

# PORTION 260 OF THE FARM RIETFONTEIN 189-IQ, MULDRSDRIFT

## NEAR-SURFACE GEOTECHNICAL INVESTIGATION REPORT



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PORTION 260 OF THE FARM RIETFontein 189-IQ, MULDRSDRIFT

Geotechnical Investigation and Report

Report Reference Number: 1911547/01

Revision date: December 2019

## 1. Executive Summary

Victor and Partners commissioned Geotheta (Pty) Limited to prepare a geotechnical investigation report at Portion 260 of the Farm Rietfontein 189-IQ in Muldersdrift, Gauteng.

A near-surface geotechnical investigation was done, and representative soil samples were retrieved.

The typical soil strata encountered on site comprised a layer of topsoil underlain by loose to dense transported material overlying loose to dense residual material. Hardpan ferricrete was encountered in one test pit on site during the investigation.

No groundwater seepage was encountered during the investigation.

The residual granites on site are susceptible to collapse, and therefore the following is recommended.

Remove the in-situ material below the foundations to a depth and width of 1.5 x the width of the foundation. Replace the excavated material with suitable G6 material compacted in maximum 150mm layers to 95% Mod AASHTO density at -1% to +1% of OMC. Excavation through the ferricrete layer is recommended to ensure that the soils within the foundation zone of influence comprises the compacted G6 material.

Taller buildings (greater than 2 stories) will need to be supported on piles. Further penetrative testing is required to determine the depth to bedrock. We suggest using DPSH testing and drilling (to determine if rock are core stones or not).

Adequate storm water control needs to be implemented to direct the water away from excavations and foundations. Foundations should be protected from moisture ingress.

The material tested conforms to a G6 material classification, indicating that material similar to the samples tested is suitable for use as structural fill. This can also be used for backfilling of strip footing foundations.

Excavatability of the material on site is classed as *soft* to *intermediate*, and *hard* through the hardpan ferricrete.

Soil classification of the site in terms of the NHBRC Home Building Manual is C1.

## **2. Disclaimer**

### **2.1 Data provided to Geotheta**

The opinions expressed in this Report have been based on the information supplied to Geotheta (Pty) Ltd (Geotheta) by Victor and Partners. The opinions in this report are provided in response to a specific request from Victor and Partners to do so. Geotheta has exercised all due care in reviewing the supplied information. Whilst Geotheta has compared key supplied data with expected values, the accuracy of the results and conclusions from the review are entirely reliant on the accuracy and completeness of the supplied data. Geotheta does not accept responsibility for any errors or omissions in the supplied information and does not accept any consequential liability arising from commercial decisions or actions resulting from them.

### **2.2 Data obtained by Geotheta**

Opinions presented in this report apply to the site conditions and features as they existed at the time of Geotheta's investigations, and those reasonably foreseeable. These opinions do not necessarily apply to conditions and features that may arise after the date of this report, about which Geotheta had no prior knowledge nor had the opportunity to evaluate.

## **3. Statement of Geotheta Independence**

Neither Geotheta nor any of the authors of this report have any material present or contingent interest in the outcome of this report, nor do they have any monetary or other interest that could be reasonably regarded as being capable of affecting their independence or that of Geotheta.

Geotheta has no beneficial interest in the outcome of the technical assessment being capable of affecting its independence.

Geotheta's fee for completing this report is based on its normal professional rates and/or fees plus incidental expenses. The payment of that professional fee or expense is not contingent upon the outcome of the report.

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**5. List of abbreviations**

CBR	:	California Bearing Ratio
Civilab	:	Civilab (Pty) Limited
DPSH	:	Dynamic Probe Super Heavy
Geotheta	:	Geotheta (Pty) Limited
kPa	:	kilo Pascal
Mod	:	Modified
N	:	Weinert N-value
OMC	:	Optimum Moisture Content
TP	:	Test Pit

## 6. Introduction

- 6.1 Victor and Partners commissioned Geotheta (Pty) Limited to prepare a geotechnical investigation report at Portion 260 of the Farm Rietfontein 189-IQ in Muldersdrift, Gauteng.
- 6.2 A near-surface geotechnical investigation was done to determine the foundation conditions and appropriate founding depth for the proposed development.
- 6.3 The investigation comprised test pit excavations and retrieval of samples for laboratory testing. The test results were analysed to determine the foundation conditions and the suitability of the in-situ soil for use in the construction works.
- 6.4 The site investigation work commenced on 15 November 2019 and the laboratory test results were received on 06 December 2019.

## 7. Terms of reference

- 7.1 Geotheta submitted proposal reference 1911547 - Victor and Partners - Ptn 260 Rietfontein Geotech - P01 on 07 November 2019.
- 7.2 Victor and Partners confirmed the appointment on 11 November 2019.

