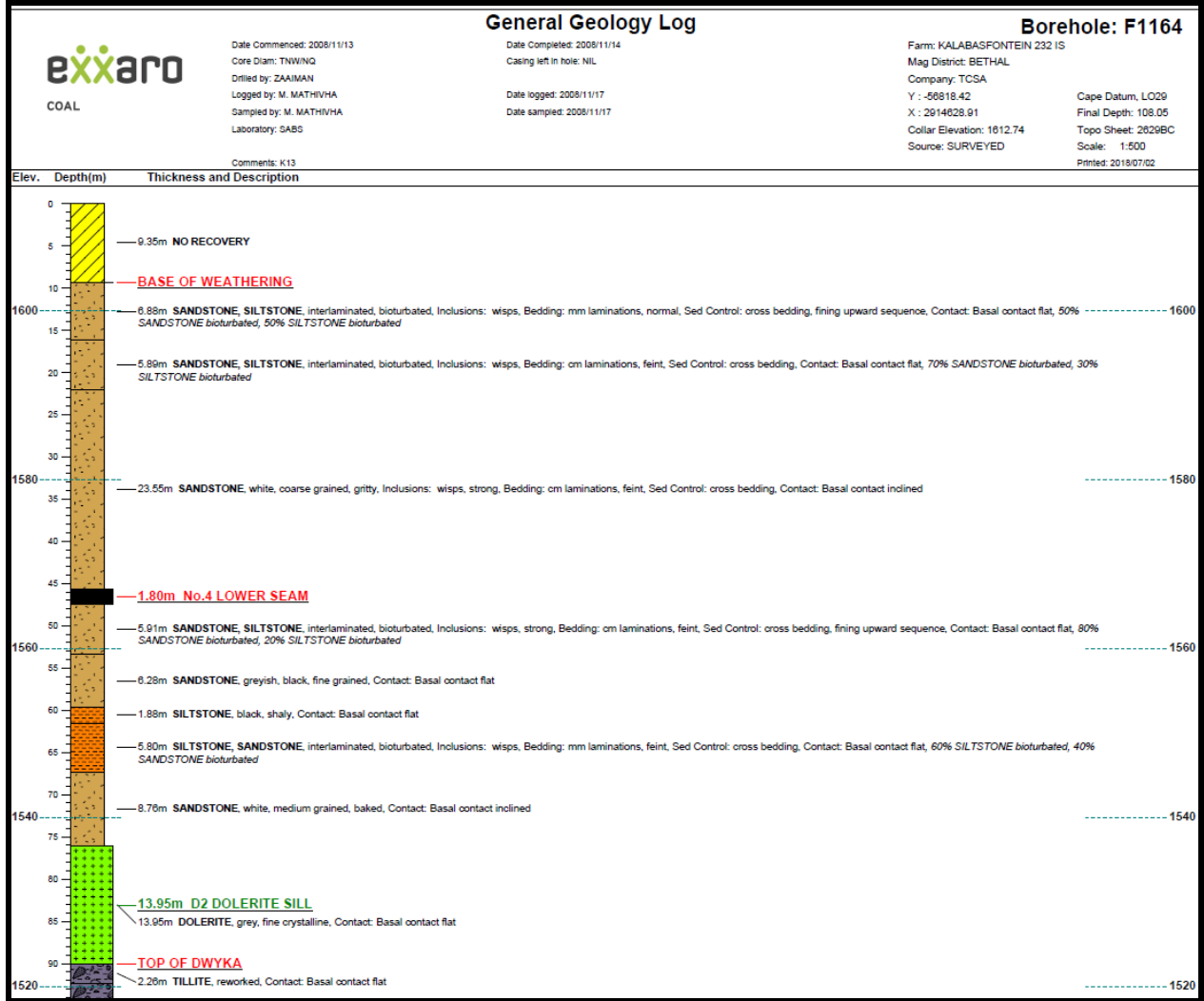
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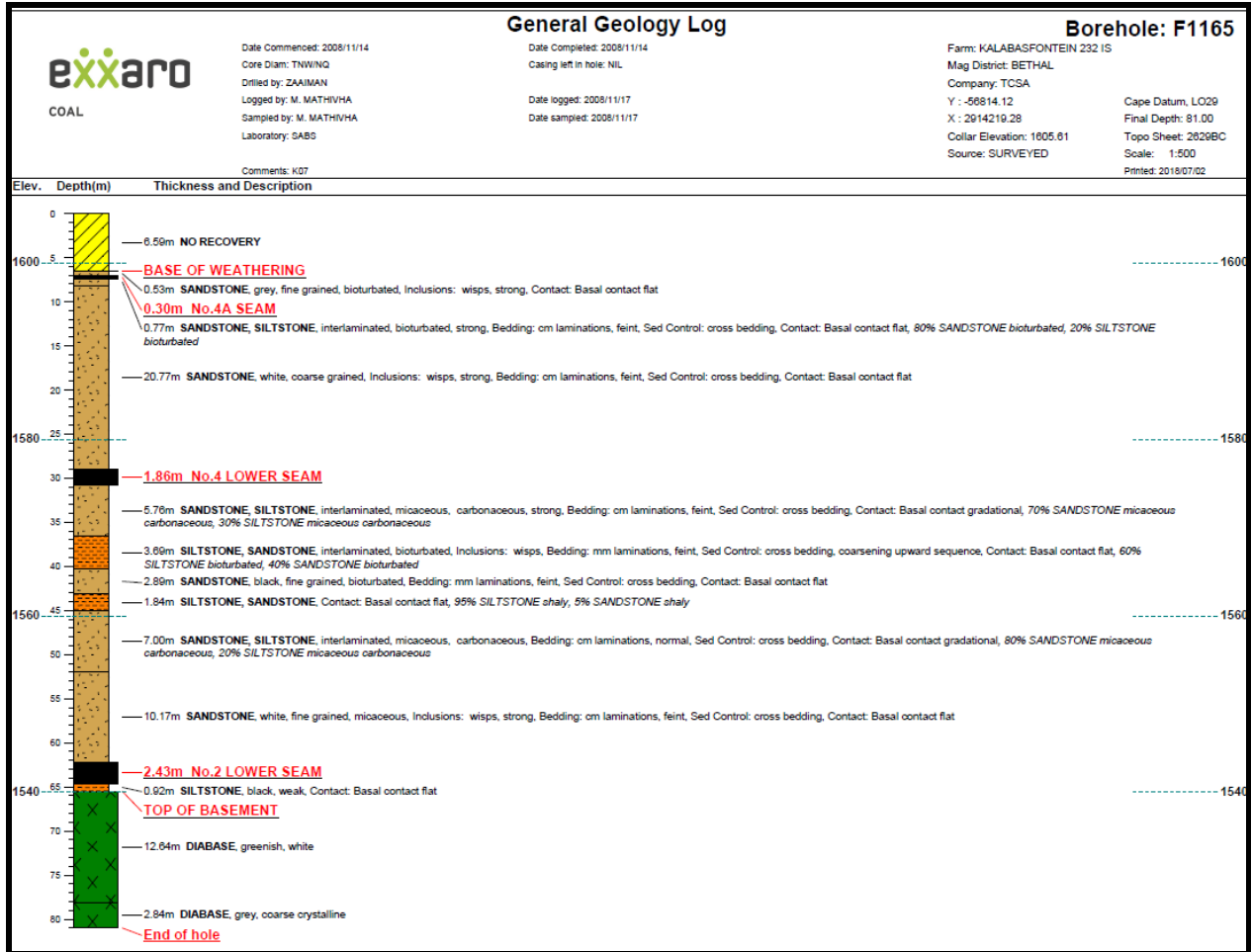
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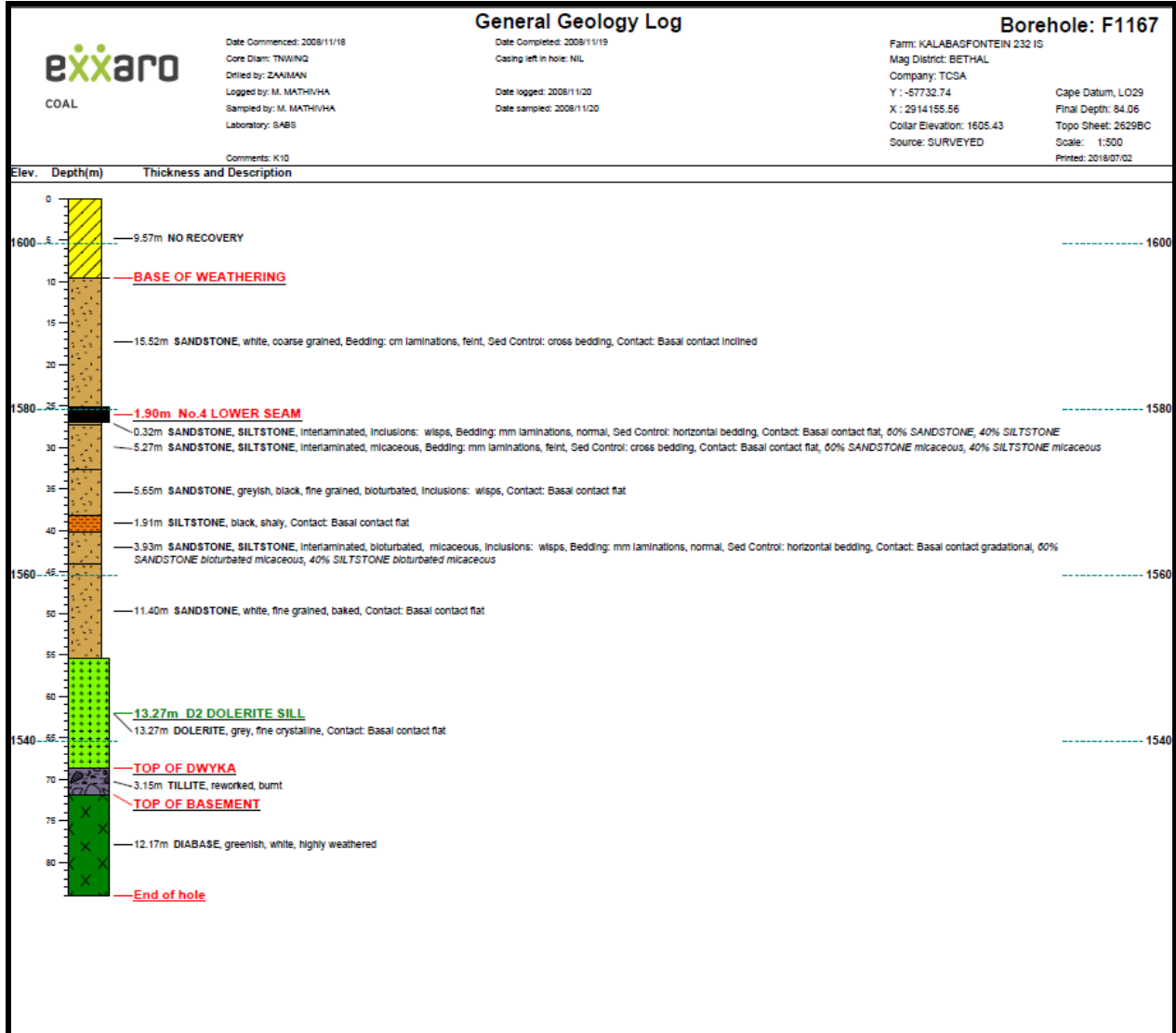
