



REPORT NO. MK 18/480/rev.01

PHASE 1, INTERPRETIVE GEOTECHNICAL INVESTIGATION REPORT



PROPOSED TOWNSHIP DEVELOPMENT, AERORAND SOUTH, MIDDELBURG, MPUMALANGA

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Title : **PHASE 1, INTERPRETIVE GEOTECHNICAL INVESTIGATION FOR THE PROPOSED TOWNSHIP DEVELOPMENT AT AERORAND SOUTH, MIDDLEBURG, MPUMALANGA**

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Coordinates : 29°27'42.02"S, 25°48'17.83"E

Location : Aerorand South, Middelburg, Mpumalanga

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EXECUTIVE SUMMARY

Mukona Consulting Engineers (Pty) Ltd were appointed to carry out a near surface geotechnical investigation for the proposed township development at Aerorand South, Middelburg, situated in Mpumalanga.

The proposed township development is located within an area of approximately 101 hectares and comprises of a total of 624 stands earmarked for various uses such as: residential units, institutional use, municipal use and public open spaces. The proposed site is a “greenfield” site and is located within the Steve Tshwete Local Municipality, south of Middelburg in Mpumalanga.

The investigation was aimed at identifying geotechnical factors that could have an impact on the proposed development, evaluating the suitability of the site for the proposed engineering works and to enable an adequate and economical design to be prepared.

The geotechnical investigation comprised a site walkover, excavation of thirty-five (35) test pits and subsequent sampling of the in-situ soils for laboratory testing. In addition, nine (9) Dynamic Probe Light (DPL) tests and six (6) Dynamic Cone Penetrometer (DCP) tests were carried out at selected locations across the site, to provide an estimation of the consistency of the subsoil profile.

The investigation revealed that the site is underlain by transported soils (colluvium) and residual soils (sandstone, quartzitic sandstone and shale) derived from sedimentary bedrock. Pedogenic material, in the form of ferricrete, was also encountered below the site. No groundwater seepage was encountered within the test pits excavated on site.

It is anticipated that the site will classify as “soft excavation”, as per SANS 1200D, to depths of between 0.9m and 1.5m in areas where pedogenic material is encountered, and between 1.7m and 2.5m in areas where residual material is encountered.

The residual quartzitic sandstone and pedogenic material classify as **G6** (COLTO) quality material. It is therefore considered suitable for use in the construction of engineered fills or as selected layers in the pavement structure for roads.

The residual sandstone classifies as **G7** (COLTO) quality material. It is therefore considered suitable for use in the construction of engineered fills or as selected layers in the pavement structure for roads.

The site can be classified into three zones, namely; **Zone 1** - Site Class R/S, **Zone 2** - Site Class S1, and **Zone 3** - Site Class P (potential flood zone). Foundations for structures should be placed on either an engineered fill below individual strip footings, a reinforced concrete raft, or reinforced strip footing.

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1. INTRODUCTION

Mukona Consulting Engineers (Pty) Ltd were appointed by Steve Tshwete Local Municipality to carry out a feasibility-level geotechnical investigation for the proposed township development at Aerorand South, Middelburg which is situated within the Steve Tshwete Local Municipality in Mpumalanga Province.

This report describes the geotechnical investigation including fieldwork, laboratory testing and analysis, undertaken for the proposed development and provides preliminary geotechnical recommendations including site preparation, foundation type(s), earthworks and excavatability classification.

According to the Client, this geotechnical investigation acts as an infill study for a previous geotechnical investigation carried out within this site. This historic report was not made available to Mukona Consulting Engineers during this investigation.

1.1 Purpose

The purpose of the geotechnical investigation can be summarized as follows:

- Provide an overview of the geology of the site;
- Present the fieldwork and testing carried out during the geotechnical investigation;
- Assess and discuss the soil and rock profile, with a specific interest in the depth to a competent founding horizon;
- Assess groundwater conditions as encountered during the site investigation;
- Assess and provide site classification in accordance with the SAICE Code of Practice (for Single Storey Residential Buildings of Masonry Construction, 1995) in so far as it is relevant to the proposed development;
- Highlight the geotechnical considerations that may have an influence on the proposed development;
- Provide geotechnical recommendations, such as founding solutions and re-use potential of existing materials;
- Provide recommendations on the founding depths and the allowable bearing capacity to be adopted for preliminary design;
- Comment on the suitability of the site for the proposed development;
- Provide an excavatability classification for the site as per SANS1200 specification;

- Comment on the corrosivity of soils to buried metals.

1.2 Proposed Development

It is understood that the planned township is located within an area of approximately 101 hectares, and will include residential units (612 stands), institutional buildings (4 stands), municipal buildings (2 stands), public open spaces (6 stands) and construction of road pavements.

1.3 Available Information

The following published information was used during this investigation:

- The 1:250 000 scale geological series map, 2528 PRETORIA, produced by the Council for Geoscience, Pretoria;
- The 1:50 000 scale topographical map, 2529 CD MIDDELBURG, produced by the Surveyor General.
- SANS 10160-4 (2011): Basis of Structural Design and Actions for Buildings and Industrial Structures, Part 4: Seismic Actions and General Requirements for Building. SABS Standards Division; and
- Seismic hazard maps from Kijko et al. (2003) - Probabilistic Peak Ground Acceleration and Spectral Seismic Hazard Maps for South Africa. Report number 2003-0053, Council for Geoscience, Pretoria.
- Inception report for the geotechnical investigation at Aerorand South Township, Middelburg, Mpumalanga, prepared for the Steve Tshwete Local Municipality by Mukona Consulting Engineers, referenced Report No. MK/18/480, dated 13 November 2018.

1.4 Information Supplied

The following information was supplied by the Client:

- Site locality plan in pdf format;
- A layout map showing underground services (wet and dry) within the site.

2. SITE DESCRIPTION

2.1 Location

The proposed site is located south of Middelburg approximately 3km north of the N4 highway, within the Steve Tshwete Local Municipality in Mpumalanga Province. The proposed site is bound to the east by Sondagsrivier Street and Middelburg Mall. To the north it is bound by Mandela drive and a township. The remaining boundaries comprise undeveloped land.

Access to the site is via unpaved tracks along Sondagsrivier Street and Mandela Drive. The site is a “greenfield” site located at the approximate centre coordinates of 25°48'33.05"S, 29°26'53.10"E. The location of the site is shown in **Appendix A**.

2.2 Topography

The site slopes gently towards the west and northwest at a gradient of approximately 2%. The area occurs at elevations ranging between 1522m and 1537m above mean sea level (amsl).

Surface runoff, particularly during periods of heavy or prolonged rainfall is expected to be in the form of sheetwash towards the west and northwest.

An extract of the 1:50 000 topographical map series is attached in **Appendix B**.

2.3 Climate

The climate in Aerorand is generally warm in summer and moderately cold in winter. The average annual rainfall is 831mm per annum, most of which occurs in heavy isolated falls between November and April. The greatest amount of rainfall occurs in January with an average of 230mm. The average midday temperatures range from 23°C in June to 38°C in October.

The climatic regime plays a fundamental role in the development of the soil profile and the weathering of rock. Weinert (1964) demonstrated that chemical decomposition is the predominant mode of rock weathering in areas where the climatic “N-value” is less than 5. In areas where the climatic N-value is between 5 and 10, disintegration is the predominant form of weathering, although some chemical decomposition of the primary rock minerals still takes place. Where the climatic N-value is greater than 10, secondary minerals do not develop to an appreciable extent and all weathering takes place by mechanical disintegration of the rock.

Weinert’s climatic N-value for the area is less than 2. This implies that rocks are extensively weathered, often to depths of several metres, and decomposition is pronounced.

3. GEOHAZARD

3.1 Seismic Hazard / Activities

Two types of seismic activities occur in South Africa, namely:

- Regions of natural seismic activity (Zone I), and
- Regions of mining-induced and natural seismic activity (Zone II).

In accordance with the seismic hazard zones contained in SANS 10160-4 (2011), the site falls outside Zone I and Zone II, as shown in Figure 1.

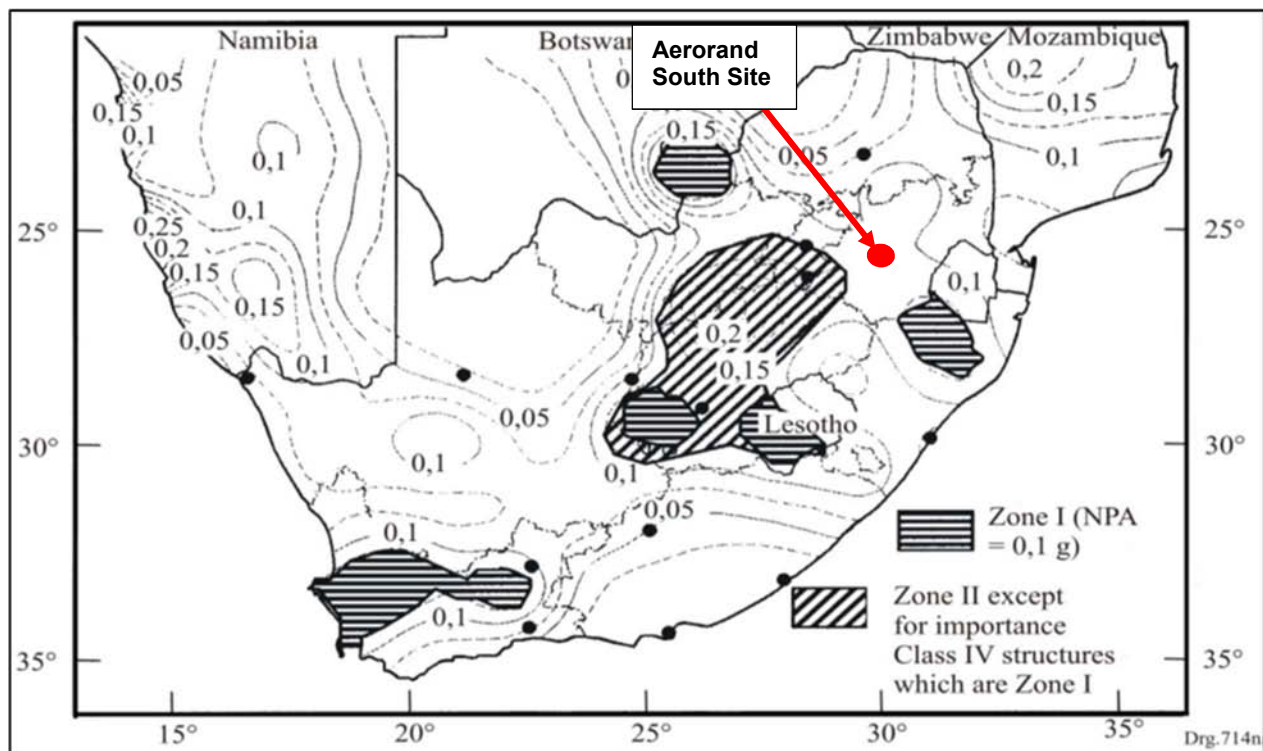


Figure 1: Seismic Hazard Zones of South Africa (SANS 10160-4, 2011)

Both the seismic hazard zones map (Figure 1 above) and the seismic hazard map of South Africa (Figure 2 below) produced by Kijko (2003) show that the site is situated in the area where the peak ground acceleration with a 10% probability of exceedance in a 50-year period is approximately 0.10 to 0.12g.

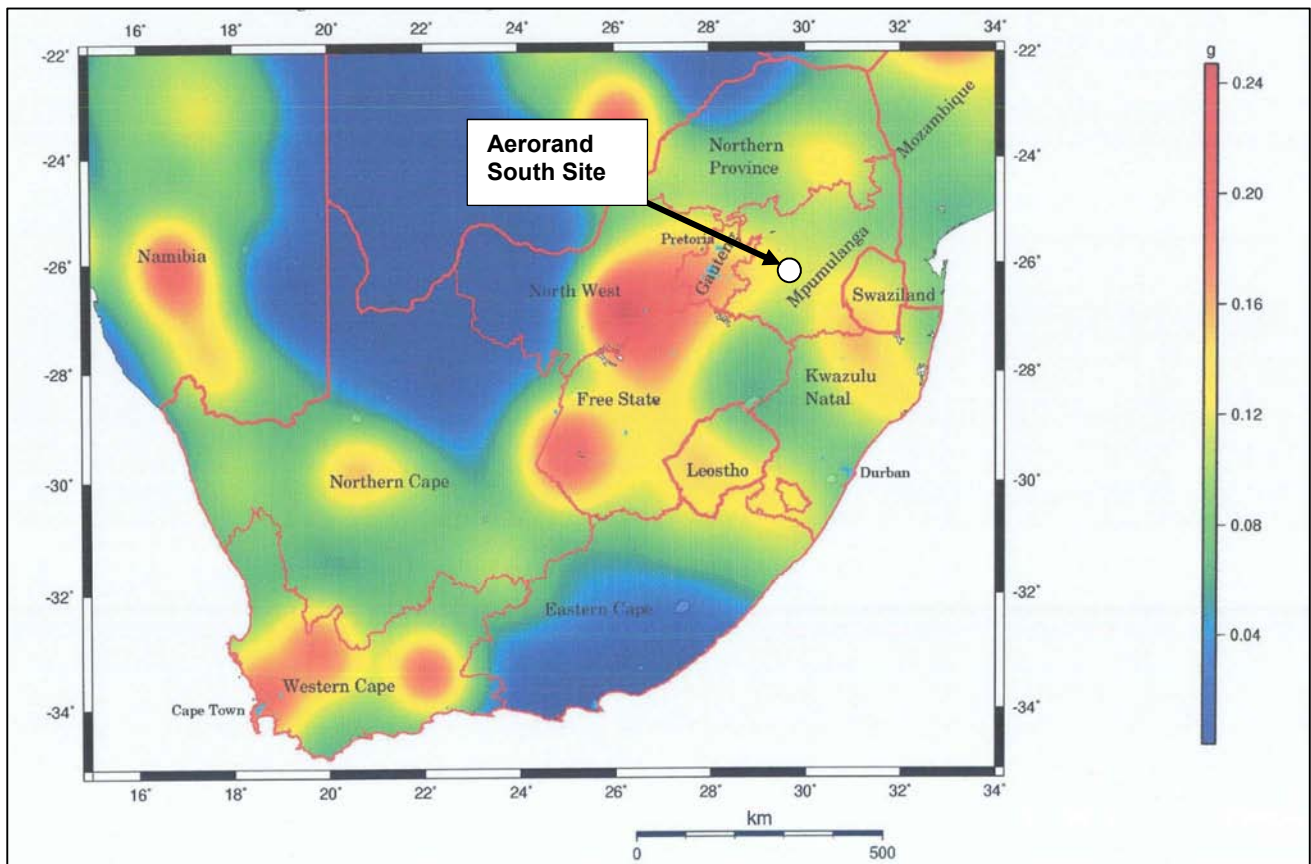


Figure 2: Seismic Hazard Map of South Africa, Kijko et. al. (2003)

3.2 Ground Subsidence

Subsidence occurs in areas with large underground cavities typically resulting from large scale shallow to very shallow mining and from dolomite/limestone dissolution. It may also appear where thick deposits of unconsolidated material exist.

No signs of previous subsidence were evident during the site investigation and no mining activity has occurred in this area.

3.3 Sinkhole Formation

Similar to subsidence, sinkhole formation occurs in areas with very large to extremely large underground cavities resulting from poorly designed shallow underground activities. Dissolution of dolomites or limestones over millions of years, may lead to cavity formations which later manifest as sinkholes.

The available geological map and field observations indicate that the site is not underlain by dolomite.

3.4 Landslides and Mudslides

The probability of landslides and mudslides occurring within this area are remote. This is primarily due to the low relief and relatively flat gradient of the area.

3.5 Rockfalls and Rockslides

The probability of the occurrence of rockfalls and rockslides is low due to the low relief and shallow gradient.

3.6 Volcanic Activities

South Africa has seen its last volcanic activity approximately 65 million years ago during the massive historical eruption of the Drakensberg Lava forming the Basaltic Drakensberg Mountain Ranges that we see today. Recent studies showed no signs of the possibility of volcanic eruption in the foreseeable future.

4. METHOD OF INVESTIGATION

Based on the “Site Investigation Code of Practice” (SAICE Geotechnical Division, 2010), which provides standards for “acceptable engineering practice”, the level of this investigation should be considered as feasibility level, which entails a detailed desktop study and a limited intrusive investigation to a maximum depth of 3m below current ground level within the footprint of the proposed development.

This investigation has accordingly been designated as a Phase 1 investigation. The requirements for a Phase 2 investigation should be based on the nature of the proposed structures.

4.1 Desktop Study

The desktop study included a review of the regional topographical and geological maps and seismic hazard maps of South Africa.

4.2 Test Pits

Thirty-five (35) test pits designated TP1 through to TP35 were excavated across the site on the 15th November 2018 (20no.) and 24th May 2019 (15no.) using a Tractor Loader Backhoe (TLB), supplied by Coastal Hire Contractors.

Each test pit, which was deemed safe to enter, was profiled by an engineering geologist in accordance with the “Guidelines for Soil and Rock Logging in South Africa”, 2nd Impression 2002, sampled as necessary and loosely backfilled.

The test pits were positioned such that broad coverage of the underlying geological and subsoil conditions could be determined. The test pit coordinates and depth of excavation are provided in Table 1.

The test pit positions are indicated on the layout drawing attached as **Appendix C**. Detailed test pit profiles and site pictures are attached in **Appendix D** respectively.

Table 1: Summary of test pit information

| TP ID. | Handheld GPS Coordinates | | Final Depth (m) | Comment |
|--------|--------------------------|---------------|-----------------|--|
| | Latitude (S) | Longitude (E) | | |
| TP01 | 25°48'23.276" | 29°26'50.236" | 1.7 | Partial refusal of TLB on residual shale |
| TP02 | 25°48'20.642" | 29°26'52.875" | 2.5 | Partial refusal of TLB on soft shale |
| TP03 | 25°48'19.577" | 29°26'50.651" | 2.3 | Partial refusal of TLB on residual shale |
| TP04 | 25°48'24.658" | 29°26'55.712" | 2.3 | Partial refusal of TLB on residual shale |
| TP05 | 25°48'21.500" | 29°26'57.558" | 1.2 | Refusal of TLB on Honeycomb Ferricrete |
| TP06 | 25°48'18.213" | 29°26'59.050" | 1.3 | Refusal of TLB on honeycomb ferricrete |
| TP07 | 25°48'28.322" | 29°27'0.802" | 2.4 | Refusal of TLB on ferruginised residual quartzitic sandstone |
| TP08 | 25°48'25.849" | 29°27'3.172" | 1.8 | Refusal of TLB on ferruginised residual quartzitic sandstone |
| TP09 | 25°48'21.614" | 29°27'1.972" | 1.4 | Refusal of TLB on ferruginised residual quartzitic sandstone |
| TP10 | 25°48'17.869" | 29°27'3.759" | 2.1 | Refusal of TLB on residual sandstone |
| TP11 | 25°48'30.512" | 29°27'6.087" | 2.3 | Refusal of TLB on residual sandstone |
| TP12 | 25°48'24.300" | 29°27'6.500" | 0.9 | Refusal of TLB on hardpan ferricrete |
| TP13 | 25°48'22.111" | 29°27'6.905" | 2.5 | Refusal of TLB on ferruginised residual quartzitic sandstone |
| TP14 | 25°48'18.467" | 29°27'6.834" | 2.0 | Partial refusal of TLB on ferruginised residual quartzitic sandstone |
| TP15 | 25°48'27.787" | 29°27'8.428" | 2.1 | Partial refusal on residual sandstone |
| TP16 | 25°48'20.936" | 29°27'9.953" | 2.5 | Refusal of TLB on ferruginised residual quartzitic sandstone |
| TP17 | 25°48'16.991" | 29°27'9.603" | 1.7 | Partial refusal of TLB on ferruginised residual quartzitic sandstone |
| TP18 | 25°48'31.695" | 29°27'11.804" | 0.9 | Refusal of TLB on honeycomb ferricrete |
| TP19 | 25°48'25.077" | 29°27'12.609" | 2.1 | Partial refusal of TLB on ferruginised residual quartzitic sandstone |
| TP20 | 25°48'17.931" | 29°27'13.033" | 1.8 | Partial refusal of TLB on quartzitic sandstone |
| TP21 | 25°48'26.78"S | 29°26'37.81"E | 2.3 | Partial refusal of TLB on very dense to very soft rock sandstone |
| TP22 | 25°48'27.74"S | 29°26'45.18"E | 2.4 | Partial refusal of TLB on boulders (Colluvium) |
| TP23 | 25°48'31.32"S | 29°26'40.19"E | 2.2 | Partial refusal of TLB on very stiff residual shale |
| TP24 | 25°48'30.24"S | 29°26'50.76"E | 0.95 | Refusal of TLB on hardpan ferricrete |
| TP25 | 25°48'32.51"S | 29°26'59.79"E | 2.4 | Partial refusal of TLB on very soft rock sandstone |
| TP26 | 25°48'38.28"S | 29°27'6.32"E | 2.3 | Partial refusal of TLB on dense ferruginised residual shale |

| Test Pit ID. | Handheld GPS Coordinates | | Final Depth (m) | Comment |
|--------------|--------------------------|---------------|-----------------|--|
| TP27 | 25°48'37.33"S | 29°26'57.09"E | 2.4 | Partial refusal of TLB on dense ferruginised residual shale |
| TP28 | 25°48'36.09"S | 29°26'46.41"E | 2.6 | Partial refusal of TLB on very soft rock shale |
| TP29 | 25°48'38.16"S | 29°26'36.96"E | 0.8 | Refusal of TLB on hardpan ferricrete |
| TP30 | 25°48'45.74"S | 29°26'38.31"E | 0.75 | Refusal of TLB on hardpan ferricrete |
| TP31 | 25°48'45.12"S | 29°26'54.38"E | 2.5 | Partial refusal of TLB on medium dense ferruginised shale |
| TP32 | 25°48'45.28"S | 29°27'4.00"E | 2.5 | Partial refusal of TLB on medium dense ferruginised shale |
| TP33 | 25°48'45.50"S | 29°27'10.60"E | 2.4 | Partial refusal of TLB on very soft rock sandstone sandstone |
| TP34 | 25°48'53.38"S | 29°27'4.83"E | 2.7 | Partial refusal of TLB on medium dense ferruginised shale |
| TP35 | 25°48'43.25"S | 29°26'45.44"E | 2.3 | Partial refusal of TLB on stiff residual shale |

4.3 Dynamic Probe Light (DPL)

Although DPL testing was not part of the scope of work for the near surface geotechnical investigation, nine (9) DPL tests were carried out adjacent to selected test pits in order to provide an empirical indication of the consistency of the subsoils with depth. The DPL tests were designated according to its position adjacent to the respective test pits.

The DPL test is carried out by driving a 36mm diameter, 90-degree cone into the soil with a 10kg hammer falling through 500mm. The penetration resistance is expressed as number of blows per 300mm penetration. The locations of the DPL tests are indicated on the layout drawing attached in **Appendix B**, with the DPL test results attached in **Appendix E**. The summary of information obtained from the DPL test is shown below in Table 2.

Table 2: Summary of DPL location and refusal depths

| DPL ID. | Handheld GPS Coordinates | | Location | Final Depth (m) | Comment |
|---------|--------------------------|---------------|------------------|-----------------|----------------|
| | Latitude (S) | Longitude (E) | | | |
| DPL02 | 25°48'20,642 | 29°26'52,875" | Adjacent to TP02 | 1.2 | Refusal of DPL |
| DPL04 | 25°48'24,658" | 29°26'55,712" | Adjacent to TP04 | 0.9 | Refusal of DPL |
| DPL05 | 25°48'21,500" | 29°26'57,558" | Adjacent to TP05 | 1.5 | Refusal of DPL |
| DPL06 | 25°48'18,213" | 29°26'59,050" | Adjacent to TP06 | 0.6 | Refusal of DPL |
| DPL08 | 25°48'25,849" | 29°27'3,172" | Adjacent to TP08 | 0.3 | Refusal of DPL |
| DPL11 | 25°48'30,512" | 29°27'6,087" | Adjacent to TP11 | 0.6 | Refusal of DPL |
| DPL14 | 25°48'18,467" | 29°27'6,834" | Adjacent to TP14 | 0.6 | Refusal of DPL |
| DPL15 | 25°48'27,787" | 29°27'8,428" | Adjacent to TP15 | 0.3 | Refusal of DPL |
| DPL20 | 25°48'17,931" | 29°27'13,033" | Adjacent to TP20 | 0.9 | Refusal of DPL |

4.4 Dynamic Cone Penetrometer (DCP)

As part of the near surface geotechnical investigation, six (6) Dynamic Cone Penetrometer (DCP) tests were carried out adjacent to selected test pits on the site.

The DCP test provides an empirical indication of the consistency of the subsoils with depth. It is carried out by driving a 20mm diameter, 60-degree cone into the soil with an 8kg hammer falling through 575mm. The penetration resistance is expressed as no. of blows per 100mm penetration. A summary of location and depths of the DCP tests are shown in Table 3. Full DCP results are presented in **Appendix F**.

Table 3: Summary of DCP location and refusal depths

| TP ID. | Handheld GPS Coordinates | | Final Depth (m) | Comment |
|--------|--------------------------|---------------|-----------------|---------------|
| | Latitude | Longitude | | |
| DCP23 | 25°48'31.32"S | 29°26'40.19"E | 1.0 | Maximum Depth |
| DCP27 | 25°48'37.33"S | 29°26'57.09"E | 1.0 | Maximum Depth |
| DCP28 | 25°48'36.09"S | 29°26'46.41"E | 1.0 | Maximum Depth |
| DCP29 | 25°48'38.16"S | 29°26'36.96"E | 0.2 | Refusal |
| DCP32 | 25°48'45.28"S | 29°27'4.00"E | 1.0 | Maximum Depth |
| DCP34 | 25°48'53.38"S | 29°27'4.83"E | 1.0 | Maximum Depth |

4.5 Laboratory Testing

To confirm the visual assessments of the engineering properties of the soil, a number of representative disturbed samples were taken and submitted for laboratory testing. The laboratory testing comprised of the following:

- Sixteen (16) foundation indicator tests were taken to determine the basic engineering properties of the in-situ materials;
- Three (3) bulk samples were taken for moisture / density relationship and CBR testing to determine the compaction characteristics of the in-situ material;
- Six (6) samples were taken for chemical tests to determine the pH and conductivity characteristics of the in-situ material.

The individual test results are summarised and discussed in section 6.

5. REGIONAL & SITE GEOLOGY

5.1 Regional Geology

From a review of the 1:250 000 geological series map, **2528 PRETORIA**, the site is mantled by shale, sandstone, conglomerate and some volcanic rocks. The sedimentary rocks belong to the Loskop Formation within the Transvaal Sequence. The sandstone within the area is pink to grey in colour with massive to coarsely bedded feldspathic texture with grit and conglomeratic layers, interbedded with lesser maroon fine-grained sandstone and siltstone.

These rocks are underlain by tillite and shale of the Dwyka Group within the Karoo Sequence. An extract of the geological map is presented in **Appendix G**.

5.2 Site Geology

A summary of the generalised soil profiles encountered during the site investigation is provided in Table 4.

Table 4: Summary of test pit profiles

| TP ID. | Depth (m) | | | | | | | | | | | | |
|--------|-------------|---------------|-----------------------------|-----------------------------|--|-------------------------------|----------------------|-------------------------|-----------------|----------------|------------|-------------|----------------------------------|
| | Transported | Pebble Marker | Reworked residual sandstone | Residual sandstone | Reworked Residual Quartzitic Sandstone | Residual Quartzitic Sandstone | Quartzitic Sandstone | Ferricrete | Shaly Sandstone | Residual Shale | Soft Shale | Groundwater | Depth of Refusal/ End of hole |
| TP01 | 0-0.45 | - | - | - | - | - | - | - | - | 0.45-1.7 | - | - | 1.7 |
| TP02 | 0-0.45 | - | - | - | - | - | - | - | - | 0.45-1.7 | 1.7-2.5 | - | 2.5 |
| TP03 | 0-0.5 | - | - | - | - | - | - | - | - | 0.5-2.3 | - | - | 2.3 |
| TP04 | 0.0-0.2 | 0.2-0.7 | - | - | - | - | - | - | - | 0.7-2.3 | - | - | 2.3 |
| TP05 | 0.0-0.25 | - | - | 0.25-0.5 | - | - | - | 0.5-1.2 (honeycomb) | - | - | - | - | 1.2 |
| TP06 | 0.0-0.5 | - | - | 0.5-1.2 (ferruginised) | - | - | - | 1.2-1.35 (honeycomb) | - | - | - | - | 1.3 |
| TP07 | 0.0-0.4 | - | 0.4-0.9 | - | - | 0.9-2.4 (ferruginised) | - | - | - | - | - | - | 2.4 |
| TP08 | 0.0-0.25 | - | - | - | - | 0.25-1.8 (ferruginised) | - | - | - | - | - | - | 1.8 |
| TP09 | 0.0-0.4 | - | 0.4-0.8 | - | - | 0.8-1.4 (ferruginised) | - | - | - | - | - | - | 1.4 |
| TP10 | 0.0-0.52 | - | - | 0.52-1.5 (ferruginised). | - | - | - | - | - | - | - | - | 2.1 |
| | | | | 1.5-2.1 | | | | | | | | | |
| TP11 | 0.0-0.5 | - | - | 0.5-2.3 | - | - | - | - | - | - | - | - | 2.3 |
| TP12 | 0.0-0.3 | - | - | - | - | - | - | 0.3-0.9 (nodular) | - | - | - | - | 0.9 |
| TP13 | 0.0-0.45 | 0.45-0.7 | - | - | - | 0.7-2.5 (ferruginised) | - | - | - | - | - | - | 2.5 |
| TP14 | 0.0-0.3 | 0.3-0.5 | - | - | - | 0.5-0.9. | - | - | - | - | - | - | 2 |

| TP ID. | Depth (m) | | | | | | | | | | | | |
|--------|-------------|---------------|-----------------------------|----------------------------|--|------------------------------------|----------------------|------------------------|-----------------|----------------|------------|-------------|----------------------------------|
| | Transported | Pebble Marker | Reworked residual sandstone | Residual sandstone | Reworked Residual Quartzitic Sandstone | Residual Quartzitic Sandstone | Quartzitic Sandstone | Ferricrete | Shaly Sandstone | Residual Shale | Soft Shale | Groundwater | Depth of Refusal/ End of hole |
| | | | | | | 0.9-2.0 (ferruginised) | | | | | | | |
| TP15 | 0.0-0.3 | - | 0.3-0.9 | 0.9-1.6 (ferruginised). | - | - | - | - | - | - | - | - | 2.1 |
| | | | | 1.6-2.1 | | | | | | | | | |
| TP16 | 0.0-0.4 | - | - | - | 0.4-0.8 | 0.8-2.5 (ferruginised) | - | - | - | - | - | - | 2.5 |
| TP17 | 0.0-0.3 | 0.3-0.4 | - | - | - | 0.4-1.7 (ferruginised) | - | - | - | - | - | - | 1.7 |
| TP18 | 0.0-0.4 | - | - | 0.4-0.7 | - | - | - | 0.7-0.9 (honeycomb) | - | - | - | - | 0.9 |
| TP19 | 0.0-0.5 | - | - | - | - | 0.5-2.3 (ferruginised) | - | - | - | - | - | - | 2.1 |
| TP20 | 0.0-0.4 | - | - | - | - | 0.4-1.3 (ferruginised); 1.3-1.8 | 1.3-1.8 | - | - | - | - | - | 1.8 |
| TP21 | 0.0-1.4 | - | - | 1.4-1.8 | - | - | - | - | 1.8-2.3 | - | - | - | 2.3 |
| TP22 | 0.0-1.1 | - | - | - | - | - | - | - | - | - | - | - | 2.4 |
| | 1.1-2.4 | | | | | | | | | | | | |
| TP23 | 0.0-0.8 | - | - | - | - | - | - | | - | 0.8-1.9 | - | - | 2.2 |
| | | | | | | | | | | 1.9-2.2 | | | |
| TP24 | 0.0-0.55 | - | - | - | - | - | - | 0.55-0.85 | - | - | - | - | 0.95 |
| | | | | | | | | 0.85-0.95 | | | | | |
| TP25 | 0.0-0.3 | - | - | - | - | - | - | - | 1.2-2.3 | - | - | - | 2.3 |
| | 0.3-1.2 | | | | | | | | | | | | |

| TP ID. | Depth (m) | | | | | | | | | | | | |
|--------|-------------|---------------|-----------------------------|--------------------|--|-------------------------------|----------------------|------------|-----------------|----------------|------------|-------------|----------------------------------|
| | Transported | Pebble Marker | Reworked residual sandstone | Residual sandstone | Reworked Residual Quartzitic Sandstone | Residual Quartzitic Sandstone | Quartzitic Sandstone | Ferricrete | Shaly Sandstone | Residual Shale | Soft Shale | Groundwater | Depth of Refusal/ End of hole |
| TP26 | 0.0-0.3 | - | - | - | - | - | - | - | - | 1.1-2.3 | - | - | 2.3 |
| | 0.3-1.10 | | | | | | | | | | | | |
| TP27 | 0.0-0.25 | 1.25-1.7 | - | - | - | - | - | - | - | 1.7-2.4 | - | - | - |
| | 0.25-1.25 | | | | | | | | | (ferruginised) | | | |
| TP28 | 0.0-0.45 | - | - | - | - | - | - | - | - | 0.45-1.40 | 1.65 – 2.5 | - | 2.5 |
| | | | | | | | | | | 1.40 – 1.65 | | | |
| TP29 | 0.0-0.5 | - | - | - | - | - | - | 0.5-0.80 | - | | - | - | 0.8 |
| TP30 | 0.0-0.70 | | | | | | | 0.7-0.75 | | | | | 0.75 |
| TP31 | 0.0-1.8 | 1.8-1.95 | - | - | - | - | - | - | - | 1.95-2.5 | - | - | 2.5 |
| TP32 | 0.0-2.0 | 2.0-2.2 | | | | | | | | 2.2-2.5 | | | 2.5 |
| TP33 | 0.0-0.8 | 0.8-1.4 | - | - | - | - | - | - | 1.4-2.4 | | - | - | 2.4 |
| TP34 | 0.0-2.4 | - | | | | | | | - | 2.4-2.7 | | | 2.7 |
| TP35 | 0.0-1.2 | | - | - | - | - | - | - | | 1.2-2.3 | - | - | 2.3 |

5.2.1 Transported Material

The colluvium blankets the entire site and was described as a “dry, brownish grey, loose to medium dense, silty SAND with scattered black ferruginised gravels, with abundant fine roots”. This horizon occurs at surface and extends to an average depth of 0.4m below current ground level.

In four (4) test pits, the transported layer is underlain by a (300mm thick) pebble marker which comprises light brown, dense, silty SAND, with abundant sub-rounded quartz and sandstone pebbles.

5.2.2 Residual Sandstone (fine-grained)

The residual sandstone layer encountered was overlain by a reworked layer as well as a ferruginised residual layer in some of the test pits.

The **ferruginised residual sandstone** was encountered in three (3) test pits and was described as “reddish brown grey stained orange, medium dense to dense, clayey silty SAND with abundant ferruginised black gravels”. This horizon was intersected to depths ranging between 1.2m and 1.6m below current ground level.

The **residual sandstone** layer encountered in six (6) test pits was described as “yellowish brown, dense to very dense, ferruginised GRAVEL in a matrix of silty sand”. This horizon was intersected to depths ranging between 0.5m and 2.3m below current ground level.

5.2.3 Residual Quartzitic Sandstone

The residual quartzitic sandstone was intersected in nine (9) test pits and is typically slightly ferruginised. The residual quartzitic sandstone was described as reddish brown, dense to very dense, clayey silty SAND with minor to abundant grey mottled orange, coarse grained sandstone cobbles. This horizon was intersected to depths ranging between 1.3m and 2.4m below current ground level.

5.2.4 Soft Quartzitic Sandstone

This horizon was only encountered at one test pit (TP 20), and is described as “brownish pink, highly weathered coarse grained, very soft to soft sandstone rock”. This horizon was intersected at depths ranging between 1.3m and 1.8m below current ground level.

5.2.5 Shaly Sandstone

The shaly sandstone was encountered in three (3) test pits and is described as “purple – red/purple yellowish grey, very highly weathered to completely weathered, fine to medium grained, very dense to very soft rock”. This horizon was intersected at depths ranging between 1.2m and 2.4m below current ground level.

5.2.6 Pedogenic Material (Ferricrete)

Honeycombed ferricrete was encountered in three (3) test pits and was described as “yellowish brown, dense to very dense, clayey silty SAND, in a matrix of subangular sandstone and quartz pebbles”. This horizon was intersected to depths ranging between 0.9m and 1.35m below current ground level.

5.2.7 Residual Shale

The residual shale was encountered in four (4) test pits and was described as “yellow brown and red brown, stiff to very stiff, silty CLAY with abundant red and yellowish brown (interlayered), laminated shale fragments with occasional patches of light grey silty CLAY”. This horizon was intersected to depths ranging between 1.7m and 2.3m below current ground level.

In one test pit, TP02, very soft to soft rock (shale) was encountered at depths between 1.7m and 2.5m below ground surface. The shale was described as “red and yellowish brown (interlayered), laminated, fine grained, shale fragments with minor patches of light grey silty clay”.

5.3 Groundwater

No groundwater seepage was recorded in any of the test pits excavated during this investigation. However, ferruginisation below the transported soils and within the residual soils, in some test pits, is indicative of a fluctuating water regime at shallow depths within the soil profile.

6. GEOTECHNICAL EVALUATION

The results of laboratory tests carried out on samples recovered from site are summarized and discussed in the sections below and are included as **Appendix H**.

6.1 Engineering and Material Characteristics

Thirteen (13) disturbed soil samples, considered to be representative of the material on site, were subjected to foundation indicator testing (as per SANS 3001 test methods). The laboratory testing was conducted by Soillab Laboratory Services. The results are attached in **Appendix H1** and are summarized in Table 5.

Table 5: Summary of foundation indicator test results

| Test Pit ID. | Depth (mm) | Description | Soil Composition (USCS) | | | | | Atterberg Limits | | | GM | NMC | PE | USCS | AASHTO |
|--|------------|-------------------------------|-------------------------|----------|----------|----------|------------|------------------|--------|--------|------|------|----|-------|------------|
| | | | % Passing 0.425mm | Clay (%) | Silt (%) | Sand (%) | Gravel (%) | LL (%) | PI (%) | LS (%) | | | | | |
| COLLUVIUM | | | | | | | | | | | | | | | |
| TP18 | 0.0-0.4 | Silty SAND | 84 | 13 | 14 | 71 | 2 | — | NP | 0 | 0.94 | — | L | SM | A-2-4 (0) |
| RESIDUAL SHALE | | | | | | | | | | | | | | | |
| TP01 | 0.45-1.7 | Clayey SAND with gravel | 41 | 11 | 22 | 37 | 30 | 35 | 13 | 6.5 | 1.74 | 9.5 | L | SC | A-2-6 (1) |
| TP02 | 0.9-2.5 | Sandy CLAY | 71 | 24 | 27 | 44 | 5 | 34 | 13 | 6.5 | 0.94 | 10.1 | L | CL | A-6(4) |
| REWORKED RESIDUAL SANDSTONE | | | | | | | | | | | | | | | |
| TP15 | 0.3-0.9 | Silty clayey SAND | 87 | 20 | 24 | 54 | 2 | 22 | 7 | 3.5 | 0.72 | 2.7 | L | SM-SC | A-4 (0) |
| RESIDUAL SANDSTONE | | | | | | | | | | | | | | | |
| TP11 | 0.5-2.5 | Silty clayey SAND | 80 | 11 | 24 | 60 | 5 | 17 | 5 | 1.5 | 0.93 | 3.3 | L | SM-SC | A-2-4 (0) |
| TP15 | 0.9-1.6 | Clayey SAND | 64 | 14 | 23 | 49 | 14 | 26 | 8 | 4 | 1.24 | — | L | SC | A-4 (0) |
| TP15 | 1.6-2.1 | Sandy CLAY | 91 | 20 | 53 | 26 | 1 | 43 | 19 | 5 | 0.4 | 13.1 | M | CL | A-7-6 (13) |
| TP18 | 0.4-0.7 | Clayey SAND with gravel | 56 | 11 | 15 | 55 | 19 | 23 | 9 | 4 | 1.52 | 3.5 | L | SC | A-2-4 (0) |
| RESIDUAL QUARTZITIC SANDSTONE | | | | | | | | | | | | | | | |
| TP13 | 0.7-2.5 | Clayey SAND | 54 | 21 | 21 | 48 | 10 | 36 | 13 | 6.5 | 1.35 | 7.2 | L | SC | A-6(2) |
| TP16 | 0.39-1.3 | Silty clayey SAND | 44 | 6 | 15 | 72 | 7 | 24 | 7 | 2.5 | 1.79 | - | L | SM-SC | A-2-4 (0) |
| TP16 | 1.3-2.5 | Clayey SAND | 59 | 15 | 23 | 55 | 7 | 32 | 12 | 5.5 | 1.26 | 8 | L | SC | A-6 (1) |
| PEDOGENIC MATERIAL | | | | | | | | | | | | | | | |
| TP12 | 0.3-0.9 | Silty SAND with gravel | 49 | 3 | 15 | 61 | 21 | — | NP | 0 | 1.73 | — | L | SM | A-1b (0) |
| TP18 | 0.7-0.9 | Silty clayey SAND with gravel | 47 | 8 | 15 | 53 | 24 | 26 | 6 | 2 | 1.7 | 3.7 | L | SM-SC | A-1b (0) |
| Notes: GM = Grading Modulus; LL = Liquid Limit; PI = Plasticity Index; LS = Linear Shrinkage; NMC = Natural Moisture Content; PE = Potential Expansiveness; USCS = Unified Soil Classification System; AASHTO = American Association of State Highway Officials; SC = Clayey Sands, poorly-graded, sand-clay mixtures; CL = Inorganic Clay of low to medium plasticity, gravelly clays, sandy clay, silty clay; SM = Silty Sand, sand-silt mixture; Nd = Not Determined | | | | | | | | | | | | | | | |

6.2 Compaction Characteristics Tests

Three (3) representative disturbed soil samples were submitted for moisture / density relationship and CBR (strength) tests and the results are attached in **Appendix H2** and are summarized in Table 6.

Table 6: Summary of compaction characteristics and CBR results

| Test Pit ID. | Depth (mm) | Description | OMC (%) | MDD (kg/m3) | Max Swell (%) | CBR at Mod. AASHTO Compaction Effort | | | | COLTO |
|-------------------------------|------------|-------------------------------|---------|-------------|---------------|--------------------------------------|--------|--------|--------|-------|
| | | | | | | 90 (%) | 93 (%) | 95 (%) | 98 (%) | |
| RESIDUAL SANDSTONE | | | | | | | | | | |
| TP18 | 0.4-0.7 | Clayey SAND with gravel | 8.1 | 2133 | 0 | 15 | 20 | 24 | 33 | G7 |
| RESIDUAL QUARTZITIC SANDSTONE | | | | | | | | | | |
| TP16 | 0.39-1.3 | Silty clayey SAND | 7.4 | 2157 | 0.1 | 19 | 30 | 41 | 65 | G6 |
| PEDOGENIC MATERIAL | | | | | | | | | | |
| TP18 | 0.7-0.9 | Silty clayey SAND with gravel | 8.6 | 2157 | 0 | 19 | 25 | 30 | 39 | G6 |

6.3 Chemical Tests

Three (3) samples were submitted for chemical tests to determine the pH and conductivity characteristics of the in-situ material.

Corrosive soils contain chemical constituents that can react with construction materials, such as concrete and ferrous metals, that may damage foundations and buried pipelines. Electrical resistivity, chloride content, and pH level are indicators of the soil's tendency to corrode ferrous metals. Soil corrosion is a geologic hazard that affects buried metals and concrete that is in direct contact with soil or bedrock. Metals are typically attacked by chloride solutions, whereas high sulfate levels are harmful to concrete.

Guideline values for interpretation of soil conductivity is presented in Table 7 and Table 8.

Table 7: Guideline values for interpretation of soil conductivity.

| Soil Conductivity (mS/m) | Resistivity (R) Ohm/cm | Degree of Corrosiveness |
|--------------------------|------------------------|-------------------------|
| More than 50 | 0 – 2 000 | Extremely corrosive |
| 25-50 | 2 000 – 4 000 | Very corrosive |
| 20-25 | 4 000 – 5 000 | Corrosive |
| 10-20 | 5 000 – 10 000 | Mildly corrosive |
| Less than 10 | >10 000 | Not generally corrosive |

Table 8: Guideline values for interpretation of pH tests

| pH | Degree of Acidity |
|-----------|---------------------|
| < 4.0 | Extremely acidic |
| 4 - 5.4 | Strongly acidic |
| 5.5 - 6.4 | Moderately Acidic |
| 6.5 - 7.0 | Slightly Acidic |
| 7.1 - 7.4 | Slightly Alkaline |
| 7.5 - 8.5 | Moderately Alkaline |
| >8.4 | Strongly Alkaline |

The pH and conductivity results are included as **Appendix H3** and a summary of the results is presented in Table 9.

Table 9: Interpretation of conductivity tests

| TP ID. | Depth (m) | Material Description | Conductivity mS/m | Corrosiveness | pH | Degree of Acidity |
|--------------------------------------|-----------|-------------------------------|-------------------|-------------------------|------|-------------------|
| RESIDUAL SANDSTONE | | | | | | |
| TP18 | 0.4-0.7 | Clayey SAND with gravel | 5.8 | Not generally corrosive | 6.28 | Moderately Acidic |
| RESIDUAL QUARTZITIC SANDSTONE | | | | | | |
| TP16 | 0.39-1.3 | Silty clayey SAND | 0.9 | Not generally corrosive | 6.24 | Moderately Acidic |
| PEDOGENIC MATERIAL | | | | | | |
| TP18 | 0.7-0.9 | Silty clayey SAND with gravel | 3.8 | Not generally corrosive | 6.58 | Slightly Acidic |

6.4 Discussion of Laboratory Results

6.4.1 Colluvium

The **Transported Soils** (1 sample) classifies as silty SAND with gravel (**SM**) in terms of the United Soils Classification System (USCS). The **SM** sample has a coarse fraction (>0.075mm) of 73% and is non-plastic. It exhibits low potential expansiveness based on the Van der Merwe method of heave prediction.

It classifies as A-2-4 according to the AASHTO Classification System, which rates as excellent to good quality for use as subgrade layers.

6.4.2 Residual Shale

The **Residual Shale** (2 samples) classify as sandy CLAY (**CL**), and clayey SAND with gravel (**SC**) in terms of the United Soils Classification System (USCS).