## 8. Scope of work

The scope of work done is:

### 8.1 Site geotechnical investigation

The following was done to determine the foundation geotechnical characteristics of the area:

#### 8.1.1 Test Pits

- 8.1.2 A Tractor Loader Backhoe (TLB) excavator was deployed on site to excavate test pits.
- 8.1.3 The test pits were profiled to determine the strata layers and characteristics. Soil samples were retrieved as necessary for laboratory testing.

### 8.2 Laboratory testing

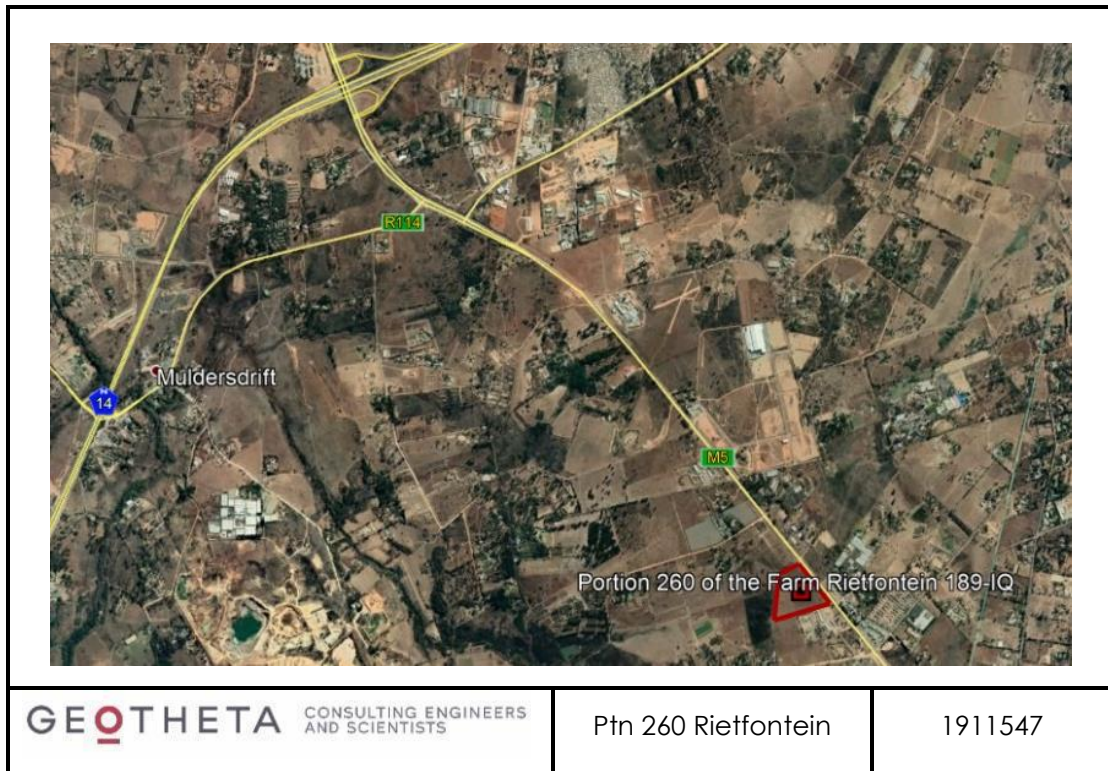
- 8.2.1 The soil samples were sent to a SANAS certified geotechnical soils laboratory for testing and analysis. Foundation indicator and Mod CBR tests were undertaken.

### 8.3 Report

- 8.3.1 This geotechnical report was written.

## 9. Site Location and Description

- 9.1 The site is situated on Bayers Naude Drive in Muldersdrift, to the southeast of the N14 Highway (see Figure 1).
- 9.2 The site comprises a grassed open plot. A small area located on the northern side of the property has been excavated in the past. Satellite images show that this has been in existence before 2007. The site slopes from east to west at an average gradient of 5.9%.