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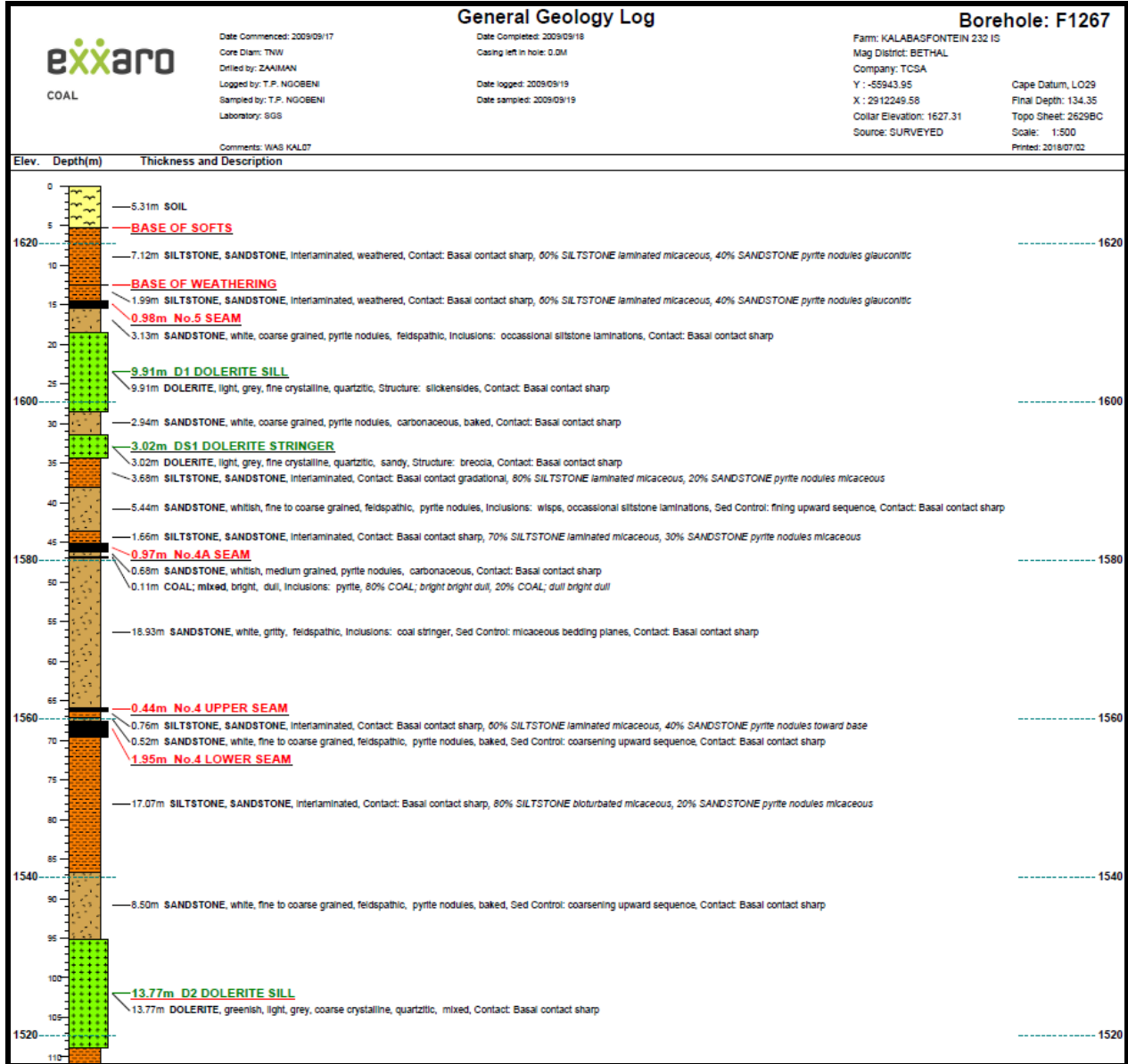
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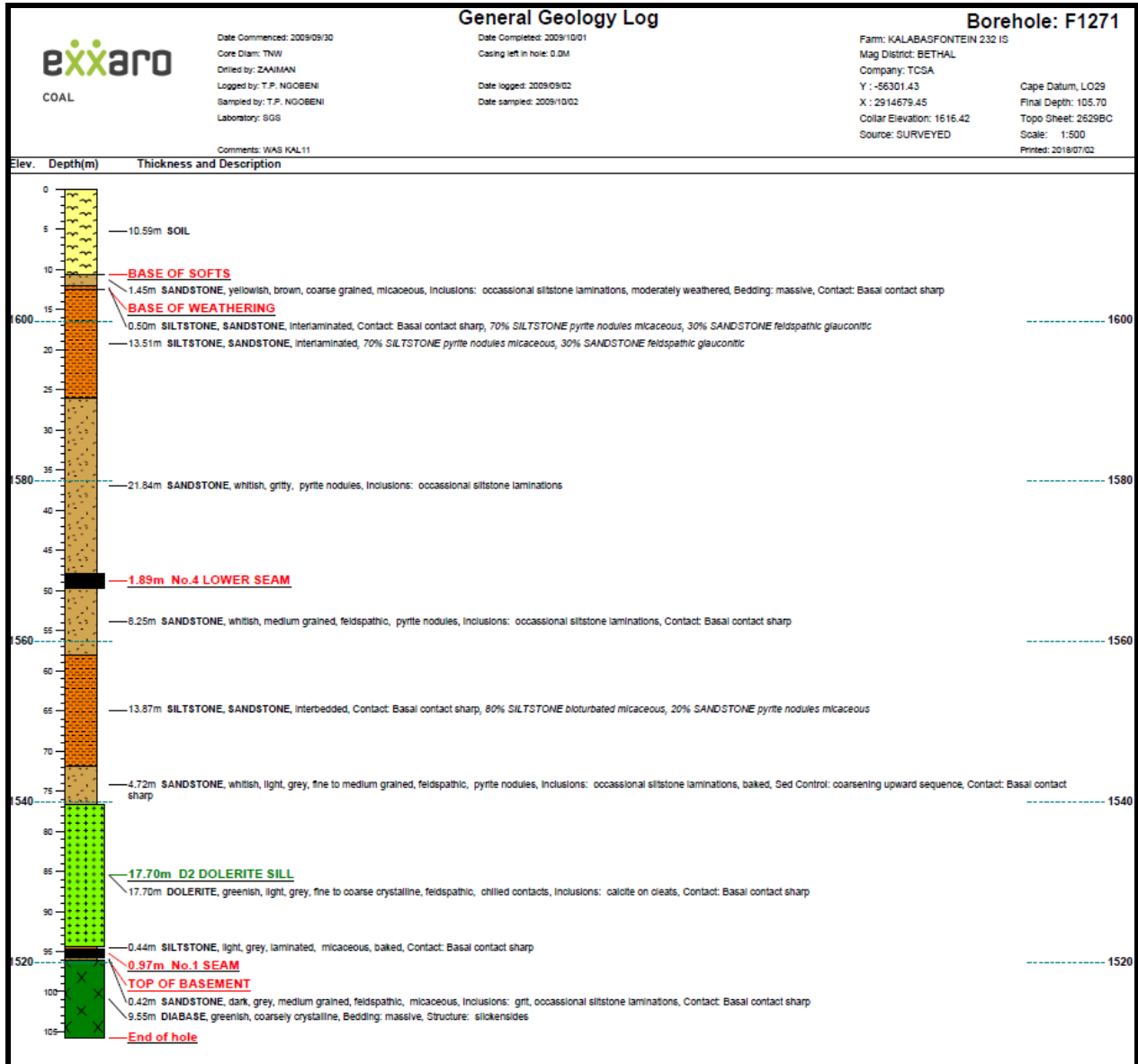