The **CL** sample has a fine fraction ($<0.075\text{mm}$) of 51% and exhibits low plasticity with a Liquid Limit (LL) of 34% and Plasticity Index (PI) of 13%. The material has an in-situ moisture content of 10.1% and exhibits low potential expansiveness based on the Van der Merwe method of heave prediction. It classifies as A-6(4) according to the AASHTO Classification System, which rates as fair to poor quality for use as subgrade layers.

The **SC** sample has a coarse fraction ($>0.075\text{mm}$) of 67% and exhibits low plasticity with a Liquid Limit (LL) of 35% and Plasticity Index (PI) of 13%. It classifies as A-2-6 according to the AASHTO Classification System, which rates as excellent to good quality for use as subgrade layers.

6.4.3 Reworked Residual Sandstone

The **Reworked Residual Sandstone** (1 sample) classifies as silty clayey SAND with gravel (**SM-SC**) in terms of the United Soils Classification System (USCS).

This sample has a coarse fraction ($>0.075\text{mm}$) of 56% and exhibits low plasticity with a Liquid Limit (LL) of 22% and Plasticity Index (PI) of 7%. The material has an in-situ moisture content of 2.7% and exhibits low potential expansiveness based on the Van der Merwe method of heave prediction.

This sample classifies as A-4(0) according to the AASHTO Classification System, which rates as fair to poor quality for use as subgrade layers.

6.4.4 Residual Sandstone

In terms of the United Soil Classification System (USCS), the residual sandstone soils classify as follows:

- 1no. silty clayey SAND (SM-SC);
- 2no. clayey SAND with gravel (SC); and
- 1no. sandy CLAY (CL).

The **SM-SC** sample has a coarse fraction ($>0.075\text{mm}$) of 65% and exhibits low plasticity with a Liquid Limit (LL) of 17% and Plasticity Index (PI) of 5%. The material has an in-situ moisture content of 3.3% and exhibits low potential expansiveness based on the Van der Merwe method of heave prediction. It classifies as A-2-4(0) according to the AASHTO Classification System, which rates as excellent to good quality for use as subgrade layers.

The **SC** sample (which is partially ferruginised) has a coarse fraction ($>0.075\text{mm}$) ranging between 63% and 74% and exhibits low plasticity with the Liquid Limit (LL) ranging between 23% and 26%, with a Plasticity Index (PI) of 9%. The material has an in-situ moisture content of 3.5% and exhibits low potential expansiveness based on the Van der Merwe method of heave prediction. It classifies as A-2-4(0), and A-4 (0) according to the AASHTO Classification System, which rates as excellent to good and fair to poor quality for use as subgrade layers respectively.

The **CL** sample has a fine fraction ($<0.075\text{mm}$) of 73% and exhibits medium plasticity with a Liquid Limit (LL) of 43% and Plasticity Index (PI) of 19%. The material has an in-situ moisture content of 13.1% and exhibits medium potential expansiveness based on the Van der Merwe method of heave prediction. It classifies as A-7-6(13) according to the AASHTO Classification System, which rates as poor quality for use as subgrade layers.

The moisture/density relationship test yielded a maximum dry density of 2133 kg/m^3 at Modified AASHTO compaction effort and optimum moisture contents of 8.1%. The swell potential is 0%, with CBR values of 20% and 24% at 93% and 95% Modified AASHTO compaction density respectively.

The **SC** material classifies as G7 (COLTO) quality material. However, the residual soils are variable between **SM-SC** and **CL** materials, and therefore careful selection of this material should be carried out for use as an engineering fill

Results of chemical tests indicate that the residual sandstone is generally not corrosive, with a degree of acidity of moderately acidic.

6.4.5 Residual Quartzitic Sandstone

In terms of the United Soil Classification System (USCS), the soils classify as follows:

- 1no. silty clayey SAND (SM-SC); and
- 2no. clayey SAND, with gravel (SC).

The **SM-SC** sample has a coarse fraction ($>0.075\text{mm}$) of 79% and exhibits low plasticity with a Liquid Limit (LL) of 24% and Plasticity Index (PI) of 7%. The material exhibits low potential expansiveness based on the Van der Merwe method of heave prediction. It classifies as A-2-4(0) according to the AASHTO Classification System, which rates as excellent to good quality for use as subgrade layers.

The **SC** sample has a coarse fraction ($>0.075\text{mm}$) ranging between 58% and 62% and exhibits low plasticity with the Liquid Limit (LL) ranging between 32% and 36%, with Plasticity Index (PI) between 12% and 13%. The material has an in-situ moisture content ranging between 7.2% and 8% and exhibits low potential expansiveness based on the Van der Merwe method of heave prediction. It classifies as A-6-(2) according to the AASHTO Classification System, which rates as fair to poor quality for use as subgrade layers.

The moisture/density relationship test yielded a maximum dry density of 2157kg/m³ at Modified AASHTO compaction effort and optimum moisture contents of 7.4%. The swell potential is 0.1%, with CBR values of 30% and 41% at 93% and 95% Modified AASHTO compaction density respectively.

The residual quartzitic sandstone classifies as G6 (COLTO) quality material. It is therefore considered suitable for use in the construction of engineered fills or as selected layers in the pavement structure for roads.

Results of chemical tests indicate that the residual quartzitic sandstone is generally not corrosive, with a degree of acidity of moderately acidic.

6.4.6 Pedogenic Material

The **Pedogenic Material** (2 samples) classify as silty clayey SAND with gravel (**SM-SC**), and silty SAND with gravel (**SM**) in terms of the United Soils Classification System (USCS).

The **SM-SC** sample has a coarse fraction (>0.075mm) of 77% and exhibits low plasticity with a Liquid Limit (LL) of 26% and Plasticity Index (PI) of 6%. The material has an in-situ moisture content of 3.7% and exhibits low potential expansiveness based on the Van der Merwe method of heave prediction.

The **SM** sample has a coarse fraction (>0.075mm) of 82% and has a non-plastic nature and exhibits low potential expansiveness based on the Van der Merwe method of heave prediction.

The sample classifies as A-1b(0) according to the AASHTO Classification System, which rates as excellent to good quality for use as subgrade layers.

The moisture/density relationship test yielded a maximum dry density of 2157kg/m³ at Modified AASHTO compaction effort and optimum moisture contents of 8.6%. The swell potential is 0%, with CBR values of 25% and 30% at 93% and 95% Modified AASHTO compaction density respectively.

The pedogenic material classifies as G6 (COLTO) quality material. It is therefore considered suitable for use in the construction of engineered fills or as selected layers in the pavement structure for roads.

Results of chemical tests indicate that the pedogenic material is generally not corrosive, with a degree of acidity of slightly acidic.

6.5 DPL Consistency / Strength

The results of the DPL tests were correlated with SPT N-values in order to determine the consistency and indicative shear strength parameters for the soil. The SPT test is widely used as an indicator of the density and compressibility of granular soils as well as the consistency of cohesive soils.

The following empirical correlation between the DPL value and the Standard Penetration Test (SPT N-value) is adopted:

$$\text{Equivalent SPT N-value} = 0.55 \times \text{DPL (no. of blows/300mm)}.$$

A summary of the DPL results, equivalent SPT N values and consistency descriptions are provided in Table 8, while the detailed DPL results are attached in **Appendix E**.

The DPL results typically indicate a medium dense upper horizon from surface to 0.3m with SPT N values ranging between 13 and 30. It is underlain by a dense layer, with medium dense zones, ranging from 0.3 to 1.2m with the SPT N values between 9 and 50. Below this, the in-situ soils are generally very dense with SPT N values between 31 and 50.

A summary of SPT N-values is given in Table 10.

Table 10: Summary of equivalent SPT N-values derived from DPL tests

| DPL ID. | Depth (m) | | | | |
|--------------------------------|---------------------|---------------|---------------------|----------------|-------------------|
| | 0.3 | 0.6 | 0.9 | 1.2 | 1.5 |
| DPL02 | 30 | 39 | 47 | Refusal | - |
| DPL04 | 13 | 28 | Refusal | - | - |
| DPL05 | 13 | 9 | 11 | 31 | Refusal |
| DPL06 | 22 | Refusal | - | - | - |
| DPL08 | Refusal | - | - | - | - |
| DPL11 | 28 | Refusal | - | - | - |
| DPL14 | 23 | Refusal | - | - | - |
| DPL15 | Refusal | - | - | - | - |
| DPL20 | 16 | 17 | Refusal | - | - |
| Average | 27 | 35 | 40 | 40 | Refusal |
| Consistency | medium dense | dense | dense | dense | very dense |
| Notes: | | | | | |
| Consistency Description | Very Loose | Loose | Medium Dense | Dense | Very Dense |
| SPT N-value | 0 – 4 | 4 – 10 | 30-Oct | 30 – 50 | >50 |

Based on the average DPL test results, the in-situ soils are generally dense becoming very dense below 0.9m. A plot of the average DPL and equivalent SPT N values is provided Figure 3.

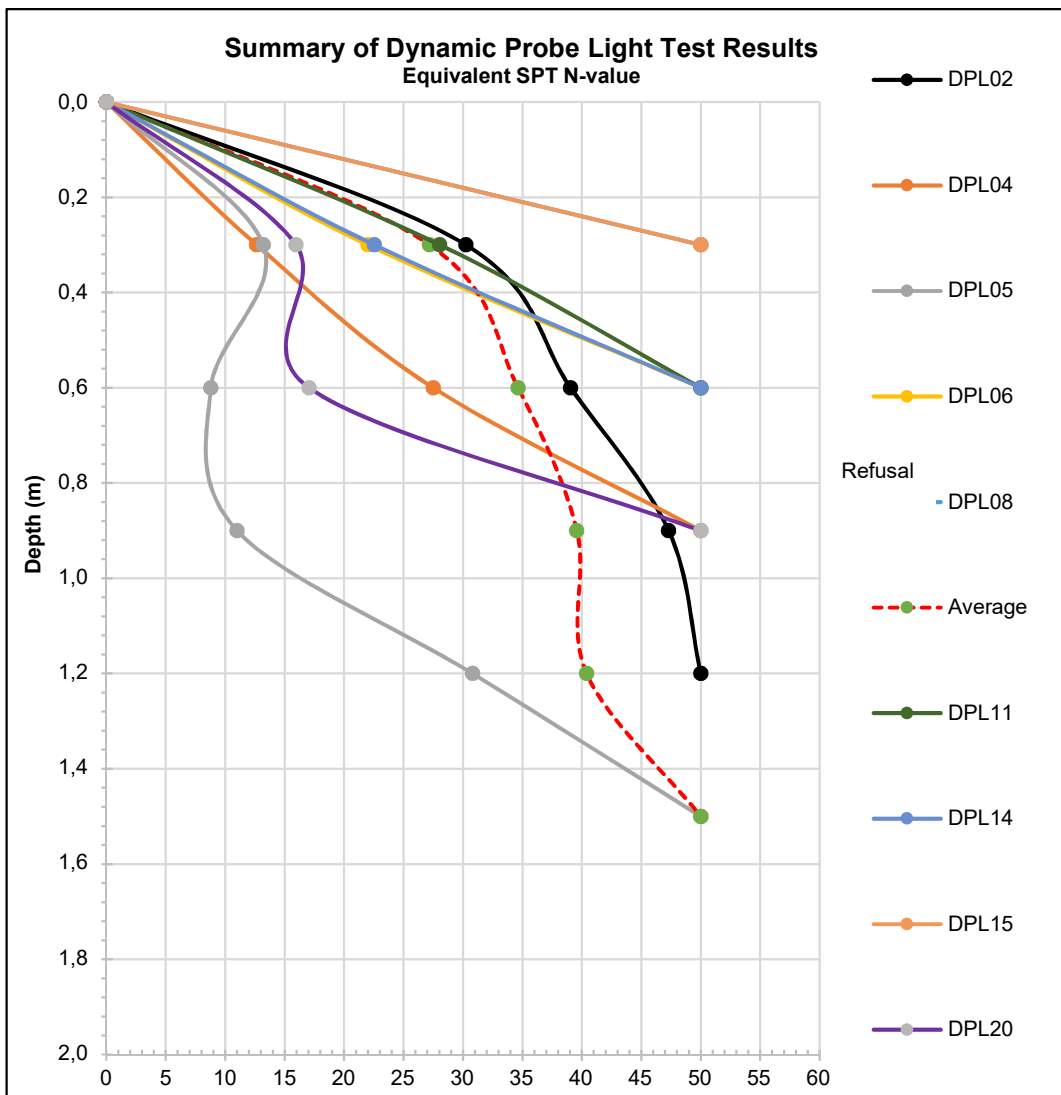


Figure 3: Plot of SPT N-value vs depth (m)

6.6 DCP Consistency / Strength

DCP tests were conducted adjacent to selected excavated test pits in order to determine the consistency and shear strength of the soils. Based on the DCP test results, the in-situ soils are generally dense to medium dense with depth.

It is inferred that in some occasions, refusal of the DCP occurred on a hardpan ferricrete layer. A plot of the DCP results is provided in Figure 4. The DCP results are provided in **Appendix F**.

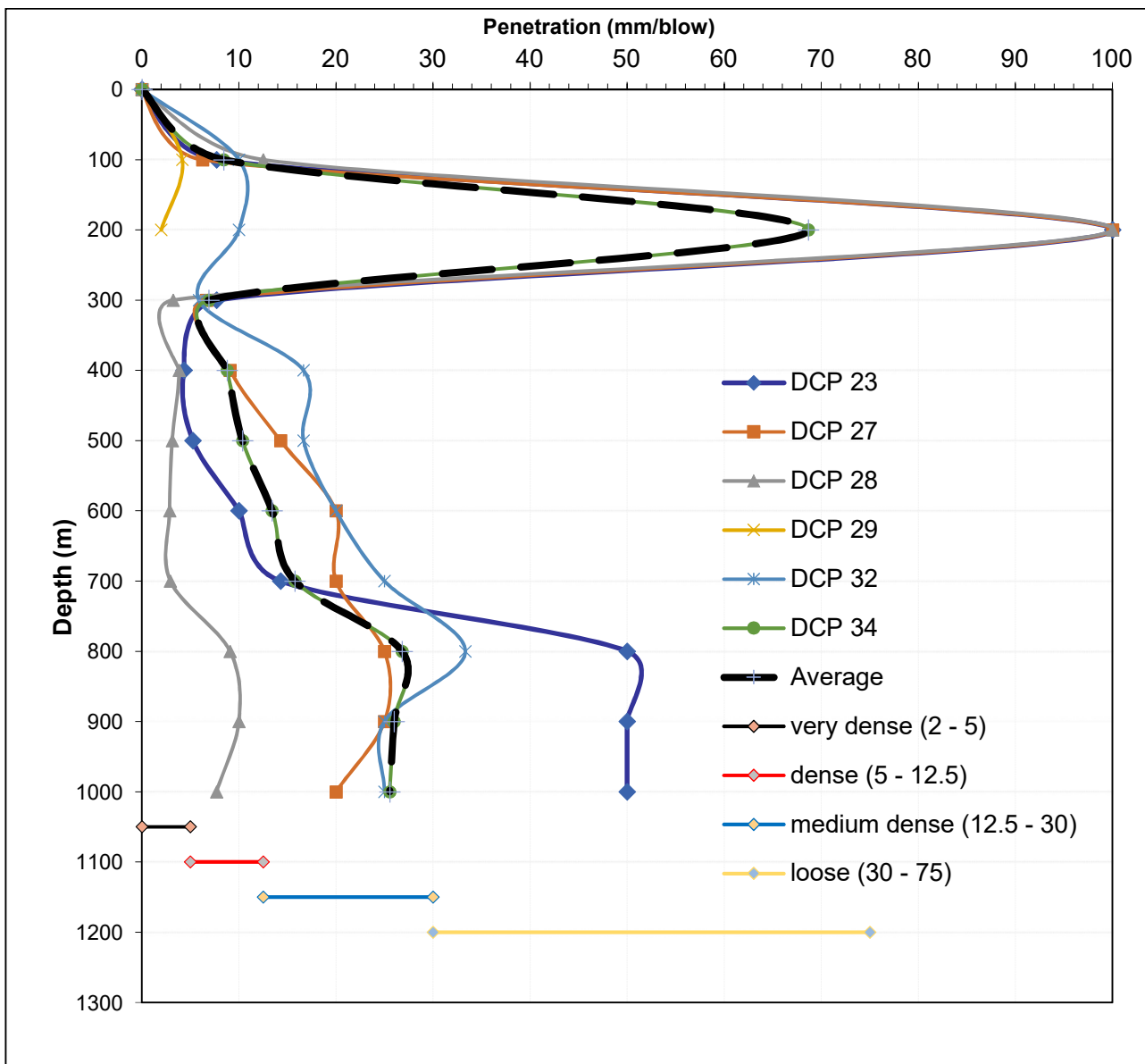


Figure 4: Plot of DCP, penetration (mm/blow) vs depth (mm)

7. RECOMMENDATIONS

7.1 Site Zonation

According to the SAICE Code of Practice (Foundations and Superstructures for Single Storey Residential Buildings of Masonry Construction, 1995), the site can be classified into three zones, namely:

- Zone1 - Site Class **R/S**;
- Zone 2 - Site Class **S1**; and
- Zone 3 - Site Class **P** (potential flood zone).

The zonation map is attached in Appendix I.

7.1.1 Zone 1 – (Site Class R/S)

Site Class R/S is defined as follows:

- Rock/hardpan/boulders (R) at shallow depth less than 1.5m.
- Compressible soils (S) with the nature of the founding material comprising fine grained soils (clayey silts and clayey sands of low plasticity), sands, sandy and gravely soils. Expected total soil movement is less than 10mm.

7.1.2 Zone 2 – (Site Class S1)

- Site Class **S1** is defined as compressible soils with the nature of the founding material comprising fine grained soils (clayey silts and clayey sands of low plasticity), sands, sandy and gravely soils. Expected total soil movement is between than 10mm and 20mm.

7.1.3 Zone 3 – (Site Class P)

- Site Class **P (potential flood zone)** is defined as a zone with a potential of flooding during heavy rains.

Considering the prevailing geotechnical conditions, the following recommendations are given, with all depths related to current ground level.

7.2 Earthworks

It is recommended that all earthworks are carried out in accordance with SANS 1200 (current version). All topsoil and transported material should be cleared from the footprint of the proposed development and stockpiled for later site rehabilitation.

7.3 Foundations

Development recommendations at this site are as follows (foundation design falls outside the scope of this geotechnical investigation):

- Concrete raft foundation
- Strip Foundation
- Modified Strip foundations

7.3.1 Concrete raft foundation

The recommended foundation type is a reinforced concrete raft foundation founded on the residual soils at a depth of 0.5m below existing ground level. The following construction procedures applies:

- All topsoil and transported soils to be stripped to spoil to a depth of 0.5m below existing ground level;
- Rip and recompact the residual soils to 93% Mod AASHTO density at –1% to +2% OMC;
- Reinforced concrete raft foundations can then be placed at a depth of 0.5m onto the compacted soil;
- The allowable bearing capacity should be limited to 100kPa with a subgrade modulus of 50kPa adopted for the in-situ soils.

7.3.2 Compaction of In-Situ Soils below Footings

An alternative recommendation is a 600mm wide strip footing to be founded at a minimum depth of 0.6m below existing ground level. The following construction procedures are applicable.

- Foundation trenches for 600mm wide strip footing to be over-excavated to 1.0m wide by 1.5m deep, below existing ground level;
- Replace with G6/G7 quality material and compact in 200mm loose thickness to 93% Modified AASHTO compaction to underside of foundation (0.6m);
- Strip footings 600mm wide should be constructed at a depth of 0.6m utilizing a maximum allowable bearing capacity of 100kPa.

7.3.3 Modified Normal Foundations

The recommended foundation type is a reinforced strip footing founded on the residual soils at a depth of 0.5m below existing ground level. The following construction procedures applies:

- Reinforced strip footings.
- Articulation joints at some internal and all external doors.
- Light reinforcement in masonry.
- Site drainage and service/plumbing precautions
- Foundation pressure not to exceed 50 kPa

7.4 Roads and Terraces

The design of the road pavement layers must take into account the traffic intensity and anticipated axle loading. The road pavement should be laid on the newly constructed earthworks, approximately 300mm thick.

The results of the CBR and indicator tests were used to classify the in-situ soils to determine their suitability for use in the construction of terraces and pavement layers. The in-situ soils all classify as G6 and G7 quality material according to TRH14 and are therefore considered suitable for use as engineering fill or for use in road pavement layer works.

7.5 Excavation Classification

Based on the test pits, it is anticipated that the site would classify as “soft excavation”, to depths of between 0.9m and 1.5m for areas with pedogenic material, and between 1.7m and 2.5m for areas with residual material. The excavation classification is in accordance with SANS 1200DA classification, using similar equipment as employed during this investigation. Below these depths very dense material is likely to be intersected.

It is recommended that the sides of any excavations deeper than 1.5m should be battered to 1:1.5, to ensure enough slope stability to prevent collapse of the sidewalls. During periods of heavy rainfall however, the sides of the excavations should be regularly examined, to ensure the safety of the excavation for personnel and equipment working in them.

7.6 Groundwater Management

Groundwater was not encountered in any of the trial pits excavated on site, however ferruginisation and moist conditions were observed in some test pits. Ferruginisation of the soil profile is of significance as it is indicative of a historically variable water regime at a shallow depth in the soil profile.

Appropriate subsoil drainage systems should be allowed during construction of buildings.

7.7 Areas Subject to Flooding

The site topography is generally flat and surface run-off water would generally be towards the north and northwest. A number of dry water pans or ponds were observed on site (closer to TP 12 and TP01) and the impact of flooding to the study area has not been assessed as it falls outside of our current scope of work. It is recommended that a formal flood line study be conducted if deemed necessary.

7.8 Construction Problems

Difficulty in excavation especially in areas where pedogenic material (ferricrete) is envisaged during construction.

7.9 Additional Investigations

It is important to note that this report is for a feasibility level investigation, and a design-level (or footprint) investigation has to be conducted once the site development plan is available.

7.10 General

All test pits were loosely backfilled upon completion of the fieldwork. In order to avoid the possibility of localised settlement occurring below structures due to the consolidation settlement of this loose backfill, it is recommended that each test hole be identified and adequately backfilled in 150mm layers, to at least 90% Mod AASHTO density.

8. CONCLUSIONS

From the above discussion, the following conclusions may be drawn:

- i. The study area is suitable for the construction of the Proposed Township development in Aerorand South, Middelburg, Mpumalanga Province.
- ii. The area investigated is underlain by transported soils (colluvium) and residual soils (sandstone and shale) derived from sedimentary bedrock. Pedogenic material (cemented in-situ soils mainly by iron, forming ferricrete) was also encountered.
- iii. Excavation on site is likely to classify as “soft” to depths of between 0.9m and 1.5m for areas where pedogenic material is encountered, and between 1.7m and 2.5m for areas where residual material is encountered.
- iv. Groundwater seepage was not observed in any of the test pits, which were excavated up to a maximum depth of 2.5m. However, ferruginisation of the soil profile is of significance, as it is indicative of a historically variable water regime at a shallow depth.
- v. The site class designation according to the building regulations is R/S, S1 and P.
- vi. Class R denotes rock/hardpan/boulders (R) at shallow depth less than 1.5m and Class S denotes compressible soils with expected total soil movement is less than 10mm.
- vii. Class S1 denotes compressible soils with expected total soil movements between 10mm and 20mm.
- viii. Class P denotes a potential flood zone.
- ix. The residual quartzitic sandstone, and pedogenic material classify as G6 (COLTO) quality material. It is therefore considered suitable for use in the construction of engineered fills or as selected layers in the pavement structure for roads.
- x. The residual sandstone classifies as G7 (COLTO) quality material. It is therefore considered suitable for use in the construction of engineered fills or as selected layers in the pavement structure for roads.
- xi. Any structures should be placed on either a concrete raft, individual strip footings on compacted soils, or reinforced strip footing foundations.

9. REPORT PROVISIONS

- i. This investigation is aimed at providing the engineers with an indication of the prevailing engineering geological conditions in the study area.
- ii. The investigation was planned as a feasibility level study to establish the suitability of the site for the proposed development.
- iii. While every effort has been made during the fieldwork phase of this investigation to identify the various soil horizons, their problems and distribution, it is impossible to guarantee that isolated zones of varying material have not been missed.
- iv. The contents of this report are valid as of the date of preparation. However, changes in the condition of the site can occur over time as a result of either natural processes or human activity.
- v. The engineers are, nevertheless, strongly urged to inspect all excavations to assure themselves that conditions are not at variance with those described in this report.
- vi. The design of geotechnical structures, analysis of structures and services and management of the risk fall outside the scope of this investigation.
- vii. Test pits were backfilled after the field investigation but were not re-compacted and some test pit positions may occur within the footprints of proposed structures.

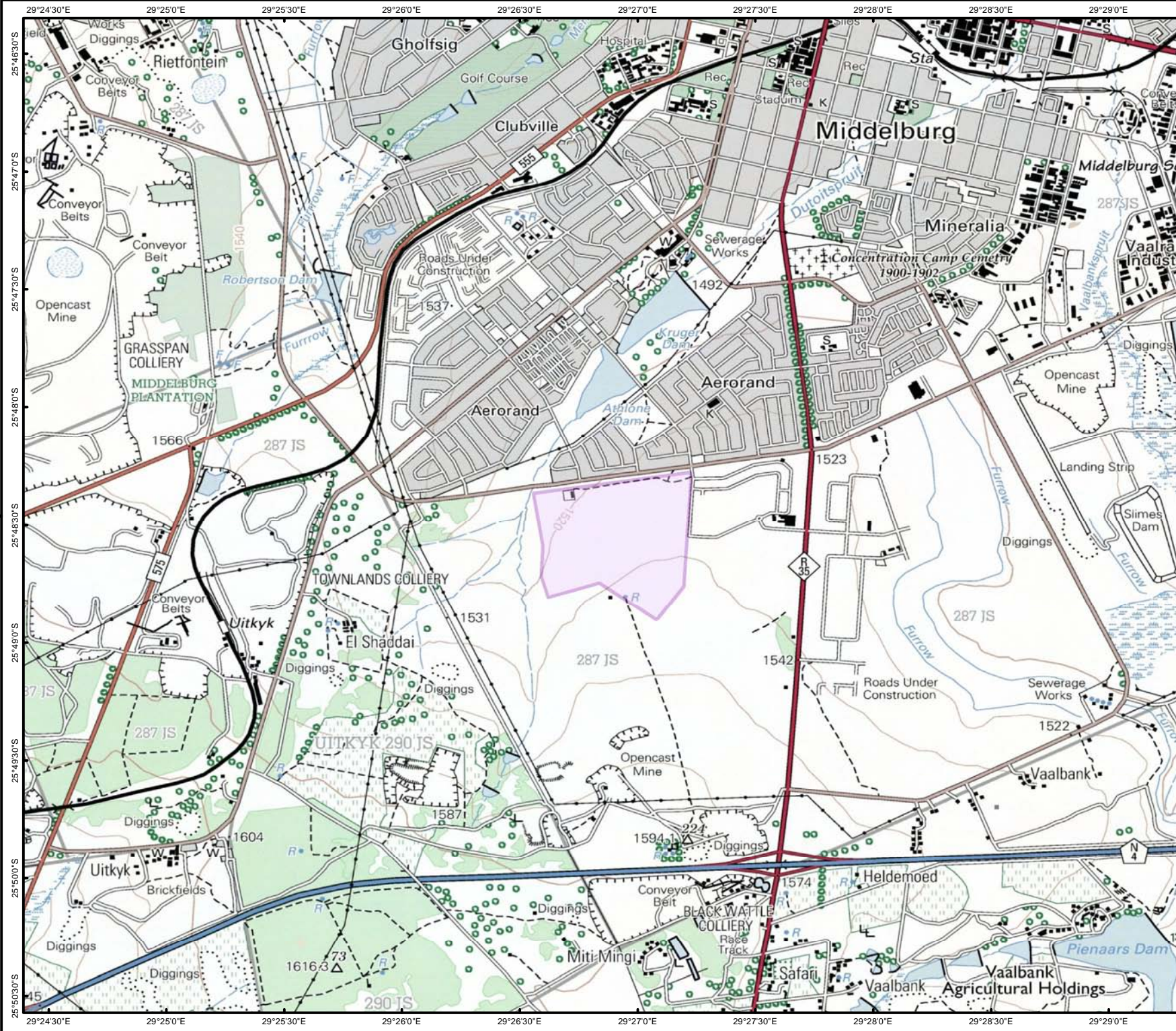
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11. APPENDICES

- APPENDIX A: TOPOGRAPHICAL MAP
- APPENDIX B: GEOTECHNICAL LAYOUT DRAWING
- APPENDIX C: TEST PIT PROFILES
- APPENDIX D: SITE & TEST PIT PICTURES
- APPENDIX E: DPL TEST RESULTS
- APPENDIX F: DCP TEST RESULTS
- APPENDIX G: GEOLOGICAL MAP
- APPENDIX H: LABORATORY TEST RESULTS
- APPENDIX I: ZONATION MAP

APPENDIX A: TOPOGRAPHICAL MAP



Legend

- Site Boundary
- Buildings / Ruins
- Cemetery / Grave
- Row of Trees
- Main Roads
- Secondary Roads
- Other Roads
- Railway
- Track and Hiking Trail
- Powerline
- Rivers
- Contour Lines
- Cadastral Boundary
- Buildings
- Build up Area
- Mine Dump / Excavation
- Erosion / Sand
- Cultivated Land
- Woodland
- Recreation Ground
- Marsh and Vlei
- Non- Perenial Water
- Water Bodies

CLIENT

**STEVE TSHWETE
LOCAL MUNICIPALITY**

PROJECT

**AERORAND SOUTH TOWNSHIP,
STEVE TSHWETE LOCALMUNICIPALITY**

TITLE

**Topographical Map of Aerorand South
Township, Mpumalanga
Extract of 1:50 000 Topographical Map
2529CD MIDDELBURG (TVL)**

| | |
|-------------------------|-------------------------------|
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| DATE: 2018/11/08 | MK- 18- 480- Topo- 020 |

00.40.81.6

Kilometers

SCALE: 1:40 000

Projection: Geographic, Datum: WGS84
Source: Chief Directorate National Geo-Spatial Information
Inset: ESRI Data and Maps

MUKONA
CONSULTING ENGINEERS

Mukona Consulting Engineers (Pty) Ltd
International Business Gateway, New Road,
Midridge Office Estate (North), Midrand, 1685
Telephone: 011 4438293
Mobile: 083 7850284
Email: Sollyp@mknconsulting.co.za

APPENDIX B: GEOTECHNICAL LAYOUT DRAWING

29°26'30"E

29°27'0"E

25°48'30"S

25°48'30"S

29°26'30"E

29°27'0"E

LEGEND

- ✖ ADDITIONAL TEST PITS
- ▲ ADDITIONAL DCP & TEST PITS
- ✖ EXISTING TEST PITS
- ▲ EXISTING DPL & TEST PITS
- FARM BOUNDARY
- MIDDELBURG FARM ERFs

CLIENT



PROJECT

**GEOTECHNICAL INVESTIGATION FOR
AERORAND SOUTH TOWNSHIP
STEVE TSHWETE MUNICIPALITY**

TITLE

**GEOTECHNICAL LAYOUT PLAN
AERIAL IMAGERY- ESRI BASEMAPS**

DRAWN: A. Qoboka

DRAWING

DATE: 2019/06/04

MK-1 8- 480- GLP097

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Kilometers

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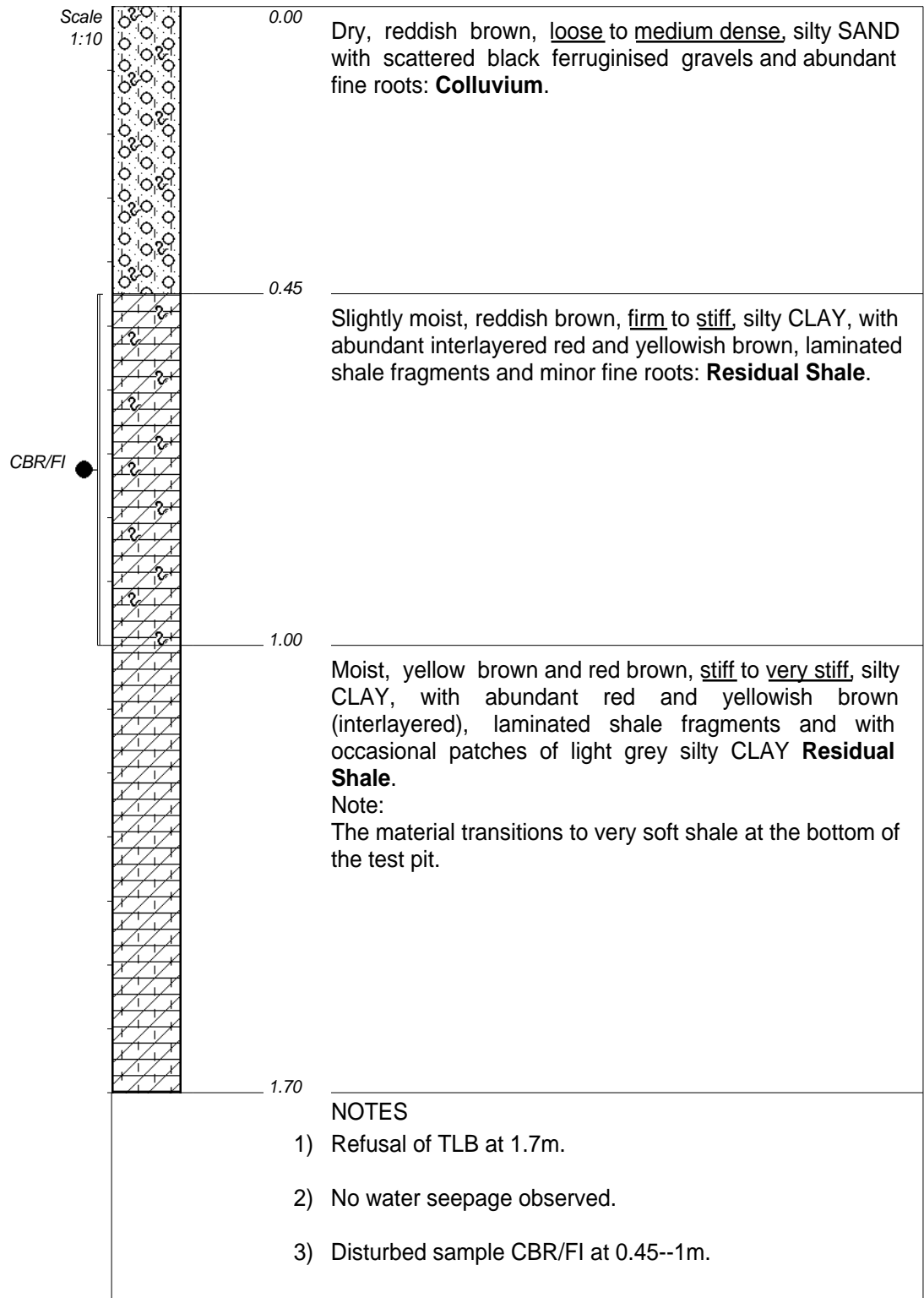
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Mukona Consulting Engineers (Pty) Ltd
International Business Gateway, New Road,
Midridge Office Estate (North), Midrand, 1685
Telephone: 011 443 8293
Mobile: 083 785 0284
Email: Sollyp@mukonagroup.com

APPENDIX C: TEST PIT PROFILES

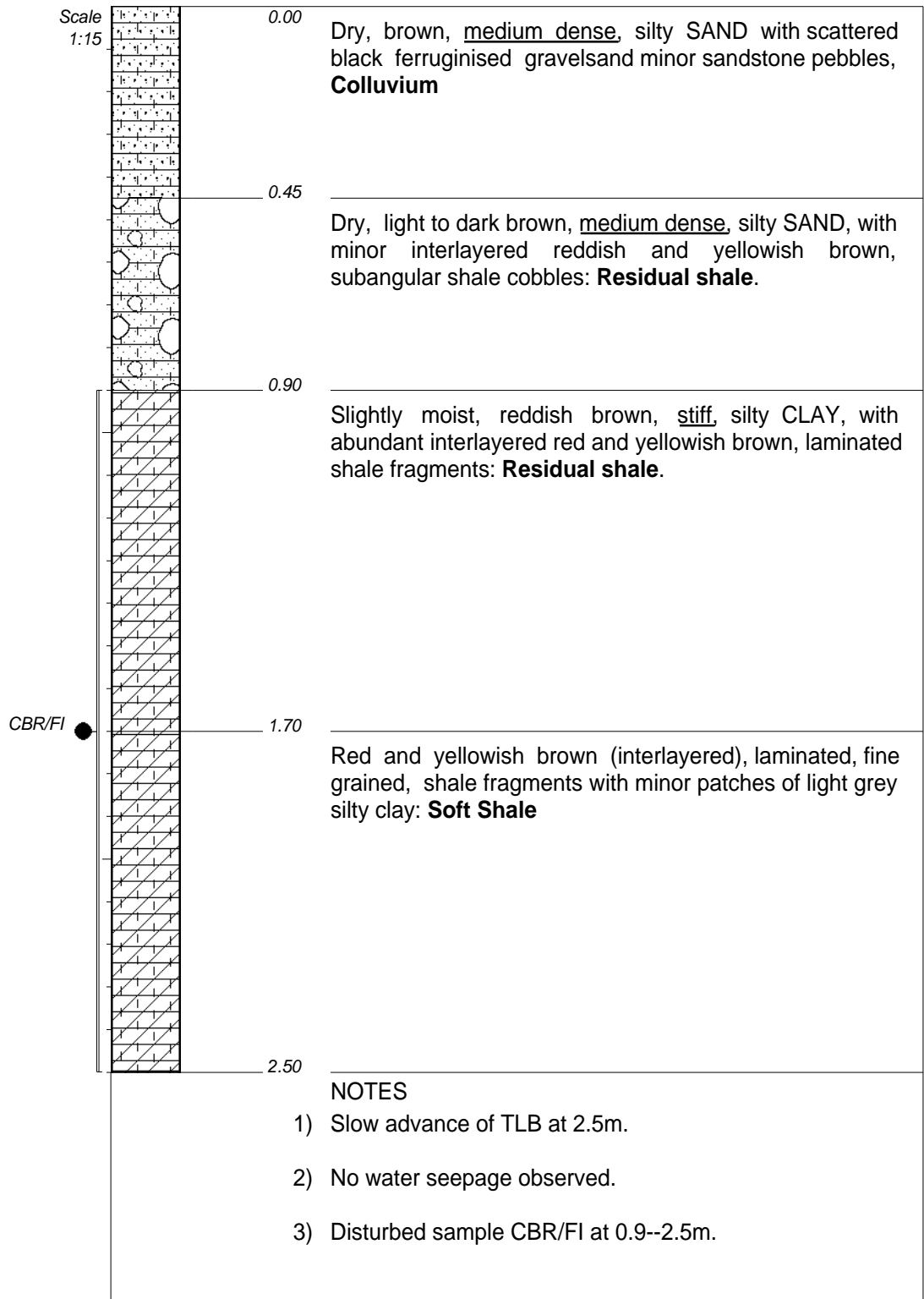


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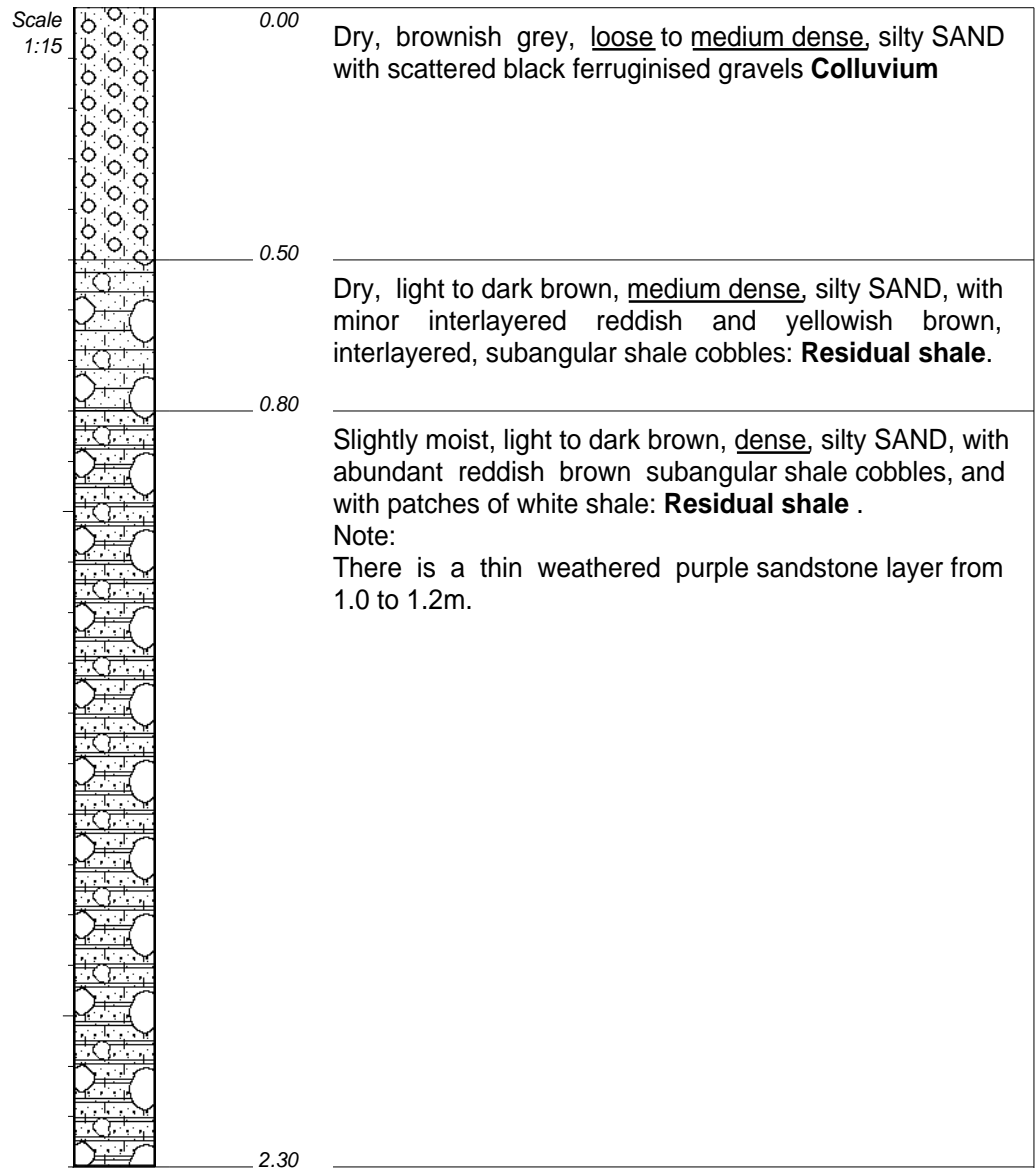