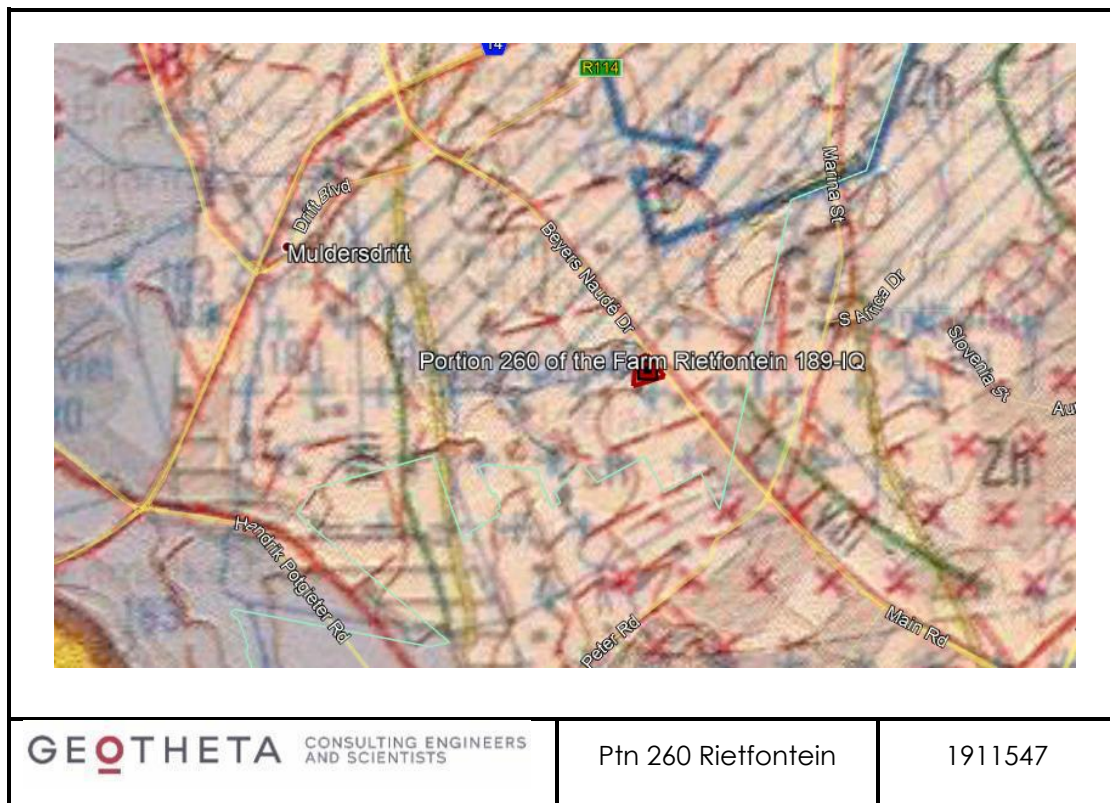


**Figure 1 : Site Location**

**10. Geology**

- 10.1 Figure 2 indicates the regional geology of the area.
- 10.2 According to the 1:250 000 West Rand 2626 geological map, the site is underlain by grey, medium grained porphyritic granodiorite of the Swazian Era.
- 10.3 The residual materials of this rock formation are usually highly collapsible.
- 10.4 During the near-surface investigation, the typical soil strata encountered on site comprised a layer of topsoil underlain by loose to dense transported material overlying loose to dense residual material. Hardpan ferricrete was also encountered in test pit TP6.





**Figure 2: Regional Geology**

**11. Engineering Geology**

- 11.1 The influence of climate on weathering is expressed by the N-value (H.H. Weinert 1980). The most important is where N=5. Where N is more than 5, disintegration is dominant, and where N is less than 5, decomposition is dominant.
- 11.2 The Weinert N-value is 2.4 for this region, indicating that decomposition is the overriding process.
- 11.3 Weinert also mentions that where N is between 2 and 5, weathering profiles develop upwards from fresh rock to residual soil.