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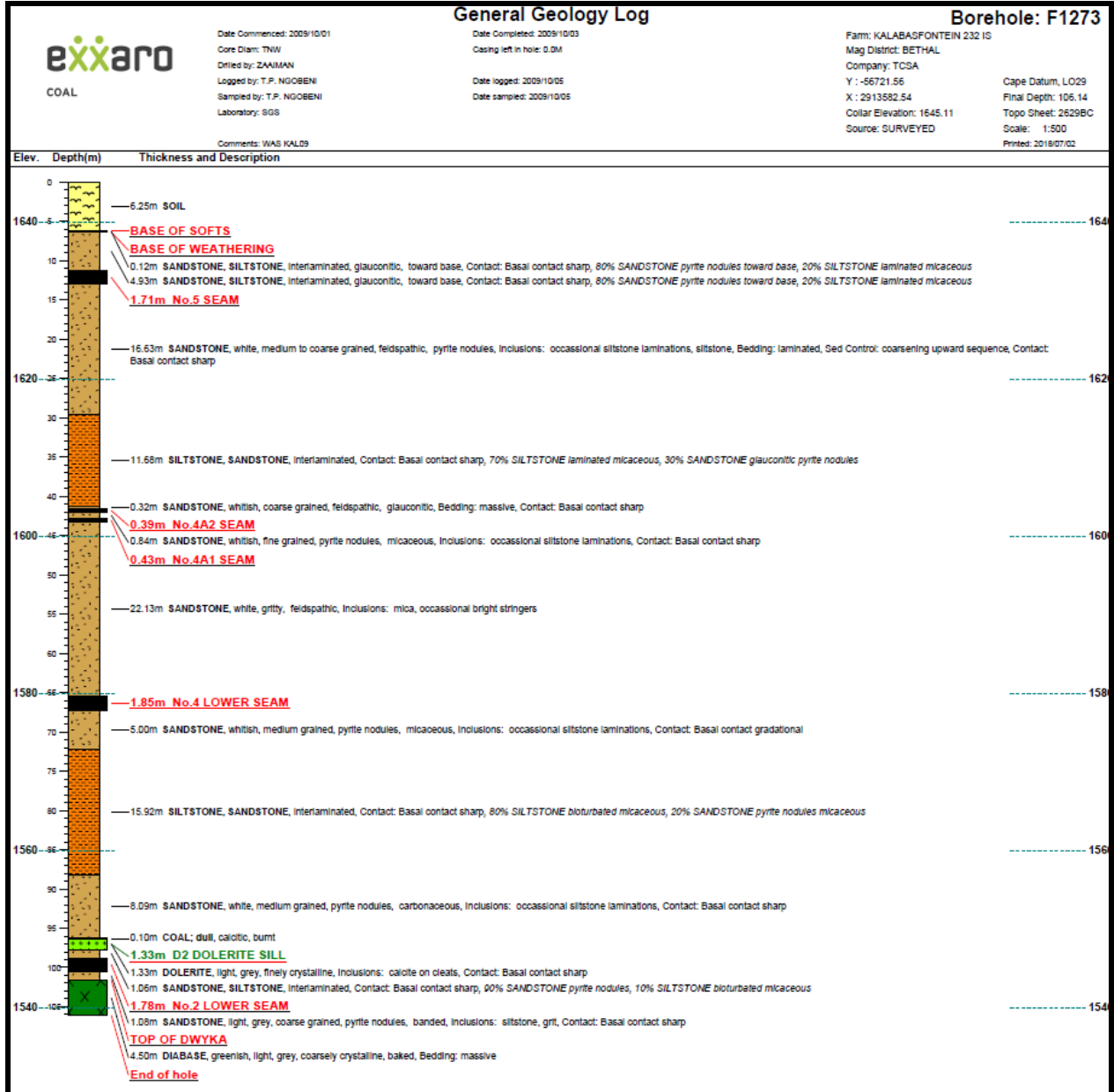
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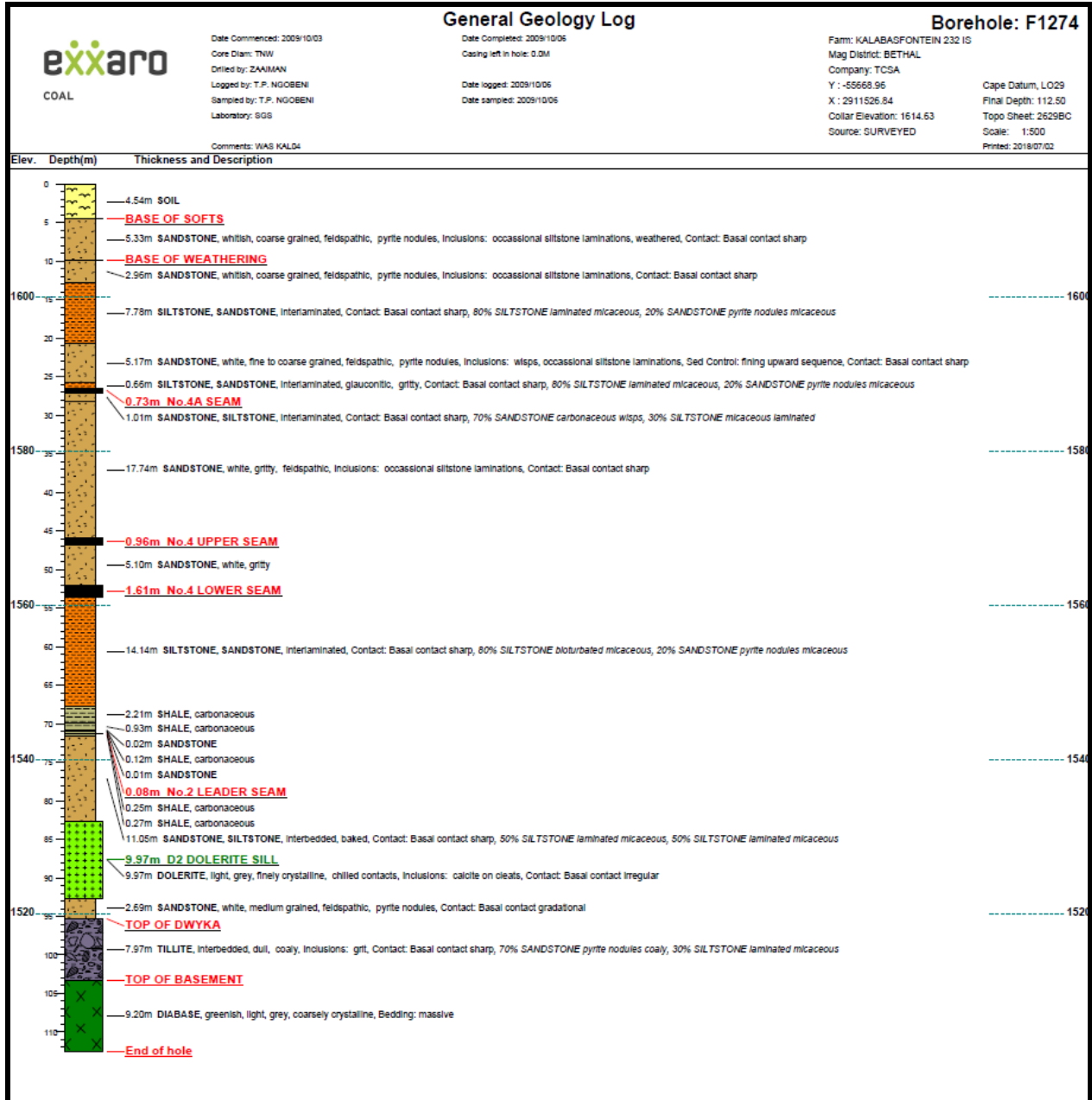
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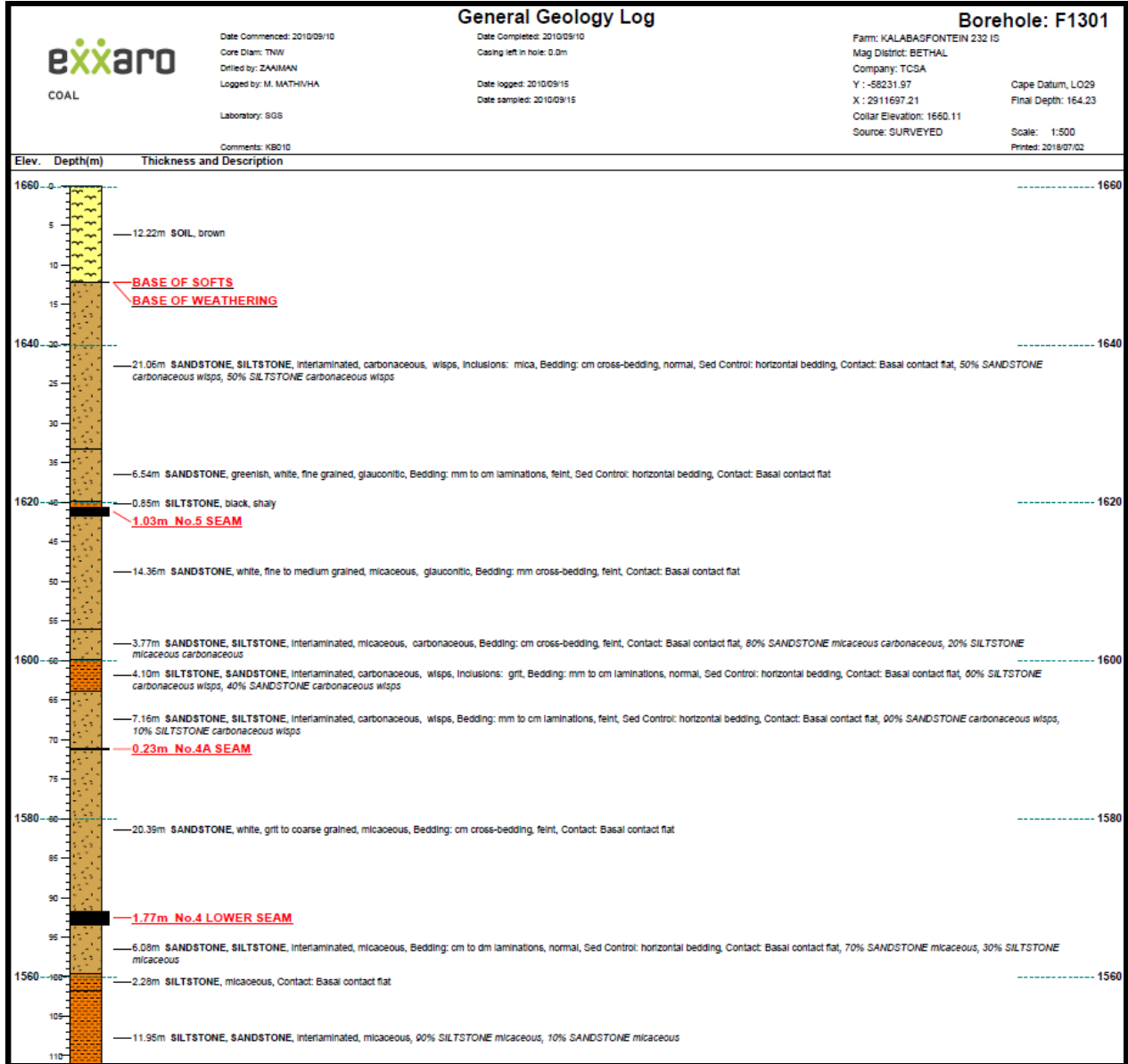