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NOTES

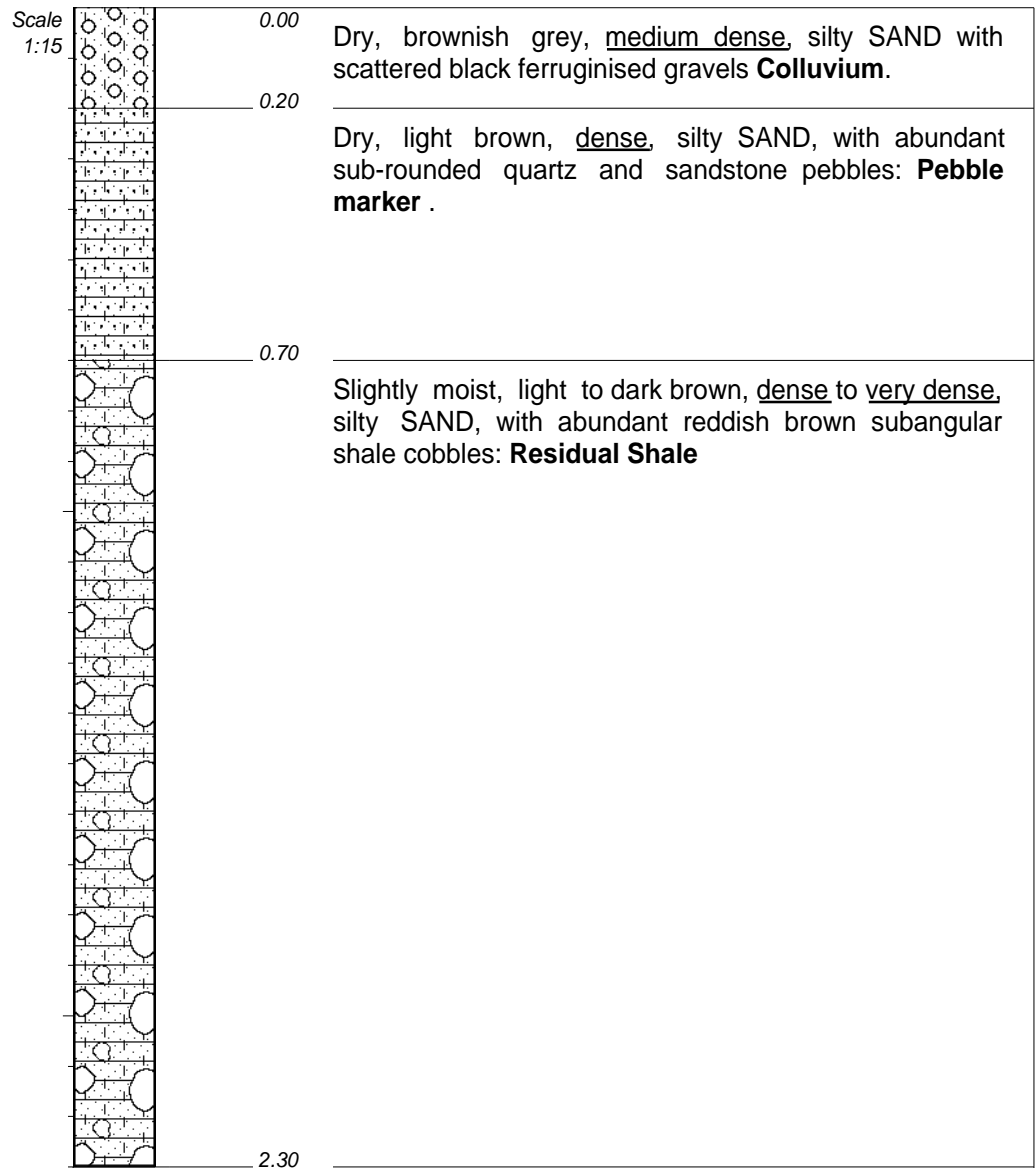
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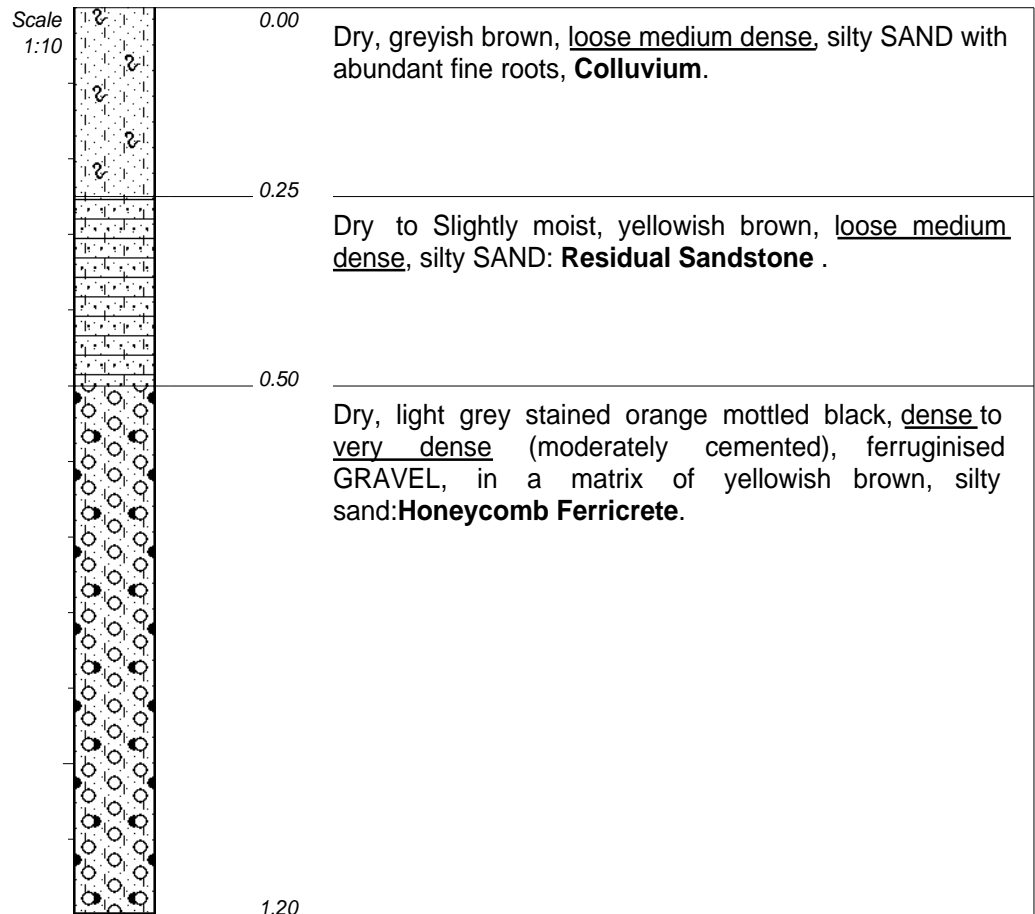
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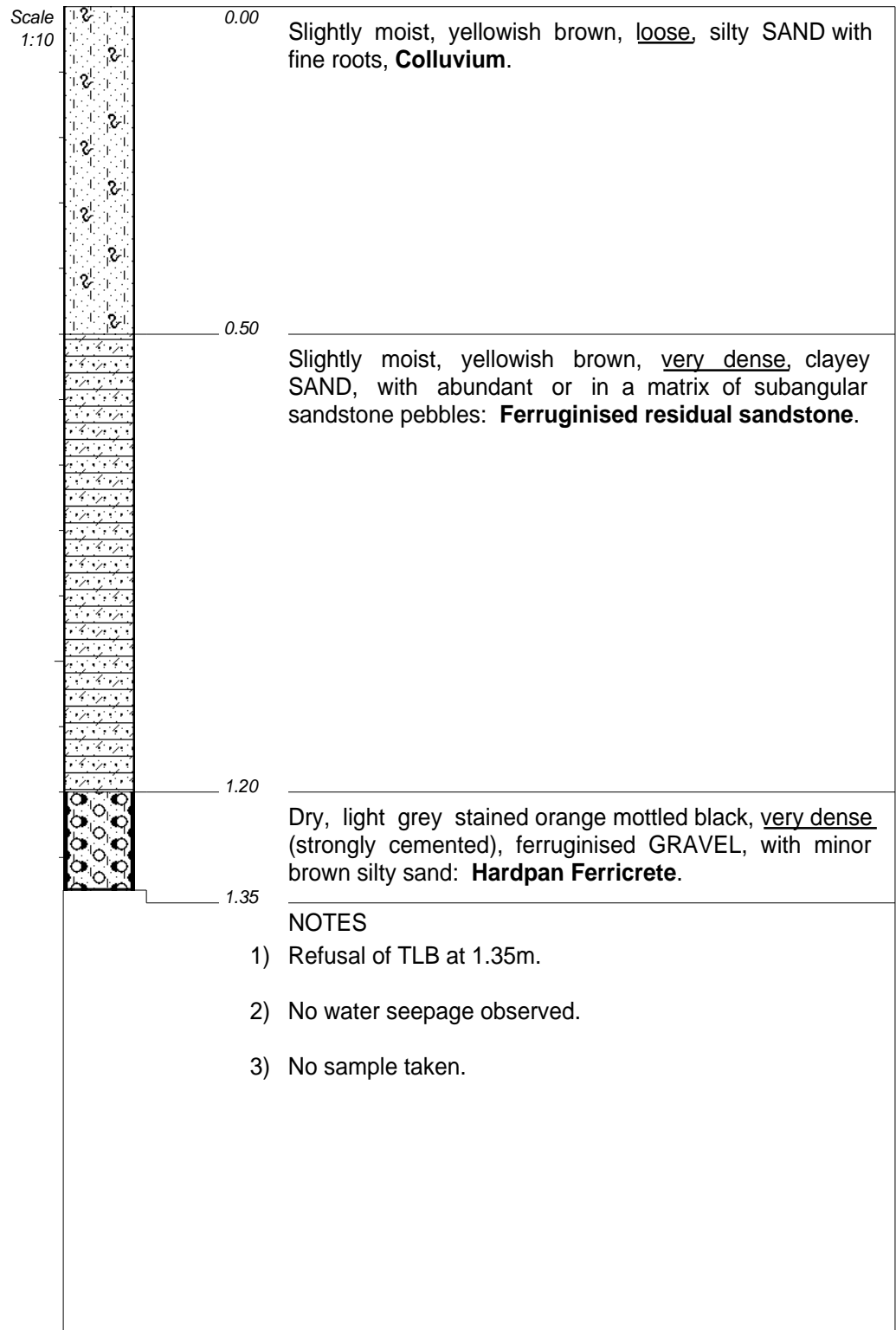
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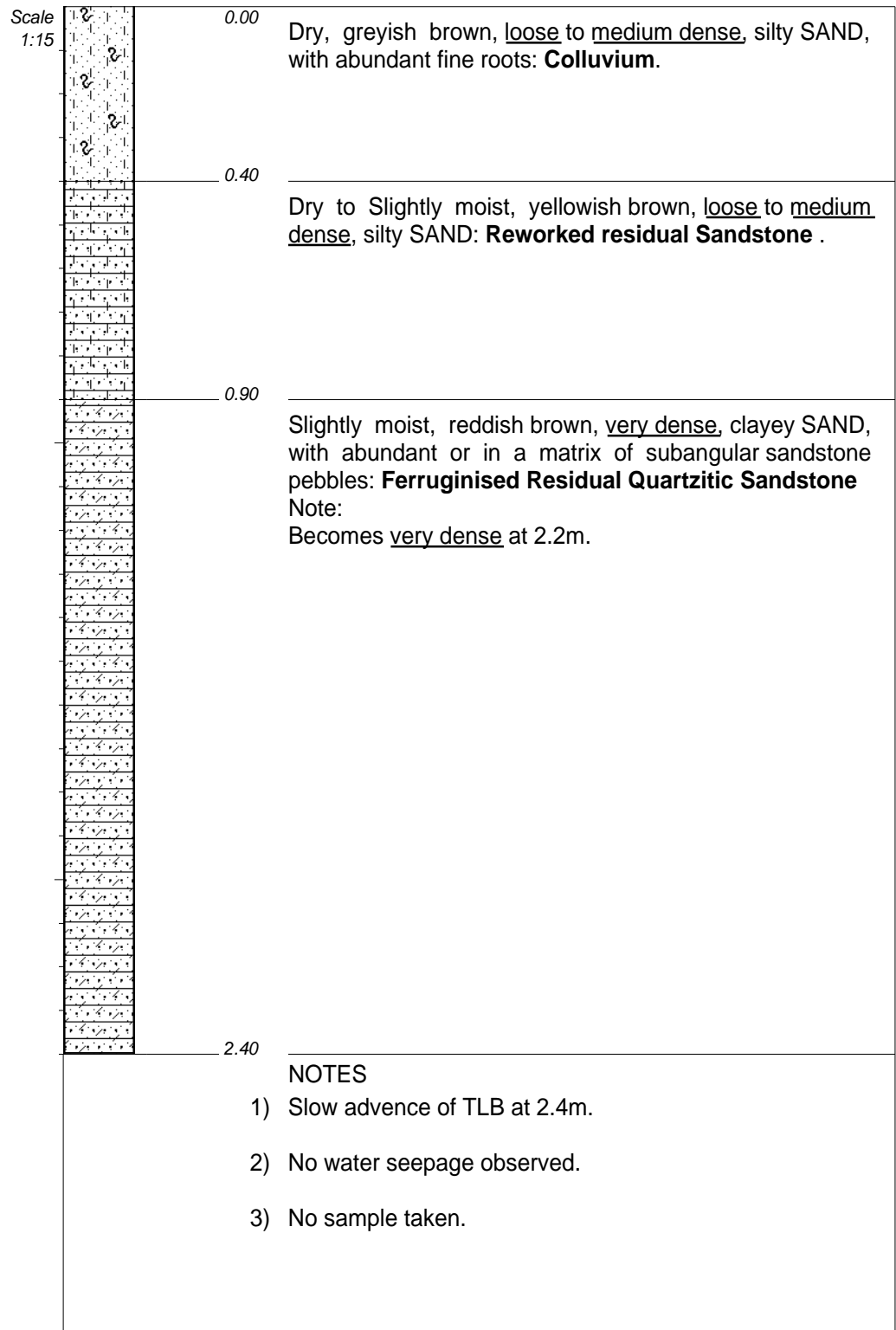


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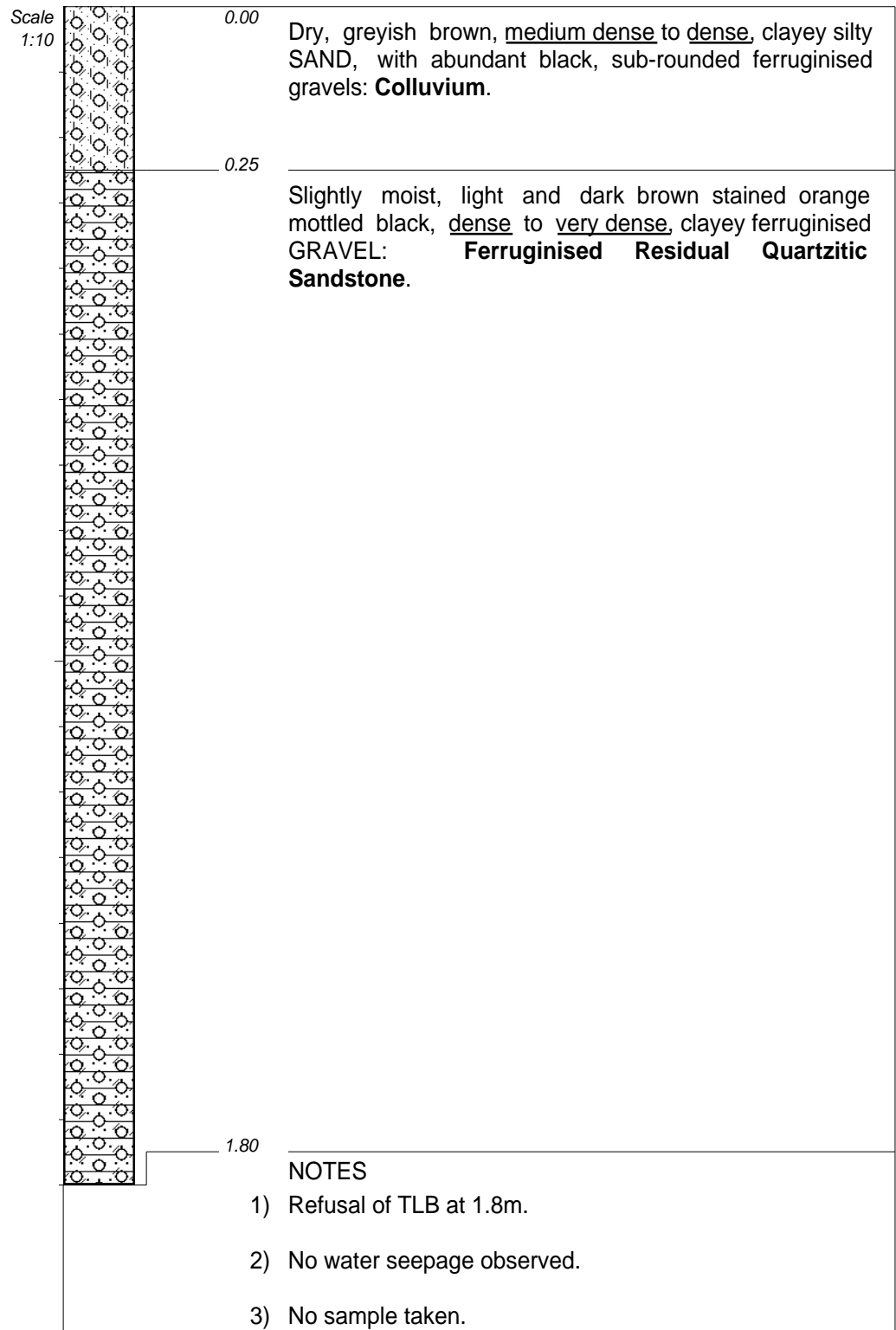


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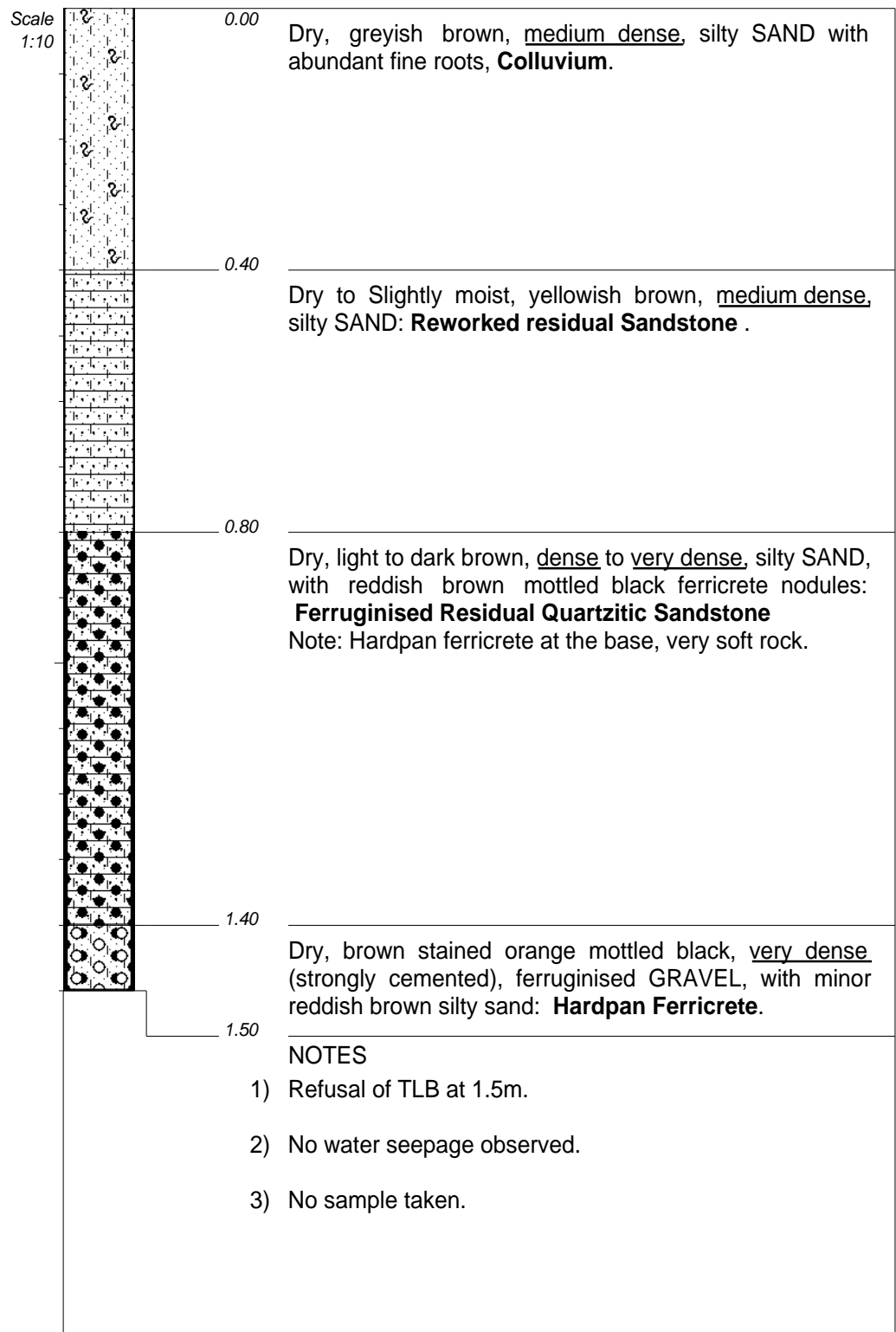


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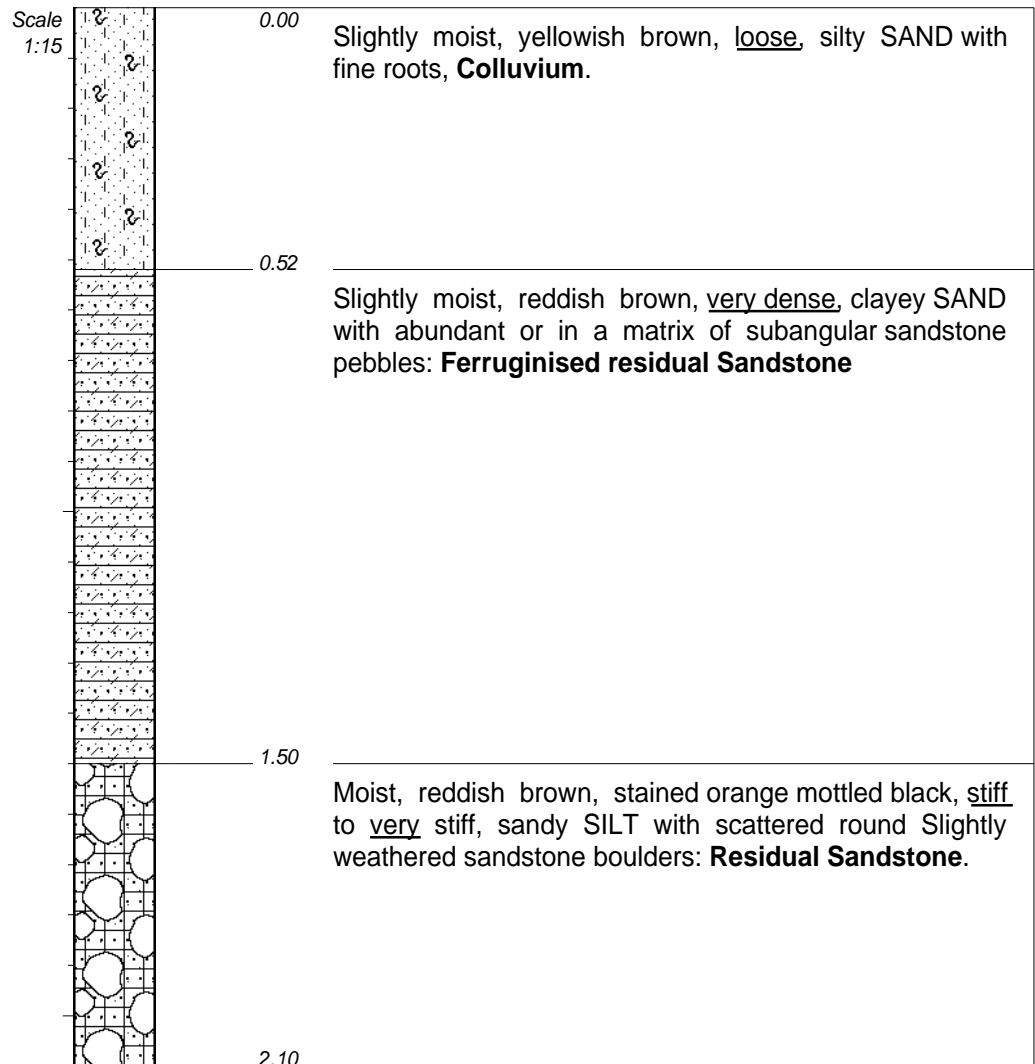


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NOTES

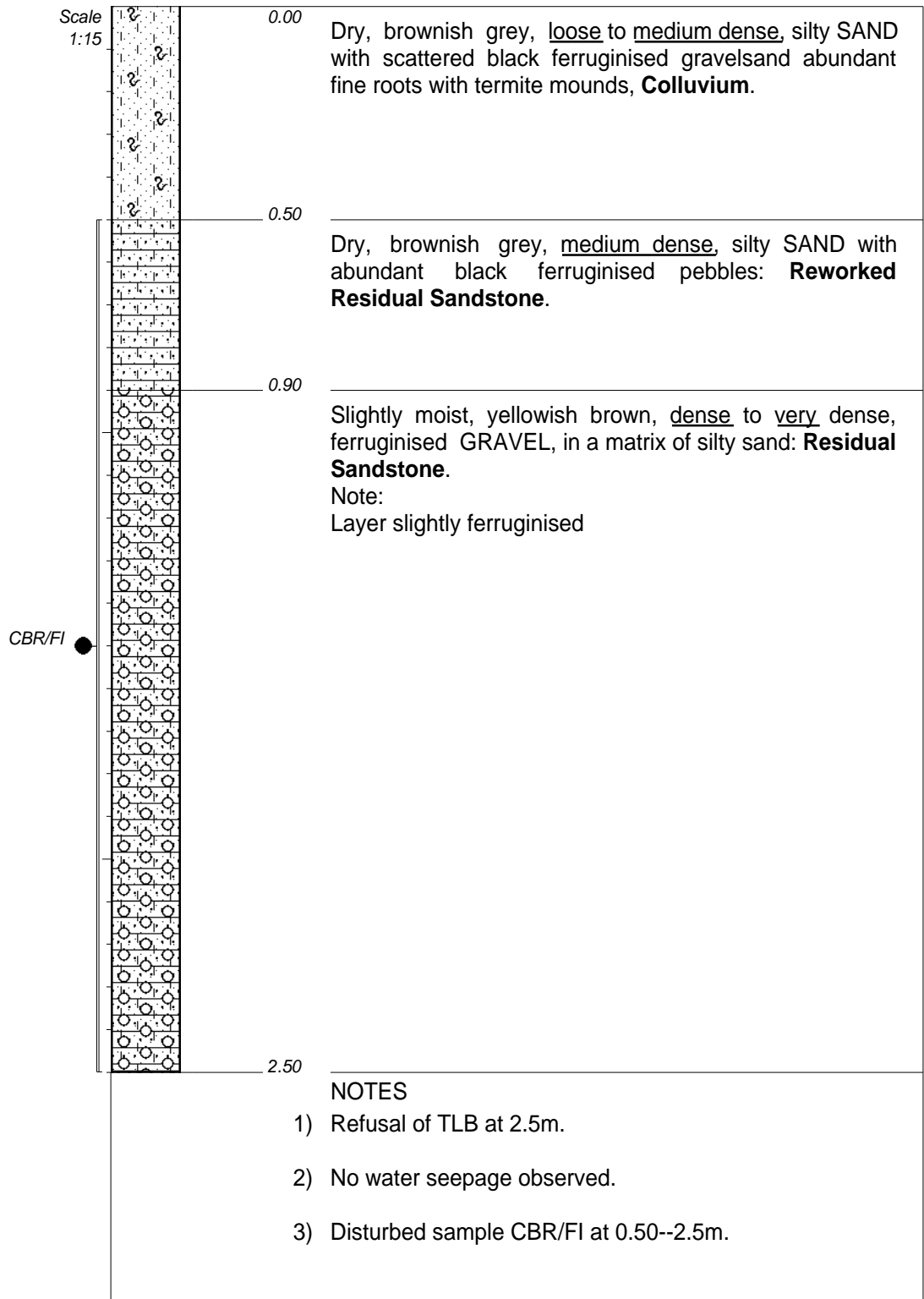
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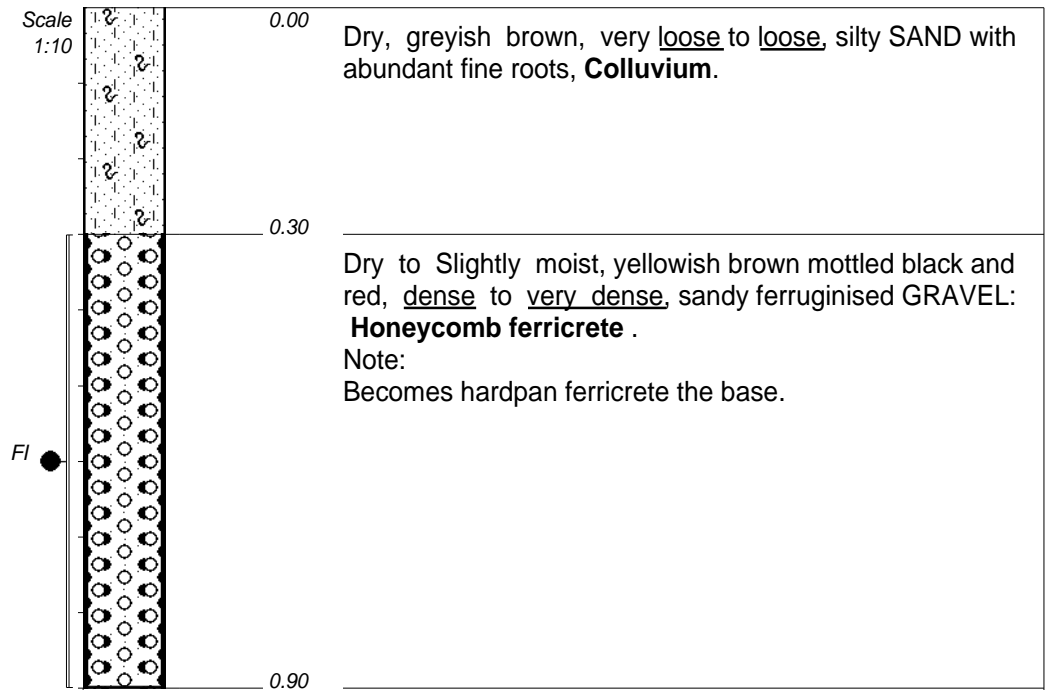


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HOLE No: TP11



NOTES

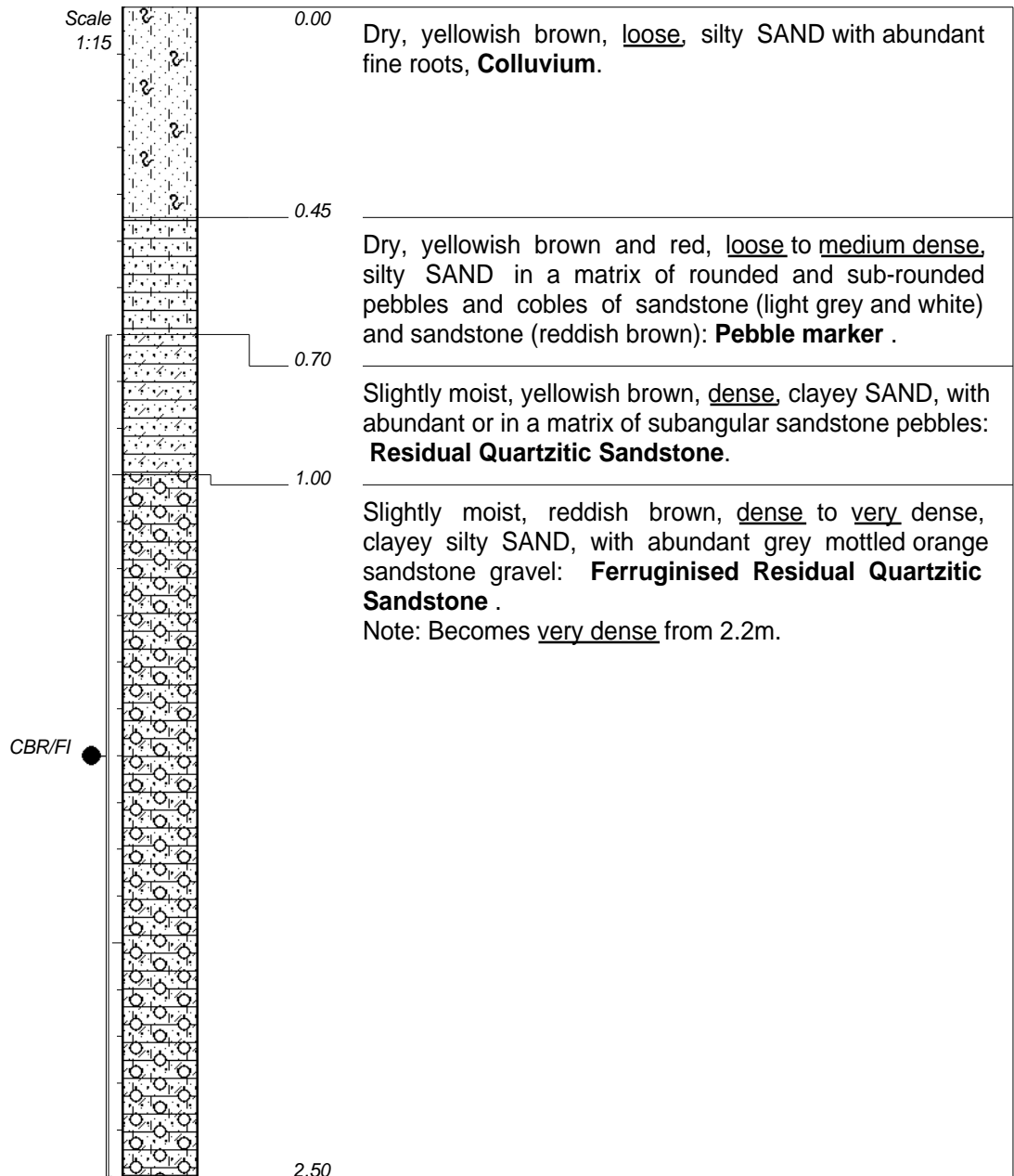
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HOLE No: TP12



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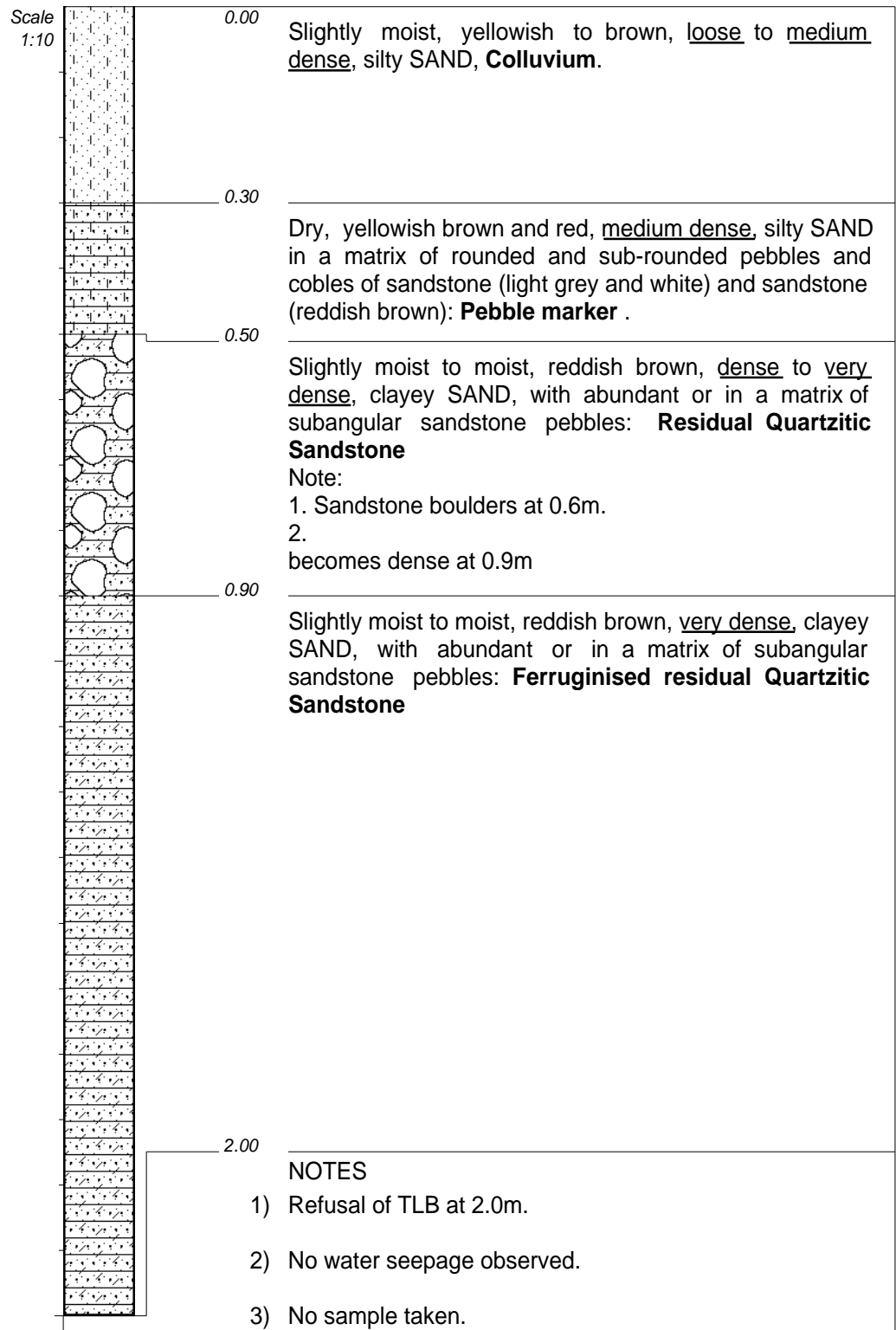
- 1) Refusal of TLB at 2.5m.
- 2) No water seepage observed.
- 3) Disturbed sample CBR/FI at 0.7--2.5m

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,806
Y-COORD : 29,45191

HOLE No: TP13

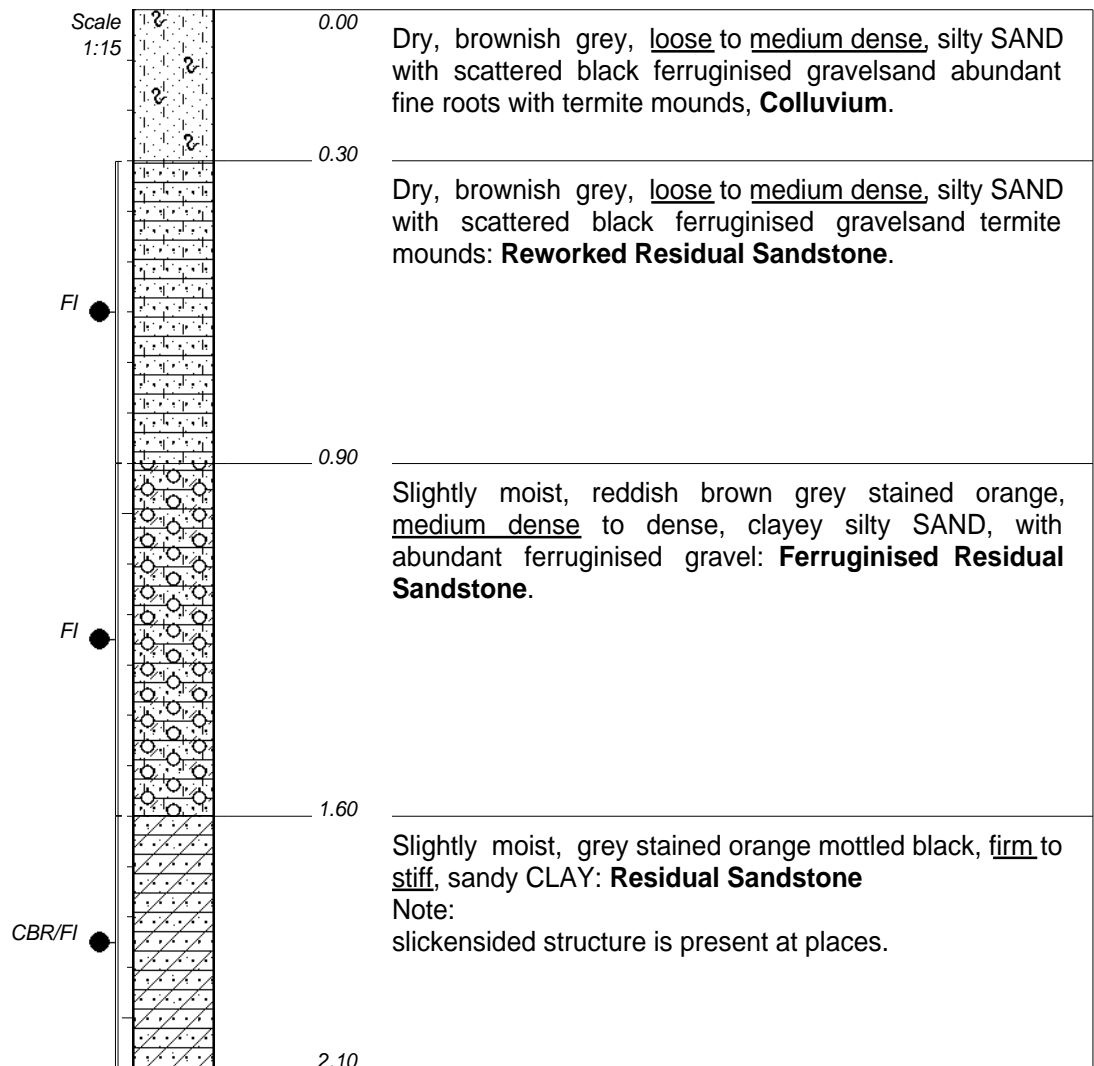


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,80512
Y-COORD : 29,4518

HOLE No: TP14



NOTES

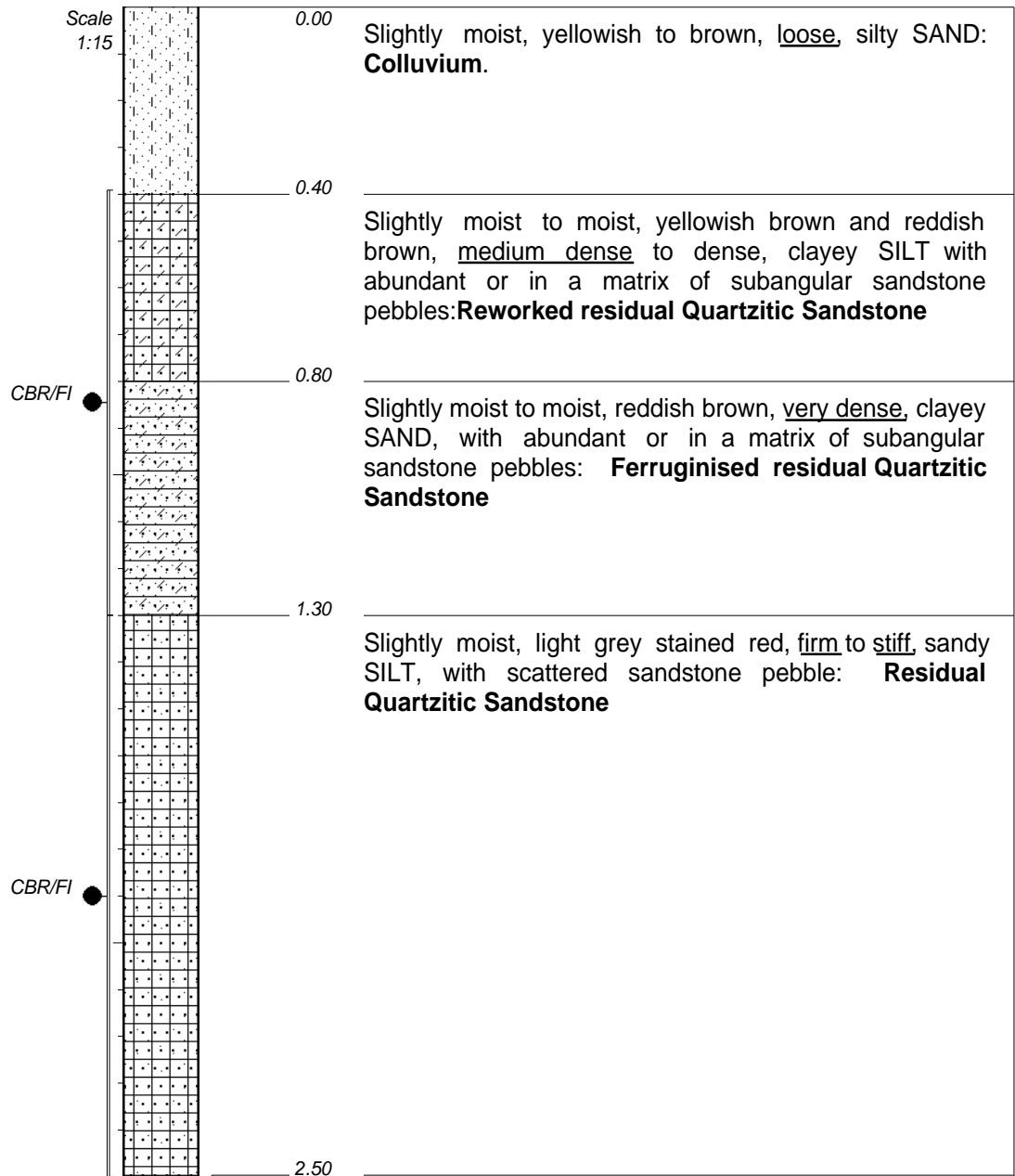
- 1) Refusal of TLB at 2.1m.
- 2) No water seepage observed.
- 3) Disturbed sample FI at 0.3--0.9m.
- 4) Disturbed sample FI at 0.9--1.6m.
- 5) Disturbed sample CBR/FI at 1.6--2.1m.

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,8077
Y-COORD : 29,452341

HOLE No: TP15



NOTES

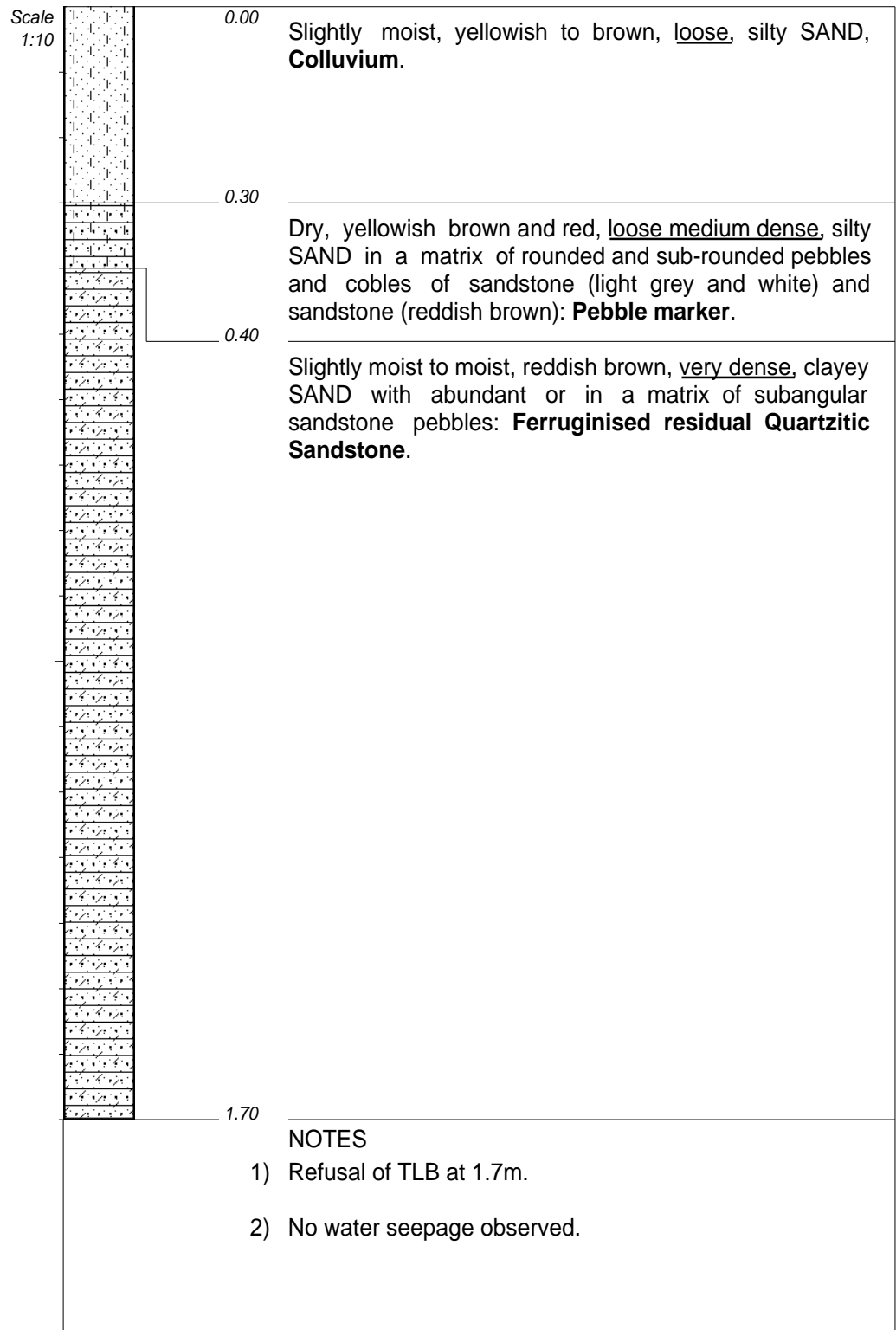
- 1) Refusal of TLB at 2.5m.
- 2) No water seepage observed.
- 3) Disturbed sample CBR/FI at 0.39--1.3m.
- 4) Disturbed sample CBR/FI at 1.3--2.5m.