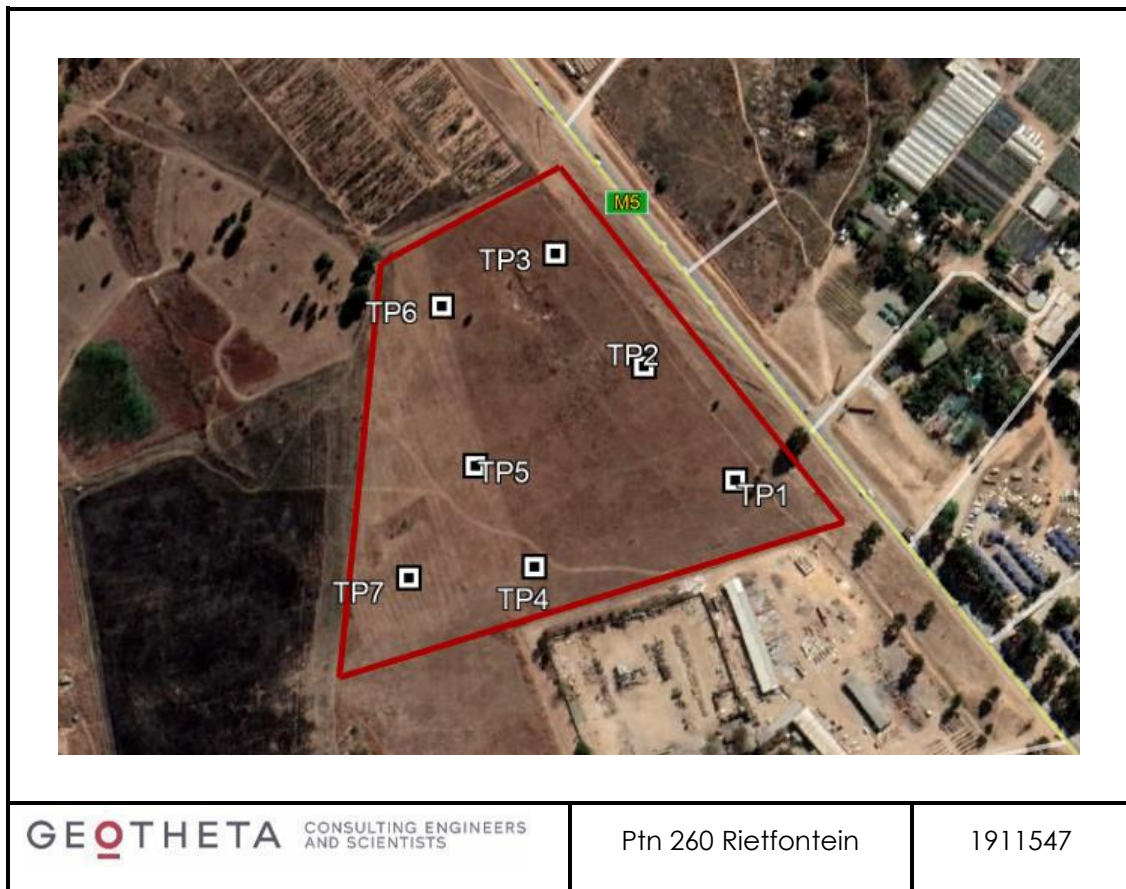
**12. Method of Investigation**

**12.1 Desk study**

- 12.1.1 The local geology was determined from the geological maps. The results of this study are discussed in sections 10 and 11 above.

**12.2 Test Pits**

- 12.2.1 No formal grid spacing was used in setting out the test pit positions. Positions were selected to adequately cover the site and to determine any variations in the site geology.
- 12.2.2 Seven test pits were excavated. The test pit positions are indicated in Figure 3.
- 12.2.3 The test pits were excavated with a JCB Tractor Loader Backhoe (TLB) and soil profiles were logged according to the standard method of Jennings, Brink and Williams (1973).
- 12.2.4 Test pit profiles and photographs are included in Appendix A and Appendix B respectively.



**Figure 3: Test Pit Positions**

**12.3 Soil Sampling**

12.3.1 Disturbed samples were taken from test pits TP2 and TP7 to determine the material classification and the parameters of the soil types as well as the potential of the excavated material to be used as backfill material.

**12.4 Laboratory Testing**

12.4.1 The retrieved samples were submitted to Civilab in Booyens Reserve, Johannesburg South, for testing.

12.4.2 Foundation Indicator and Mod CBR tests were conducted.

12.4.3 The laboratory test results are included as Appendix C.

12.4.4 The results are discussed below.

## 13. Results

### 13.1 Site soils

13.1.1 The soil profiles from the test pits encountered on the site are as follows:

Test Pit No	Topsoil	Transported Material	Residual Material	Test pit depth (m)
TP1	0 – 0.2	0.2 – 2.4	2.4 – 2.8	2.8 – Max reach
TP2	0 – 0.2	0.2 – 1.2	1.2 – 2.4	2.4 – Max reach
TP3	0 – 0.2	0.2 – 1.6	1.6 – 2.7	2.7 – Max reach
TP4	0 – 0.3	0.3 – 1.2	1.2 – 2.3	2.3 – Max reach
TP5	0 – 0.3	0.3 – 2.3		2.3 – Max reach
TP6	0 – 0.3	0.3 – 1.7		1.7 – Refusal
TP7	0 – 0.5	0.5 – 1.5	1.5 – 2.3	2.3 – Max reach

13.1.2 No groundwater seepage was encountered in any of the test pits.

13.1.3 All test pits, with the exception of test pit TP6, were excavated until the maximum reach of the TLB at depths ranging from 2.3m to 2.8m below natural ground level. Test pit TP6 was excavated until refusal of the TLB on hardpan ferricrete at a depth of 1.7m below natural ground level.

### 13.2 Laboratory Results

#### 13.2.1 TP2

- The residual material from test pit TP2 classified as a clayey sand (SC). The Plasticity Index is 13, the Liquid Limit 29 and the Linear Shrinkage 6.0. The value of the Grading Modulus is 1.91.
- The residual material plotted as LOW activity on the van der Merwe Activity Diagram.
- With a CBR value of 42 compacted to 95% MOD AASHTO, the material classifies as a G6 according to TRH14 specifications. The material tested is therefore suitable for structural fill.

#### 13.2.2 TP7

- The residual material from test pit TP7 classified as a clayey sand (SC). The Plasticity Index is 19, the Liquid Limit 40 and the Linear Shrinkage 8.0. The value of the Grading Modulus is 1.46.
- The residual material plotted as LOW activity on the van der Merwe Activity Diagram.

## 14. Discussion of results

### 14.1 Soil profiles

14.1.1 The site is underlain by loose to dense transported material overlying loose to dense residual material. Hardpan ferricrete was encountered in test pit TP6.