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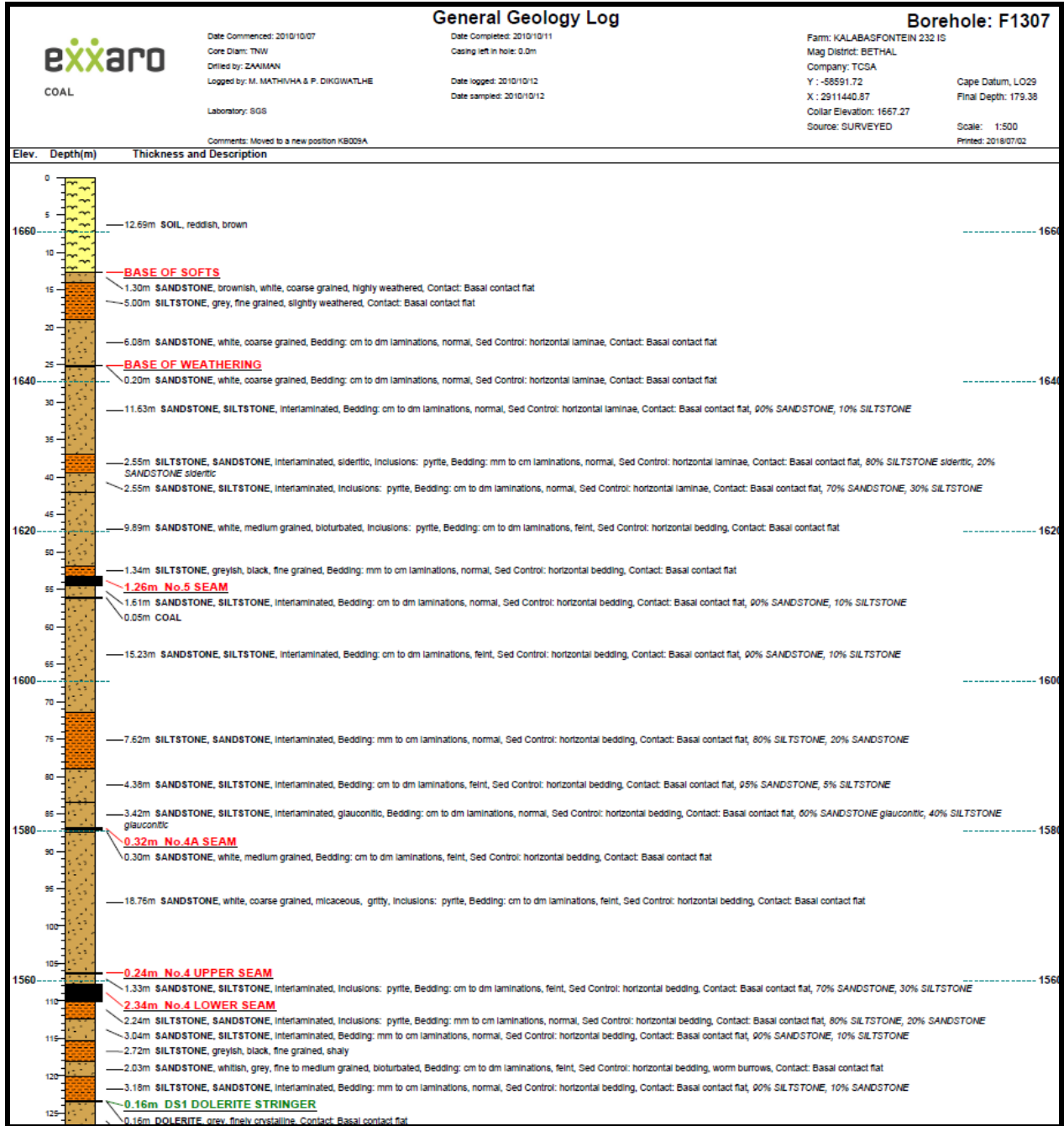
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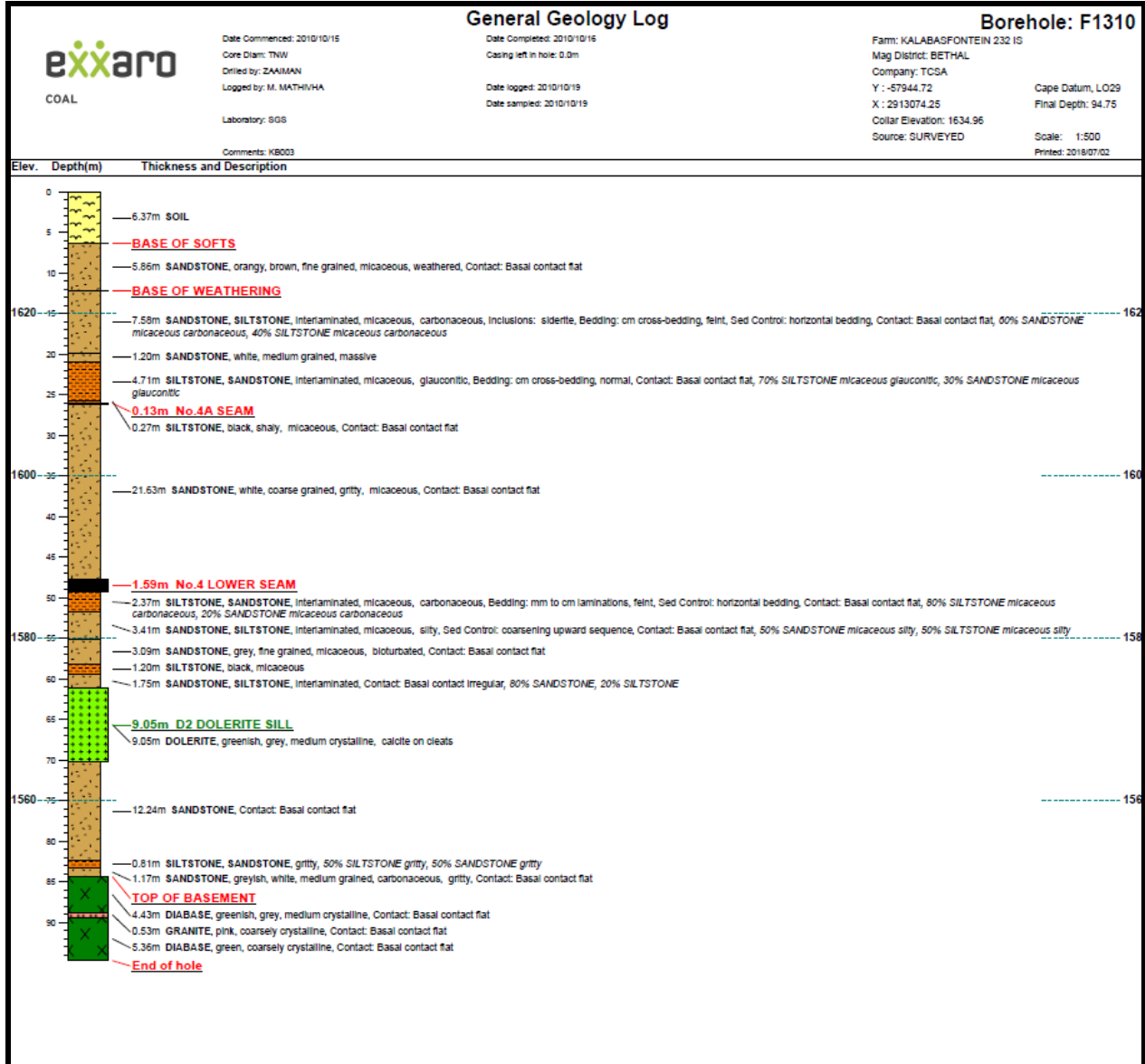