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,8058
Y-COORD : 29,45276

HOLE No: TP16

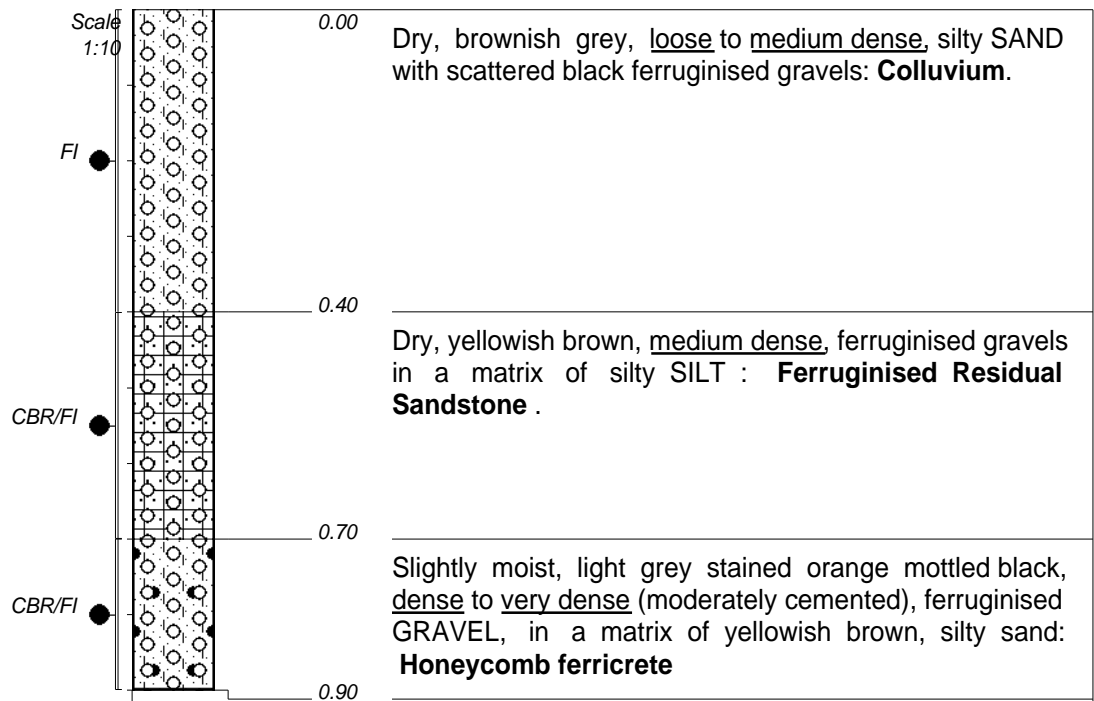


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,8047
Y-COORD : 29,45266

HOLE No: TP17



NOTES

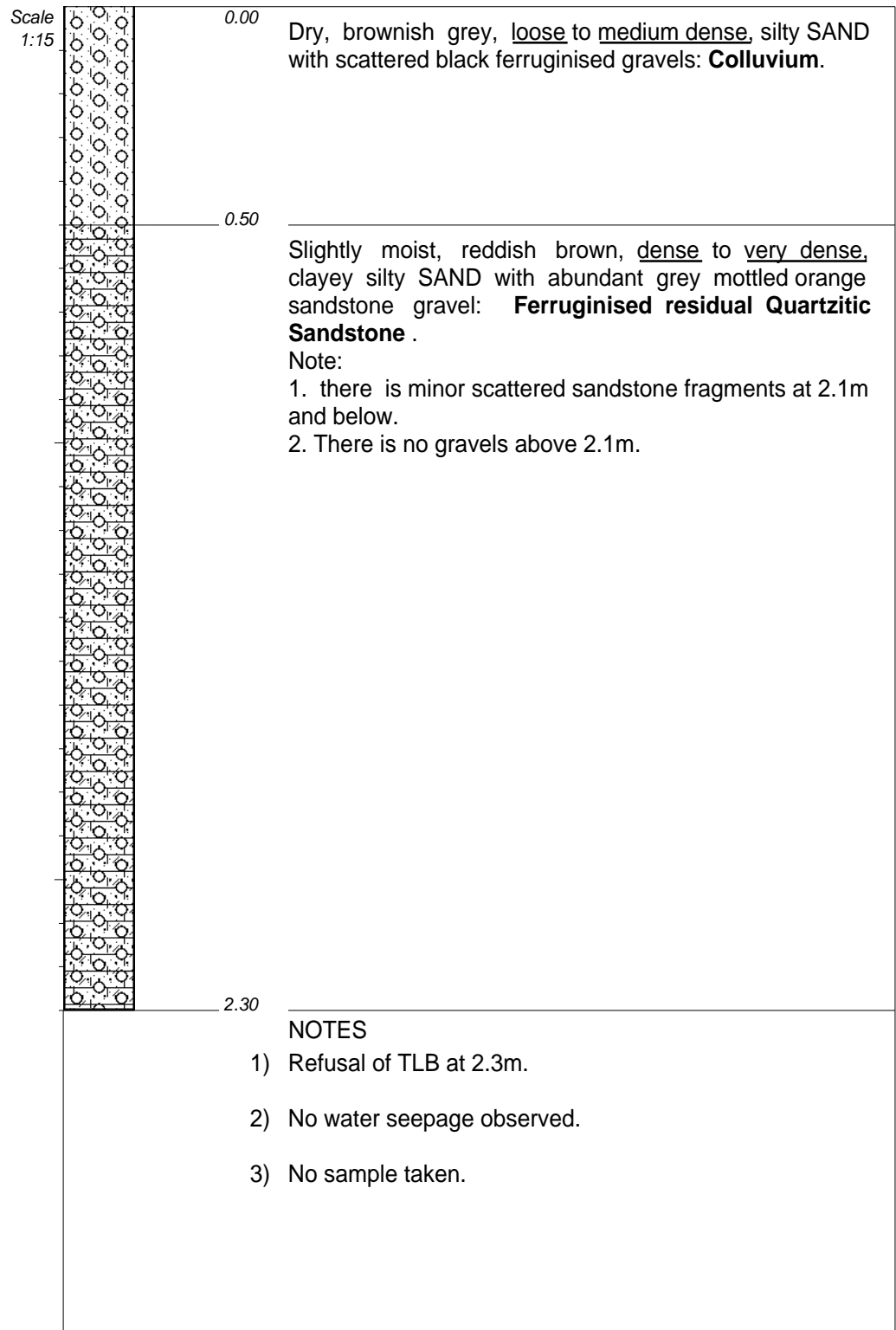
- 1) Refusal of TLB at 0.9m.
- 2) No water seepage observed.
- 3) Disturbed sample FI at 0.0--0.4m.
- 4) Disturbed sample CBR/FI at 0.4--0.7m.
- 5) Disturbed sample CBR/FI at 0.7--0.9m.

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,808
Y-COORD : 29,4532

HOLE No: TP18

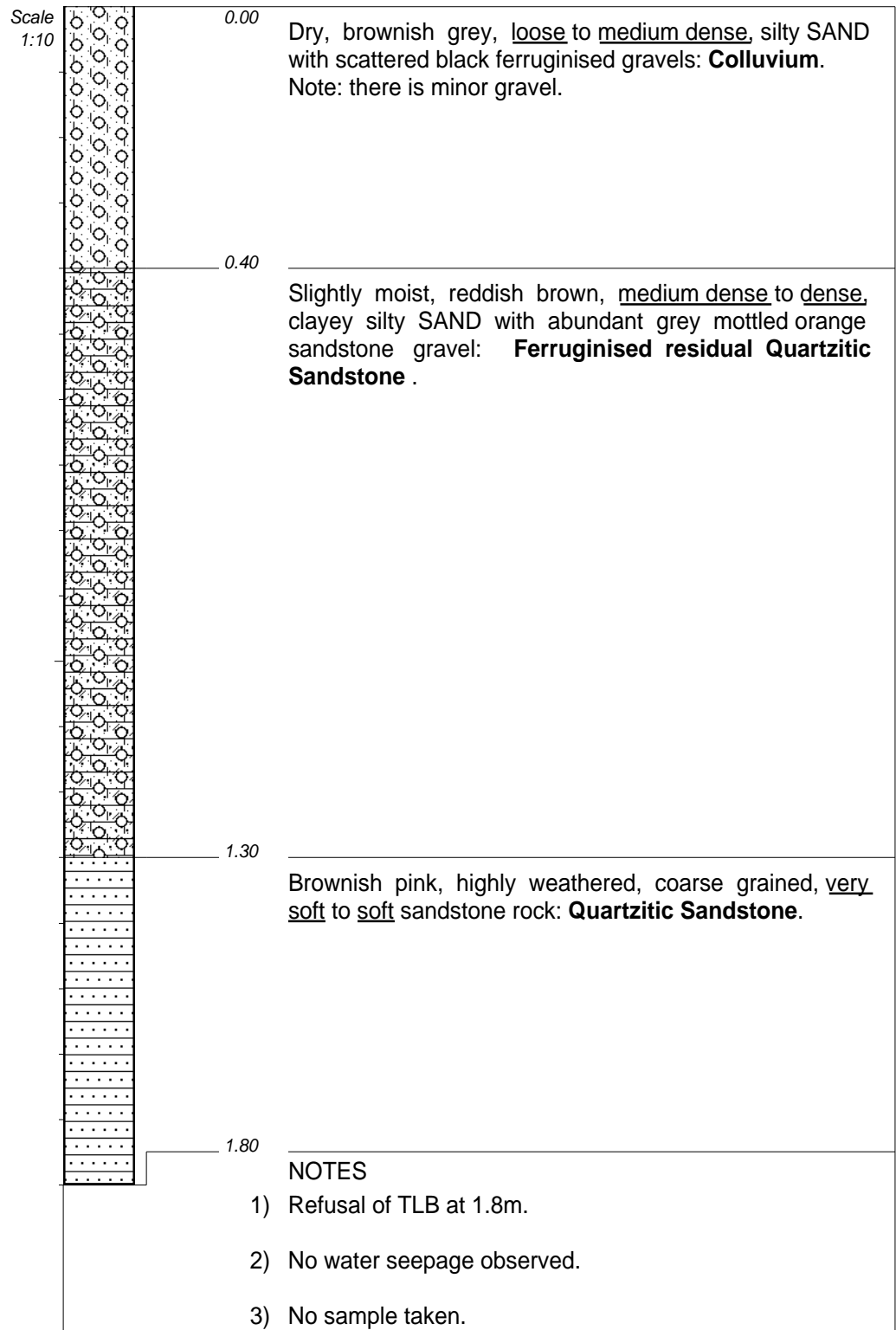


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,806
Y-COORD : 29,45350

HOLE No: TP19

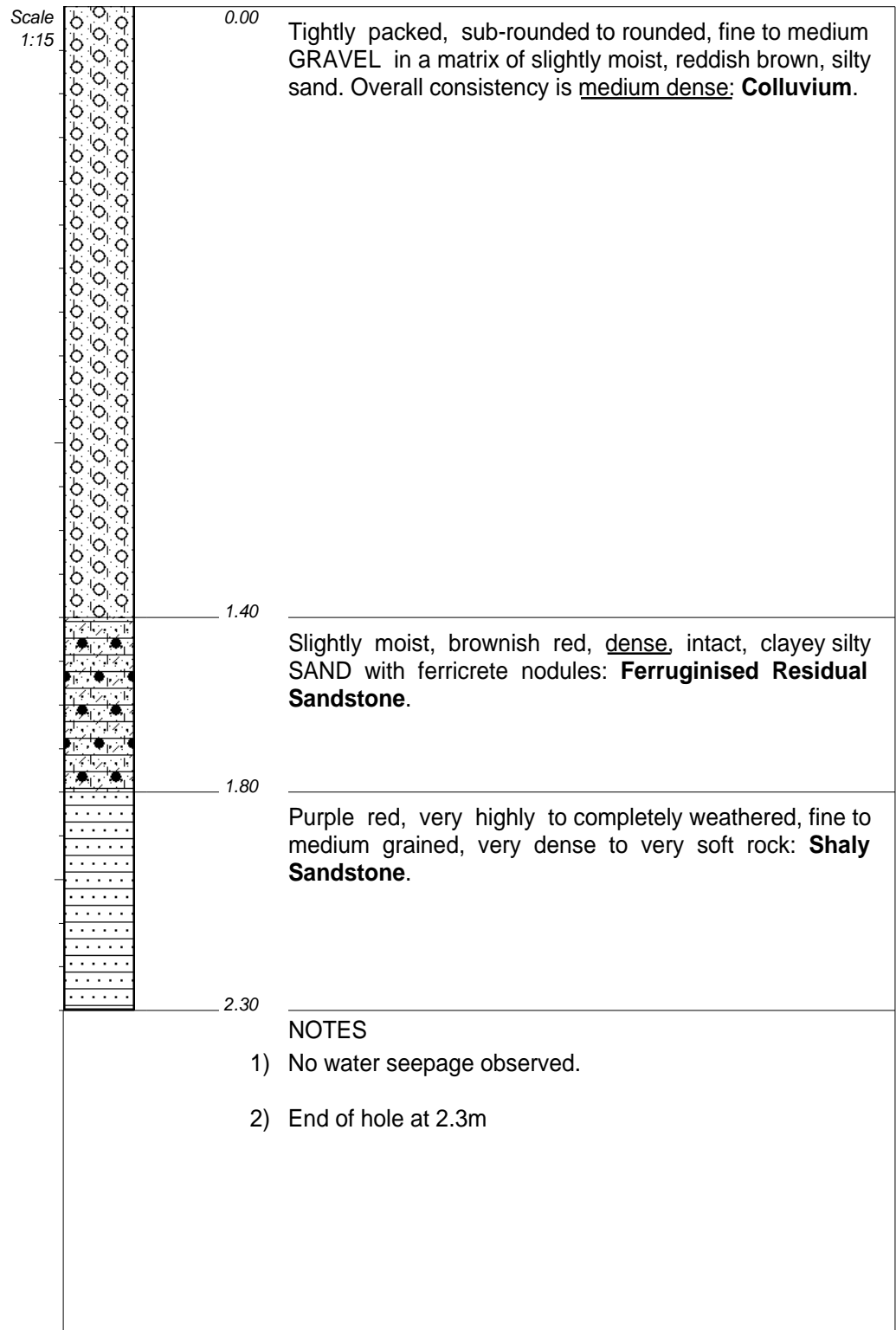


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25,8049
Y-COORD : 29,4536

HOLE No: TP20

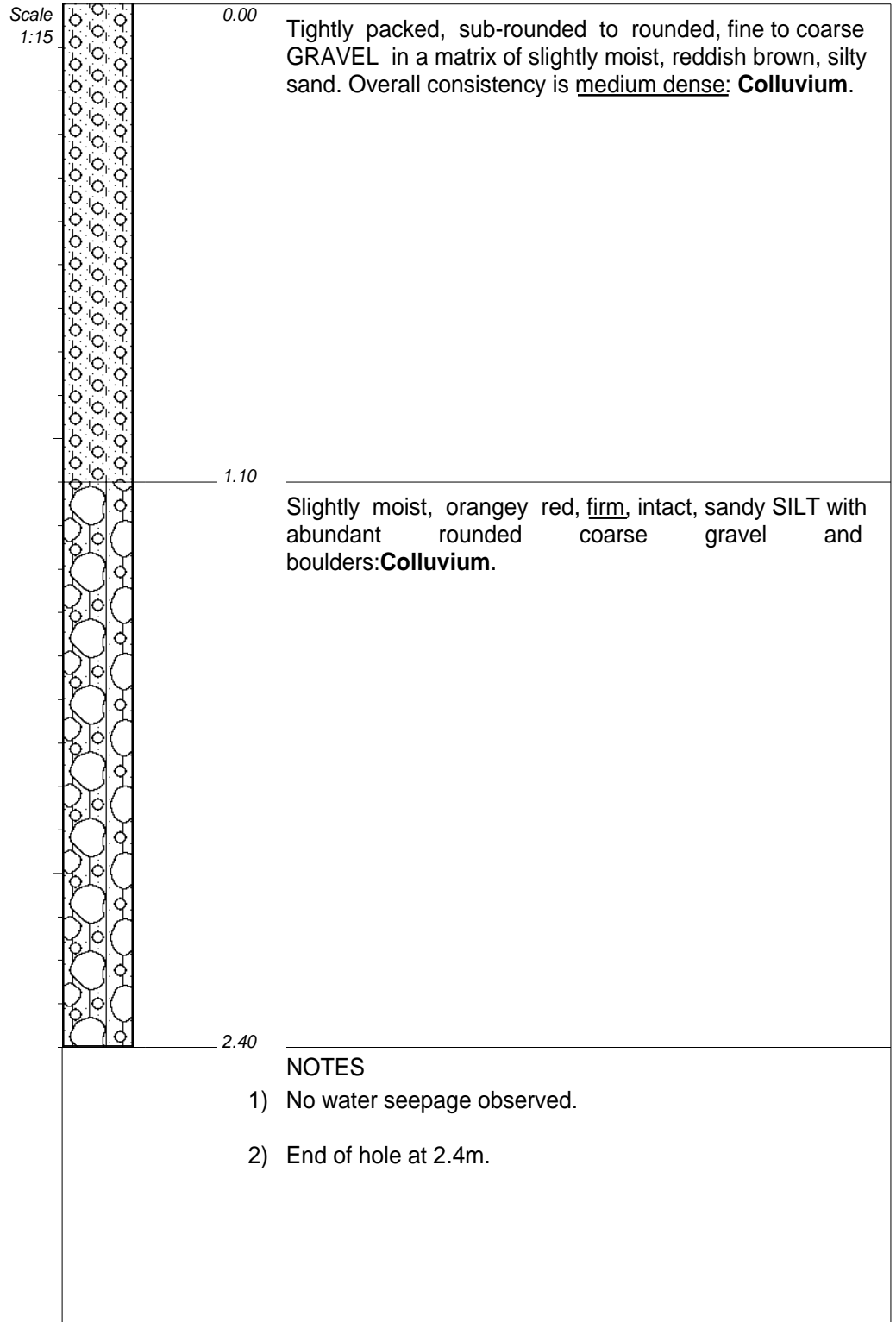


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.80744
Y-COORD : 29.44384

HOLE No: TP21

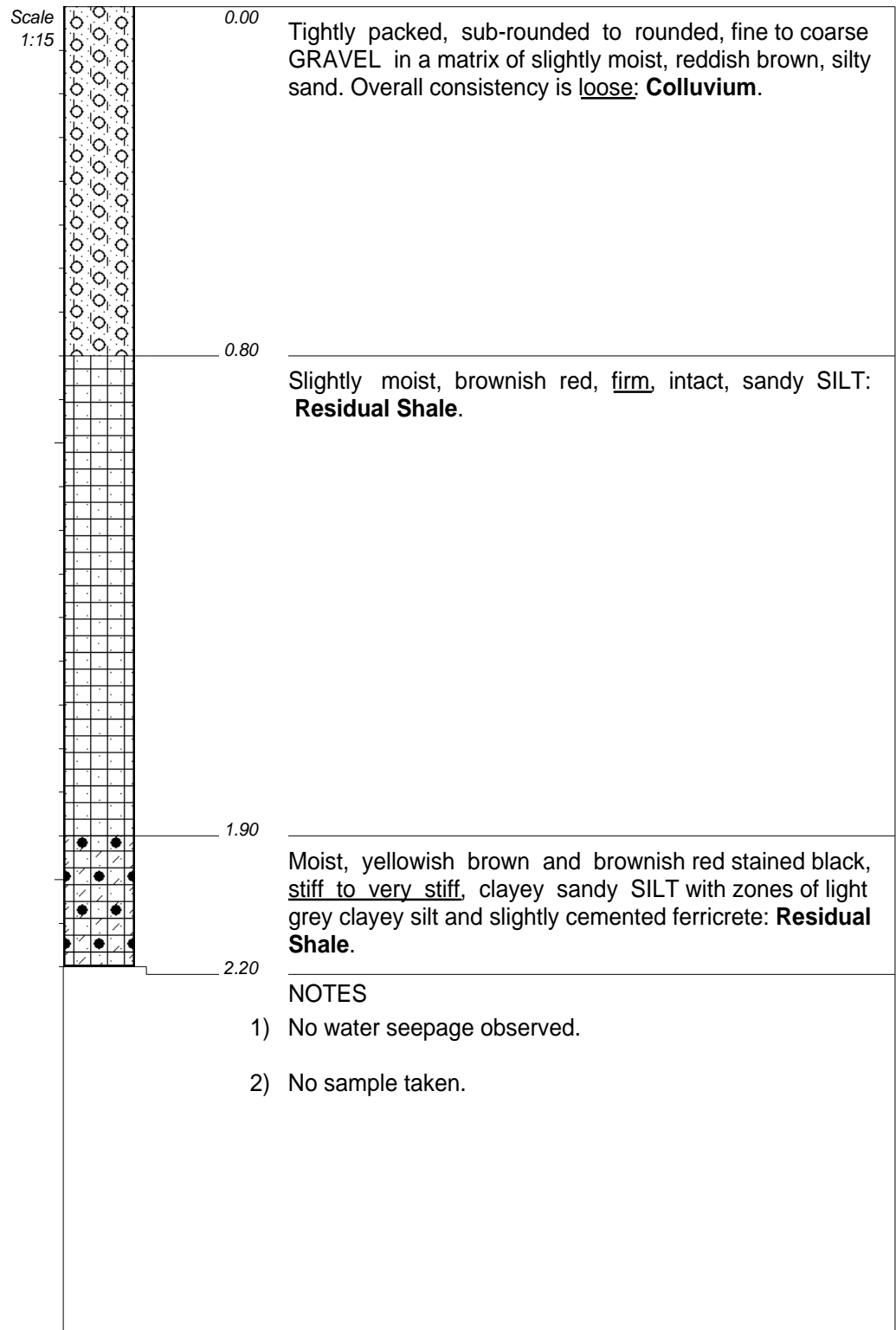


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.80771
Y-COORD : 29.44588

HOLE No: TP22

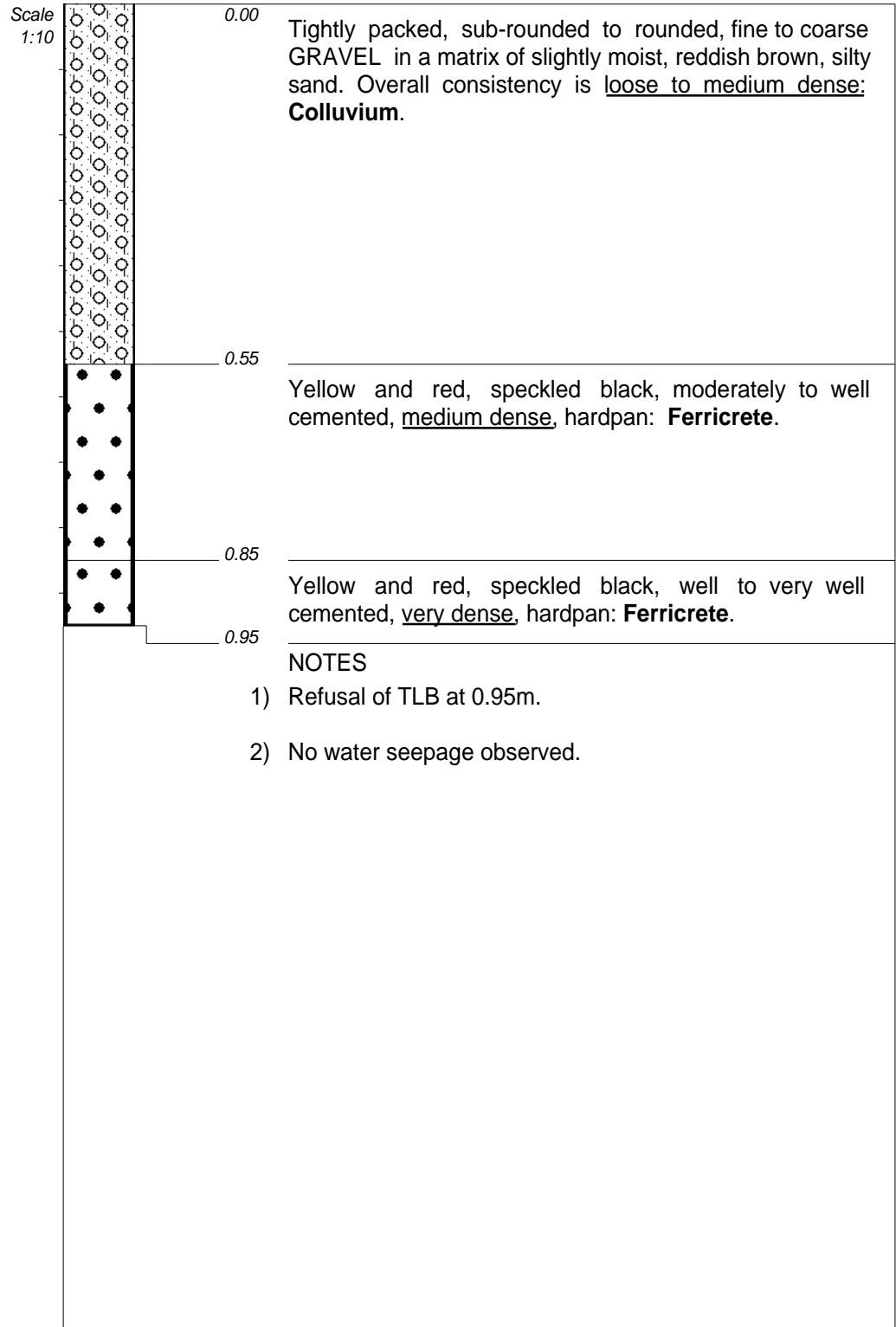


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.8087
Y-COORD : 29.4445

HOLE No: TP23

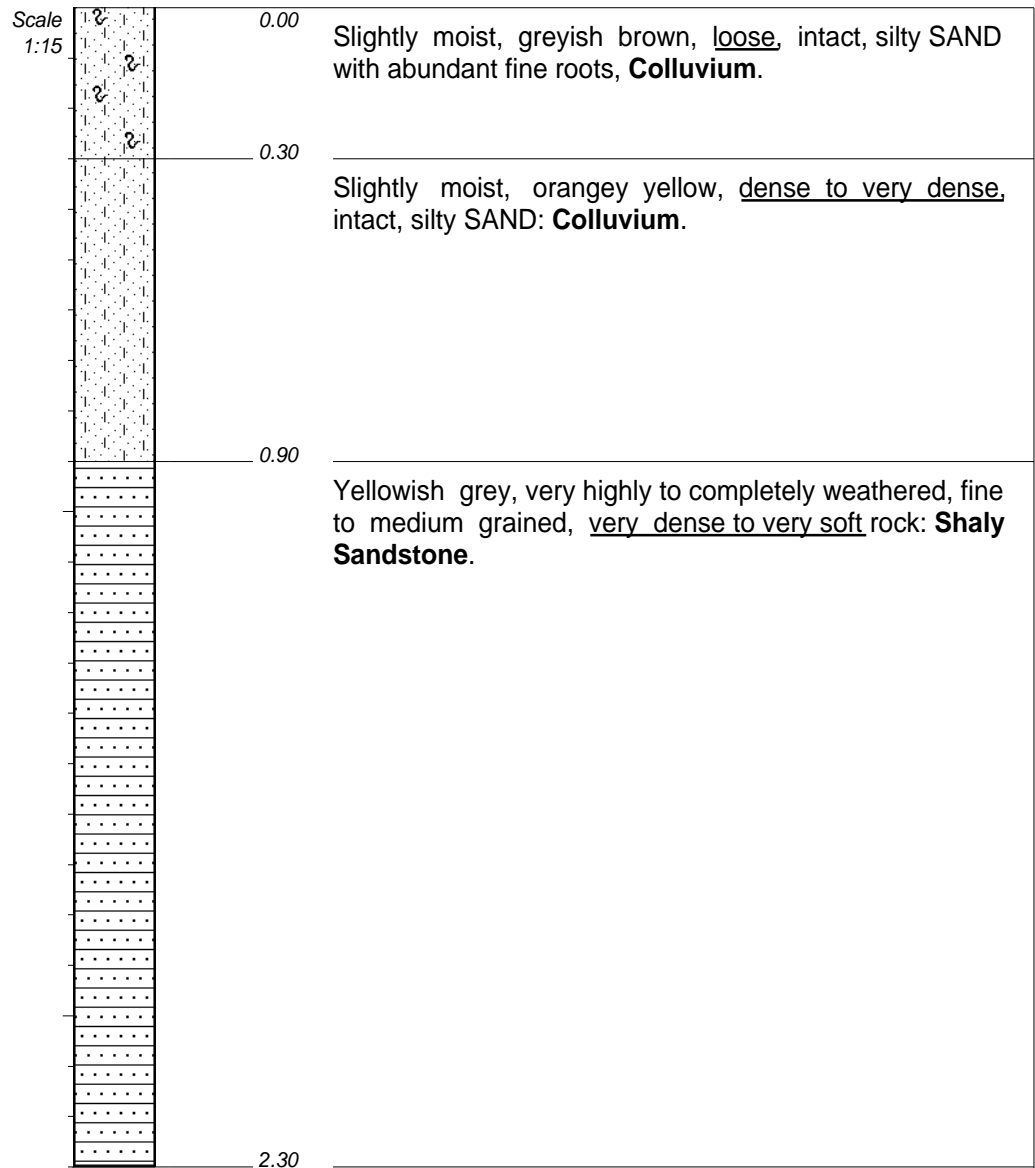


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.8084
Y-COORD : 29.44743

HOLE No: TP24



NOTES

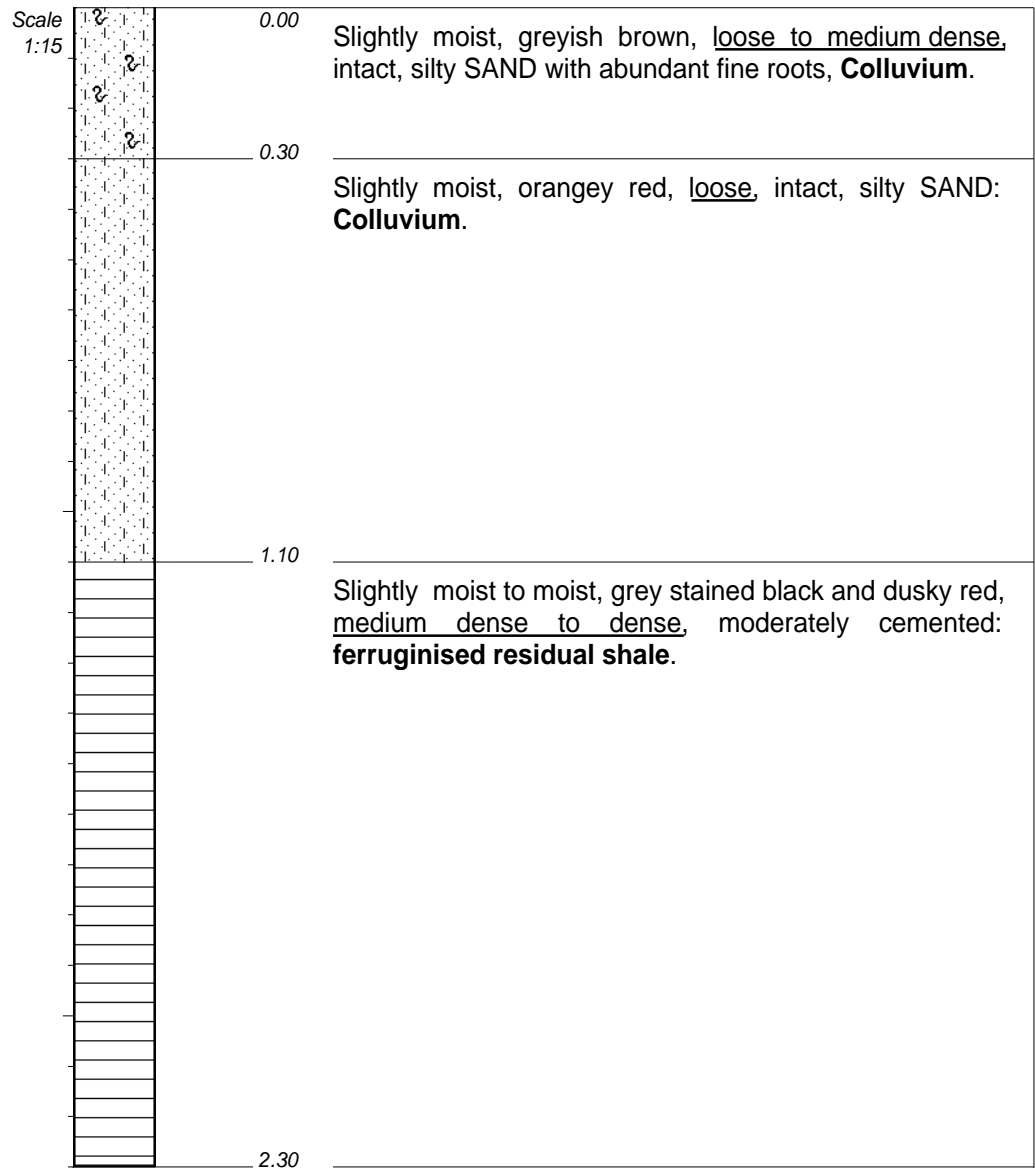
- 1) No water seepage observed.
- 2) End of hole at 2.3m.

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.80903
Y-COORD : 29.44994

HOLE No: TP25



NOTES

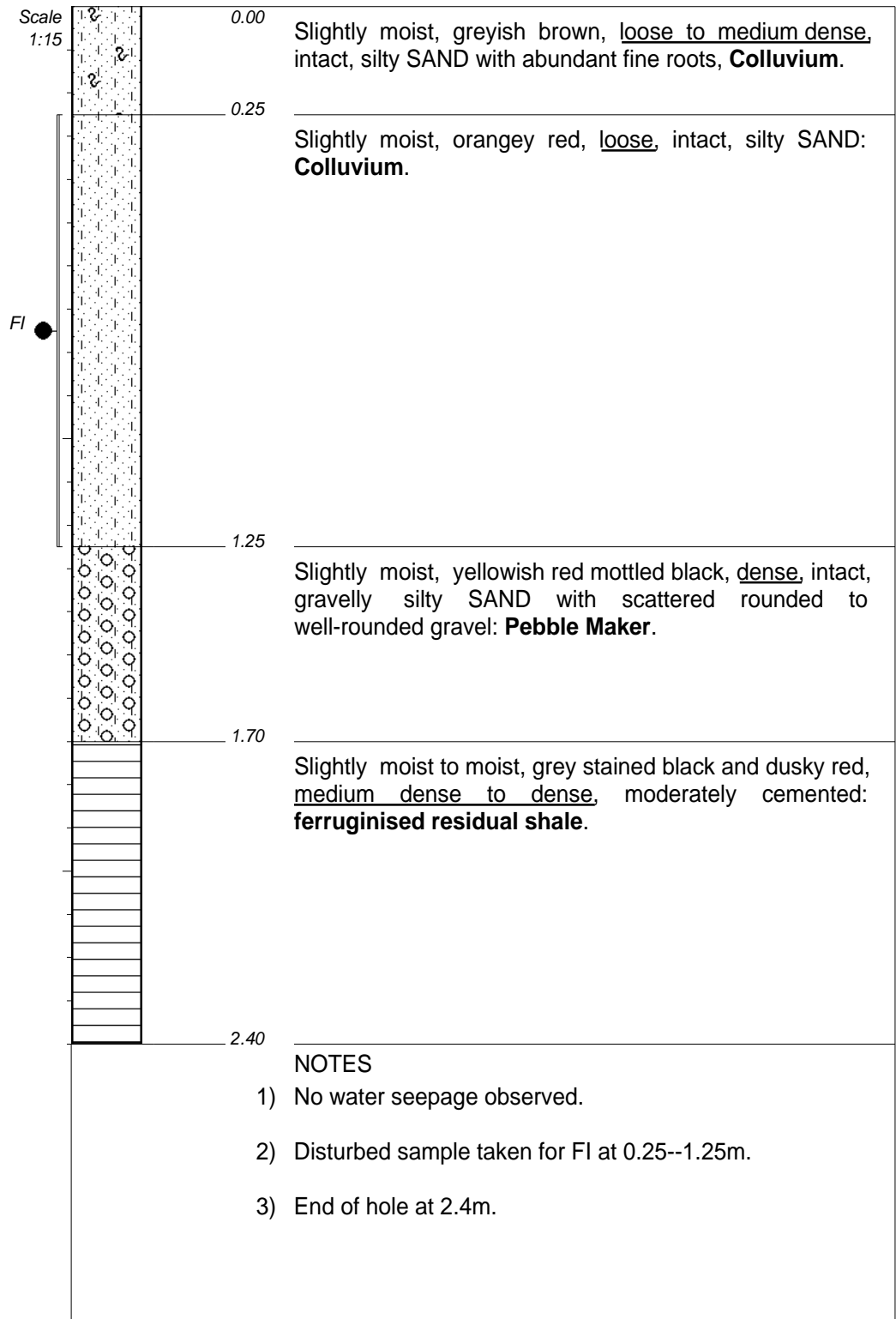
- 1) No water seepage observed.
- 2) End of hole at 2.3m.

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81063
Y-COORD : 29.45175

HOLE No: TP26

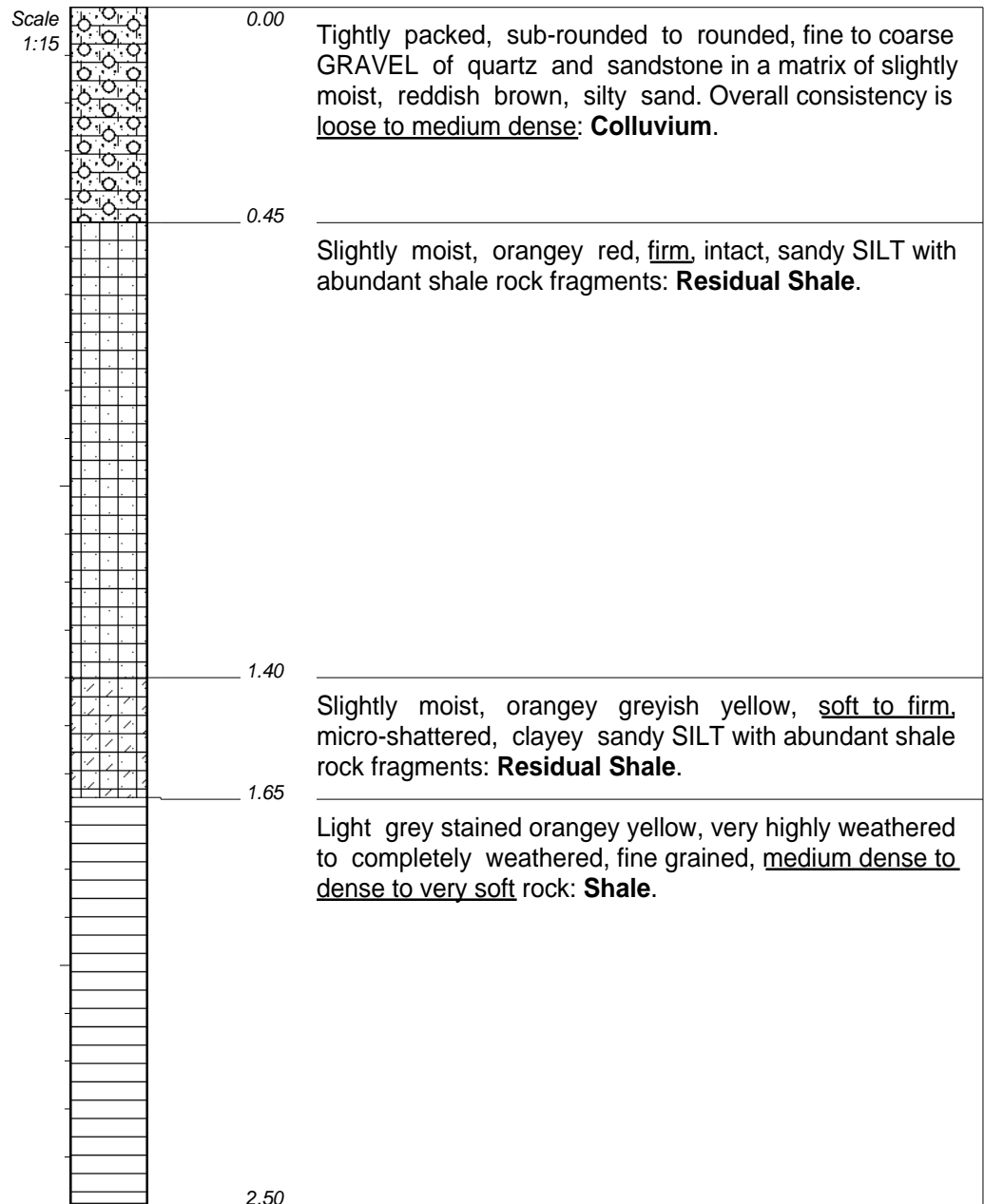


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81037
Y-COORD : 29.44919

HOLE No: TP27



NOTES

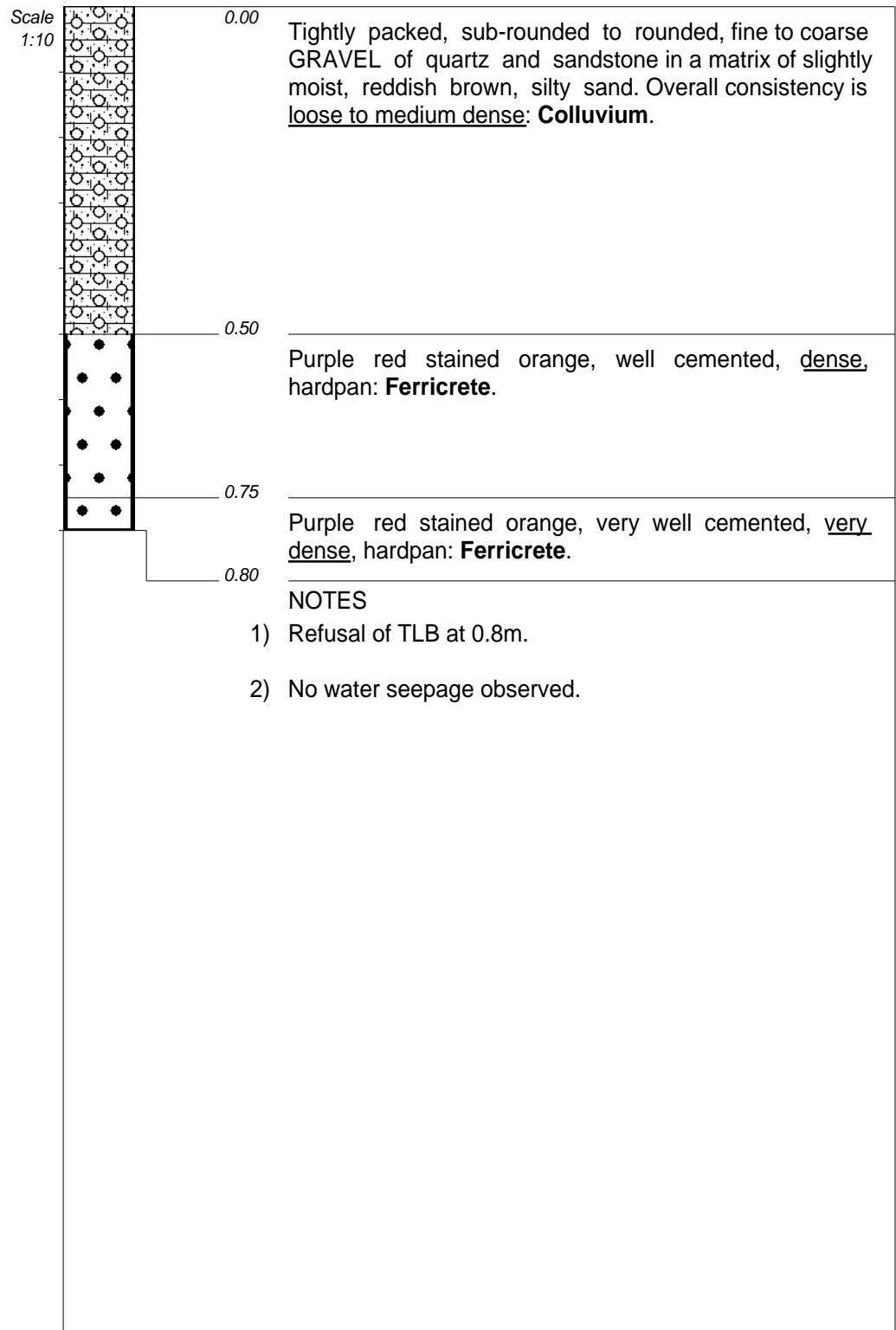
- 1) No water seepage observed.
- 2) End of hole at 2.5m.