14.1.2 Although no groundwater seepage was encountered in any of the test pits during the investigation a perched water table could arise during the rainy season.

#### **14.2 Construction material**

14.2.1 The material tested conforms to a G6 material classification, indicating that material similar to the samples tested is suitable for use as structural fill.

#### **14.3 Foundation conditions**

14.3.1 For smaller rise structures (max 2 stories), foundations can be constructed on compacted layers comprising G6 material. The following is the recommended foundation design:

- Remove the in-situ residual material to a depth and width of 1.5 x the width of the foundation from the underside of the proposed foundation.
- Backfill the excavation with suitable G6 material compacted in maximum 150mm layers to 95% Mod AASHTO density at -1% to +1% of OMC. This alleviates any potential collapse from the residual granites.
- Excavation through the ferricrete layer is recommended to ensure that the soils within the foundation zone of influence comprises the compacted G6 material.

14.3.2 This will provide a foundation with 150kPa safe bearing capacity.

14.3.3 The base of the foundations should be cleared of all loose material prior to layer works or concrete works.

14.3.4 Precautions should be taken to protect the foundations from moisture ingress. Adequate storm water control needs to be implemented to direct the water away from excavations and foundations.

14.3.5 Piles are recommended to support larger load bearing structures. The depth of piling can only be determined by doing additional penetrative testing on site.

#### **14.4 Excavatability**

14.4.1 Excavatability of the material on site is classed as *soft* to *intermediate*, and *hard* through the hardpan ferricrete.

### **15. Summary, conclusions and recommendations**

15.1 The typical soil strata encountered on site comprised a layer of topsoil underlain by loose to dense transported material overlying loose to dense residual material. Hardpan ferricrete was also encountered in test pit TP6.

15.2 Seven test pits were excavated using a TLB to determine the subsoil conditions. All test pits, with the exception of test pit TP6, were excavated until the maximum reach of the TLB at depths ranging from 2.3m to 2.8m below natural ground level. Test pit TP6 was excavated until refusal of the TLB on hardpan ferricrete at a depth of 1.7m below natural ground level.

15.3 The material excavatability is classed as *soft* to *intermediate*, and *hard* through the hardpan ferricrete.

15.4 No groundwater was encountered in any of the test pits during the investigation.

15.5 Precautions should be taken to protect the foundations from moisture ingress. Adequate storm water control needs to be implemented to direct the water away from excavations and foundations.

- 15.6 The residual granites on site are susceptible to collapse, therefore suitable soil amelioration within the foundation zone of influence is required as specified in this report.
- 15.7 Piled foundations are necessary for larger structures (greater than two storeys).
- 15.8 Soil classification of the site in terms of the NHBRC Home Building Manual is C1.

**Prepared by**



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Massimo Gollino – BSc Civil Eng

In terms of Geotheta Quality Policy, this report has been reviewed, product corrected and certified okay for distribution and use.