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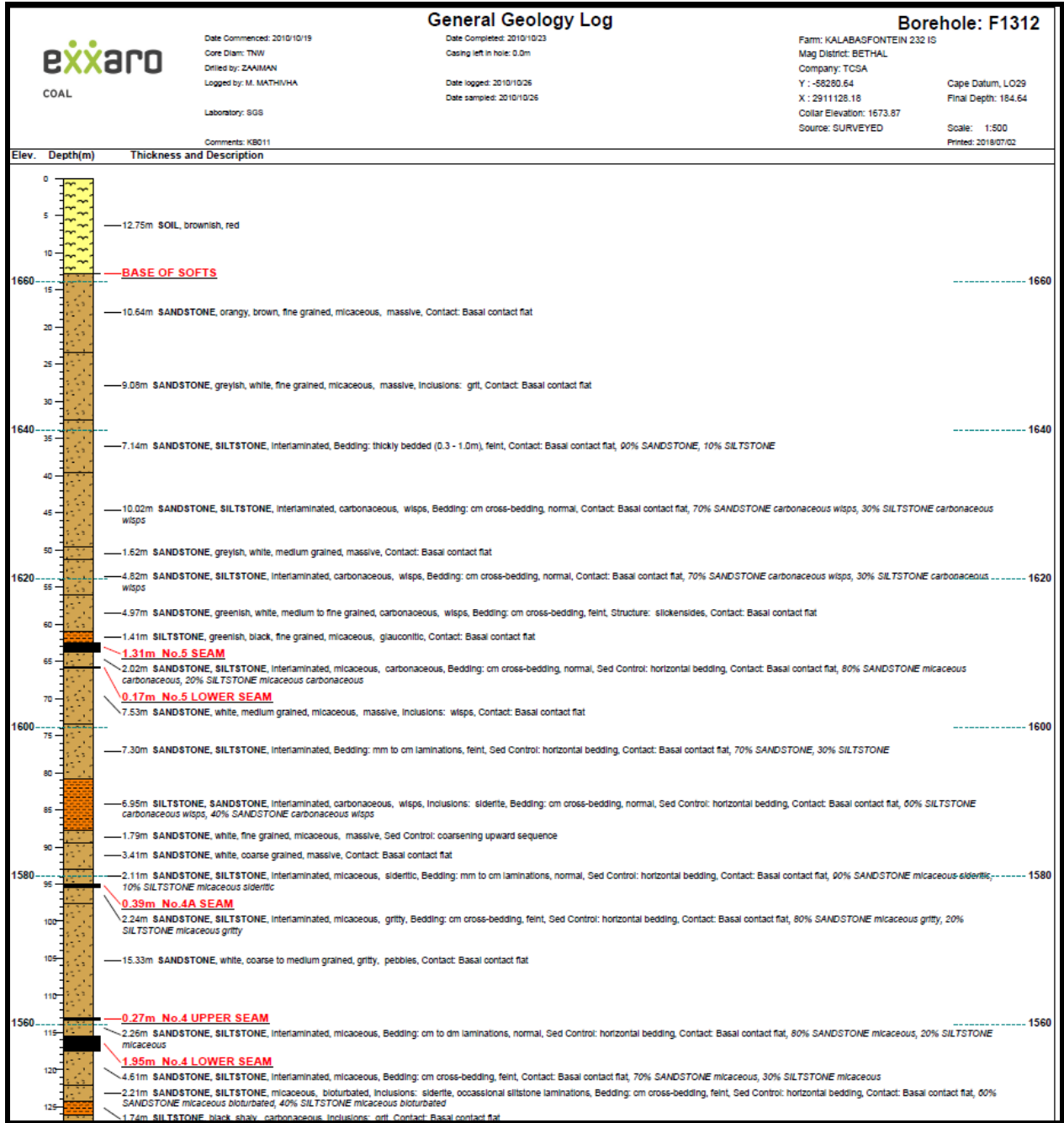
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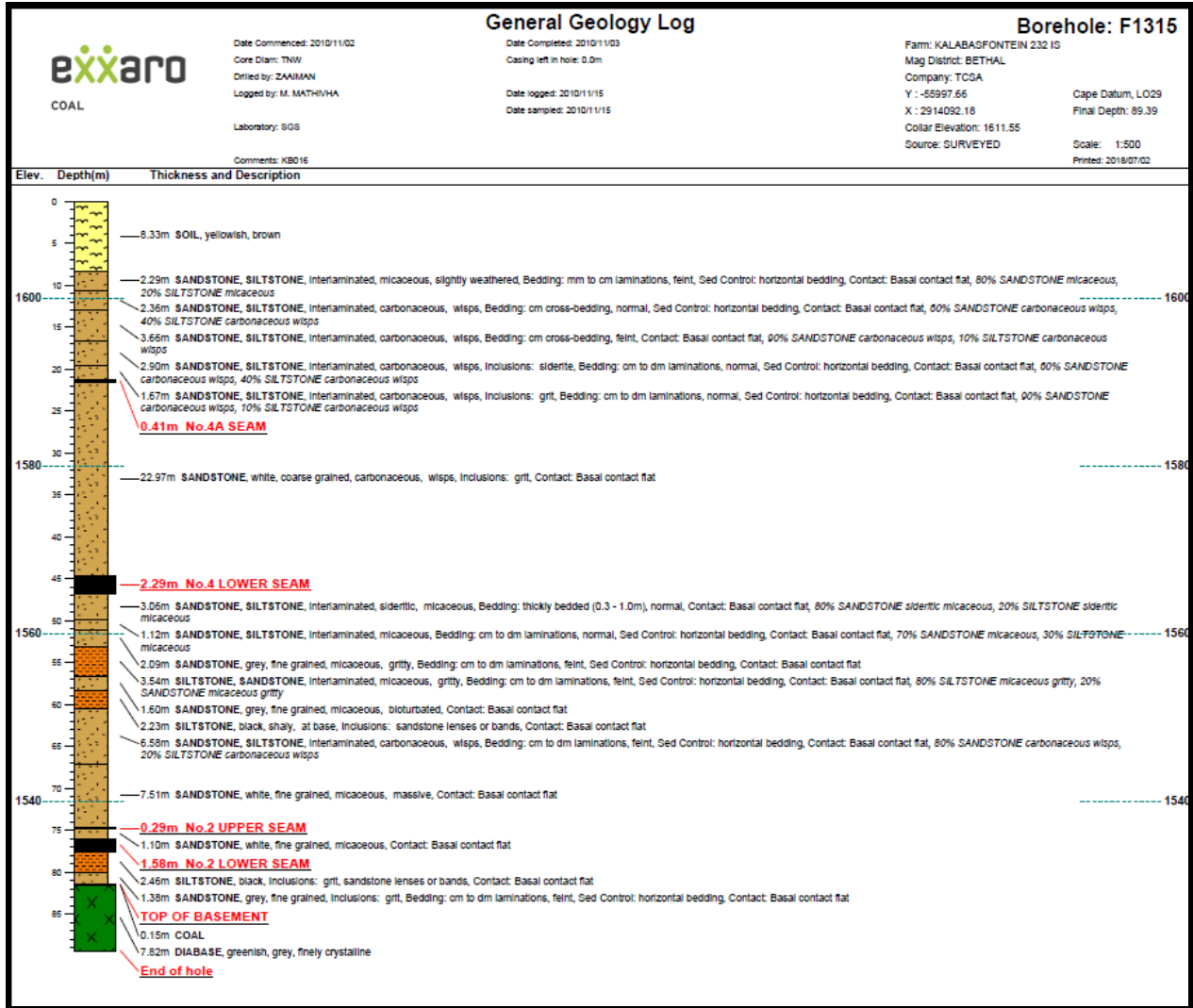
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