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81002
Y-COORD : 29.44623

HOLE No: TP28

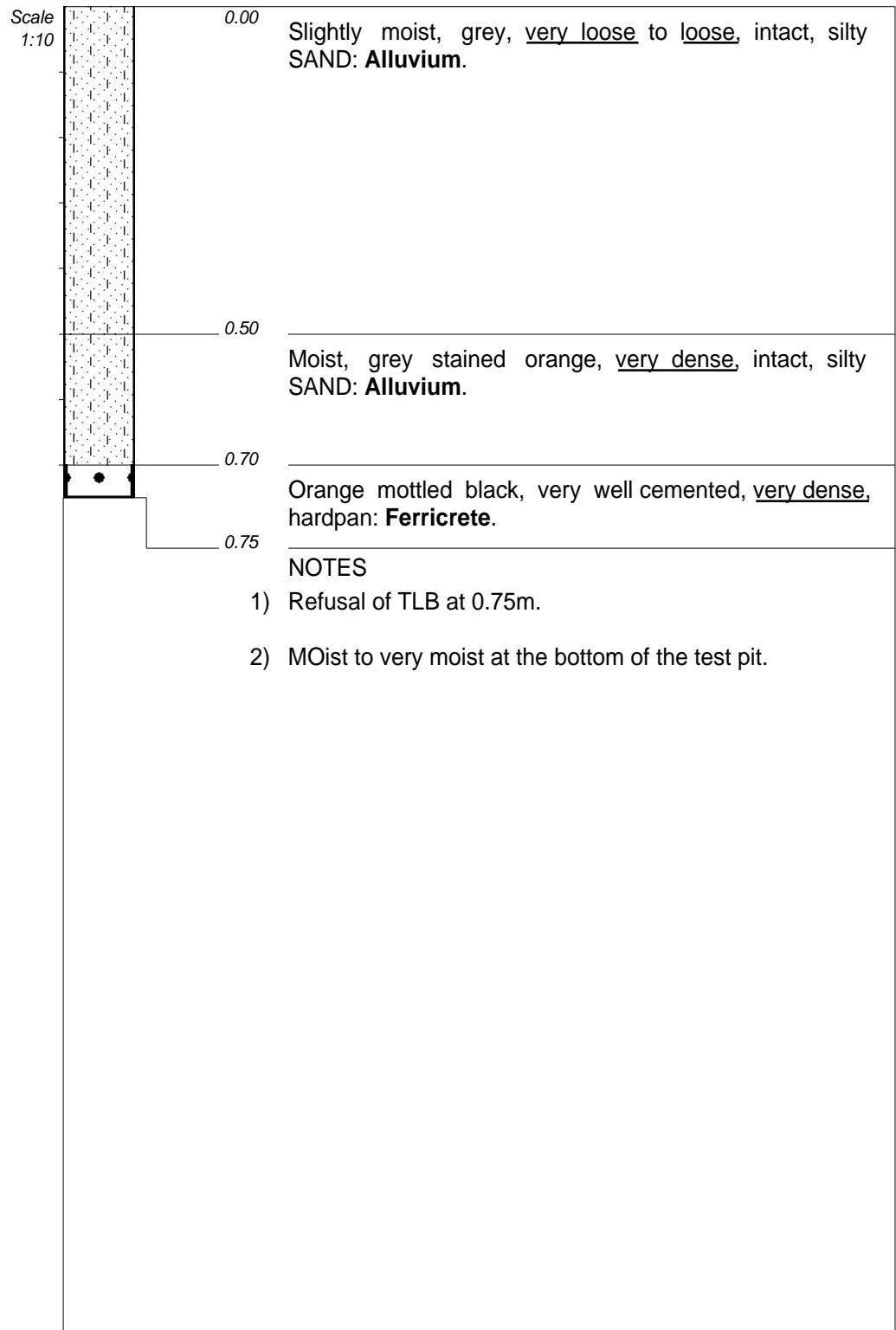


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.8106
Y-COORD : 29.4436

HOLE No: TP29

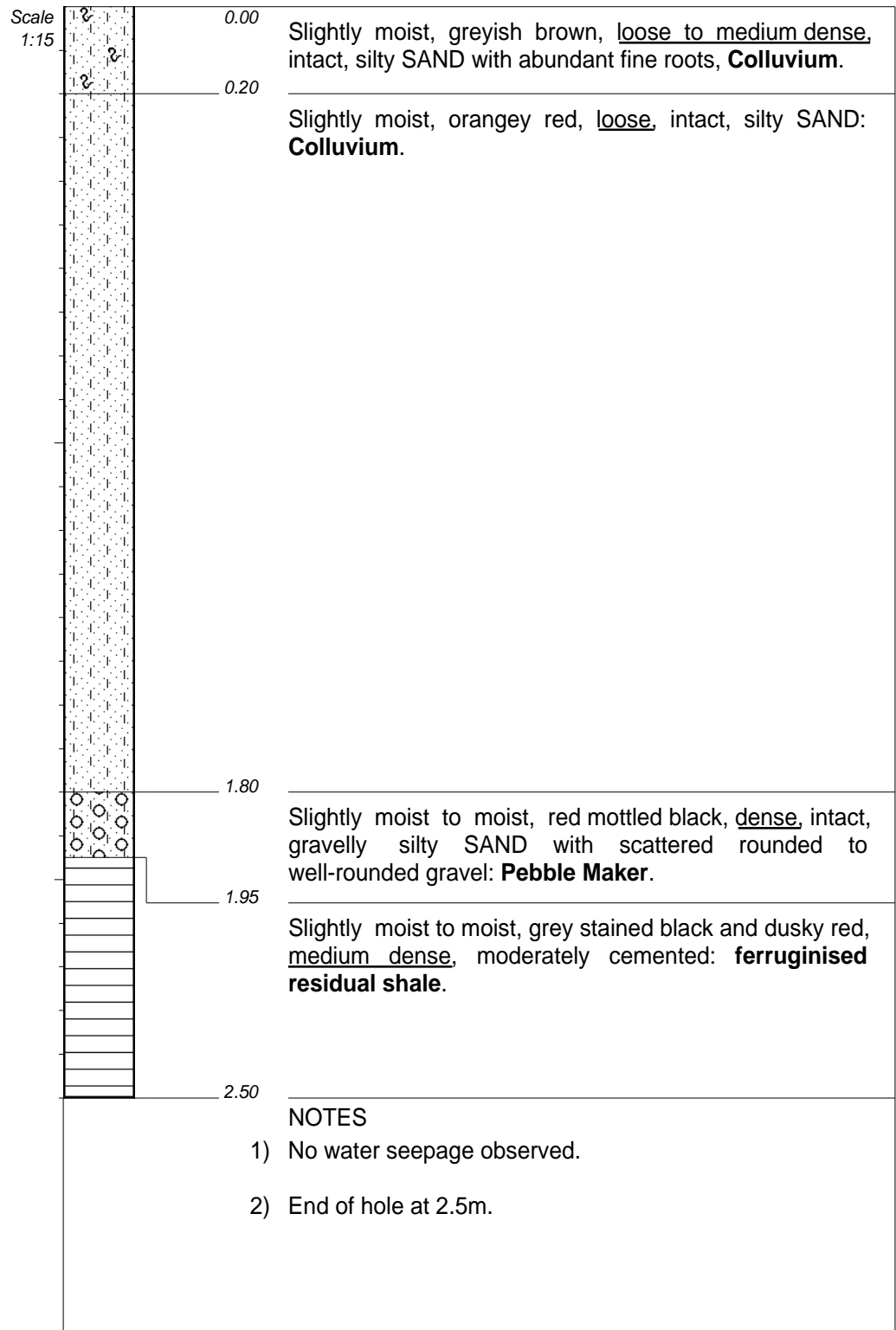


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.8127
Y-COORD : 29.44397

HOLE No: TP30

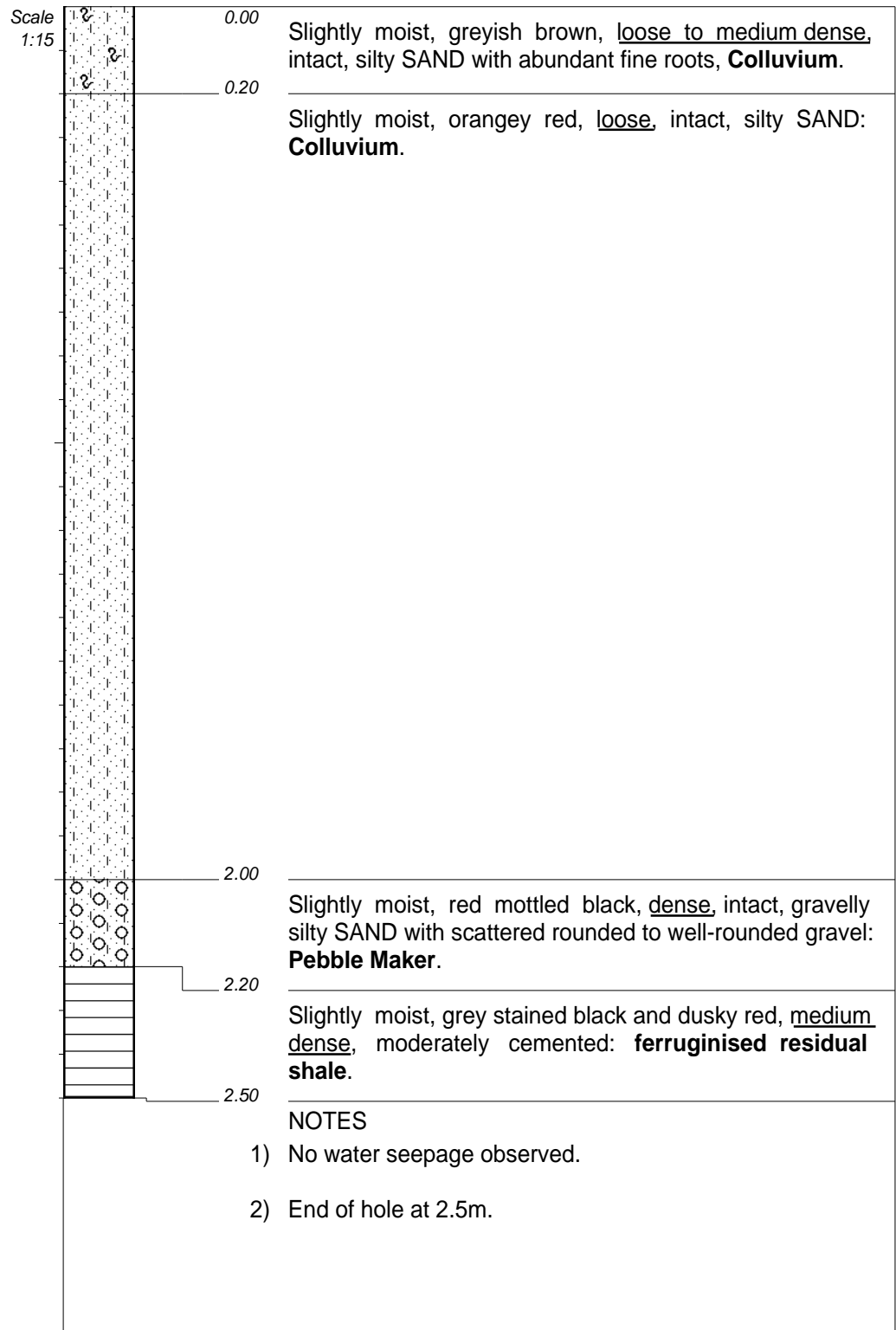


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81253
Y-COORD : 29.44844

HOLE No: TP31

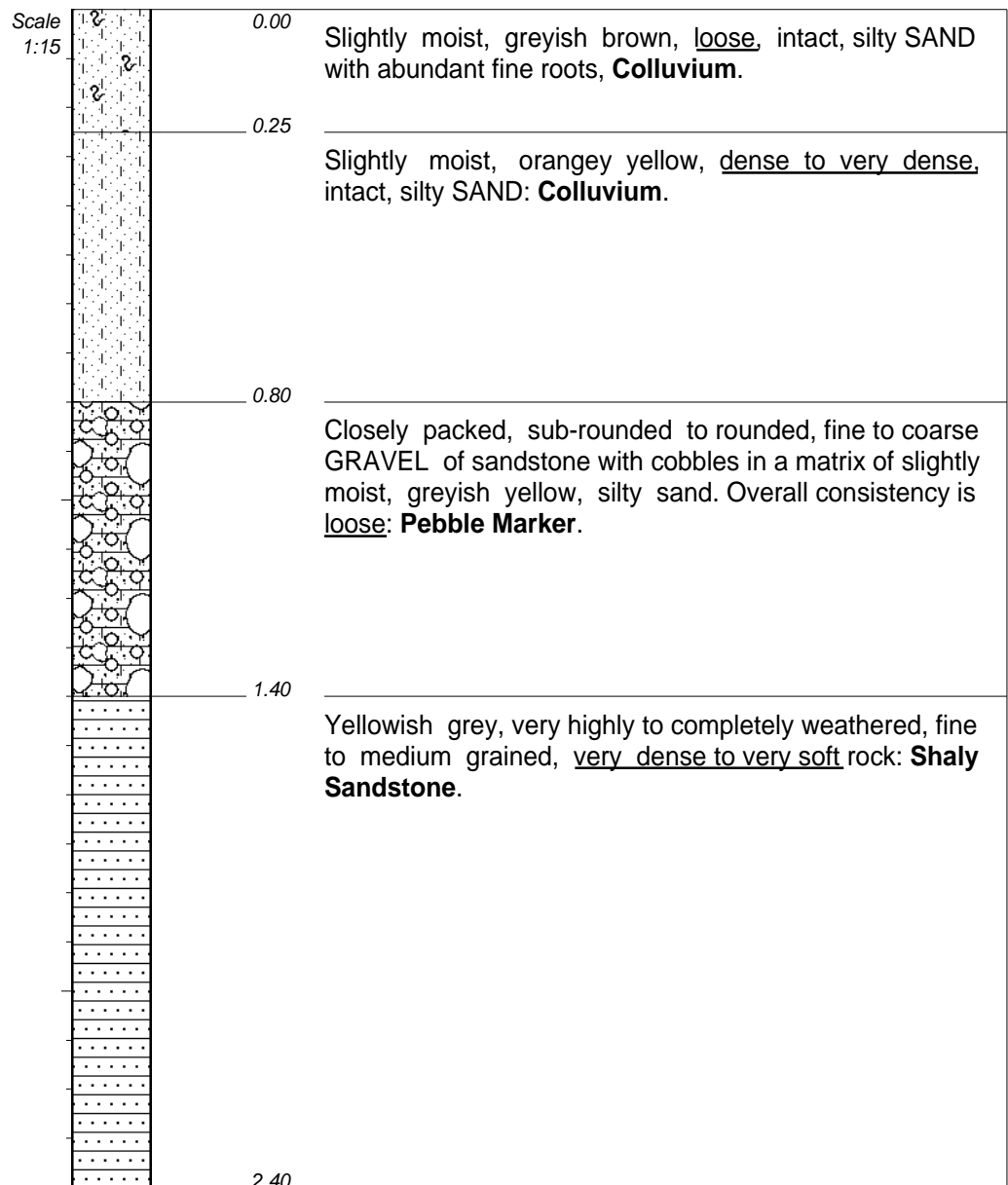


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81258
Y-COORD : 29.45111

HOLE No: TP32



NOTES

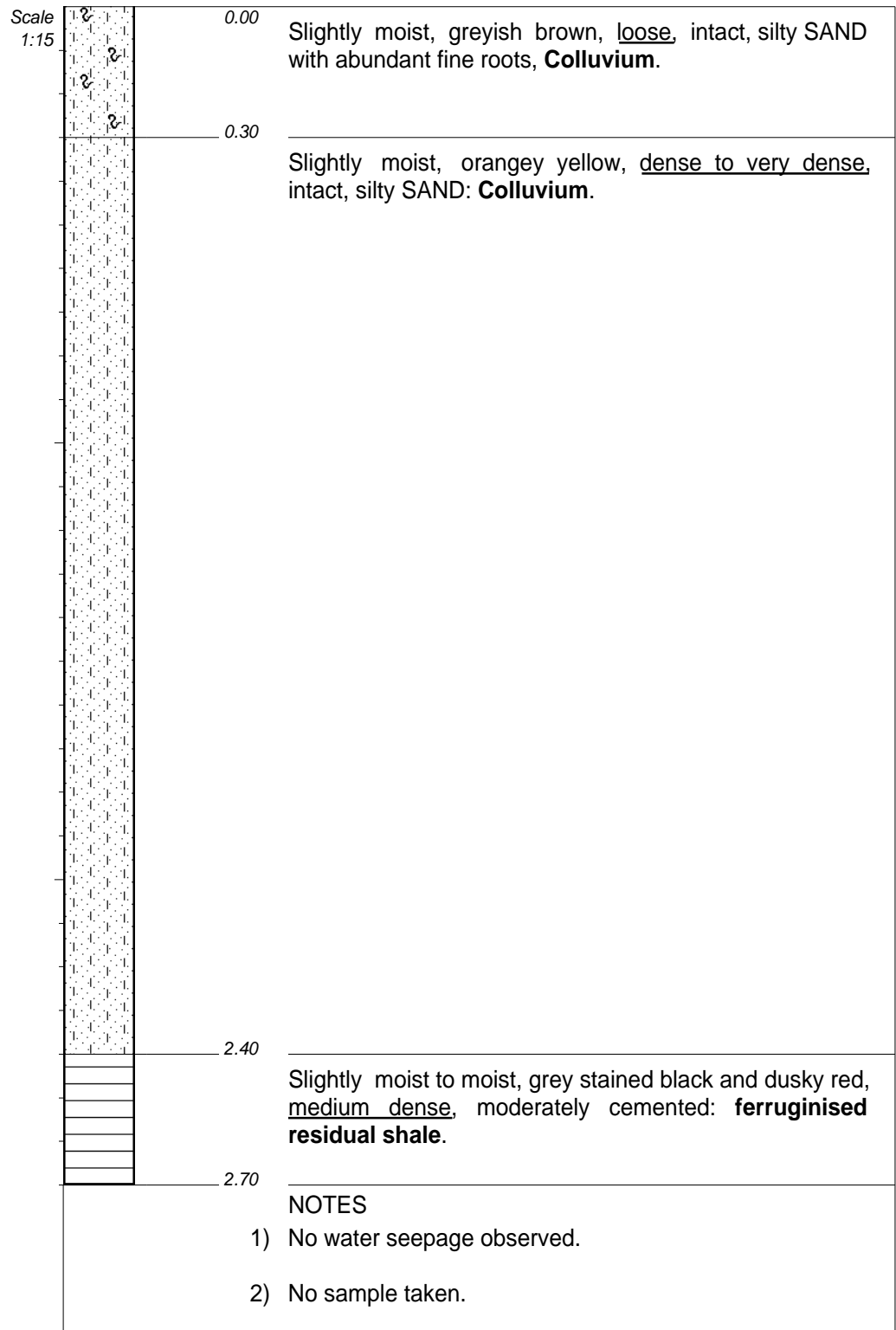
- 1) No water seepage observed.
- 2) End of hole at 2.5m.

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81264
Y-COORD : 29.45294

HOLE No: TP33

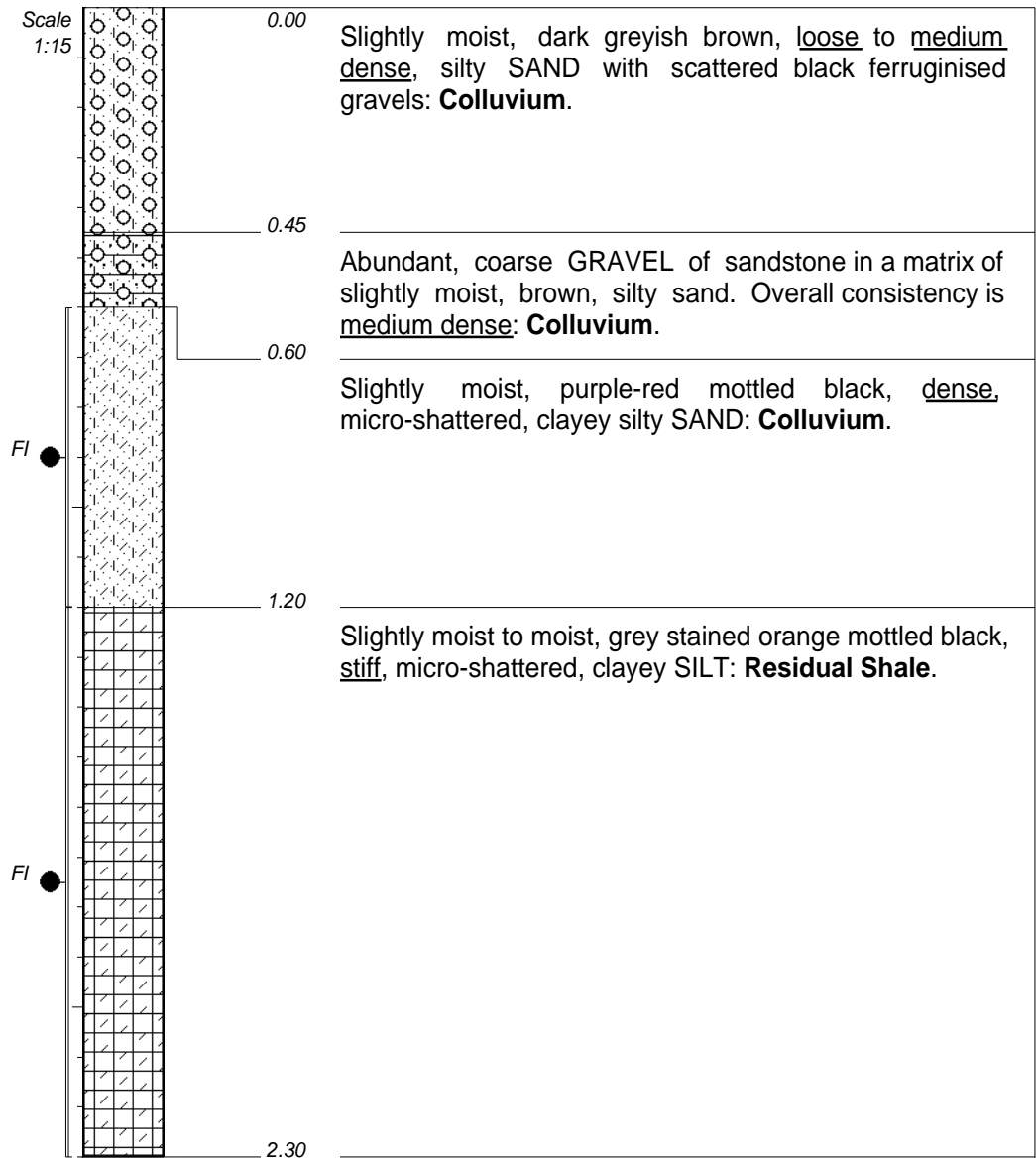


CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81483
Y-COORD : 29.45134

HOLE No: TP34



NOTES


















- 1) Slow progress due to the stiffness of the residual shale.
- 2) No water seepage observed.
- 3) Disturbed sample taken for FI at 0.6--1.2m
- 4) Disturbed sample taken for FI at 1.2--2.3m

CONTRACTOR : Coastal Hire
MACHINE : JCB 3DX Super
DRILLED BY : Takalani and Mthuthuzeli
PROFILED BY : L Netshilindi & L Pfuluwani
TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM : 0.6m
DATE : 15/11/2018 & 24/05/2019
DATE : 15/11/2018 & 24/05/2019
DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD : -25.81201
Y-COORD : 29.44596

HOLE No: TP35

| | | |
|--|---|--------------|
|  | BOULDERS | {SA01} |
|  | GRAVELS/gravel | {SA02} |
|  | GRAVELLY | {SA03} |
|  | SAND | {SA04} |
|  | SANDY | {SA05} |
|  | SILT | {SA06} |
|  | SILTY | {SA07} |
|  | CLAY | {SA08} |
|  | CLAYEY | {SA09} |
|  | SANDSTONE | {SA11} |
|  | SHALE | {SA12} |
|  | HARDPAN FERRICRETE | {SA23}{SA29} |
|  | HONEYCOMB FERRICRETE/ferricrete nodules | {SA24} |
|  | WELL CEMENTED | {SA29} |
| Name  | DISTURBED SAMPLE | {SA38} |
|  | ROOTS | {SA40} |
|  | COBBLES | {SA58} |
| | | |

CONTRACTOR :
MACHINE :
DRILLED BY :
PROFILED BY :

TYPE SET BY : LN
SETUP FILE : STANDARD.SET

INCLINATION :
DIAM :
DATE :
DATE :

DATE : 03/06/2019 16:58
TEXT : ..AerorandSouthProject.txt

ELEVATION :
X-COORD :
Y-COORD :

LEGEND
SUMMARY OF SYMBOLS

APPENDIX D: SITE & TEST PIT PICTURES

Geotechnical Investigation

Site and Test Pit Photos

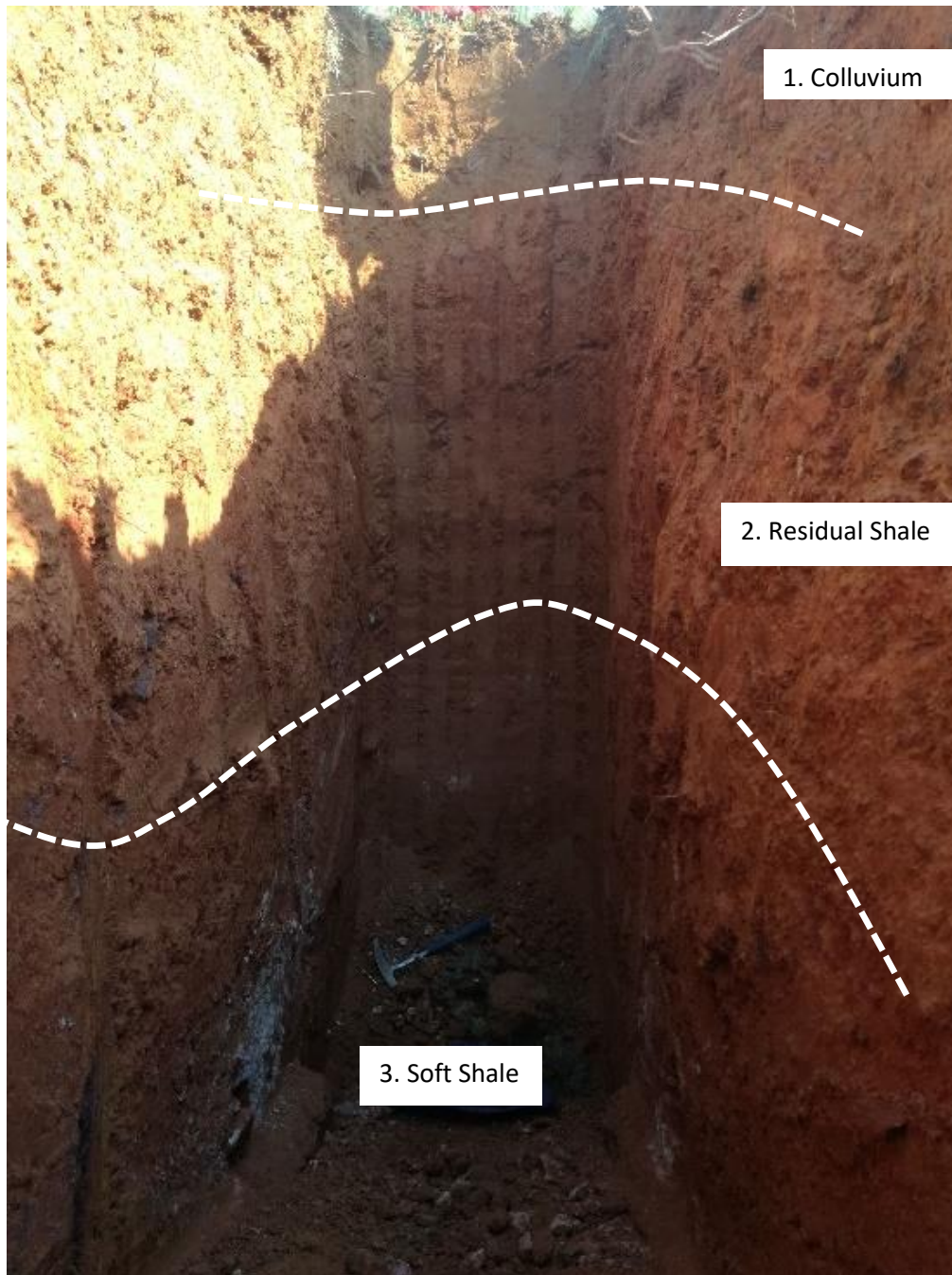


Figure 1 Typical Profile depicting residual shale at TP02



Figure 2. Soft Shale at the bottom of TP02

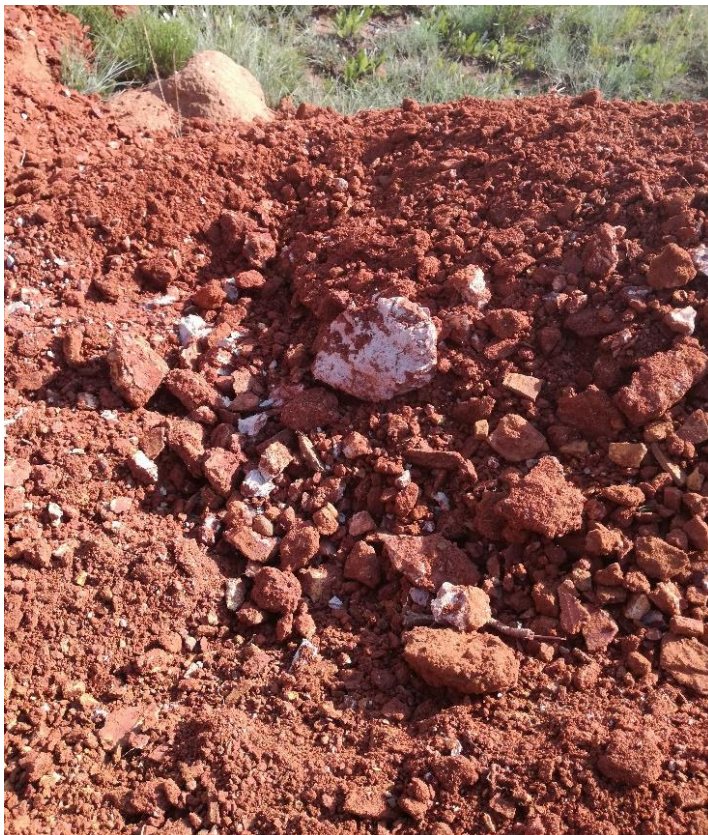


Figure 3 Typical Shale spoil at TP02

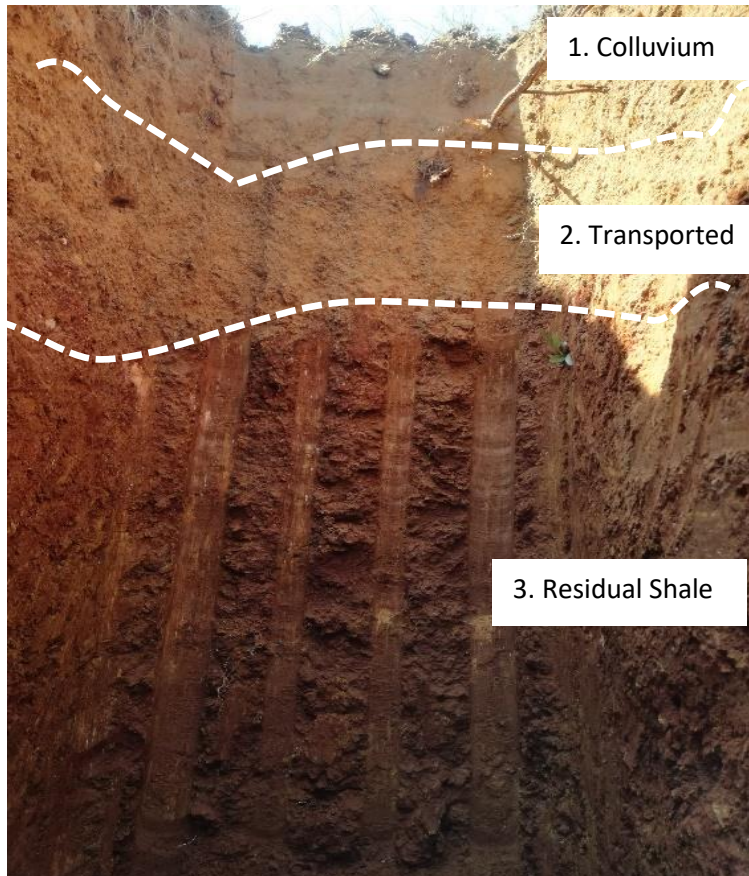


Figure 4 Typical Profile depicting residual shale at TP04



Figure 5 Typical shale fragments encountered at TP02 and TP04

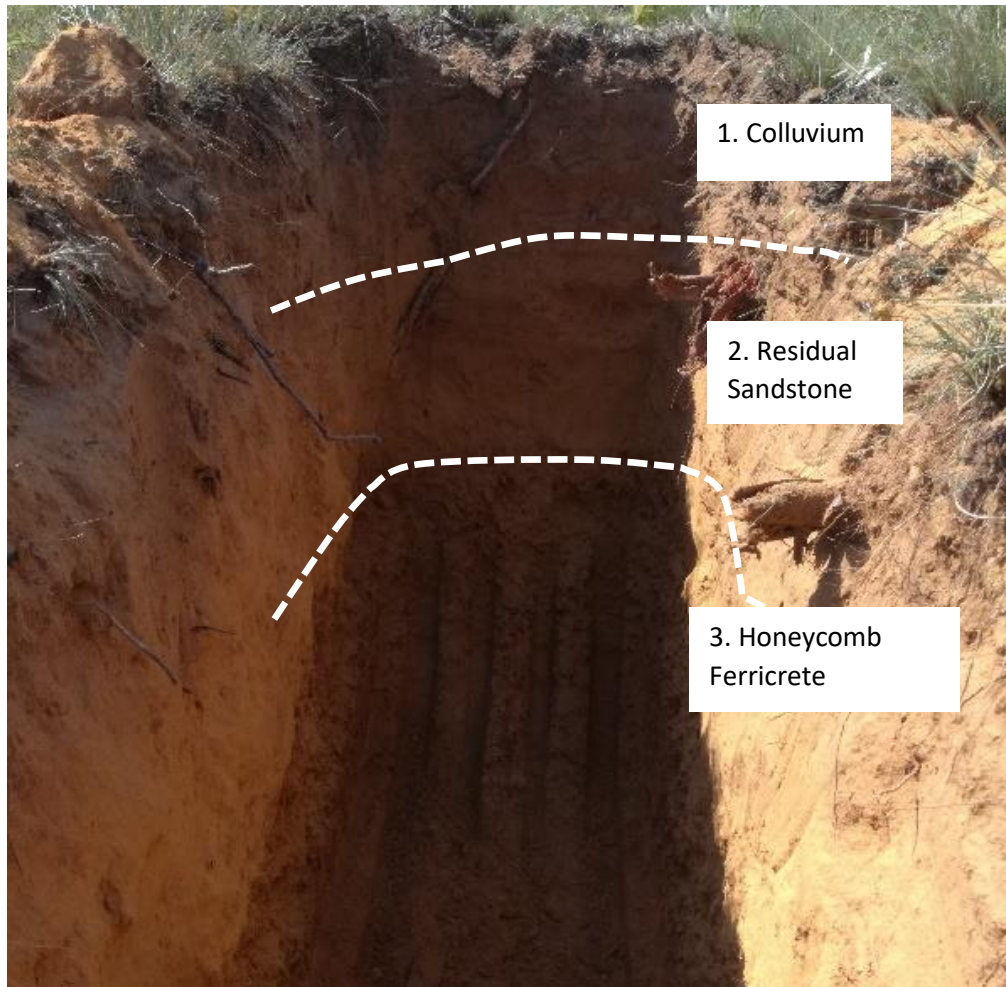


Figure 6 Typical Profile depicting Ferricrete at TP05

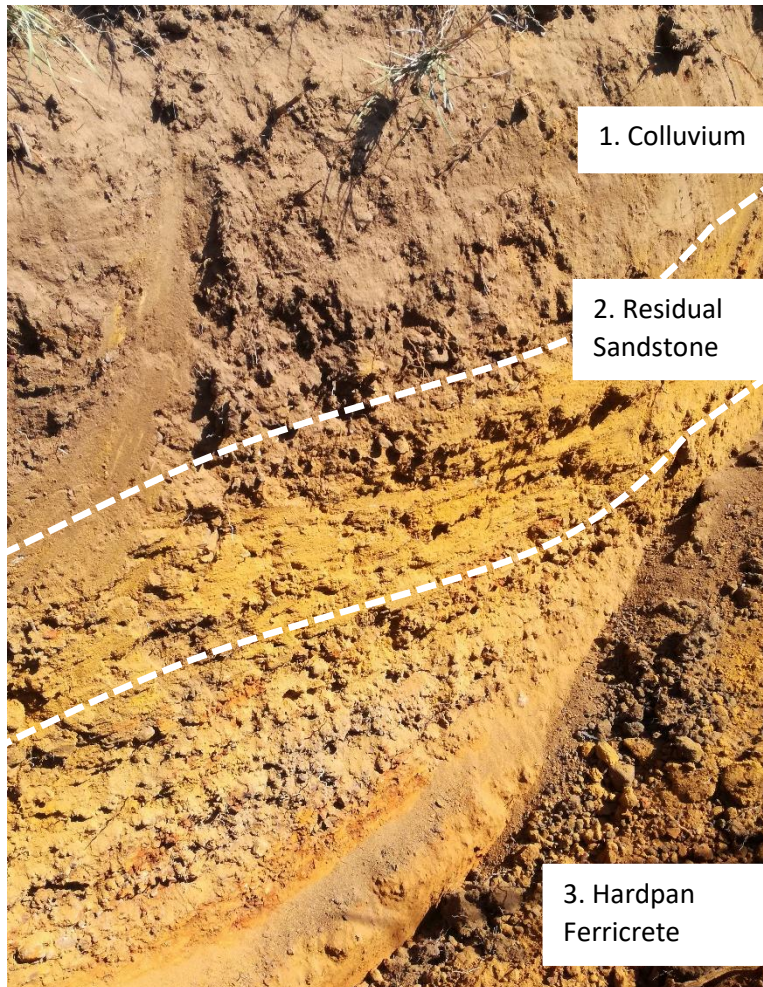


Figure 7 Typical Profile depicting Ferricrete at TP18



Figure 8 Typical Ferricrete spoil at TP18

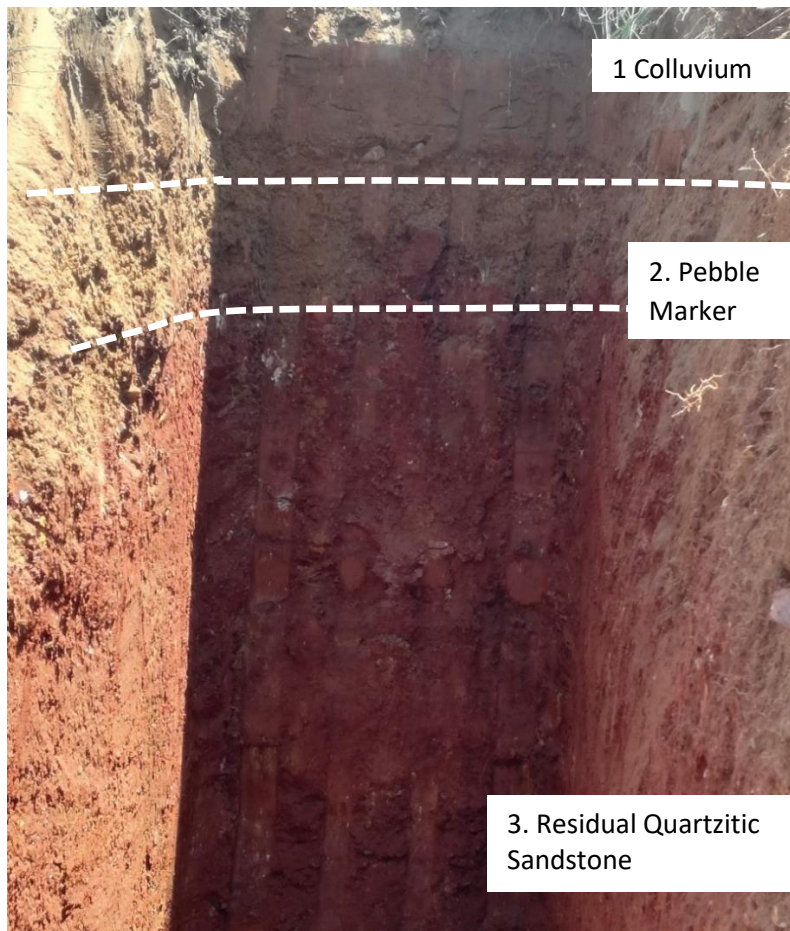


Figure 9 Typical profile depicting Residual quartzitic Sandstone at TP 14



Figure 10 Typical Residual Quartzitic Sandstone spoil at TP14



Figure 11 Typical Residual Quartzitic Sandstone spoil at TP14

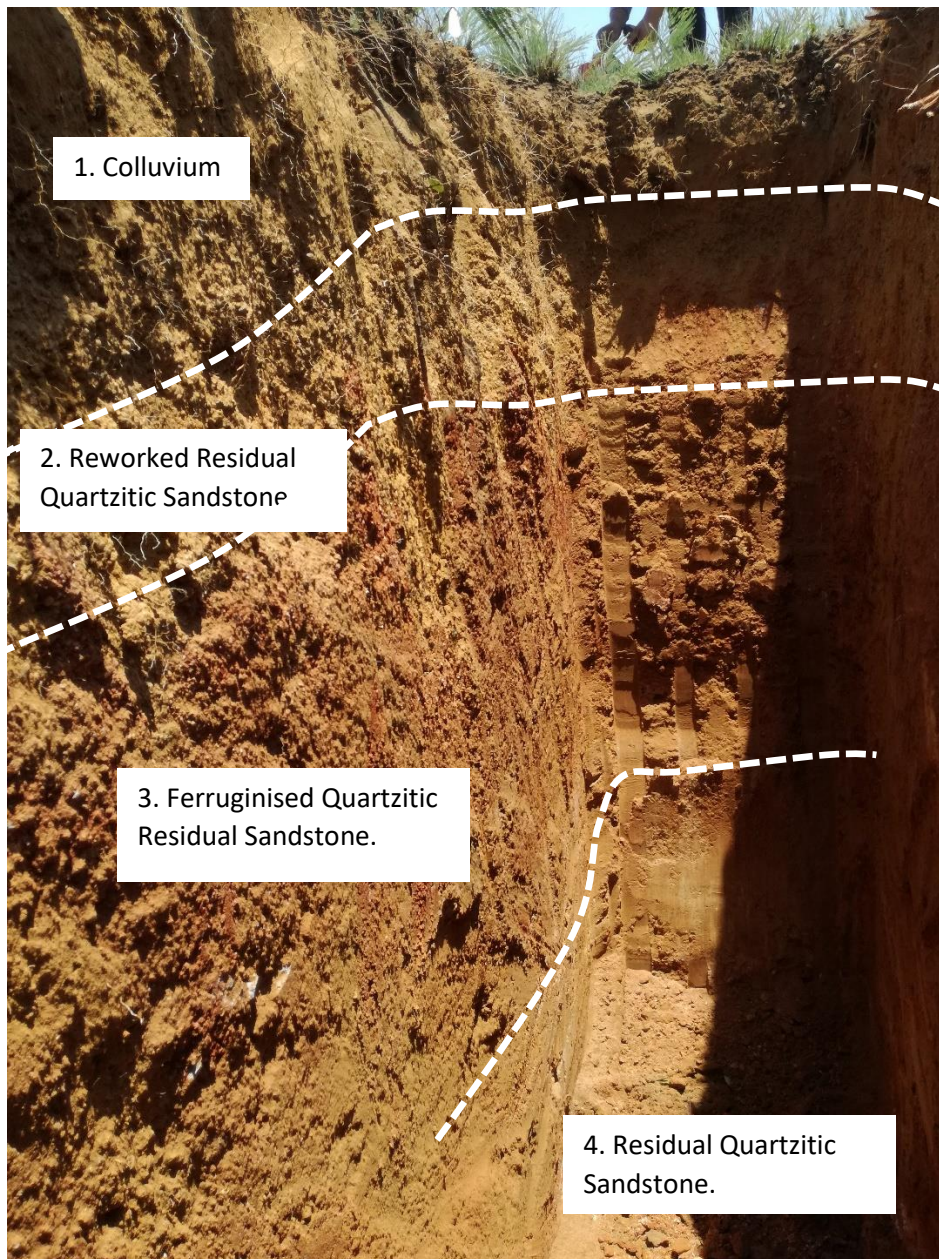


Figure 12 Typical Profile depicting Quartzitic Sandstone at TP16

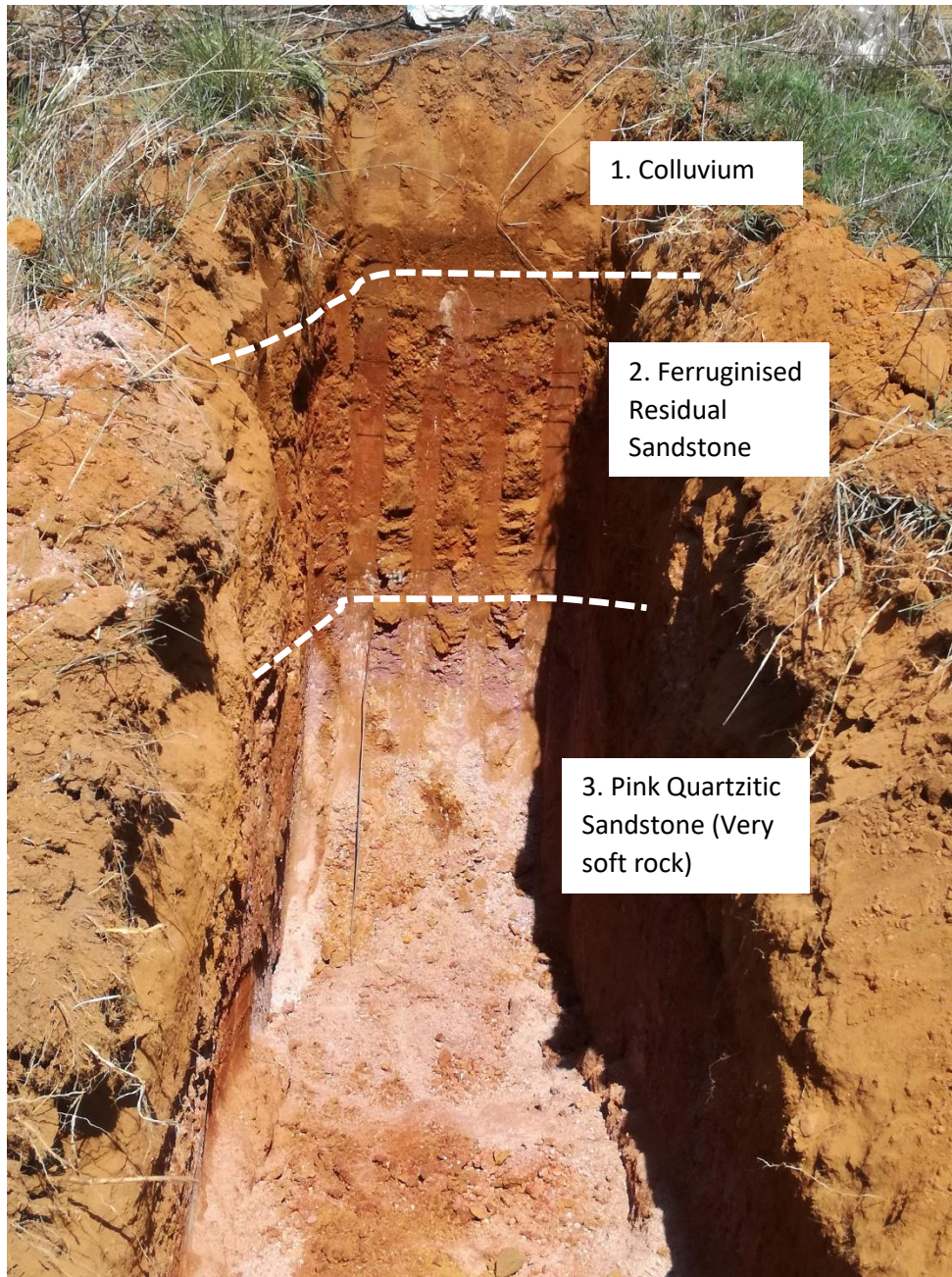


Figure 13 Typical Profile depicting Residual Quartzitic Sandstone at TP20



Figure 14 Typical Residual Quartzitic Sandstone fragments at TP20

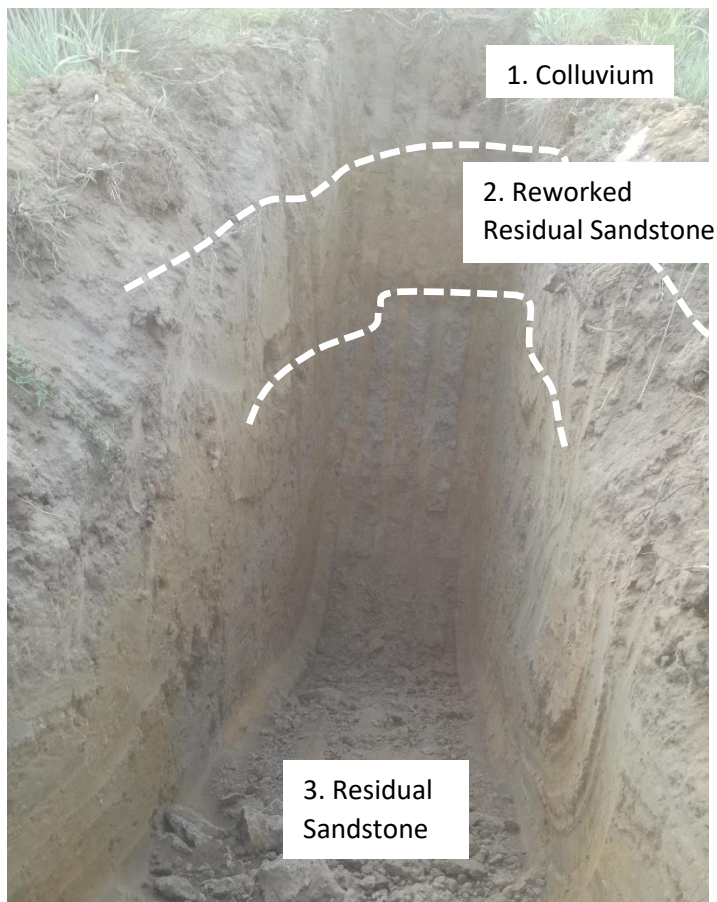


Figure 15 Typical Profile depicting Sandstone at TP11



Figure 16 Typical Residual Sandstone spoil at TP11

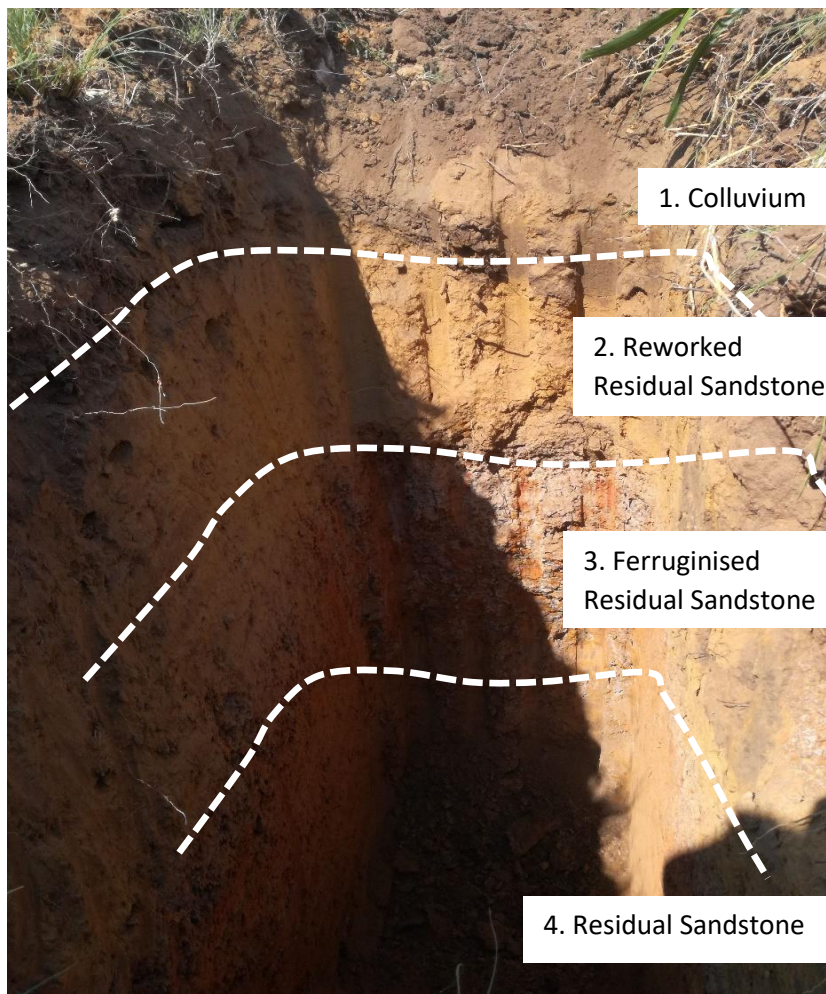


Figure 17 Typical Profile depicting Residual Sandstone at TP15



Figure 18 Typical Residual Sandstone at the bottom of TP15



Figure 19 Man-made trench (drainage channel) encountered close to TP15



Figure 20 DPL Test being conducted adjacent to TP02



Figure 21: Grey alluvial material underlain by hardpan ferricrete encountered in TP29