**Reviewed by**



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Ian Hammond Pr Eng

All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

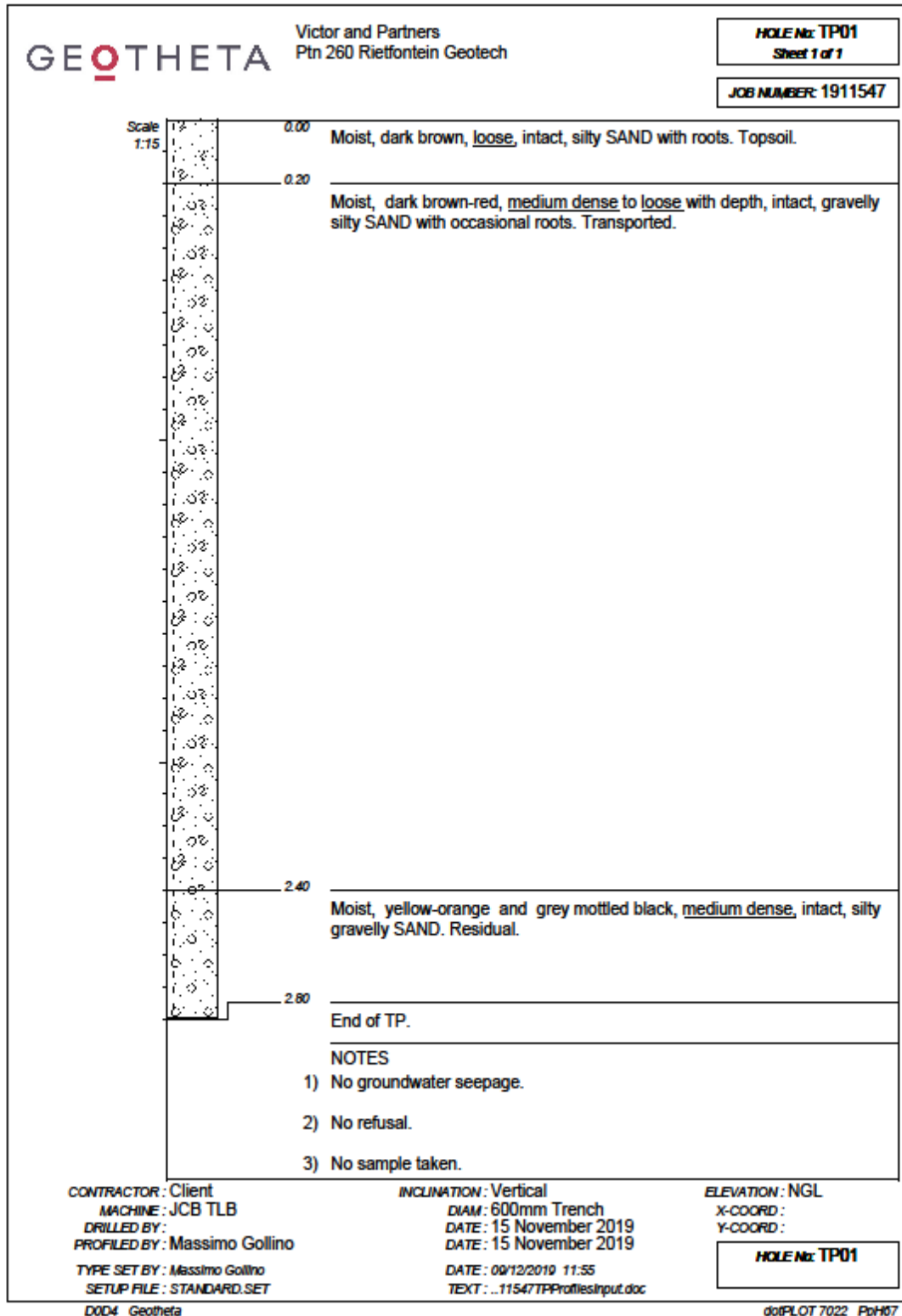
**16. References**

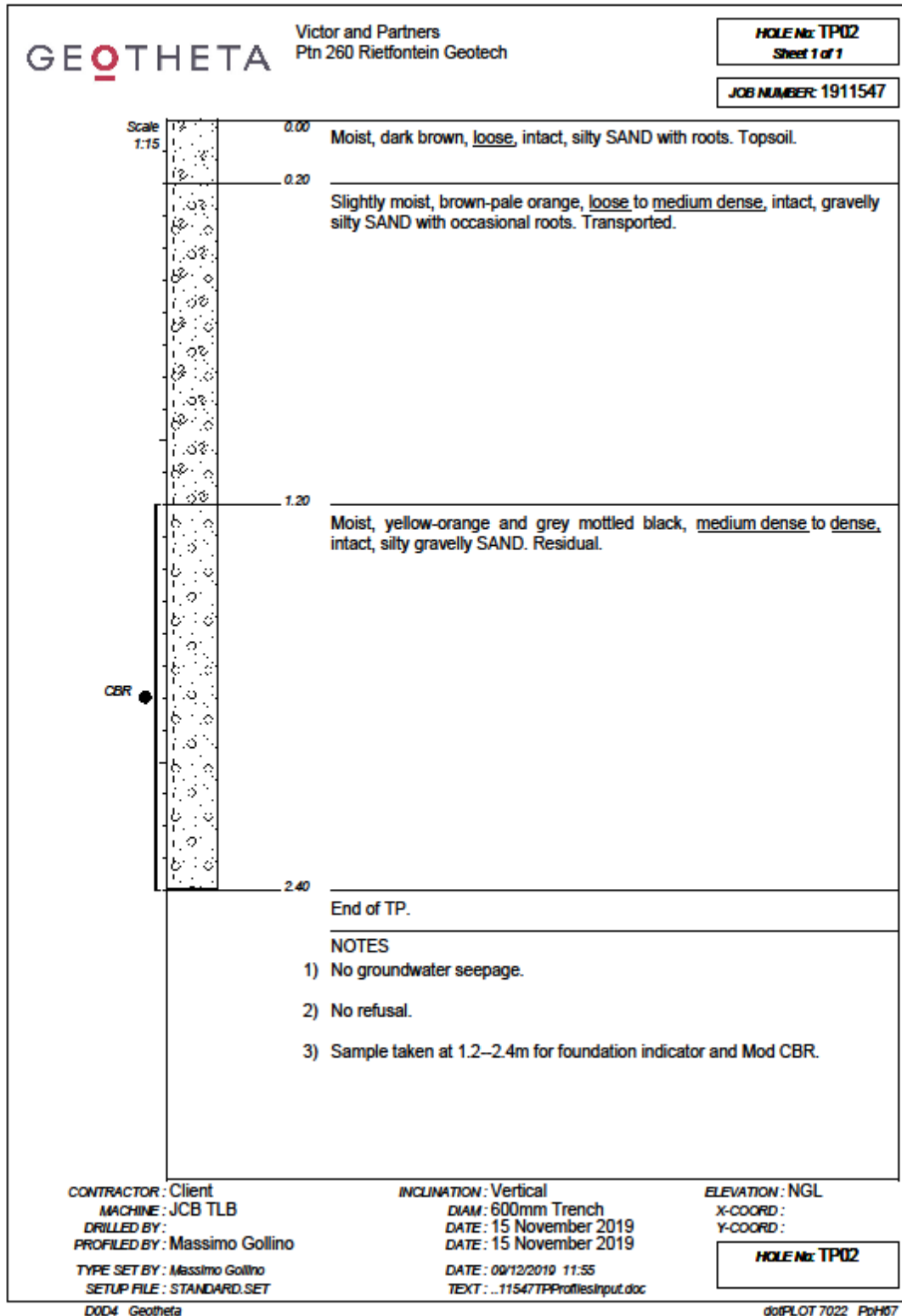
- 16.1 WEINERT, HH. 1980. The natural road construction materials of southern Africa. Pretoria: Academica.
- 16.2 JENNINGS JE, BRINK ABA, and WILLIAMS AAB. 1973. Revised guide to soil profiling for civil engineering purposes in southern Africa, The Civil Engineer in South Africa, Jan 1973 Trans SAICE, Vol 15 No 1.
- 16.3 VAN DER MERWE, DH. 1964. The prediction of heave from the plasticity index and the percentage clay fraction of soils. The Civil Engineer in South Africa. June 1964, pp 103-107.
- 16.4 UNIFIED SOIL CLASSIFICATION SYSTEM. CALTRANS