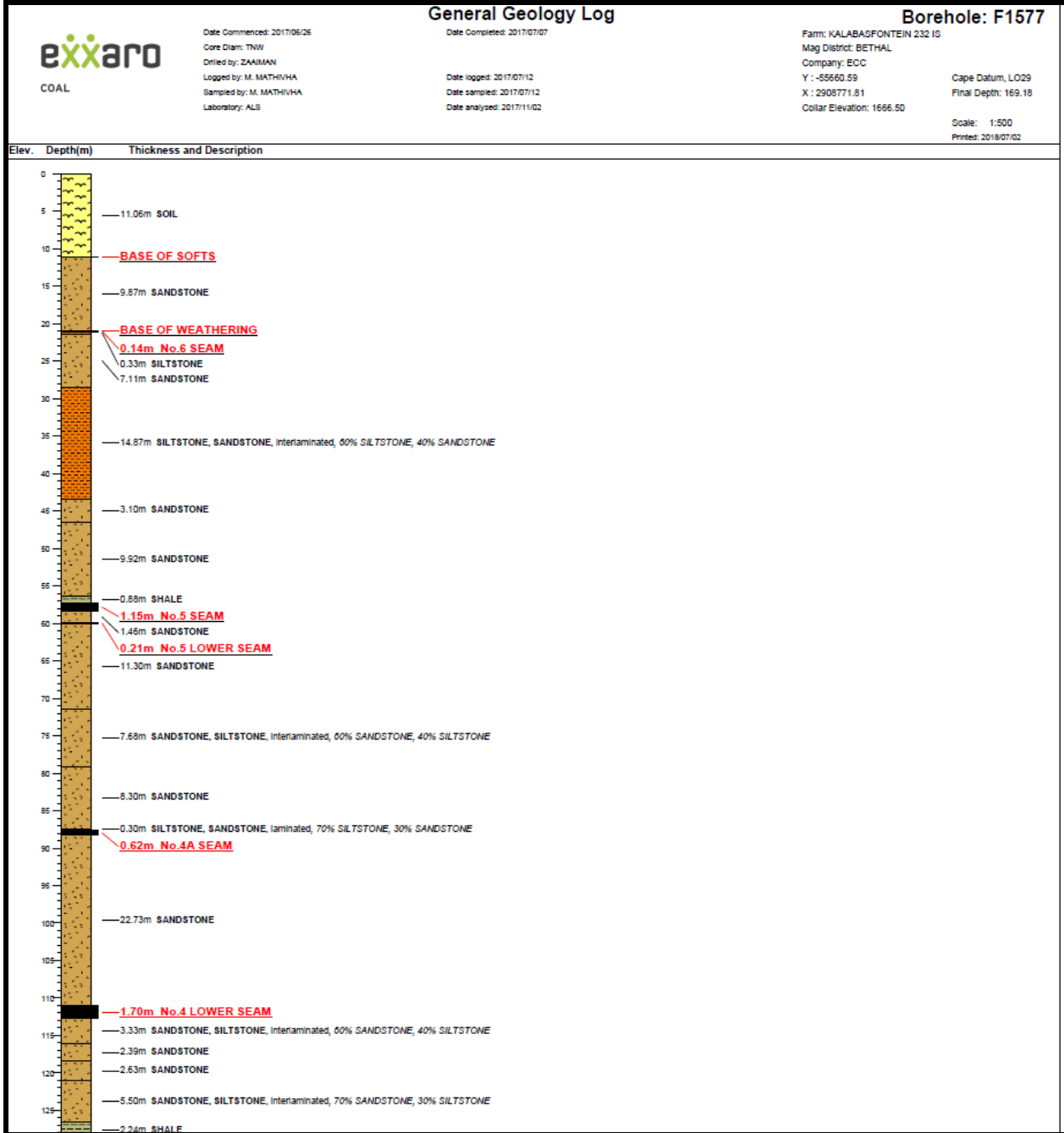
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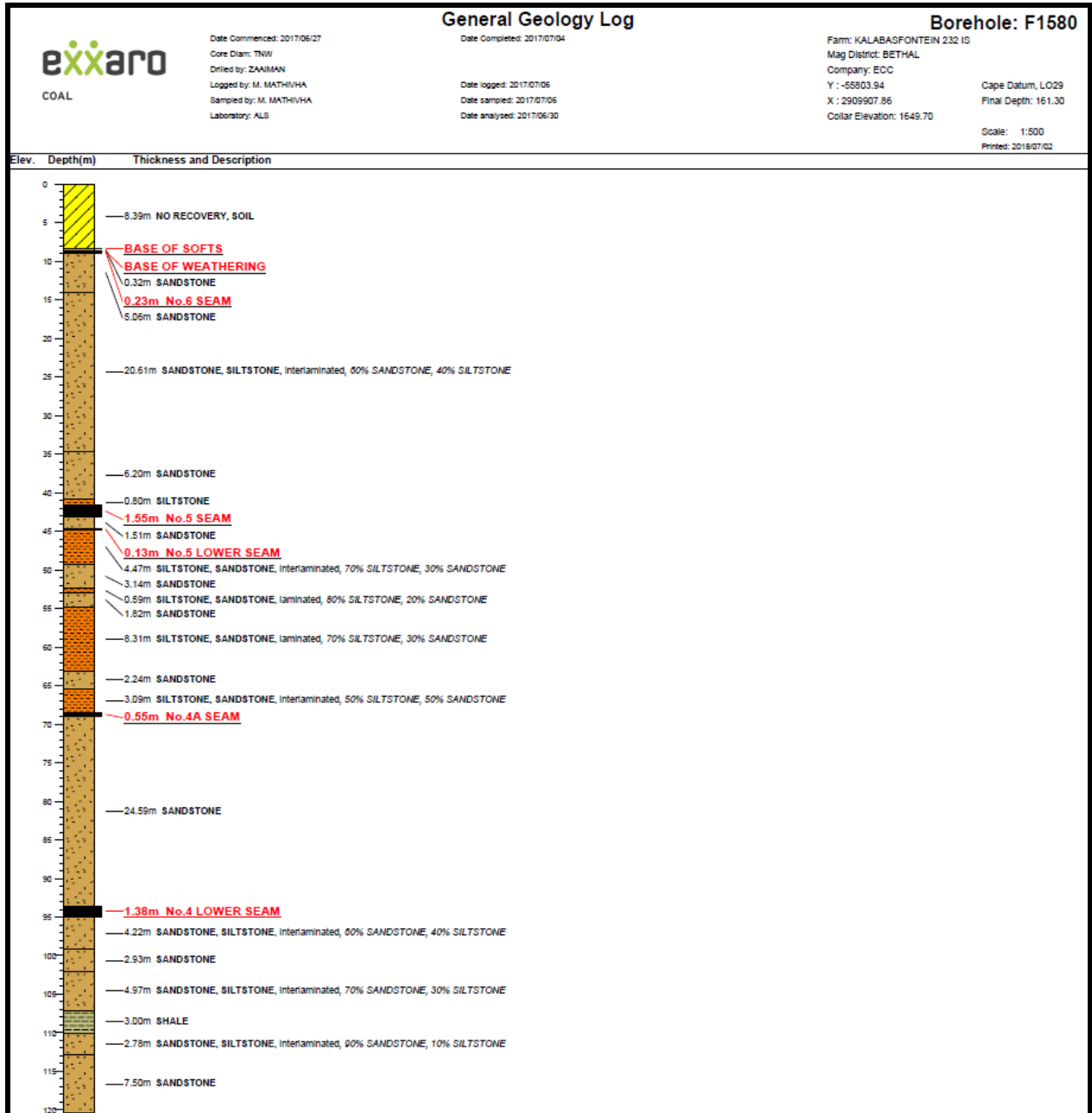
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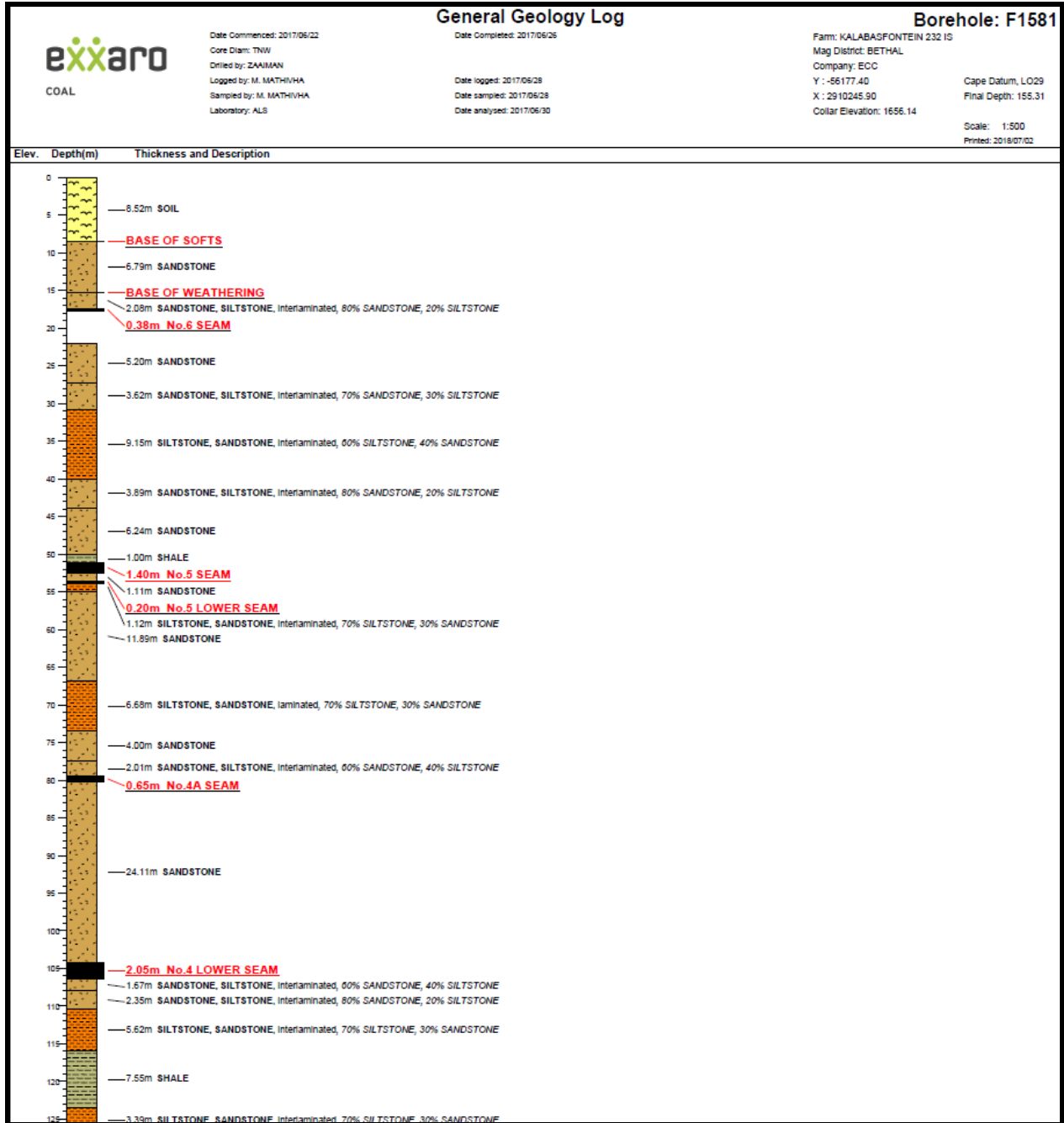