Figure 22: Yellow very dense to very soft rock shale encountered in TP28

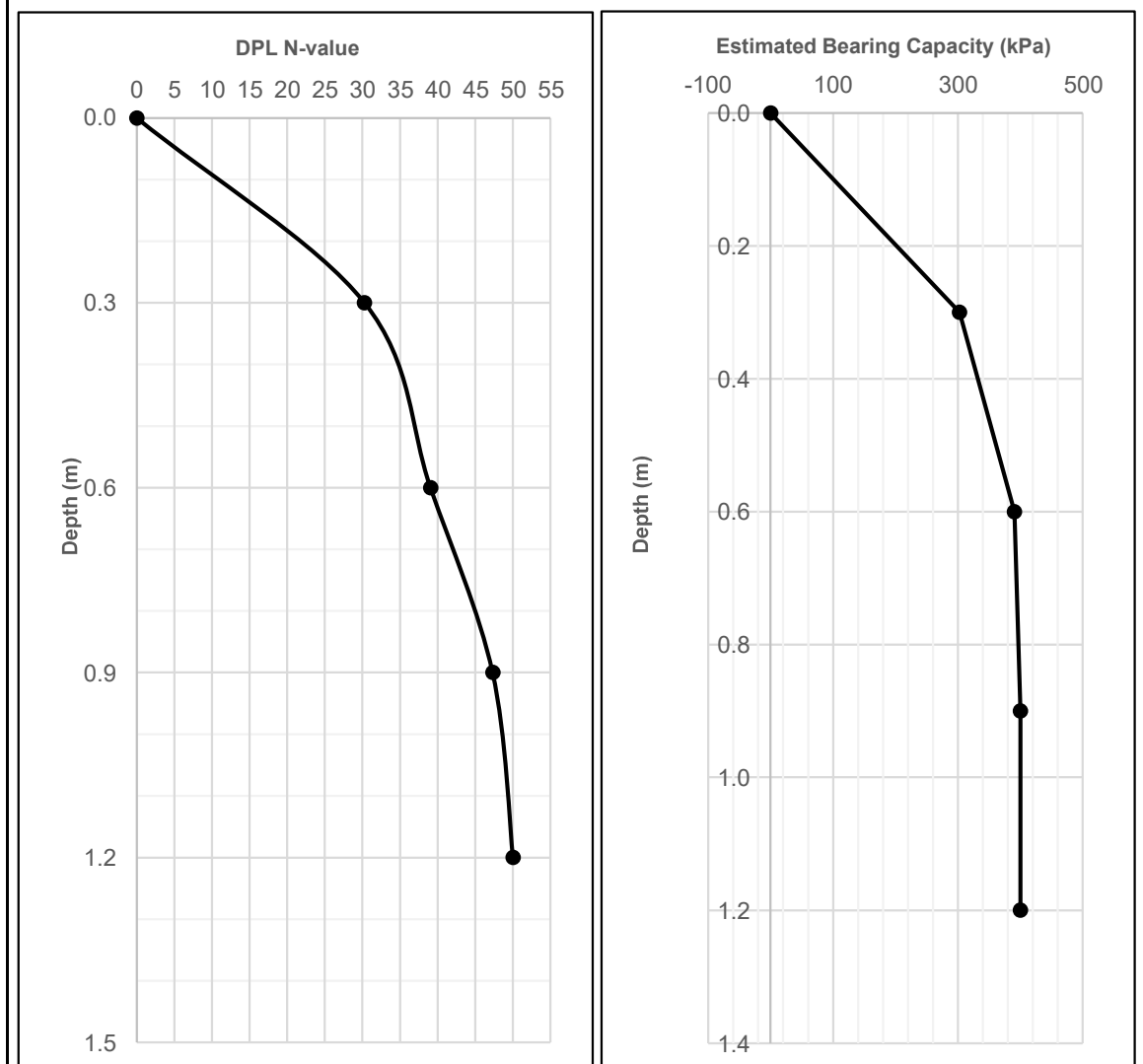


Figure 23: Orangey red transported material encountered in TP27, TP31, TP32 and TP34

APPENDIX E: DPL TEST RESULTS

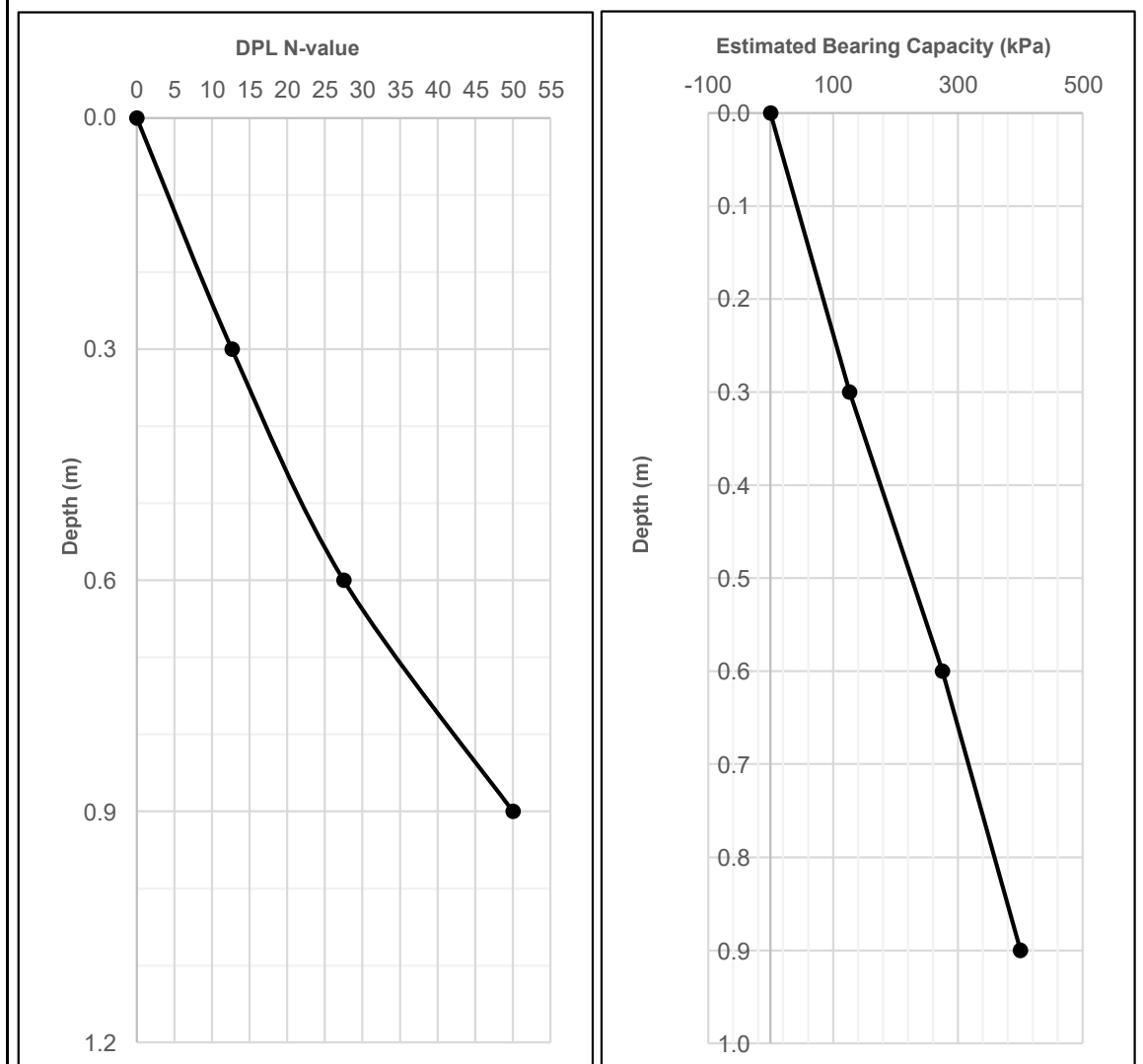


MUKONA
CONSULTING ENGINEERS

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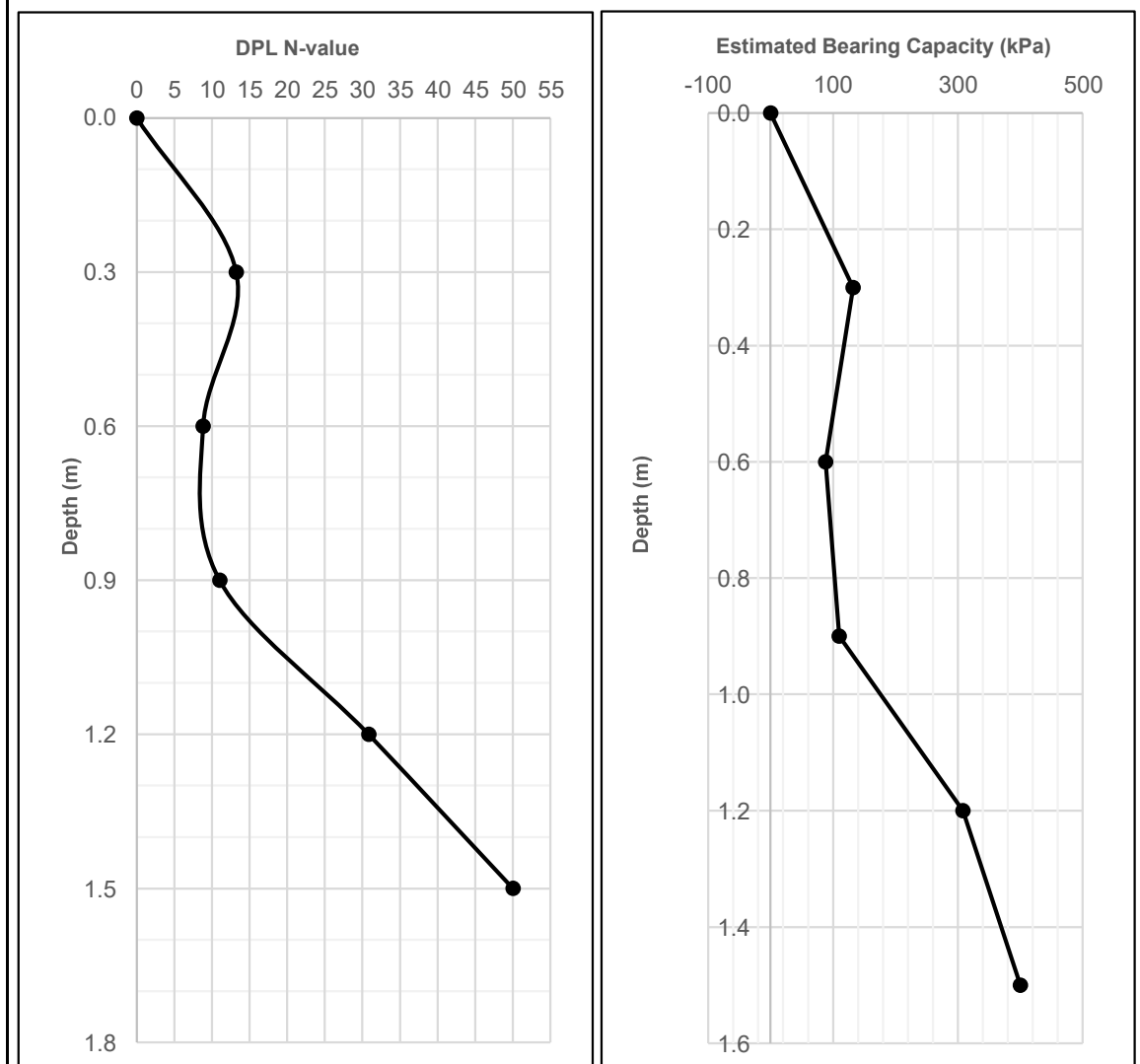


MUKONA
CONSULTING ENGINEERS

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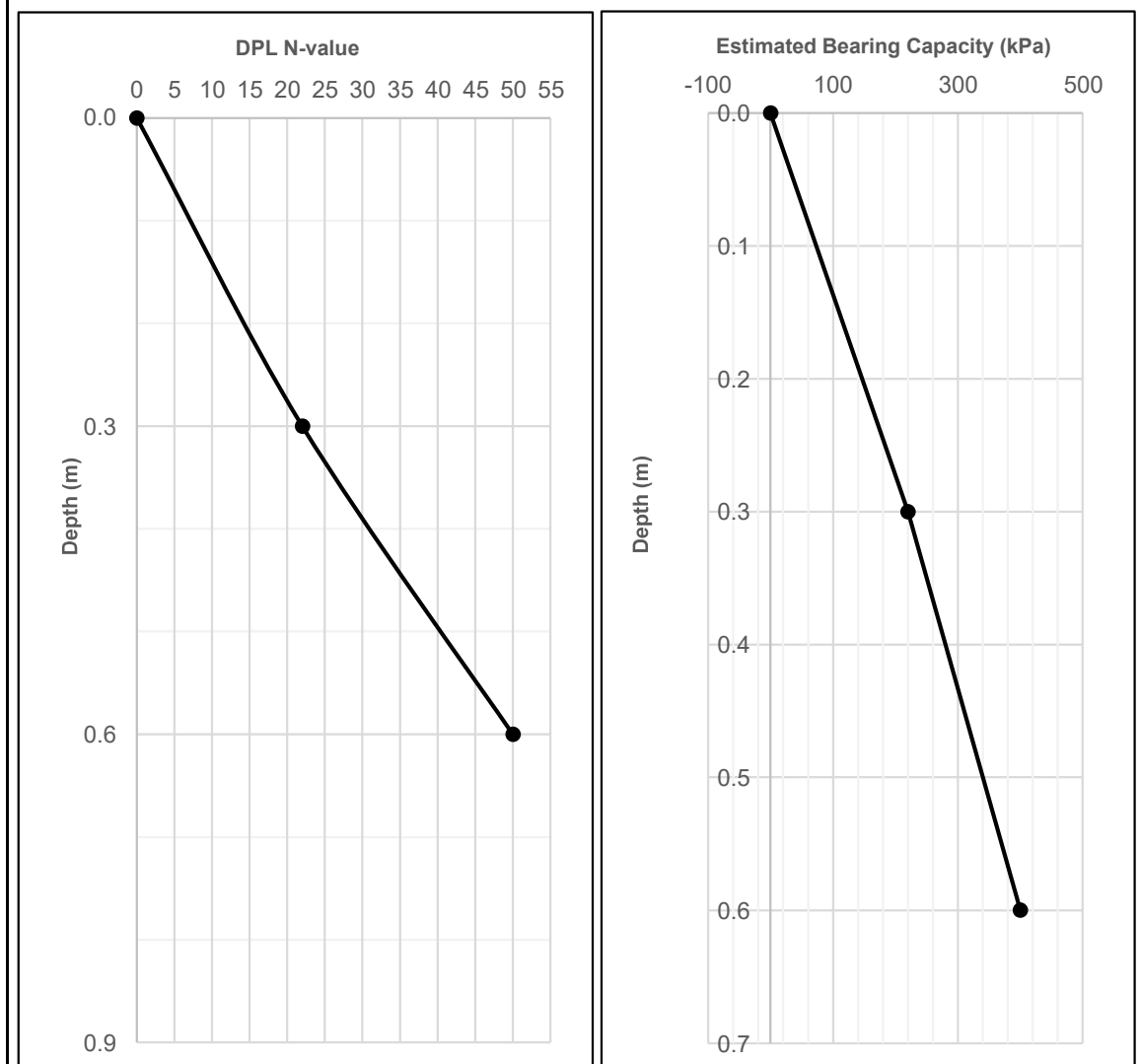


MUKONA
CONSULTING ENGINEERS

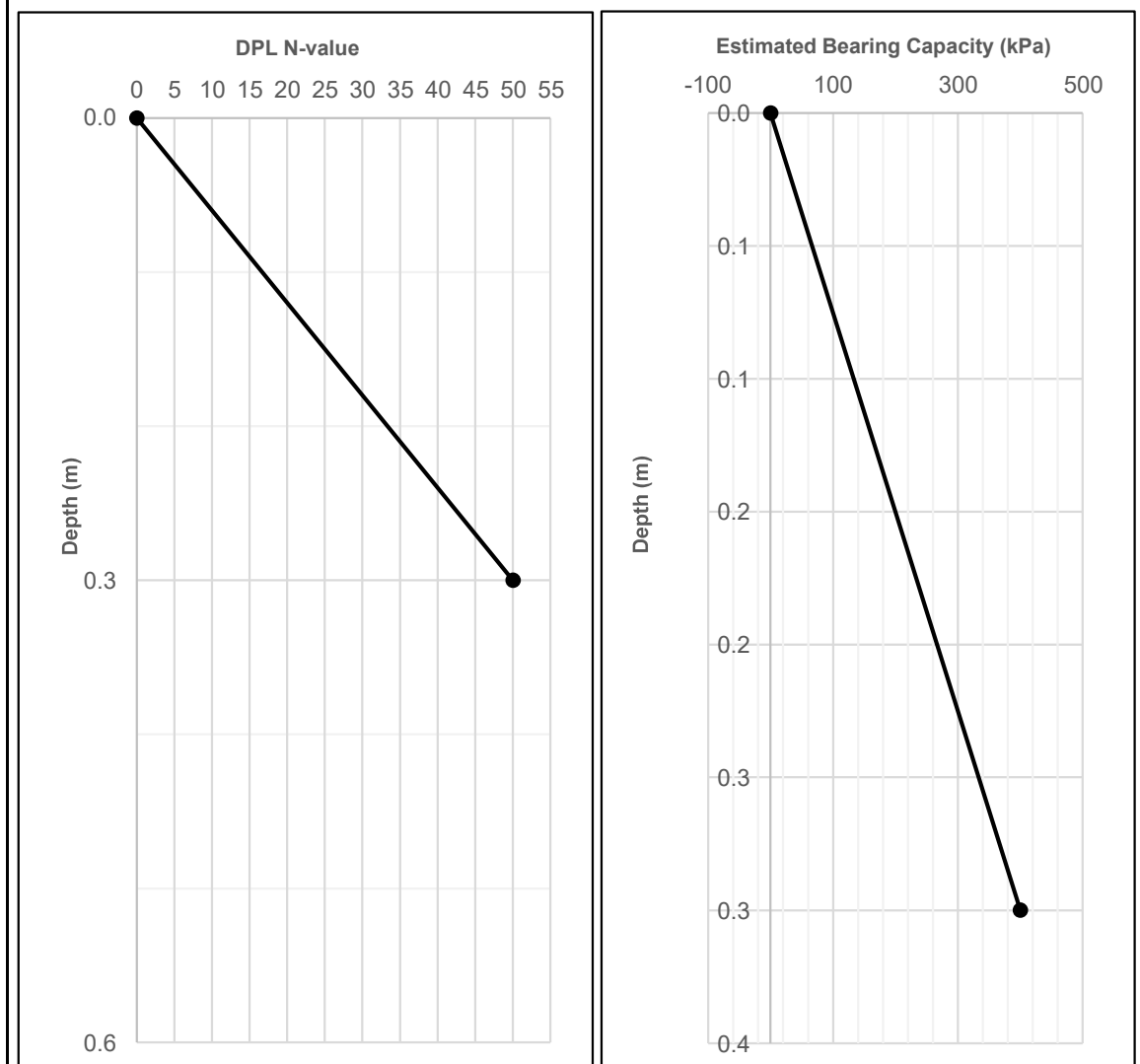
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MUKONA
CONSULTING ENGINEERS

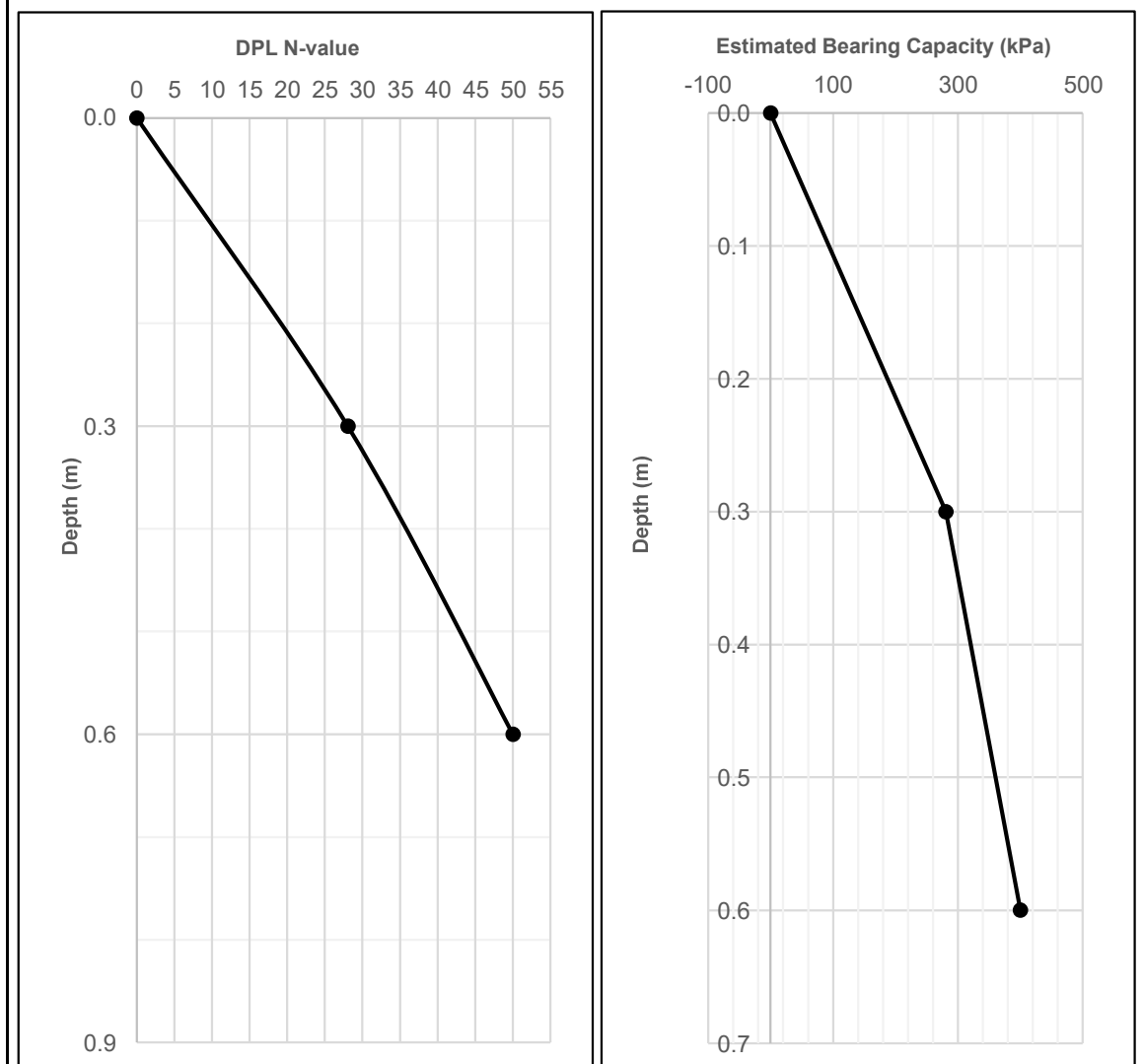
[illegible]

| | |
|----------------------|-------------------------------|
| PROJECT: | Aerorand Township Development |
| LOCATION: | Middelburg Mpumalanga |
| DATE: | 16/11/2018 |
| CONTRACTOR: | Mukona Consulting Engineers |
| DPL No: | DPL08 |
| DPL LOCATION: | Adjacent to TP08 |
| COMPLETED BY: | L Netshilindi |

[illegible]

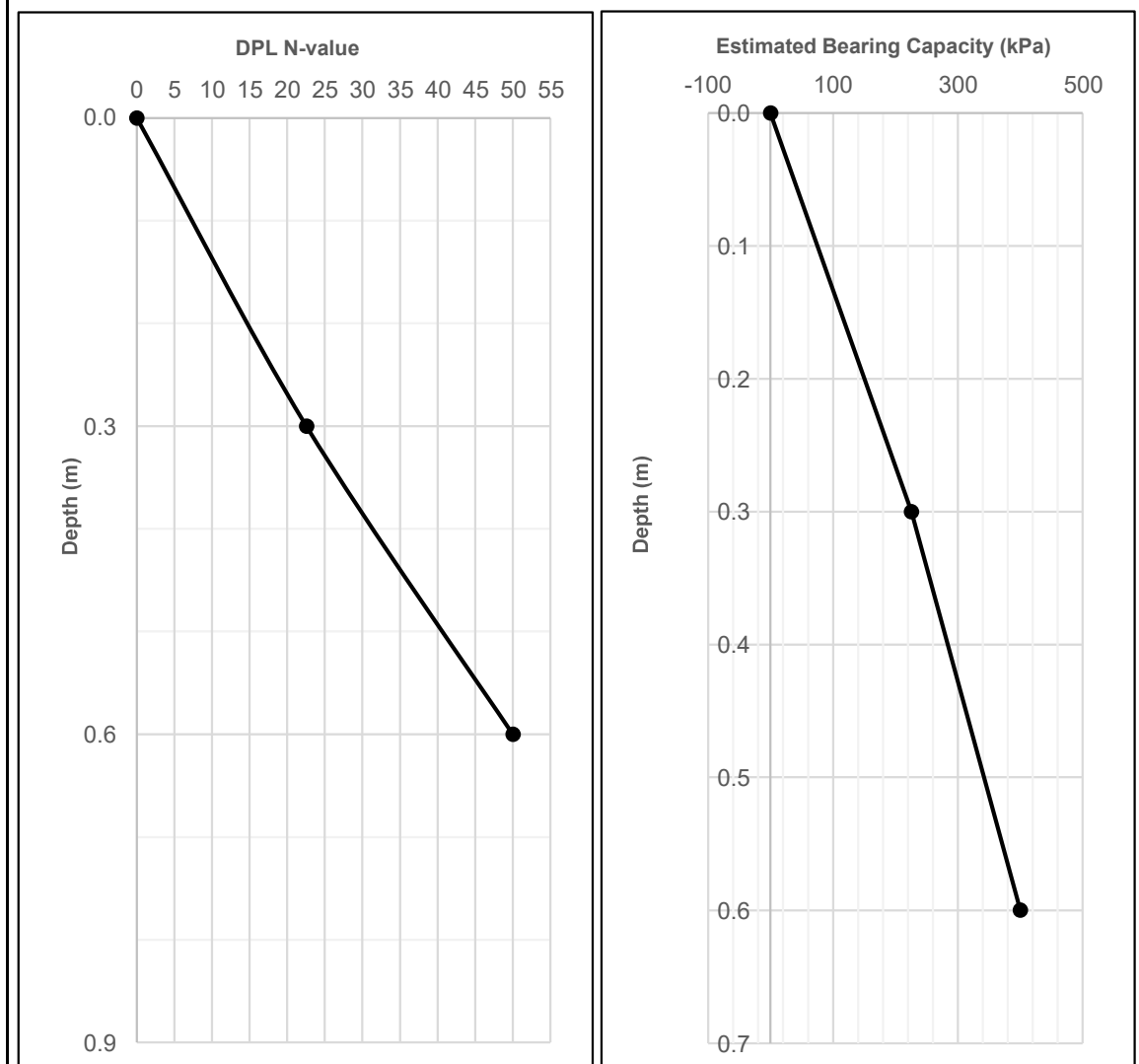


MUKONA
CONSULTING ENGINEERS

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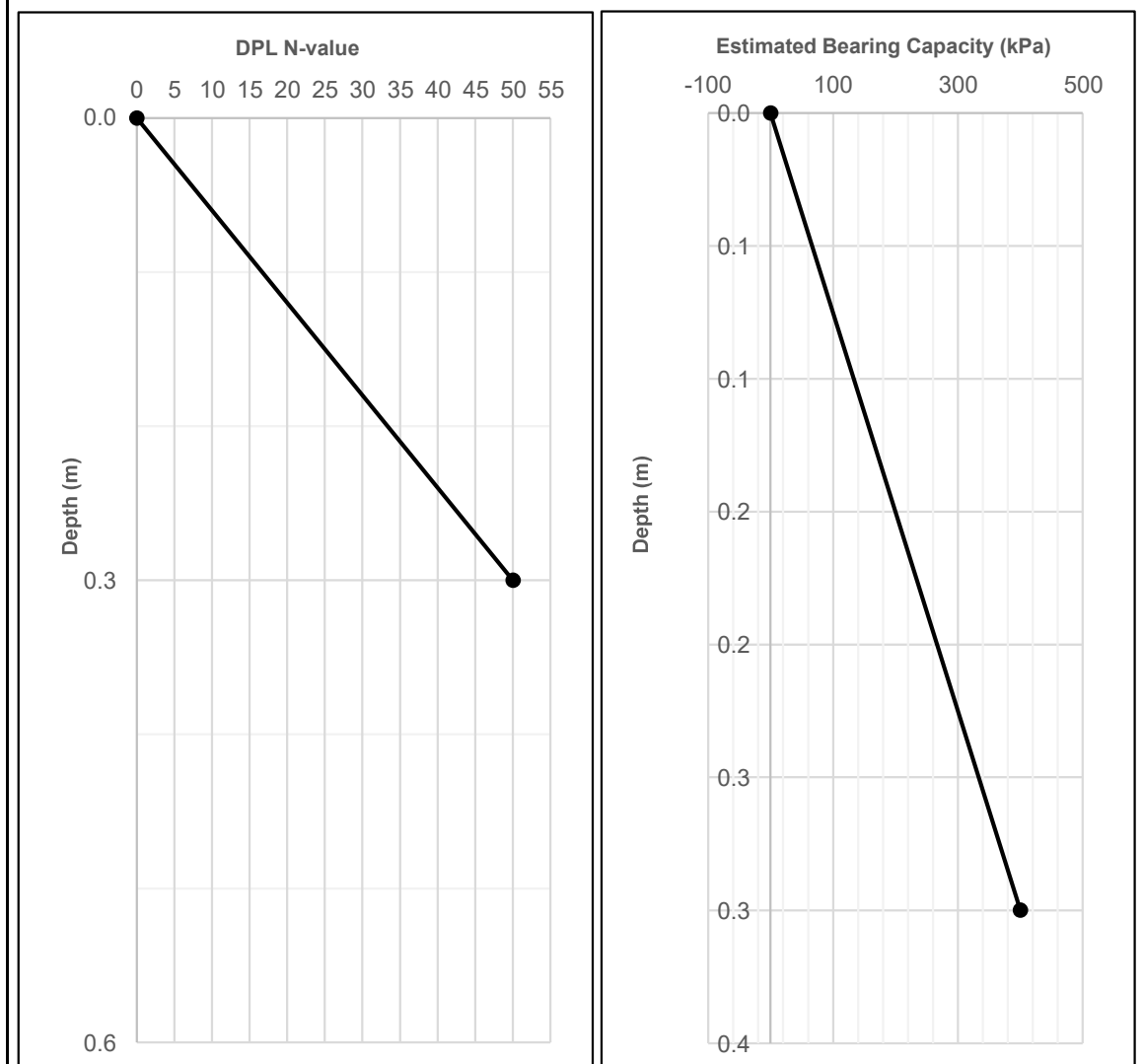


MUKONA
CONSULTING ENGINEERS

[illegible]

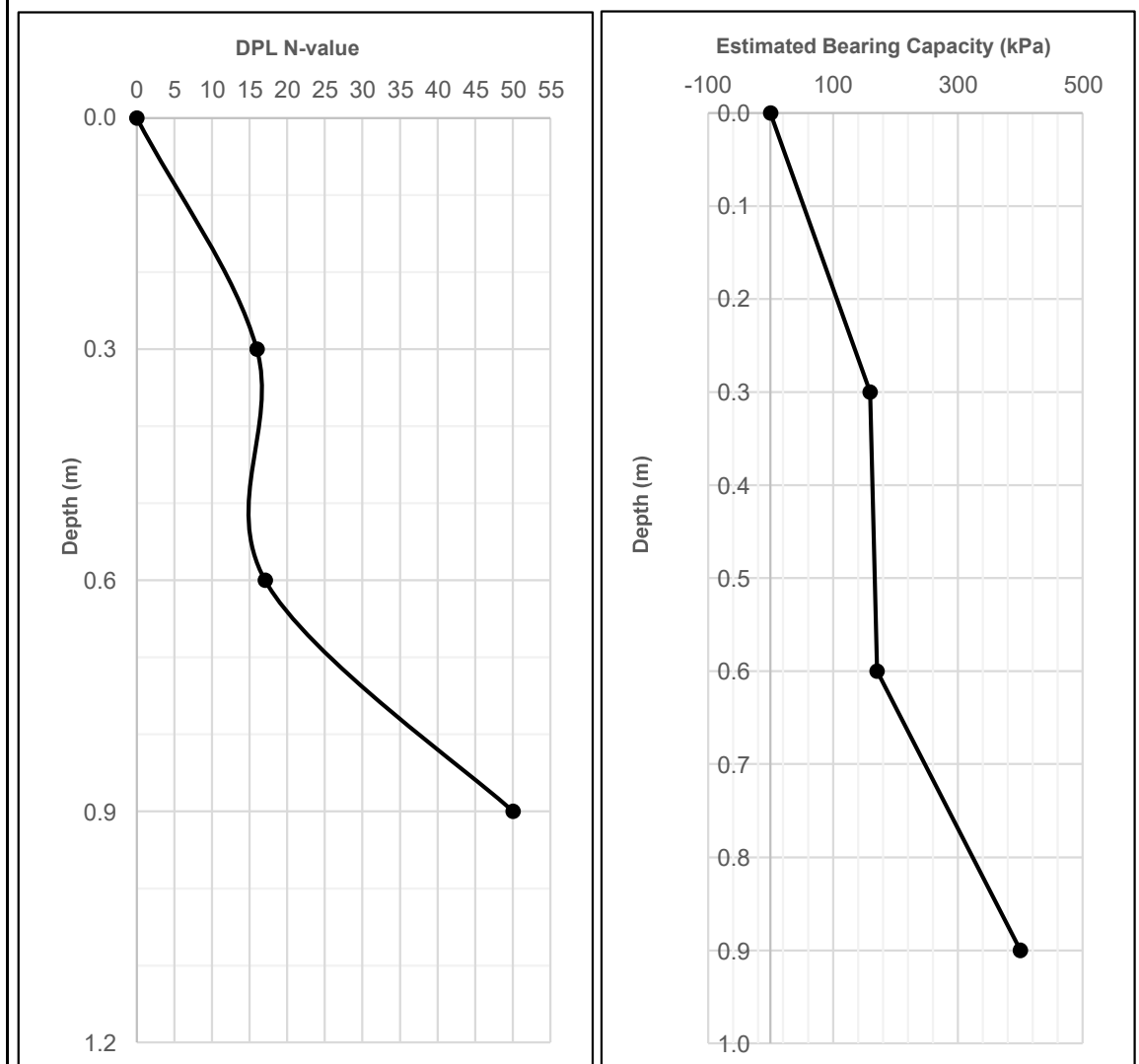


MUKONA
CONSULTING ENGINEERS

[illegible]



MUKONA
CONSULTING ENGINEERS

[illegible]

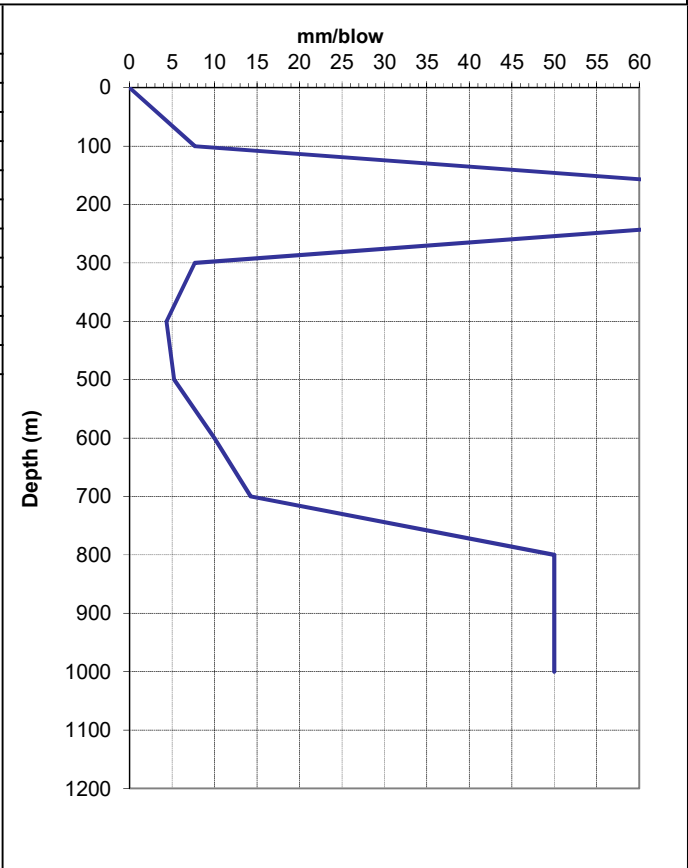
APPENDIX F: DCP FIELD TEST

| | |
|---|----------------------------------|
| Client Location Date tested Job Ref No. Contract No. Operator Final Depth Test No. | Steve Tshwete Local Municipality |
| | Aerorand South |
| | 24/05/2019 |
| | MK/18/480 |
| | |
| | Lutendo Pfuluwani |
| 1000mm | |
| DCP23 | |



DCP PENETROMETER REPORT


| Depth (mm) | blows/ 100mm | mm/blow | Inferred Consistency |
|------------|--------------|---------|----------------------|
| 0 | 0 | 0 | |
| 100 | 13 | 8 | Dense |
| 200 | 1 | 100 | V.Loose |
| 300 | 13 | 8 | Dense |
| 400 | 23 | 4 | V.Dense |
| 500 | 19 | 5 | Dense |
| 600 | 10 | 10 | Dense |
| 700 | 7 | 14 | Med.Dense |
| 800 | 2 | 50 | Loose |
| 900 | 2 | 50 | Loose |
| 1000 | 2 | 50 | Loose |



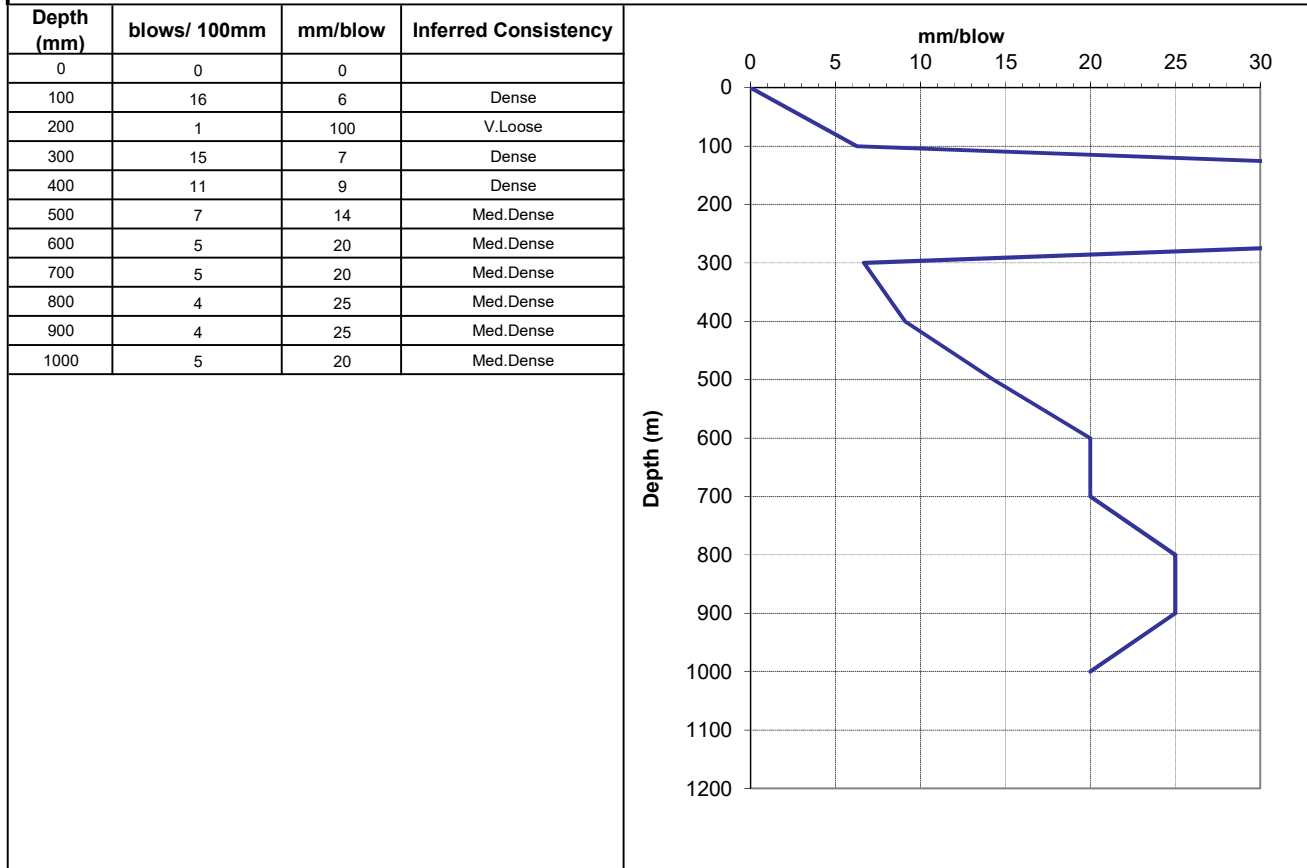
THE STRENGTH AND CBR VALUES ARE EMPIRICAL AND DEPEND ON FACTORS SUCH AS MOISTURE CONTENT WHICH HAVE NOT BEEN DETERMINED. THEY ARE THEREFORE INDICATIVE AND SHOULD BE VERIFIED BY TEST OR OBSERVATION.

Remarks

1 Started from the surface

| | | |
|---|----------------------------------|---|
| Client Location Date tested Job Ref No. Contract No. Operator Final Depth Test No. | Steve Tshwete Local Municipality |  |
| | Aerorand South | |
| | 24/05/2019 | |
| | MK/18/480 | |
| | | |
| | Lutendo Pfuluwani | |
| 1000mm | | |
| DCP27 | | |

DCP PENETROMETER REPORT




THE STRENGTH AND CBR VALUES ARE EMPIRICAL AND DEPEND ON FACTORS SUCH AS MOISTURE CONTENT WHICH HAVE NOT BEEN DETERMINED. THEY ARE THEREFORE INDICATIVE AND SHOULD BE VERIFIED BY TEST OR OBSERVATION.

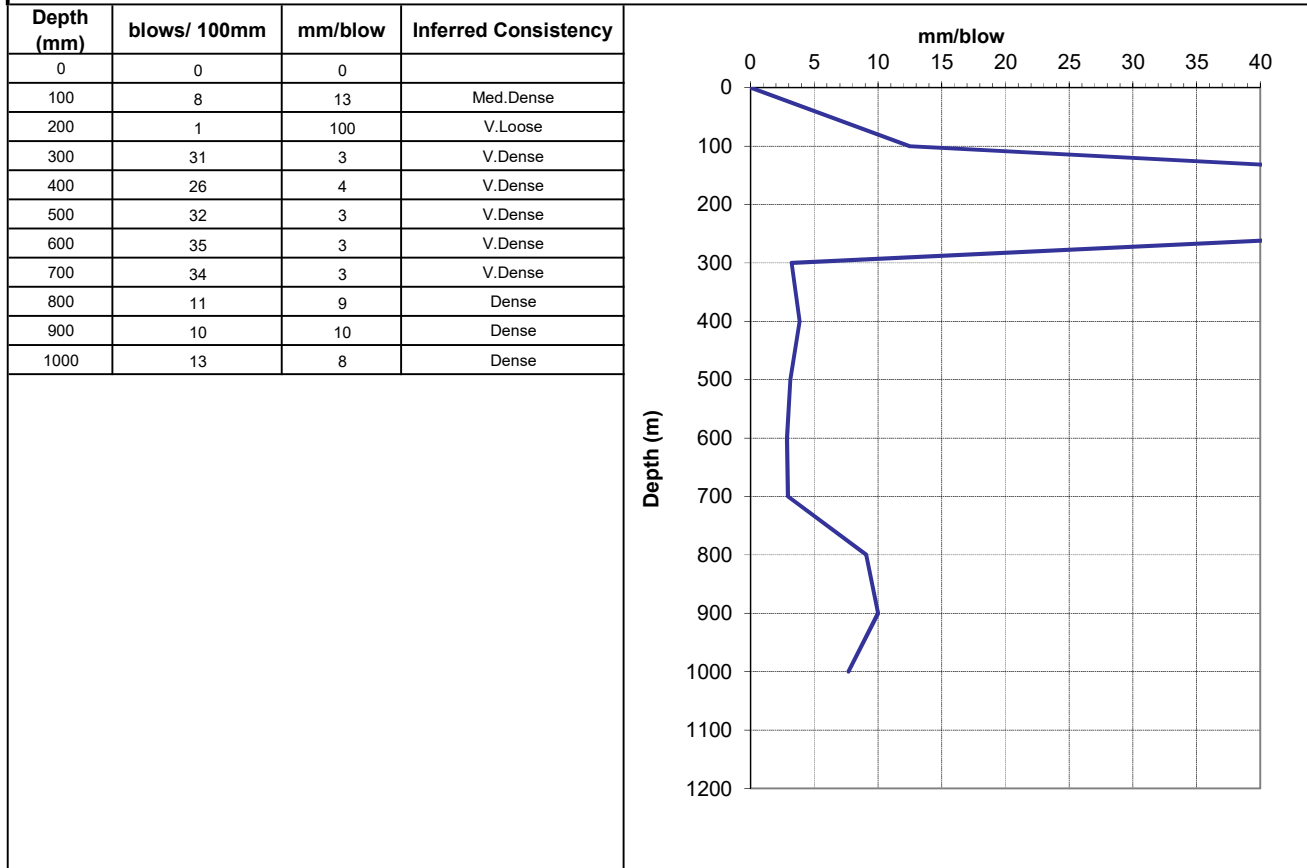
Remarks

1

Started from the surface


| | | |
|---|----------------------------------|---|
| Client Location Date tested Job Ref No. Contract No. Operator Final Depth Test No. | Steve Tshwete Local Municipality |  |
| | Aerorand South | |
| | 24/05/2019 | |
| | MK/18/480 | |
| | Lutendo Pfuluwani | |
| | 1000mm | |
| | DCP28 | |

DCP PENETROMETER REPORT

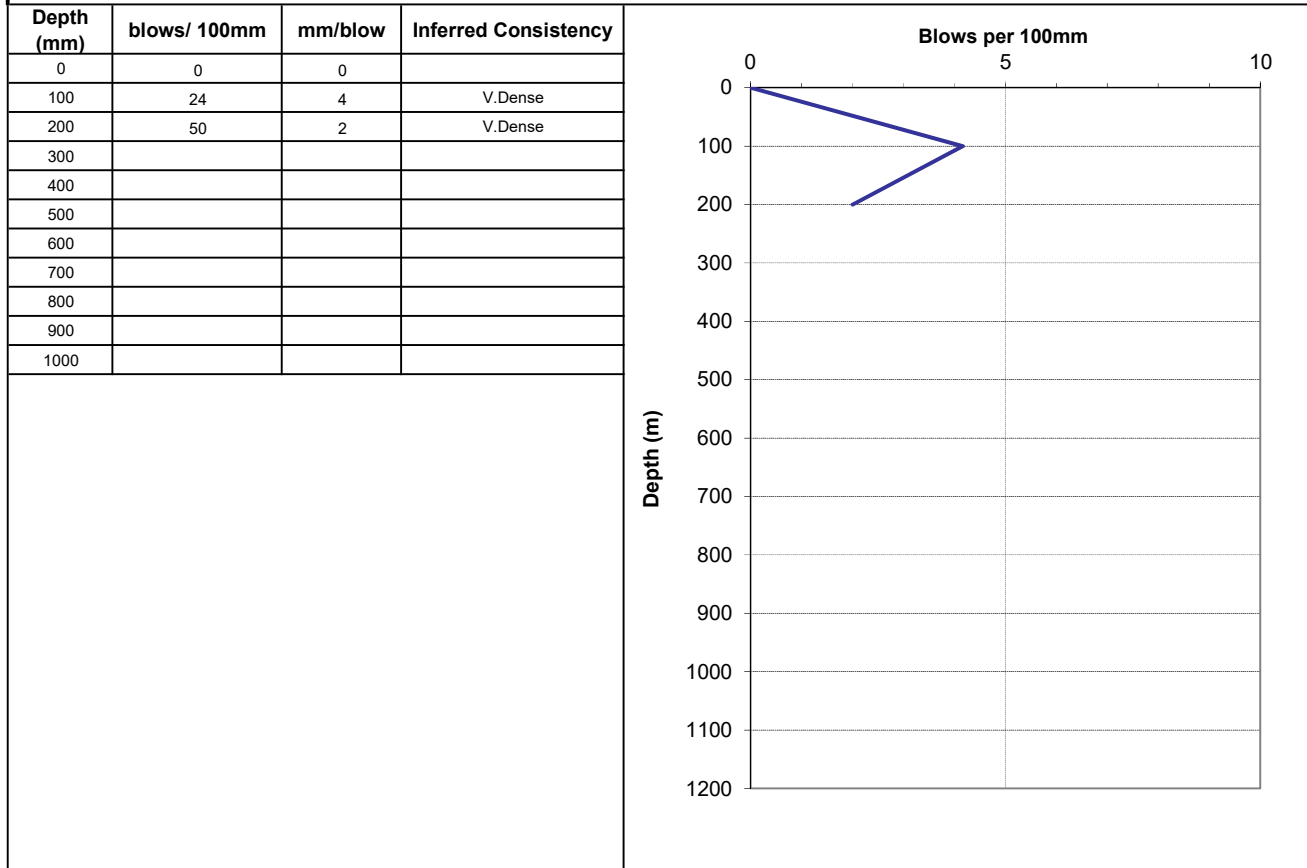


THE STRENGTH AND CBR VALUES ARE EMPIRICAL AND DEPEND ON FACTORS SUCH AS MOISTURE CONTENT WHICH HAVE NOT BEEN DETERMINED. THEY ARE THEREFORE INDICATIVE AND SHOULD BE VERIFIED BY TEST OR OBSERVATION.

| Remarks | |
|---------|--------------------------|
| 1 | Started from the surface |

| | | |
|---|----------------------------------|---|
| Client Location Date tested Job Ref No. Contract No. Operator Final Depth Test No. | Steve Tshwete Local Municipality |  |
| | Aerorand South | |
| | 24/05/2019 | |
| | MK/18/480 | |
| | Lutendo Pfuluwani | |
| | 1000mm | |
| | DCP29 | |


DCP PENETROMETER REPORT



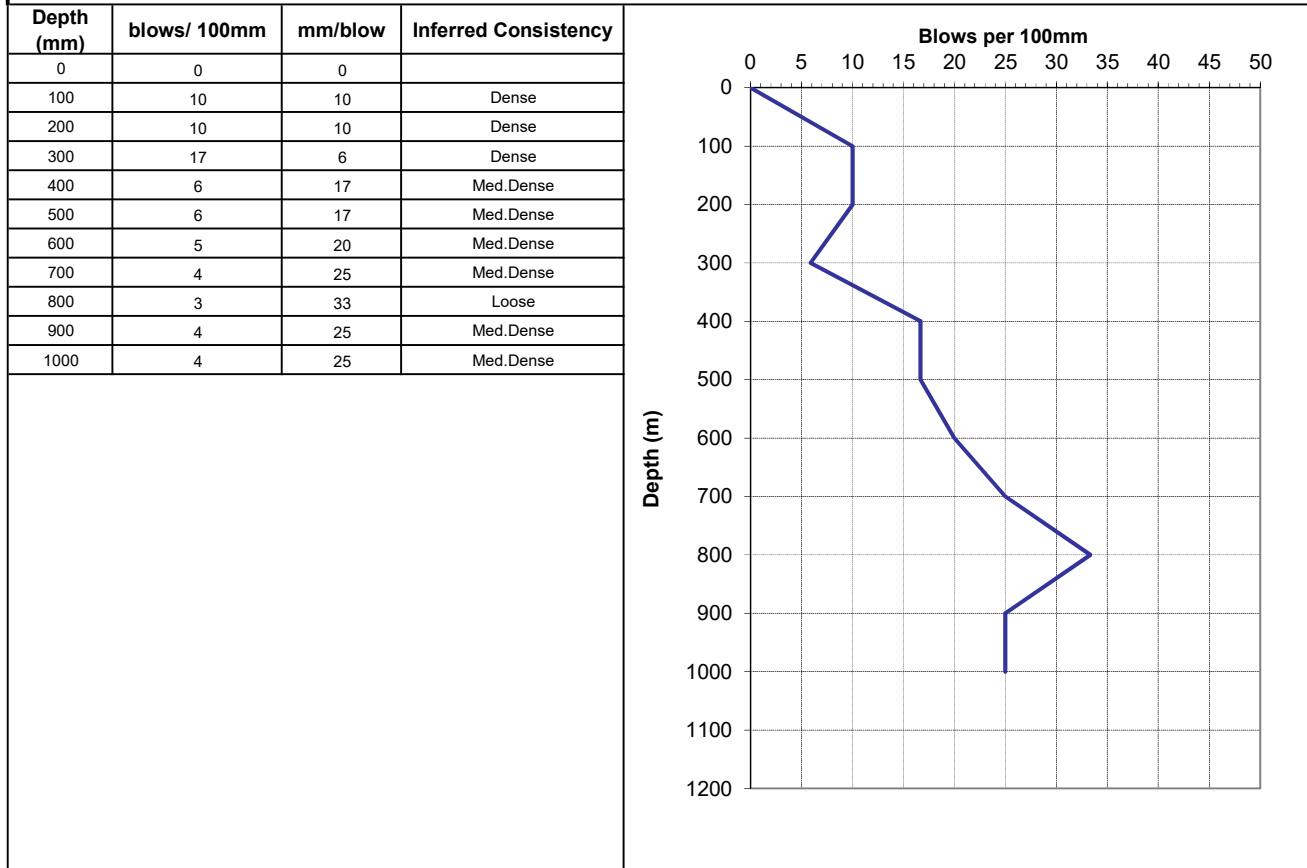
THE STRENGTH AND CBR VALUES ARE EMPIRICAL AND DEPEND ON FACTORS SUCH AS MOISTURE CONTENT WHICH HAVE NOT BEEN DETERMINED. THEY ARE THEREFORE INDICATIVE AND SHOULD BE VERIFIED BY TEST OR OBSERVATION.

Remarks

1 Started from the surface


| | | |
|---|----------------------------------|---|
| Client Location Date tested Job Ref No. Contract No. Operator Final Depth Test No. | Steve Tshwete Local Municipality |  |
| | Aerorand South | |
| | 24/05/2019 | |
| | MK/18/480 | |
| | | |
| | Lutendo Pfuluwani | |
| 1000mm | | |
| DCP32 | | |

DCP PENETROMETER REPORT

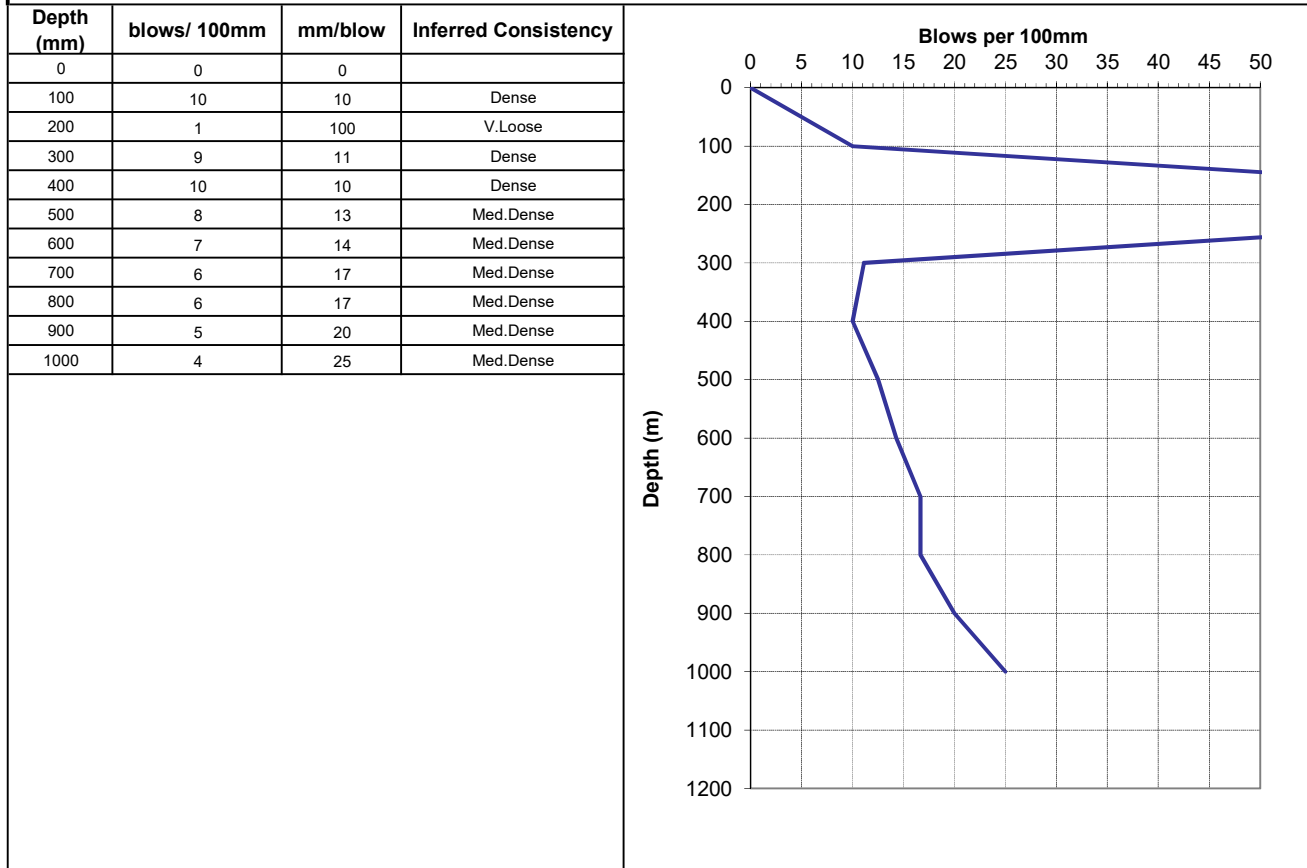


THE STRENGTH AND CBR VALUES ARE EMPIRICAL AND DEPEND ON FACTORS SUCH AS MOISTURE CONTENT WHICH HAVE NOT BEEN DETERMINED. THEY ARE THEREFORE INDICATIVE AND SHOULD BE VERIFIED BY TEST OR OBSERVATION.

| Remarks | |
|---------|--------------------------|
| 1 | Started from the surface |

| | | |
|---|----------------------------------|---|
| Client Location Date tested Job Ref No. Contract No. Operator Final Depth Test No. | Steve Tshwete Local Municipality |  |
| | Aerorand South | |
| | 24/05/2019 | |
| | MK/18/480 | |
| | | |
| | Lutendo Pfuluwani | |
| 1000mm | | |
| DCP34 | | |

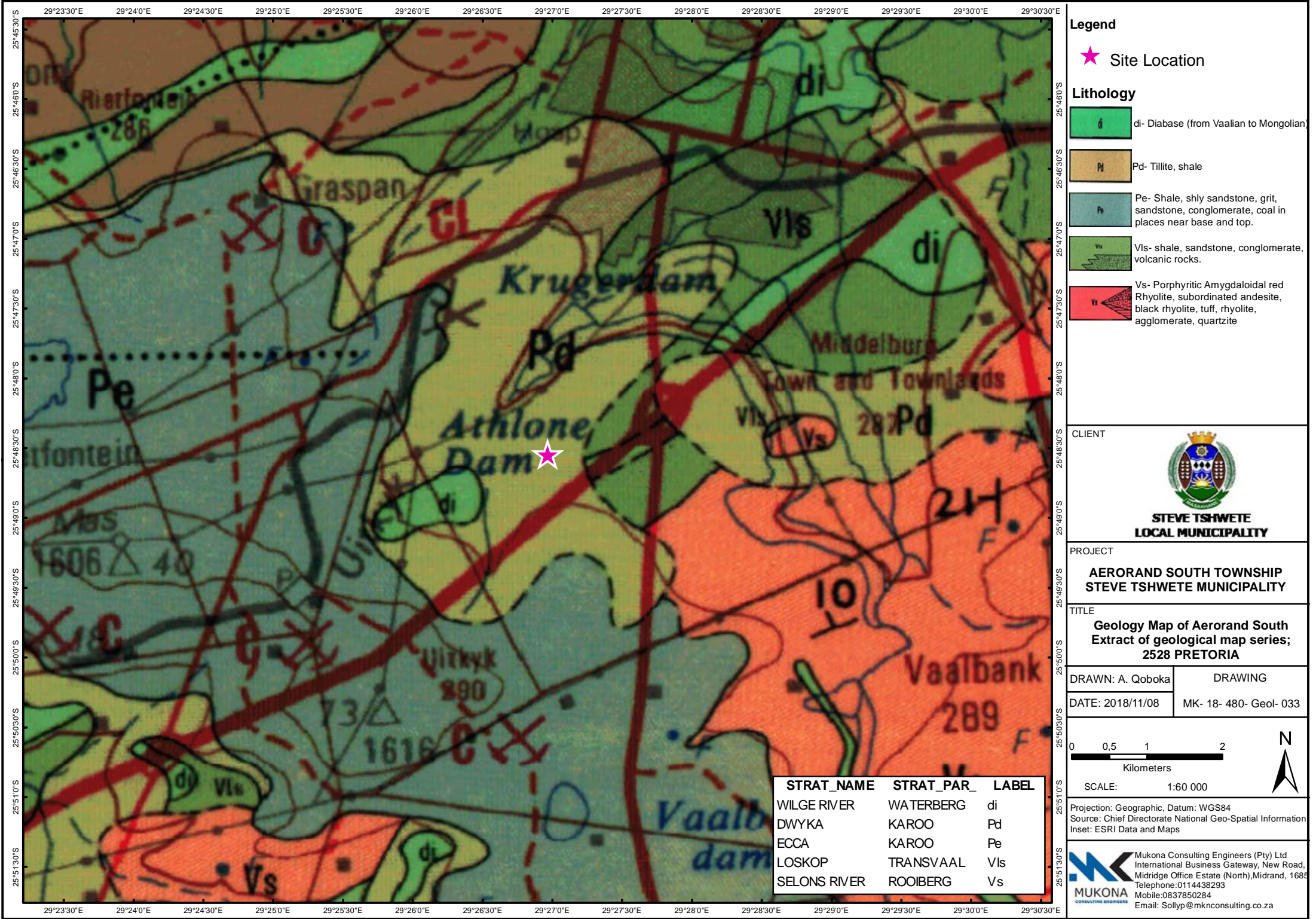
DCP PENETROMETER REPORT



THE STRENGTH AND CBR VALUES ARE EMPIRICAL AND DEPEND ON FACTORS SUCH AS MOISTURE CONTENT WHICH HAVE NOT BEEN DETERMINED. THEY ARE THEREFORE INDICATIVE AND SHOULD BE VERIFIED BY TEST OR OBSERVATION.

| Remarks | |
|---------|--------------------------|
| 1 | Started from the surface |

APPENDIX G: GEOLOGICAL MAP



Legend

Site Location

Lithology

di- Diabase (from Vaalian to Mongolian)

Pd- Tillite, shale

Pe- Shale, shly sandstone, grit, sandstone, conglomerate, coal in places near base and top.

Vls- shale, sandstone, conglomerate, volcanic rocks.

Vs- Porphyrritic Amygdaloidal red Rhyolite, subordinated andesite, black rhyolite, tuff, rhyolite, agglomerate, quartzite

CLIENT

STEVE TSHWETE
LOCAL MUNICIPALITY

PROJECT

AERORAND SOUTH TOWNSHIP
STEVE TSHWETE MUNICIPALITY

TITLE

Geology Map of Aerorand South
Extract of geological map series;
2528 PRETORIA

DRAWN: A. Qoboka

DRAWING

DATE: 2018/11/08

MK- 18- 480- Geol- 033

00.512

Kilometers

SCALE: 1:60 000

Projection: Geographic, Datum: WGS84
Source: Chief Directorate National Geo-Spatial Information
Inset: ESRI Data and Maps

Mukona Consulting Engineers (Pty) Ltd
International Business Gateway, New Road,
Midridge Office Estate (North), Midrand, 1685
Telephone: 011 443 8293
Mobile: 083 785 0284
Email: Sollyp@mknconsulting.co.za

| STRAT_NAME | STRAT_PAR | LABEL |
|--------------|-----------|-------|
| WILGE RIVER | WATERBERG | di |
| DWYKA | KAROO | Pd |
| ECCA | KAROO | Pe |
| LOSKOP | TRANSVAAL | Vls |
| SELONS RIVER | ROOIBERG | Vs |

APPENDIX H: LABORATORY RESULTS

- APPENDIX H1: FOUNDATION INDICATOR
- APPENDIX H2: MOISTURE / DENSITY & CBR
- APPENDIX H3: CHEMICAL (pH and Conductivity))

APPENDIX H1: FOUNDATION INDICATOR TEST RESULTS



(PTY) LTD
Registration Number
1971/000112/07



Tel: (+27) (12) 813 4900
Email: info@soillab.co.za

Engineering Materials Laboratory

SMEC Building, 230 Albertus Street
La Montagne, Pretoria, 0184
PO Box 72928, Lynnwood Ridge,
South Africa, 0040

Client: MUKONA CONSULTING ENGINEERS (PTY) LTD

Project: AERORAND SOUTH GEOTECH - MK-18-480

Project No.: S18-2207

Date: 2018/12/10

MOISTURE CONTENT - SANS 3001-GR20

| Sample No.: | Description: | Moisture Content (%) |
|-------------|--------------|----------------------|
| S18-2207-01 | 0.45 - 1.7 | 9.5 |
| S18-2207-02 | 0.9 - 2.5 | 10.1 |
| S18-2207-03 | 0.5 - 2.5 | 3.3 |
| S18-2207-05 | 0.7 - 2.5 | 7.2 |
| S18-2207-08 | 1.6 - 2.1 | 13.1 |
| S18-2207-09 | 0.39 - 1.3 | 2.7 |
| S18-2207-10 | 1.3 - 2.5 | 8.0 |
| S18-2207-12 | 0.4 - 0.7 | 3.5 |
| S18-2207-13 | 0.7 - 0.9 | 3.7 |
| | | |

Note: Items marked with a star (*) is Not Accredited

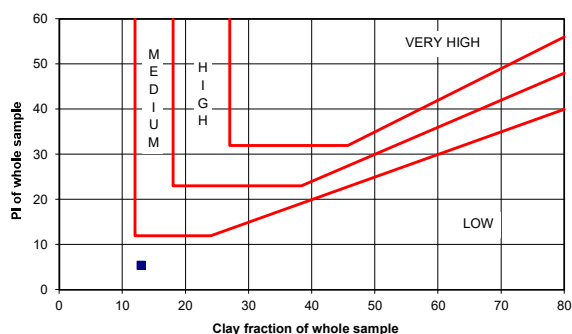
Soillab is a SANAS accredited Testing Laboratory according to the Accreditation Scope

PARTICLE SIZE ANALYSIS

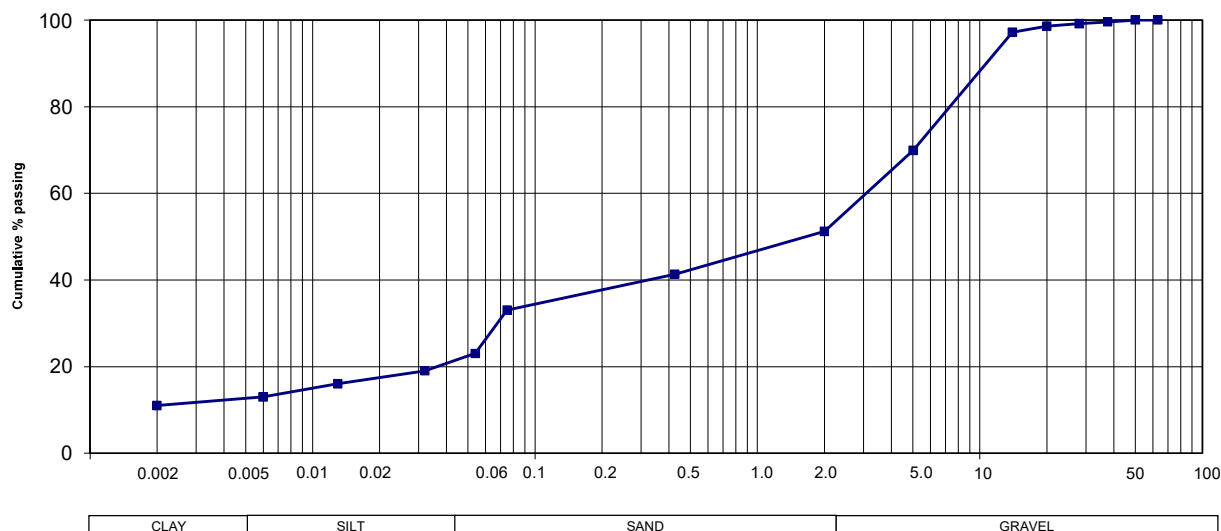
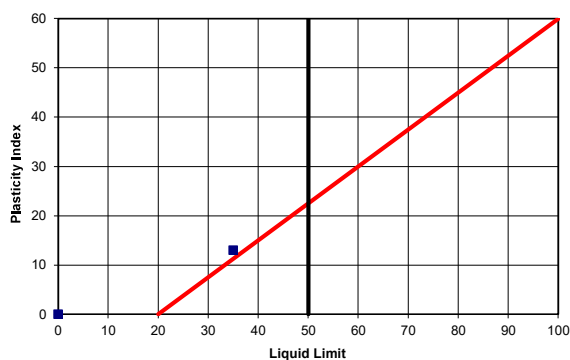
| | |
|---|---|
| Sample No. | 1 |
| Soillab Sample No. | S18-2207-01 |
| Depth (m) | 0.45 - 1.7 |
| Position | TP 01 |
| Material Description | DARK YELLOWISH ORANGE SHALE & FERRICRETE SANDY GRAVEL |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 99 |
| 20.0 mm | 99 |
| 14.0 mm | 97 |
| 5.0 mm | 70 |
| 2.00 mm | 51 |
| 0.425 mm | 41 |
| 0.075 mm | 33 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 54 µm | 23 |
| 32 µm | 19 |
| 13 µm | 16 |
| 6 µm | 13 |
| 2 µm | 11 |
| % Clay | 13 |
| % Silt | 10 |
| % Sand | 28 |
| % Gravel | 49 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 35 |
| Plasticity Index | 13 |
| Linear Shrinkage (%) | 6.5 |
| Grading Modulus | 1.74 |
| Classification | A-2-6 (1) |
| Unified Classification | SC |
| Chart Reference | |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
 JOB No. : S18-2207
 DATE : 2018-12-10


POTENTIAL EXPANSIVENESS



PLASTICITY CHART

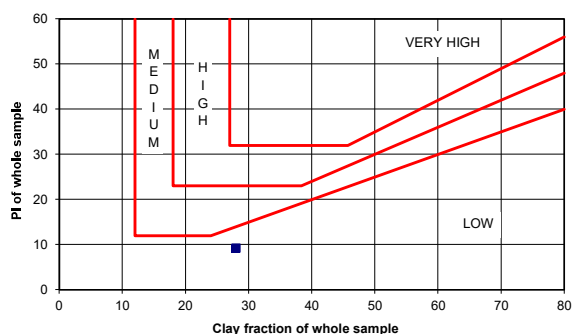


PARTICLE SIZE ANALYSIS

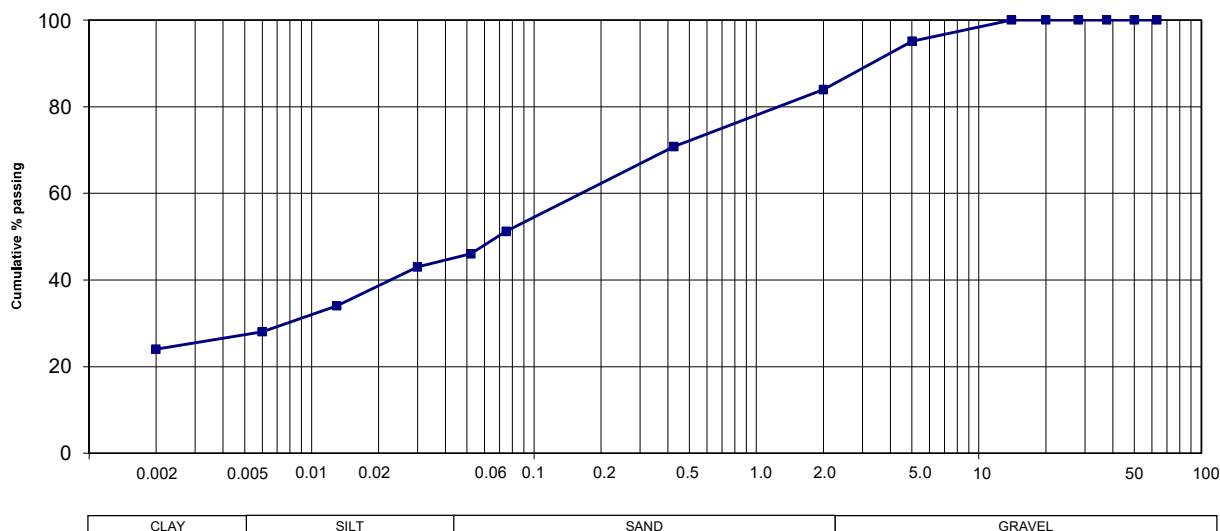
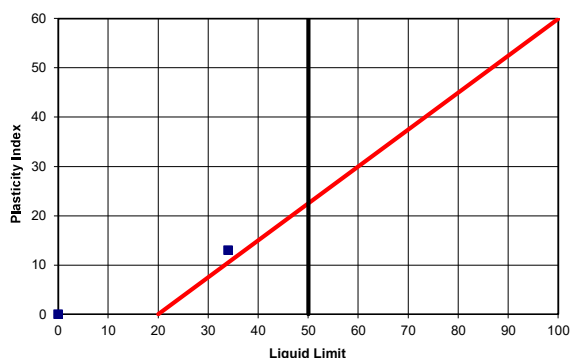
| | |
|---|---|
| Sample No. | 2 |
| Soillab Sample No. | S18-2207-02 |
| Depth (m) | 0.9 - 2.5 |
| Position | TP 02 |
| Material Description | PALE RED SHALE & FERRICRETE CLAYEY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 100 |
| 5.0 mm | 95 |
| 2.00 mm | 84 |
| 0.425 mm | 71 |
| 0.075 mm | 51 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 52 µm | 46 |
| 30 µm | 43 |
| 13 µm | 34 |
| 6 µm | 28 |
| 2 µm | 24 |
| | |
| % Clay | 28 |
| % Silt | 18 |
| % Sand | 38 |
| % Gravel | 16 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 34 |
| Plasticity Index | 13 |
| Linear Shrinkage (%) | 6.5 |
| Grading Modulus | 0.94 |
| Classification | A-6 (4) |
| Unified Classification | CL |
| Chart Reference |  |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
 JOB No. : S18-2207
 DATE : 2018-12-10

POTENTIAL EXPANSIVENESS



PLASTICITY CHART

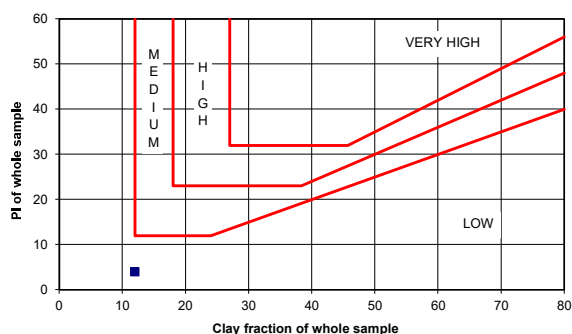


PARTICLE SIZE ANALYSIS

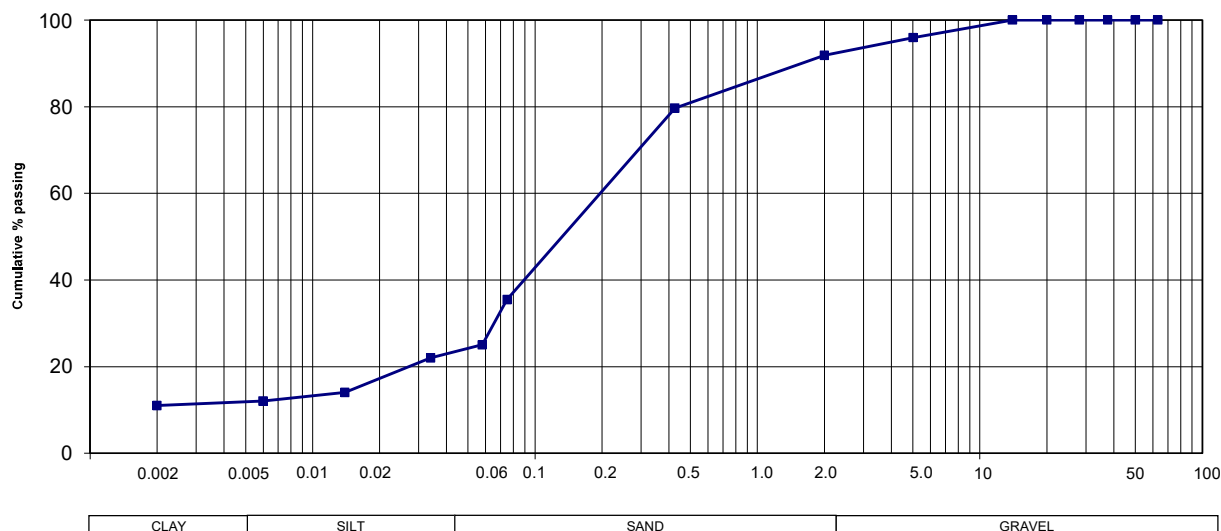
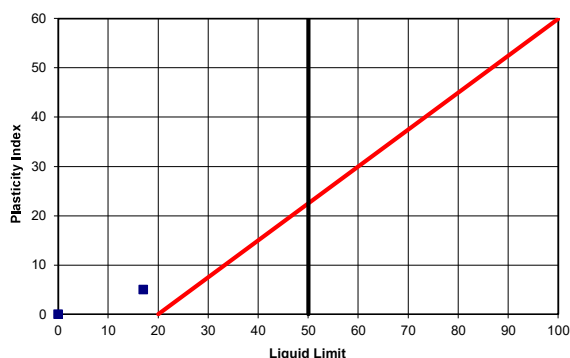
| | |
|---|--|
| Sample No. | 3 |
| Soillab Sample No. | S18-2207-03 |
| Depth (m) | 0.5 - 2.5 |
| Position | TP 11 |
| Material Description | DARK YELLOWISH ORANGE SILTY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 100 |
| 5.0 mm | 96 |
| 2.00 mm | 92 |
| 0.425 mm | 80 |
| 0.075 mm | 35 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 58 µm | 25 |
| 34 µm | 22 |
| 14 µm | 14 |
| 6 µm | 12 |
| 2 µm | 11 |
| | |
| % Clay | 12 |
| % Silt | 13 |
| % Sand | 67 |
| % Gravel | 8 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 17 |
| Plasticity Index | 5 |
| Linear Shrinkage (%) | 1.5 |
| Grading Modulus | 0.93 |
| Classification | A-2-4 (0) |
| Unified Classification | SM & SC |
| Chart Reference | |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
 JOB No. : S18-2207
 DATE : 2018-12-10


POTENTIAL EXPANSIVENESS



PLASTICITY CHART

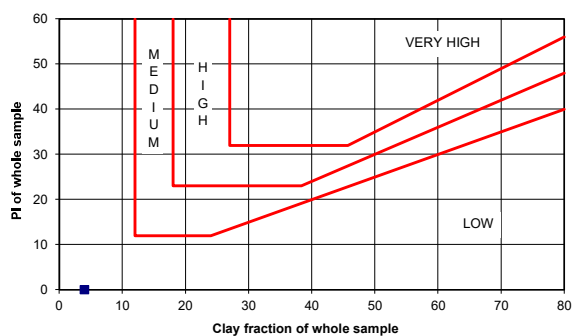


PARTICLE SIZE ANALYSIS

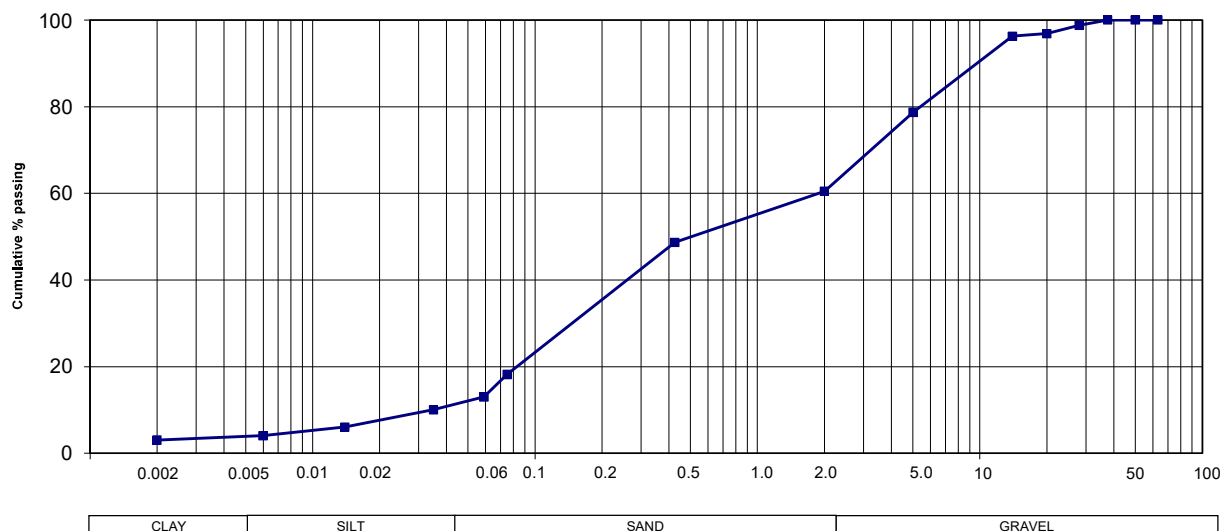
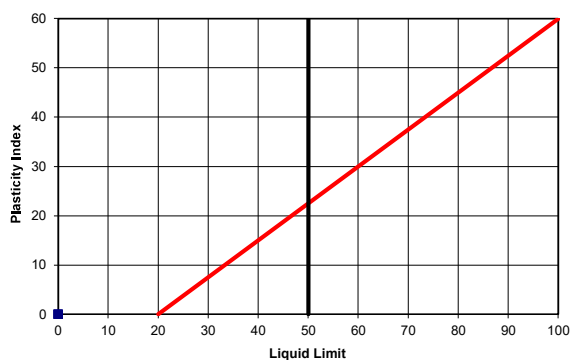
| | |
|---|---|
| Sample No. | 4 |
| Soillab Sample No. | S18-2207-04 |
| Depth (m) | 0.3 - 0.9 |
| Position | TP 12 |
| Material Description | DARK YELLOWISH ORANGE FERRICRETE GRAVELLY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 99 |
| 20.0 mm | 97 |
| 14.0 mm | 96 |
| 5.0 mm | 79 |
| 2.00 mm | 60 |
| 0.425 mm | 49 |
| 0.075 mm | 18 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 59 µm | 13 |
| 35 µm | 10 |
| 14 µm | 6 |
| 6 µm | 4 |
| 2 µm | 3 |
| | |
| % Clay | 4 |
| % Silt | 9 |
| % Sand | 47 |
| % Gravel | 40 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | |
| Plasticity Index | NP |
| Linear Shrinkage (%) | 0.0 |
| Grading Modulus | 1.73 |
| Classification | A-1-b (0) |
| Unified Classification | SM |
| Chart Reference |  |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
 JOB No. : S18-2207
 DATE : 2018-12-10


POTENTIAL EXPANSIVENESS



PLASTICITY CHART

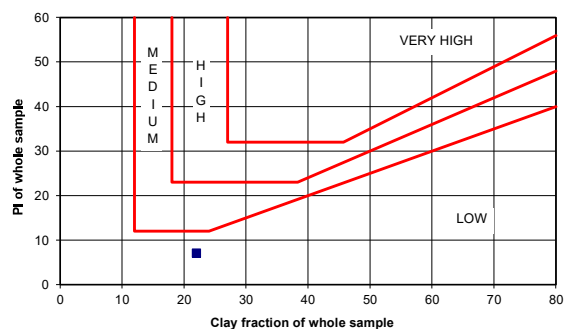


PARTICLE SIZE ANALYSIS

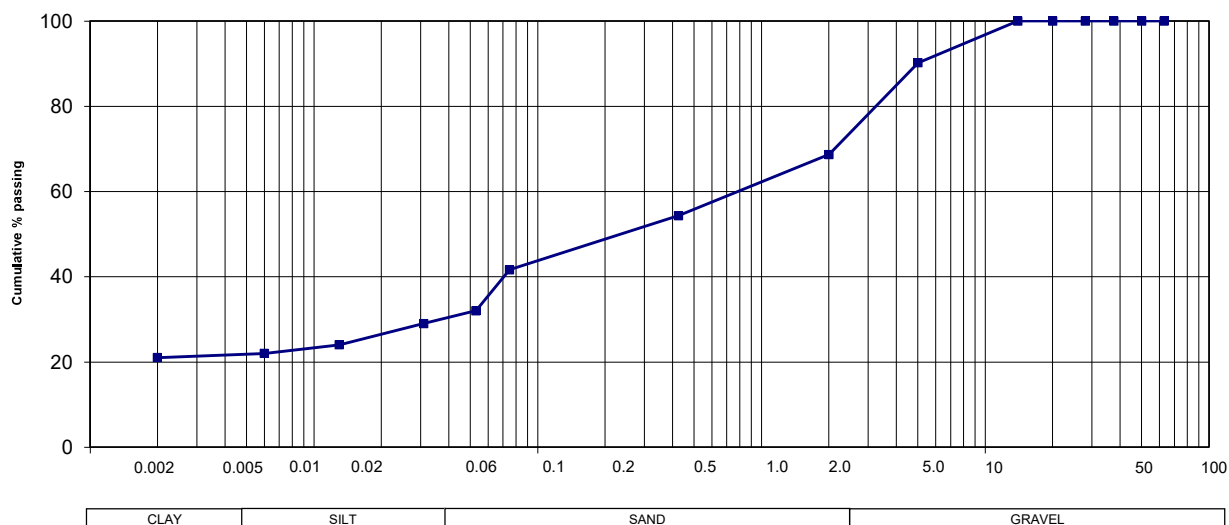
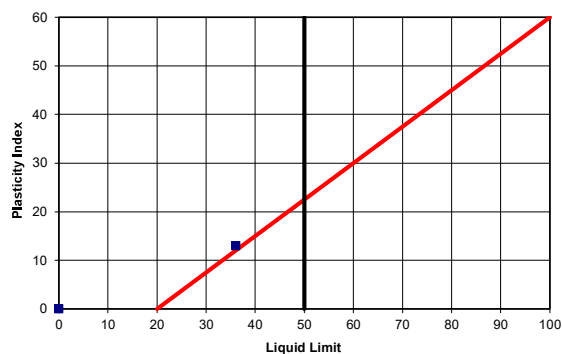
| | |
|---|---|
| Sample No. | 5 |
| Soillab Sample No. | S18-2207-05 |
| Depth (m) | 0.7 - 2.5 |
| Position | TP 13 |
| Material Description | LIGHT RED FERRICRETE & QUARTZITE GRAVELLY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 100 |
| 5.0 mm | 90 |
| 2.00 mm | 69 |
| 0.425 mm | 54 |
| 0.075 mm | 42 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 53 µm | 32 |
| 31 µm | 29 |
| 13 µm | 24 |
| 6 µm | 22 |
| 2 µm | 21 |
| % Clay | 22 |
| % Silt | 10 |
| % Sand | 37 |
| % Gravel | 31 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 36 |
| Plasticity Index | 13 |
| Linear Shrinkage (%) | 6.5 |
| Grading Modulus | 1.35 |
| Classification | A-6 (2) |
| Unified Classification | SC |
| Chart Reference |  |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
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 DATE : 2018-12-10