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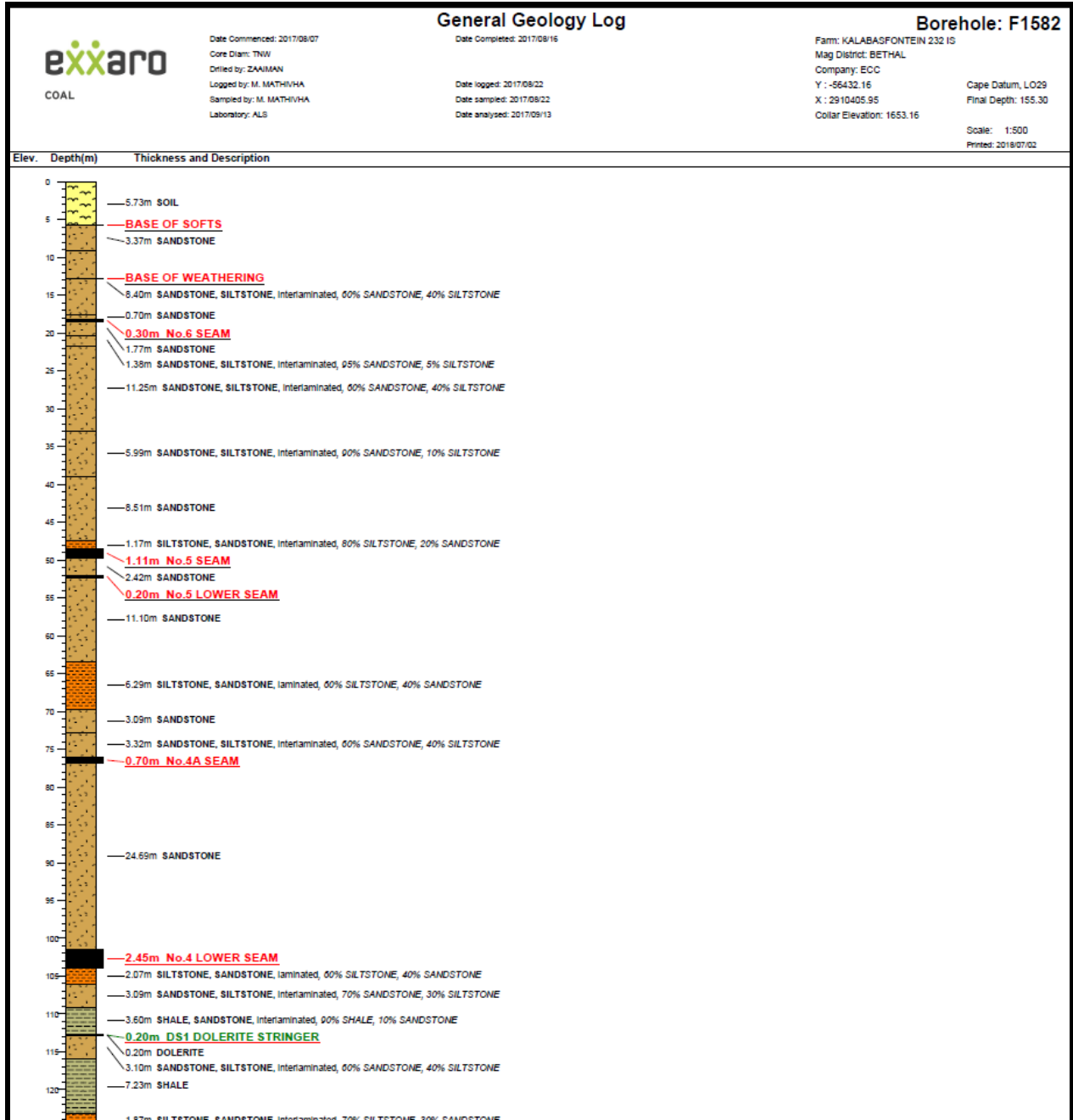
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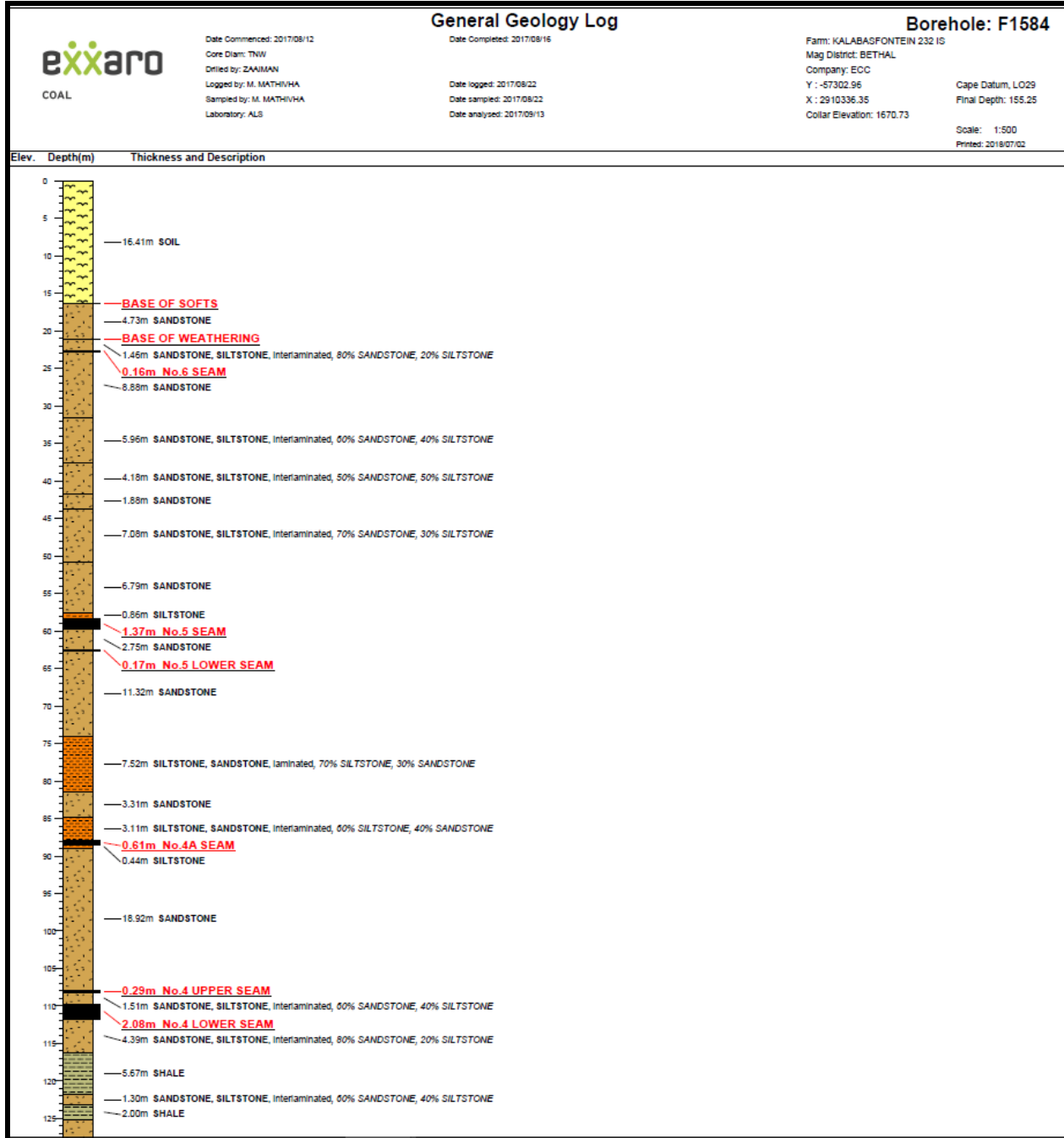