POTENTIAL EXPANSIVENESS



PLASTICITY CHART

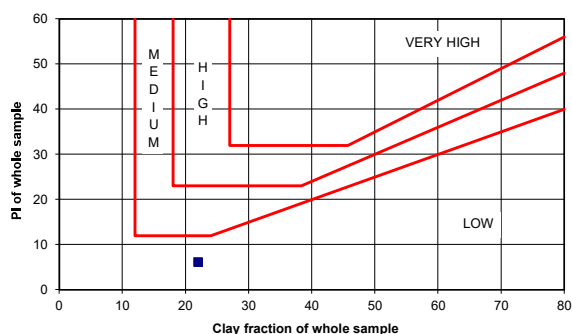


PARTICLE SIZE ANALYSIS

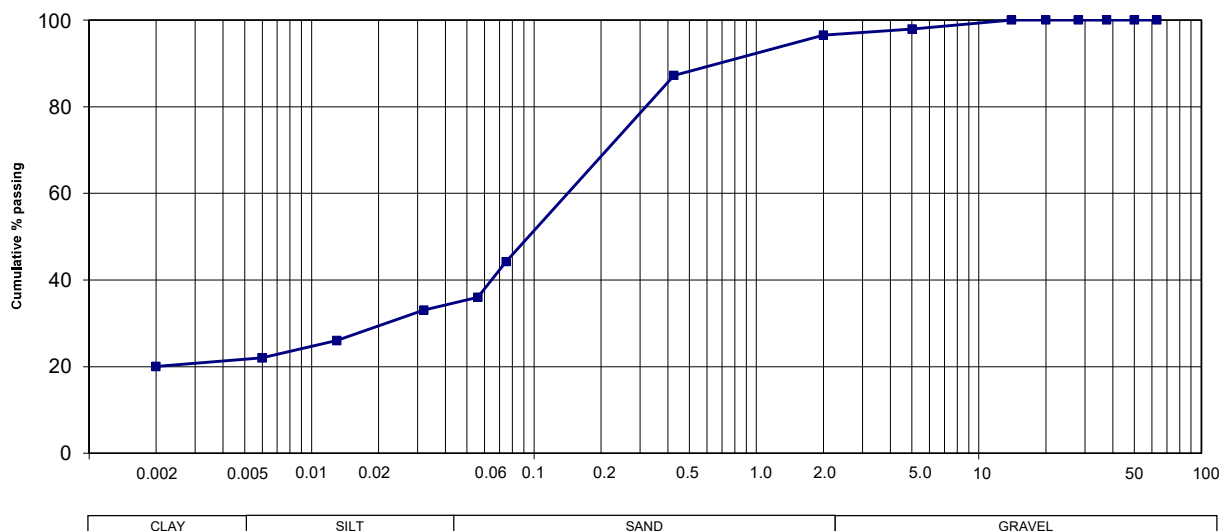
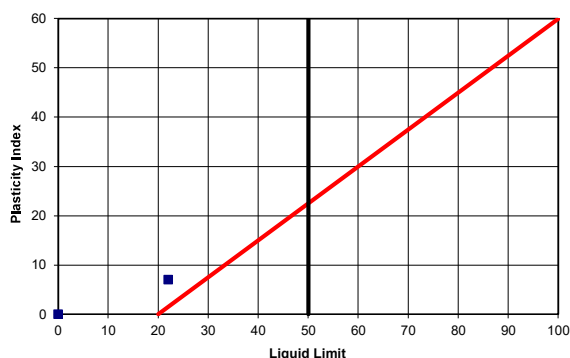
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|---|---|
| Sample No. | 6 |
| Soillab Sample No. | S18-2207-06 |
| Depth (m) | 0.3 - 0.9 |
| Position | TP 15 |
| Material Description | DARK YELLOW FERRICRETE CLAYEY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 100 |
| 5.0 mm | 98 |
| 2.00 mm | 97 |
| 0.425 mm | 87 |
| 0.075 mm | 44 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 56 µm | 36 |
| 32 µm | 33 |
| 13 µm | 26 |
| 6 µm | 22 |
| 2 µm | 20 |
| | |
| % Clay | 22 |
| % Silt | 14 |
| % Sand | 61 |
| % Gravel | 3 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 22 |
| Plasticity Index | 7 |
| Linear Shrinkage (%) | 3.5 |
| Grading Modulus | 0.72 |
| Classification | A-4 (0) |
| Unified Classification | SM & SC |
| Chart Reference |  |

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POTENTIAL EXPANSIVENESS



PLASTICITY CHART

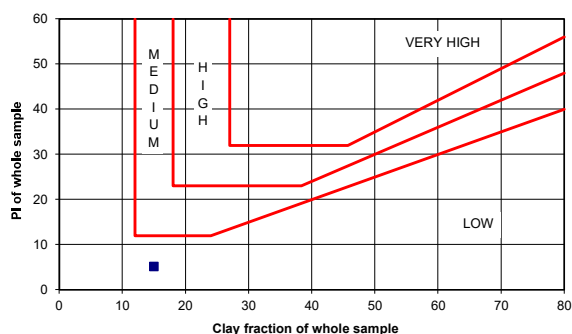


PARTICLE SIZE ANALYSIS

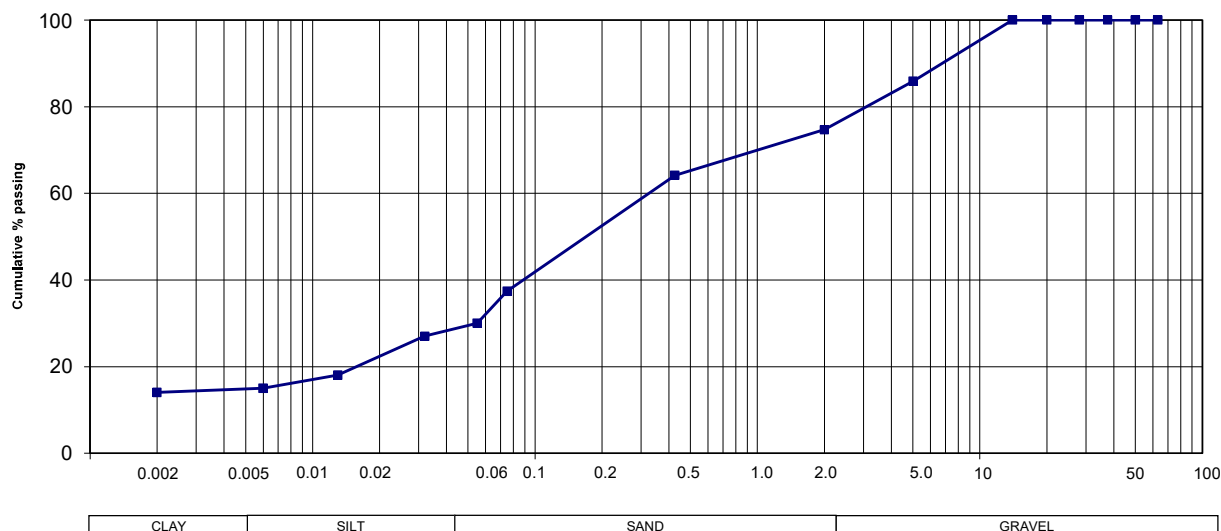
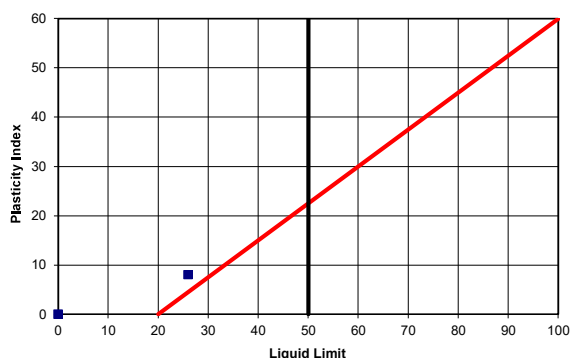
| | |
|---|--|
| Sample No. | 7 |
| Soillab Sample No. | S18-2207-07 |
| Depth (m) | 0.9 - 1.6 |
| Position | TP 15 |
| Material Description | DARK YELLOW FERRICRETE GRAVELLY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 100 |
| 5.0 mm | 86 |
| 2.00 mm | 75 |
| 0.425 mm | 64 |
| 0.075 mm | 37 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 55 µm | 30 |
| 32 µm | 27 |
| 13 µm | 18 |
| 6 µm | 15 |
| 2 µm | 14 |
| | |
| % Clay | 15 |
| % Silt | 15 |
| % Sand | 45 |
| % Gravel | 25 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 26 |
| Plasticity Index | 8 |
| Linear Shrinkage (%) | 4.0 |
| Grading Modulus | 1.24 |
| Classification | A-4 (0) |
| Unified Classification | SC |
| Chart Reference | |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
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POTENTIAL EXPANSIVENESS



PLASTICITY CHART

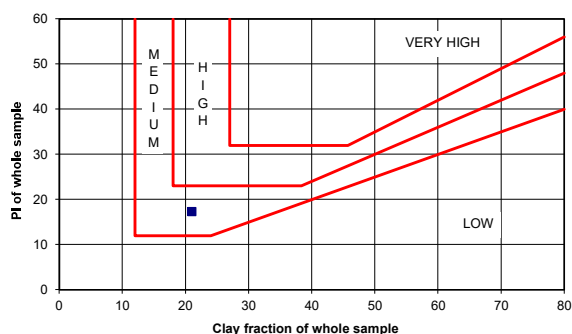


PARTICLE SIZE ANALYSIS

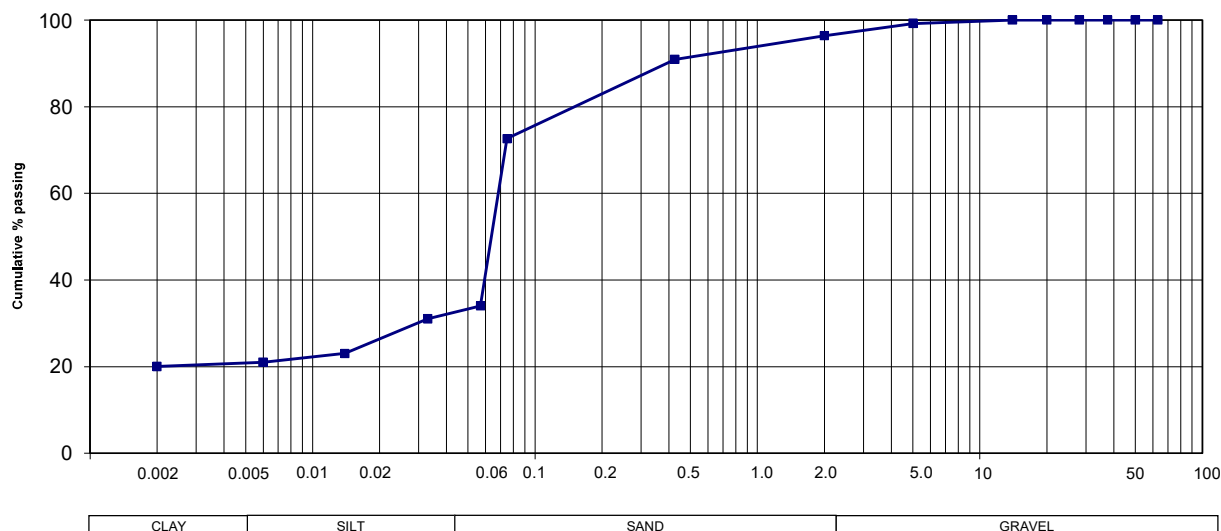
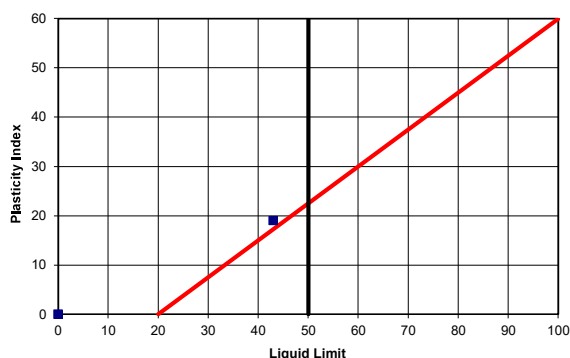
| | |
|---|---|
| Sample No. | 8 |
| Soillab Sample No. | S18-2207-08 |
| Depth (m) | 1.6 - 2.1 |
| Position | TP 15 |
| Material Description | DARK YELLOW CLAYEY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 100 |
| 5.0 mm | 99 |
| 2.00 mm | 96 |
| 0.425 mm | 91 |
| 0.075 mm | 73 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 57 µm | 34 |
| 33 µm | 31 |
| 14 µm | 23 |
| 6 µm | 21 |
| 2 µm | 20 |
| % Clay | 21 |
| % Silt | 13 |
| % Sand | 62 |
| % Gravel | 4 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 43 |
| Plasticity Index | 19 |
| Linear Shrinkage (%) | 5.0 |
| Grading Modulus | 0.40 |
| Classification | A-7-6 (13) |
| Unified Classification | CL |
| Chart Reference |  |

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POTENTIAL EXPANSIVENESS



PLASTICITY CHART

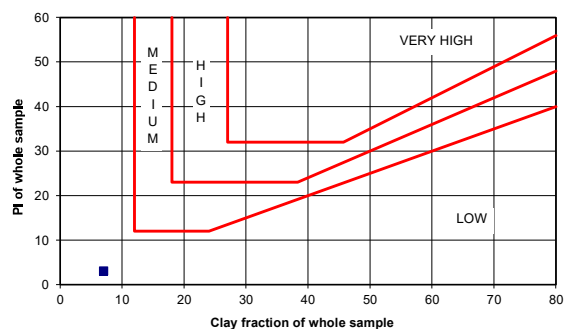


PARTICLE SIZE ANALYSIS

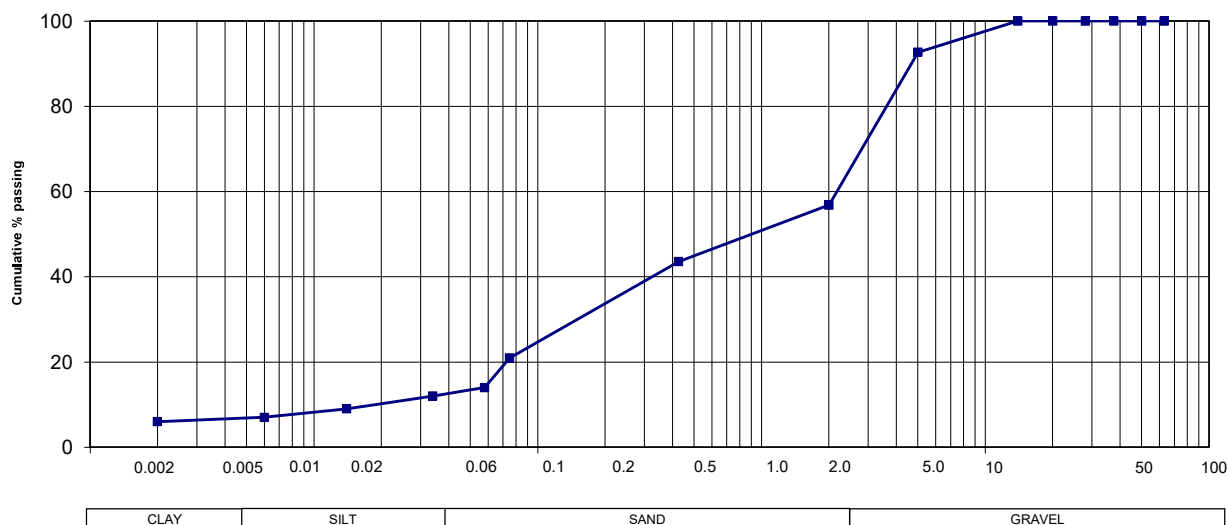
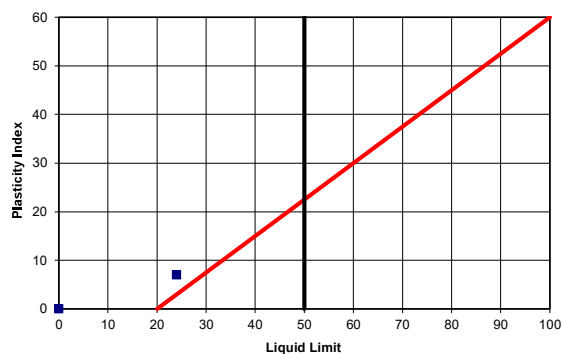
| | |
|---|---|
| Sample No. | 9 |
| Soillab Sample No. | S18-2207-09 |
| Depth (m) | 0.39 - 1.3 |
| Position | TP 16 |
| Material Description | DARK YELLOWISH ORANGE QUARTZITE & FERRICRETE SANDY GRAVEL |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 100 |
| 5.0 mm | 93 |
| 2.00 mm | 57 |
| 0.425 mm | 44 |
| 0.075 mm | 21 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 58 µm | 14 |
| 34 µm | 12 |
| 14 µm | 9 |
| 6 µm | 7 |
| 2 µm | 6 |
| % Clay | 7 |
| % Silt | 7 |
| % Sand | 43 |
| % Gravel | 43 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 24 |
| Plasticity Index | 7 |
| Linear Shrinkage (%) | 2.5 |
| Grading Modulus | 1.79 |
| Classification | A-2-4 (0) |
| Unified Classification | SM & SC |
| Chart Reference |  |

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 DATE : 2018-12-10

POTENTIAL EXPANSIVENESS



PLASTICITY CHART

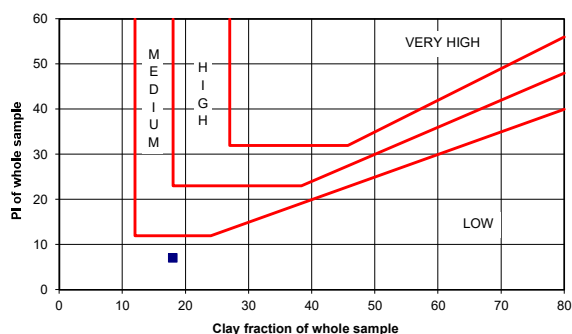


PARTICLE SIZE ANALYSIS

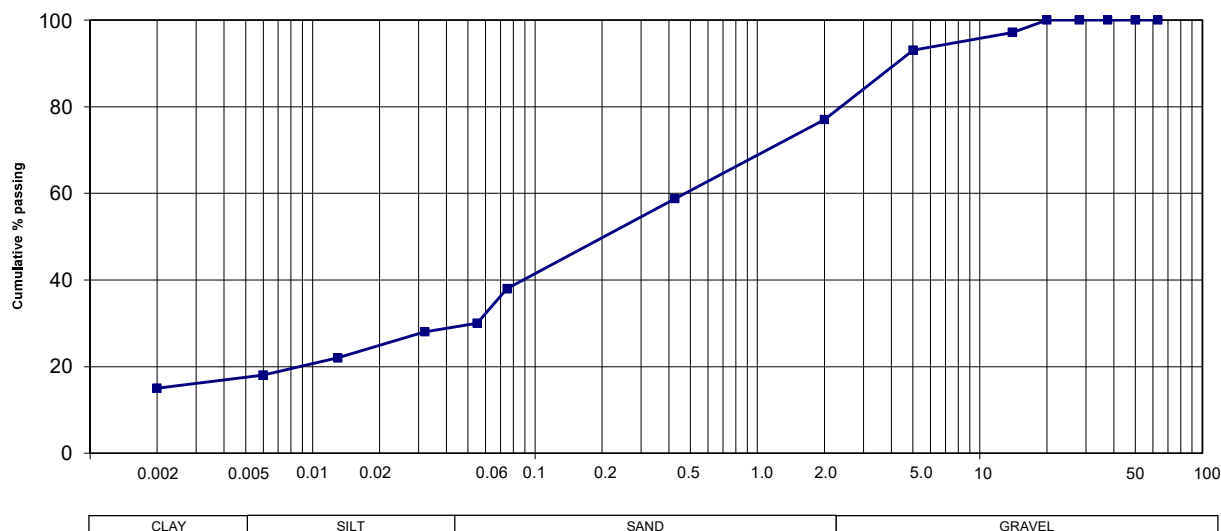
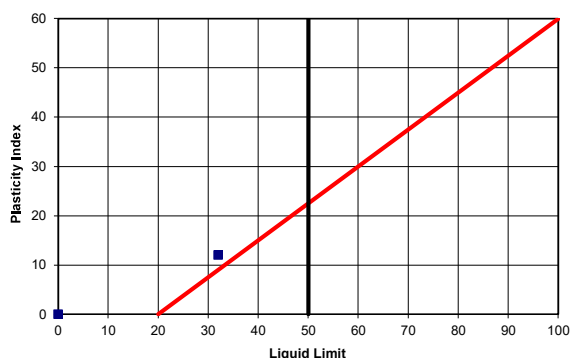
| | |
|---|--|
| Sample No. | 10 |
| Soillab Sample No. | S18-2207-10 |
| Depth (m) | 1.3 - 2.5 |
| Position | TP 16 |
| Material Description | LIGHT REDDISH ORANGE GRAVELLY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 97 |
| 5.0 mm | 93 |
| 2.00 mm | 77 |
| 0.425 mm | 59 |
| 0.075 mm | 38 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 55 µm | 30 |
| 32 µm | 28 |
| 13 µm | 22 |
| 6 µm | 18 |
| 2 µm | 15 |
| % Clay | 18 |
| % Silt | 12 |
| % Sand | 47 |
| % Gravel | 23 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 32 |
| Plasticity Index | 12 |
| Linear Shrinkage (%) | 5.5 |
| Grading Modulus | 1.26 |
| Classification | A-6 (1) |
| Unified Classification | SC |
| Chart Reference | |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
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POTENTIAL EXPANSIVENESS



PLASTICITY CHART

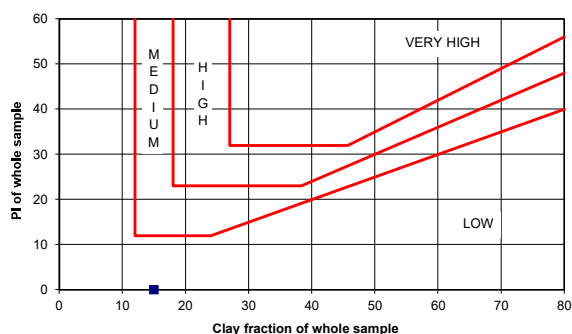


PARTICLE SIZE ANALYSIS

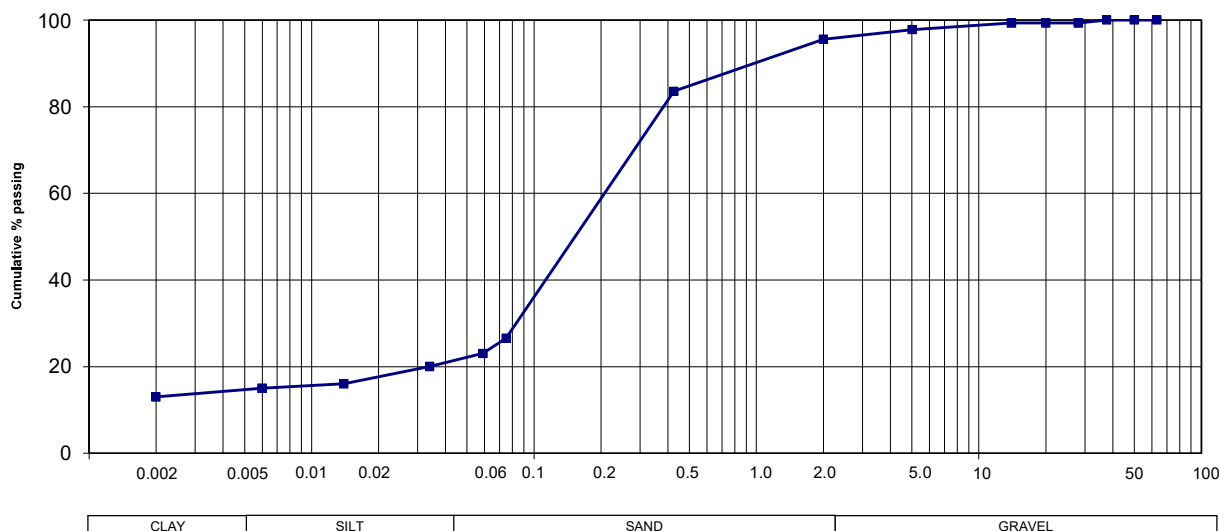
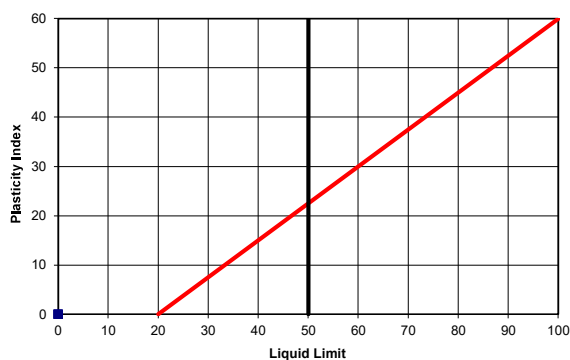
| | |
|---|---|
| Sample No. | 11 |
| Soillab Sample No. | S18-2207-11 |
| Depth (m) | 0.0 - 0.4 |
| Position | TP 18 |
| Material Description | DARK BROWN FERRICRETE CLAYEY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 99 |
| 20.0 mm | 99 |
| 14.0 mm | 99 |
| 5.0 mm | 98 |
| 2.00 mm | 96 |
| 0.425 mm | 84 |
| 0.075 mm | 27 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 59 µm | 23 |
| 34 µm | 20 |
| 14 µm | 16 |
| 6 µm | 15 |
| 2 µm | 13 |
| | |
| % Clay | 15 |
| % Silt | 8 |
| % Sand | 73 |
| % Gravel | 4 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | |
| Plasticity Index | NP |
| Linear Shrinkage (%) | 0.0 |
| Grading Modulus | 0.94 |
| Classification | A-2-4 (0) |
| Unified Classification | SM |
| Chart Reference |  |

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 DATE : 2018-12-10

POTENTIAL EXPANSIVENESS



PLASTICITY CHART

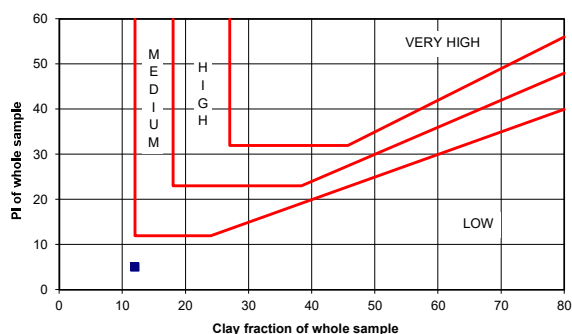


PARTICLE SIZE ANALYSIS

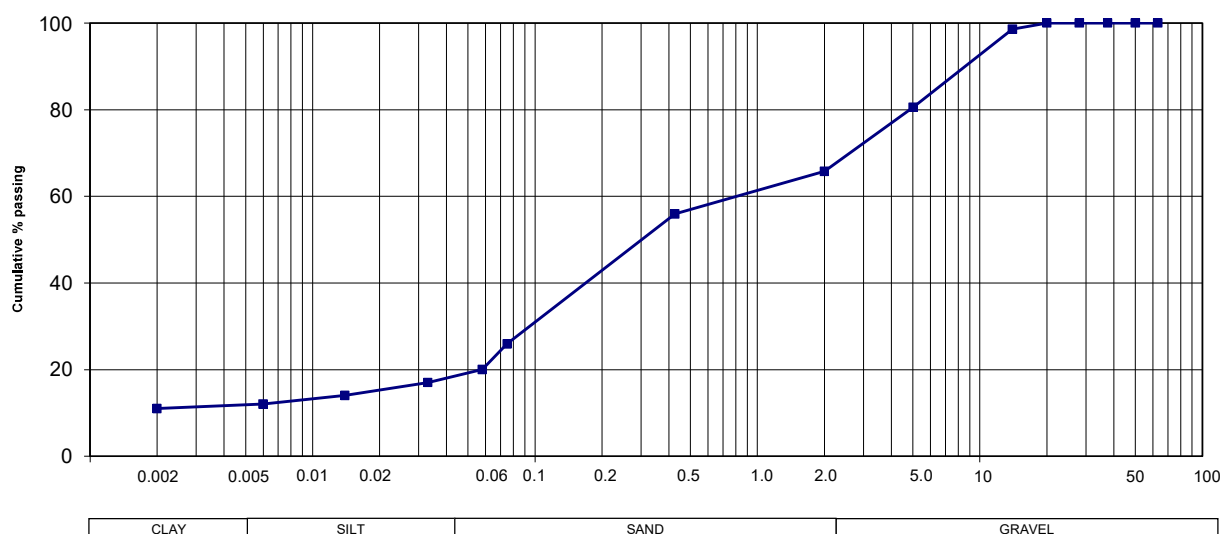
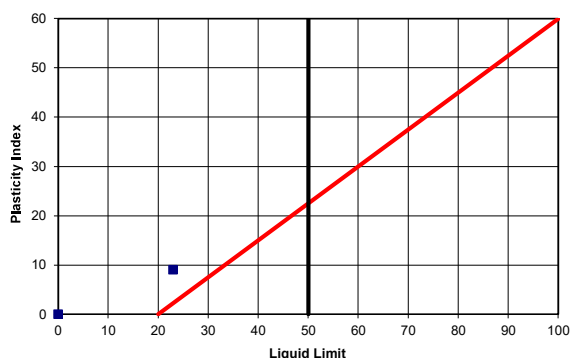
| | |
|---|---|
| Sample No. | 12 |
| Soillab Sample No. | S18-2207-12 |
| Depth (m) | 0.4 - 0.7 |
| Position | TP 18 |
| Material Description | DARK YELLOWISH ORANGE GRAVELLY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 100 |
| 20.0 mm | 100 |
| 14.0 mm | 99 |
| 5.0 mm | 81 |
| 2.00 mm | 66 |
| 0.425 mm | 56 |
| 0.075 mm | 26 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 58 µm | 20 |
| 33 µm | 17 |
| 14 µm | 14 |
| 6 µm | 12 |
| 2 µm | 11 |
| | |
| % Clay | 12 |
| % Silt | 8 |
| % Sand | 46 |
| % Gravel | 34 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 23 |
| Plasticity Index | 9 |
| Linear Shrinkage (%) | 4.0 |
| Grading Modulus | 1.52 |
| Classification | A-2-4 (0) |
| Unified Classification | SC |
| Chart Reference | |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
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POTENTIAL EXPANSIVENESS



PLASTICITY CHART

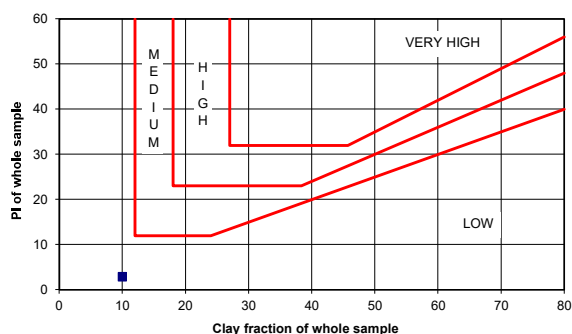


PARTICLE SIZE ANALYSIS

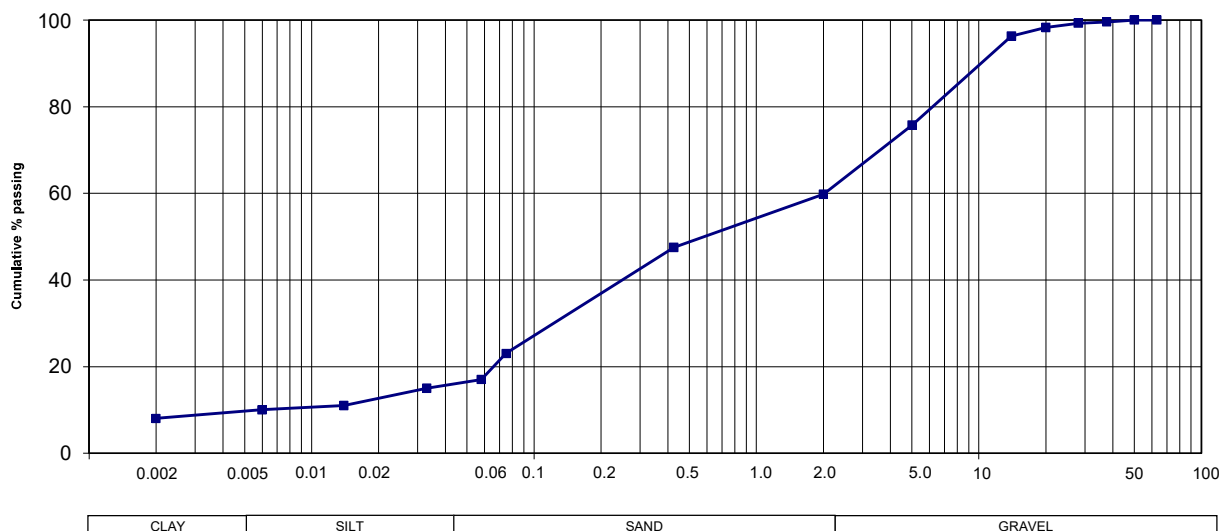
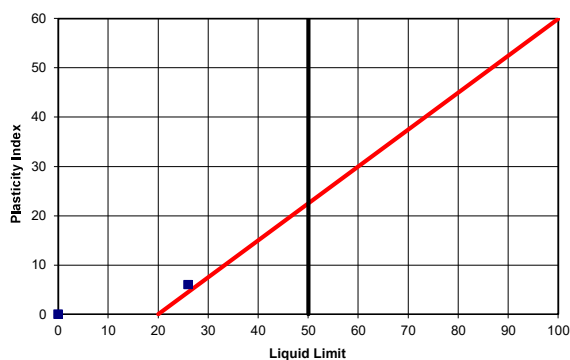
| | |
|---|---|
| Sample No. | 13 |
| Soillab Sample No. | S18-2207-13 |
| Depth (m) | 0.7 - 0.9 |
| Position | TP 18 |
| Material Description | DARK YELLOWISH ORANGE GRAVELLY SAND |
| Relative density on < 2 mm (SANS 5844) | 2.65 |
| Organic Material | |
| Moisture (%) / Dispersion (%) | |
| SCREEN ANALYSIS (% PASSING) (SANS 3001:GR1) | |
| 63.0 mm | 100 |
| 50.0 mm | 100 |
| 37.5 mm | 100 |
| 28.0 mm | 99 |
| 20.0 mm | 98 |
| 14.0 mm | 96 |
| 5.0 mm | 76 |
| 2.00 mm | 60 |
| 0.425 mm | 47 |
| 0.075 mm | 23 |
| HYDROMETER ANALYSIS (% PASSING) (SANS 3001:GR3) | |
| 58 µm | 17 |
| 33 µm | 15 |
| 14 µm | 11 |
| 6 µm | 10 |
| 2 µm | 8 |
| % Clay | 10 |
| % Silt | 7 |
| % Sand | 43 |
| % Gravel | 40 |
| ATTERBERG LIMITS (SANS 3001:GR10) | |
| Liquid Limit | 26 |
| Plasticity Index | 6 |
| Linear Shrinkage (%) | 2.0 |
| Grading Modulus | 1.70 |
| Classification | A-1-b (0) |
| Unified Classification | SM & SC |
| Chart Reference |  |

PROJECT : AERORAND SOUTH GEOTECH-MK-18-480
 JOB No. : S18-2207
 DATE : 2018-12-10

POTENTIAL EXPANSIVENESS



PLASTICITY CHART



APPENDIX H2: COMPACTION TEST RESULTS

Project Description

| | | | |
|------------------|---------------------------------------|-------------------|----------|
| Client: | MUKONA CONSULTING ENGINEERS (PTY) LTD | Soillab Job No.: | S18-2207 |
| Job Description: | AERORAND SOUTH GEOTECH-MK-18-480 | Contract Number: | |
| Date: | 2018/12/10 | Reference Number: | |

Sample Description

| | | | | |
|-----------------------|--|--------------------------|--------------------------|--|
| Soillab Sample No.: | S18-2207-09 | S18-2207-12 | S18-2207-13 | |
| Sample Description: | TP 16 | TP 18 | TP 18 | |
| Sample Depth: | 0.39 - 1.3 | 0.4 - 0.7 | 0.7 - 0.9 | |
| Material Description: | DARK YELLOWISH ORANGE QUARTZITE & FERRICRETE | DARK YELLOWISH ORANGE | DARK YELLOWISH ORANGE | |

Screen Analysis (% Passing) - SANS 3001-GR1

| | | | | |
|----------|-----|-----|-----|--|
| 75,00 mm | 100 | 100 | 100 | |
| 63,00 mm | 100 | 100 | 100 | |
| 50,00 mm | 100 | 100 | 100 | |
| 37,50 mm | 100 | 100 | 100 | |
| 28,00 mm | 100 | 100 | 99 | |
| 20,00 mm | 100 | 100 | 98 | |
| 14,00 mm | 100 | 99 | 96 | |
| 5,00 mm | 93 | 81 | 76 | |
| 2,000 mm | 57 | 66 | 60 | |
| 0,425 mm | 44 | 56 | 47 | |
| 0,075 mm | 21 | 26 | 23 | |

Soil-mortar percentages - SANS 3001-PR5

| | | | | | |
|------------------|---------------|----|----|----|--|
| Coarse Sand | 2.000-0.425mm | 23 | 15 | 21 | |
| Coarse Fine Sand | 0.425-0.250mm | 15 | 13 | 13 | |
| Medium Fine Sand | 0.250-0.150mm | 13 | 16 | 14 | |
| Fine Fine Sand | 0.150-0.075mm | 12 | 16 | 15 | |
| Silt and clay | <0.075mm | 37 | 39 | 39 | |

Constants

| | | | | | |
|------------------|----------------|------|------|------|--|
| Grading Modulus | SANS 3001-PR5 | 1.79 | 1.52 | 1.70 | |
| Liquid Limit | | 24 | 23 | 26 | |
| Plasticity Index | SANS 3001-GR10 | 7 | 9 | 6 | |
| Linear Shrinkage | | 2.5 | 4.0 | 2.0 | |

MOD AASHTO - SANS 3001-GR30

| | | | | |
|------------------------------|------|------|------|--|
| Max Dry Density (kg/m³) | 2157 | 2133 | 2157 | |
| Optimum Moisture Content (%) | 7.4 | 8.1 | 8.6 | |

CBR - SANS 3001-GR40

| | | | | |
|-------------------------------|-----------|-----------|-----------|--|
| MOD AASHTO | | | | |
| Moulding Moisture Content (%) | 7.4 | 8.0 | 8.6 | |
| Dry Density (kg/m³) | 2167 | 2118 | 2187 | |
| % of Max Dry Density | 100.5 | 99.3 | 101.4 | |
| 100% MOD CBR (%) | 94 | 37 | 53 | |
| % Swell | 0.1 | 0.0 | 0.0 | |
| NRB | | | | |
| Dry Density (kg/m³) | 2073 | 2025 | 2078 | |
| % of Max Dry Density | 96.1 | 94.9 | 96.3 | |
| 100% NRB CBR (%) | 48 | 24 | 34 | |
| % Swell | 0.1 | 0.1 | 0.0 | |
| PROCTOR | | | | |
| Dry Density (kg/m³) | 1955 | 1922 | 1967 | |
| % of Max Dry Density | 90.6 | 90.1 | 91.2 | |
| 100% PROCTOR CBR (%) | 21 | 15 | 21 | |
| % Swell | 0.1 | 0.1 | 0.1 | |
| CBR (%) | | | | |
| 100% Mod AASHTO | 88 | 40 | 47 | |
| 98% Mod AASHTO | 65 | 33 | 39 | |
| 97% Mod AASHTO | 55 | 30 | 36 | |
| 95% Mod AASHTO | 41 | 24 | 30 | |
| 93% Mod AASHTO | 30 | 20 | 25 | |
| 90% Mod AASHTO | 19 | 15 | 19 | |
| COLTO Classification: | G6 | G7 | G6 | |

APPENDIX H3: CHEMICAL TEST RESULTS

Client: MUKONA CONSULTING ENGINEERS
Project: AERORAND SOUTH GEOTECH - MK-18-480
Project No.: S18-2207
Date: 2018/11/26

pH & CONDUCTIVITY - TMH 1 A20 & A21T

| Sample No | Sample Position | Depth (m) | pH | Electrical Conductivity S/m |
|-------------|-----------------|-----------|------|-----------------------------|
| S18-2207-09 | TP 16 | 0.39-1.3 | 6.24 | 0.0009 |
| S18-2207-12 | TP 18 | 0.4-0.7 | 6.28 | 0.0058 |
| S18-2207-13 | TP 18 | 0.7-0.9 | 6.58 | 0.0038 |
| | | | | |

Comments:

Note: Items marked with a star (*) is Not Accredited
Soillab is a SANAS accredited Testing Laboratory according to the Accreditation Scope

APPENDIX I: ZONATION MAP

29°26'30"E

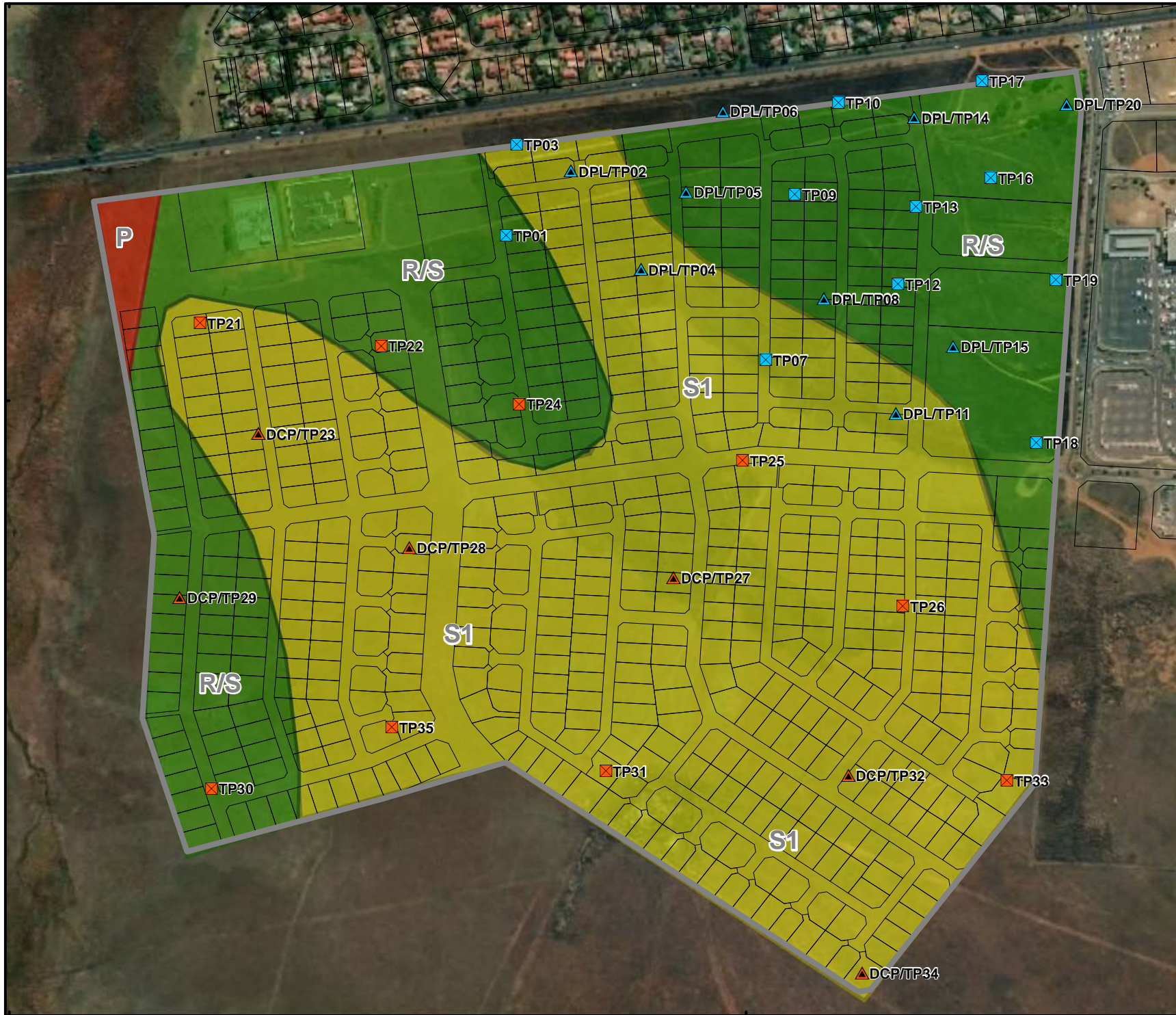
29°27'0"E

25°48'30"S

25°48'30"S

29°26'30"E

29°27'0"E



LEGEND

- ADDITIONAL TEST PITS
- ADDITIONAL DCP & TEST PITS
- EXISTING TEST PITS
- EXISTING DPL & TEST PITS
- FARM BOUNDARY
- MIDDELBURG FARM ERFs

ZONES

- ZONE 1 - R/S
- ZONE 2 - S1
- ZONE 3 - P (Potential Flood Zone)

| NHBR SITE CLASS | GEOTECHNICAL PROBLEM | FOUNDATION RECOMMENDATIONS |
|-----------------|--|---|
| R/S | Low Settlement Difficulty of excavation | Strip Foundation Concrete Raft |
| S1 | Moderate Settlement | Modified Normal Foundation Concrete Raft |
| P | Potential Flood Zone | No Development |

CLIENT



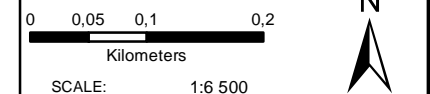
PROJECT

**GEOTECHNICAL INVESTIGATION FOR
AERORAND SOUTH TOWNSHIP
STEVE TSHWETE MUNICIPALITY**

TITLE

**ZONATION MAP &
GEOTECHNICAL LAYOUT PLAN
AERIAL IMAGERY- ESRI BASEMAPS**

| | |
|------------------|---------------------|
| DRAWN: A. Qoboka | DRAWING |
| DATE: 2019/06/03 | MK-1 8- 480- GLP062 |



Projection: Geographic, Datum: WGS84
Source: Chief Directorate National Geo-Spatial Information
Inset: ESRI Data and Maps

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