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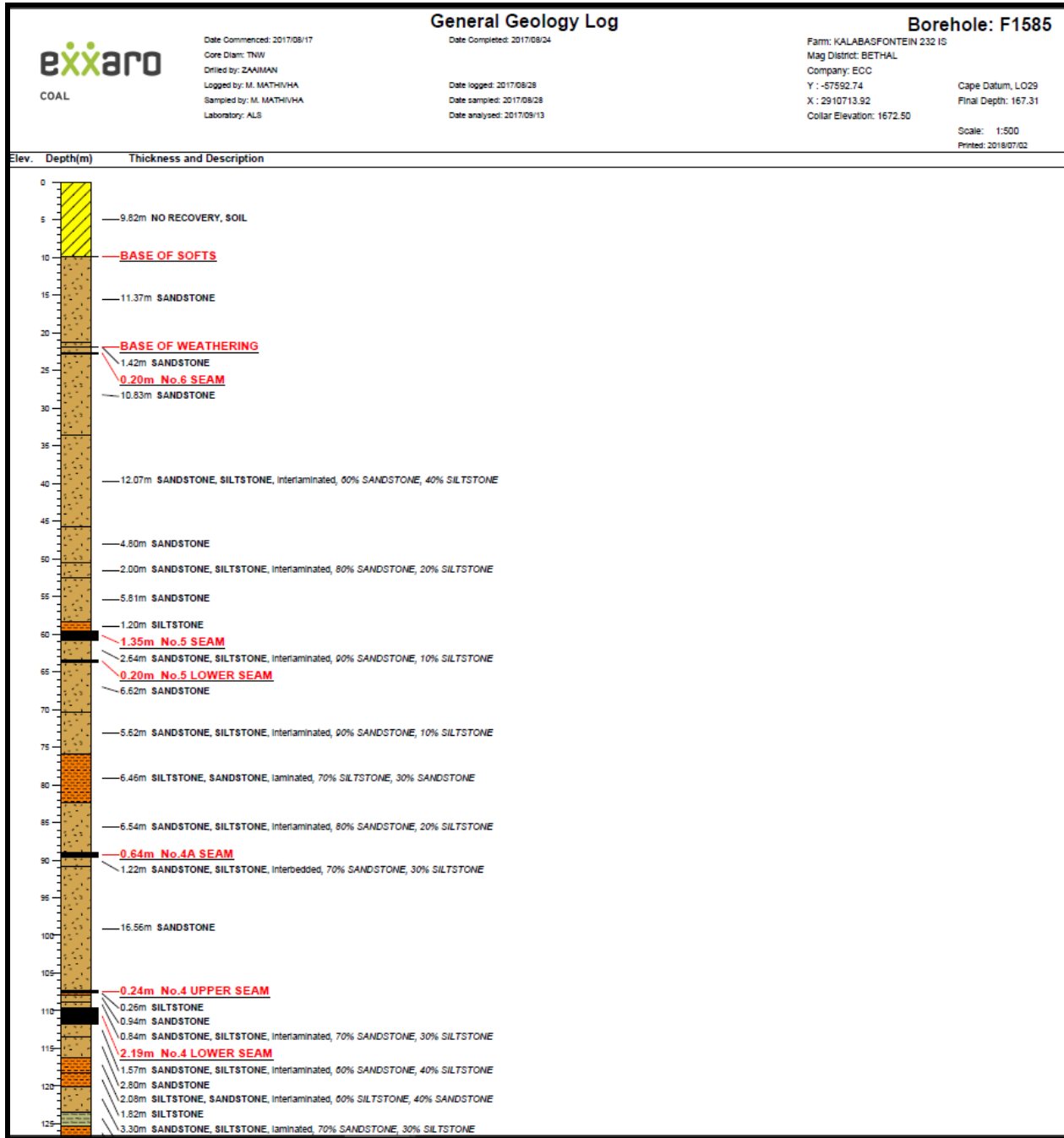
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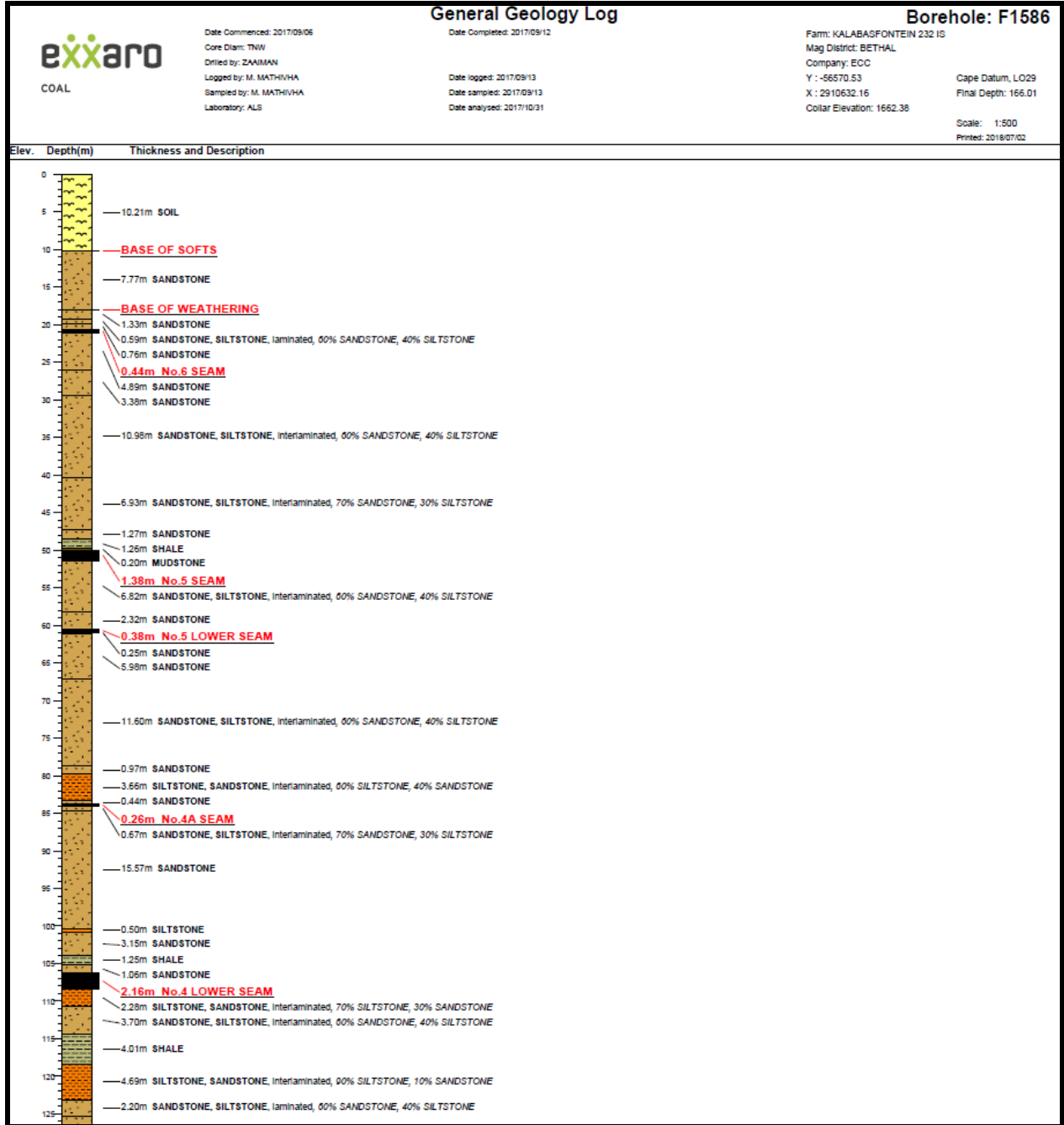
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