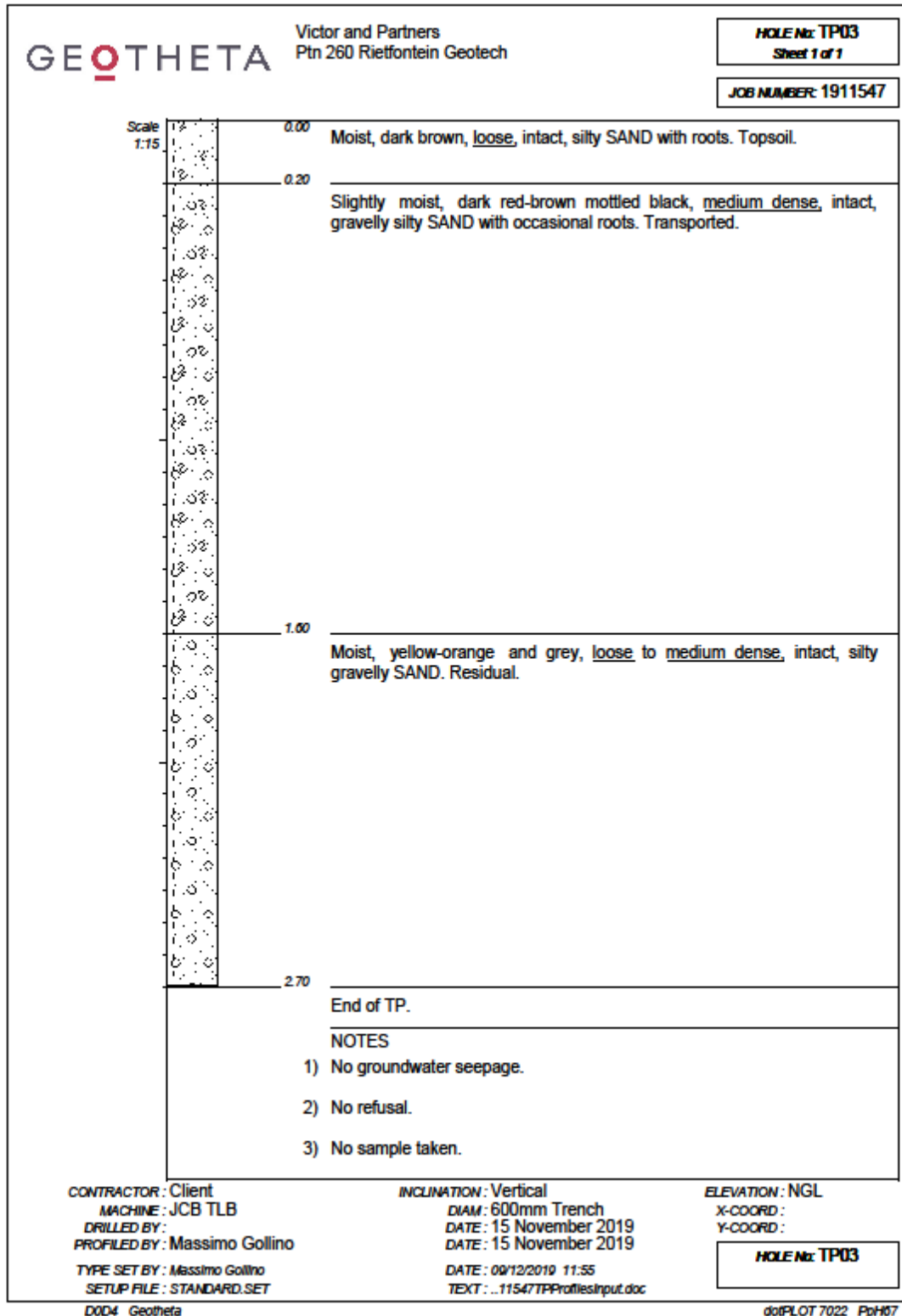
## **APPENDICES**

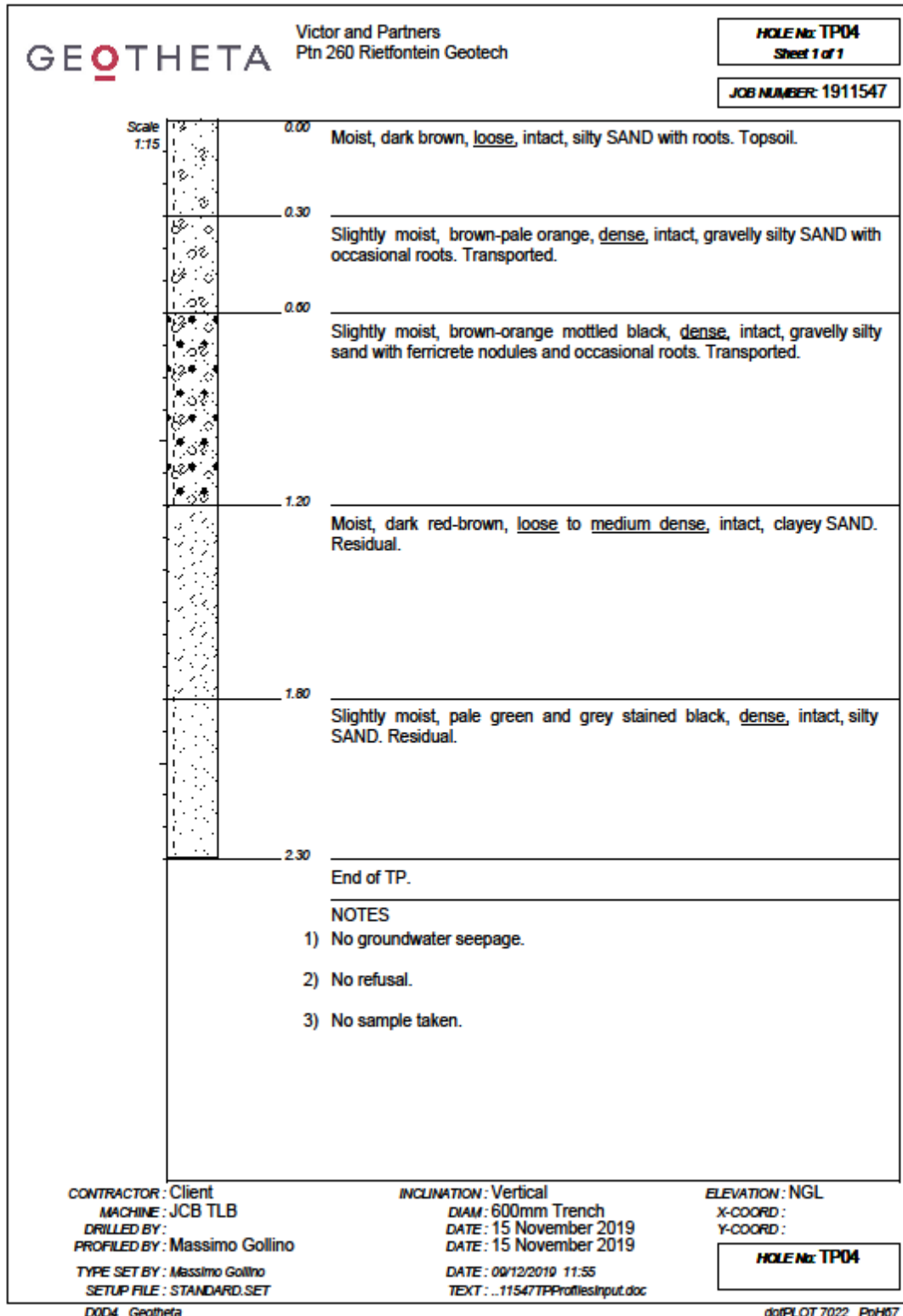
## **Appendix A: Test Pit Profiles**

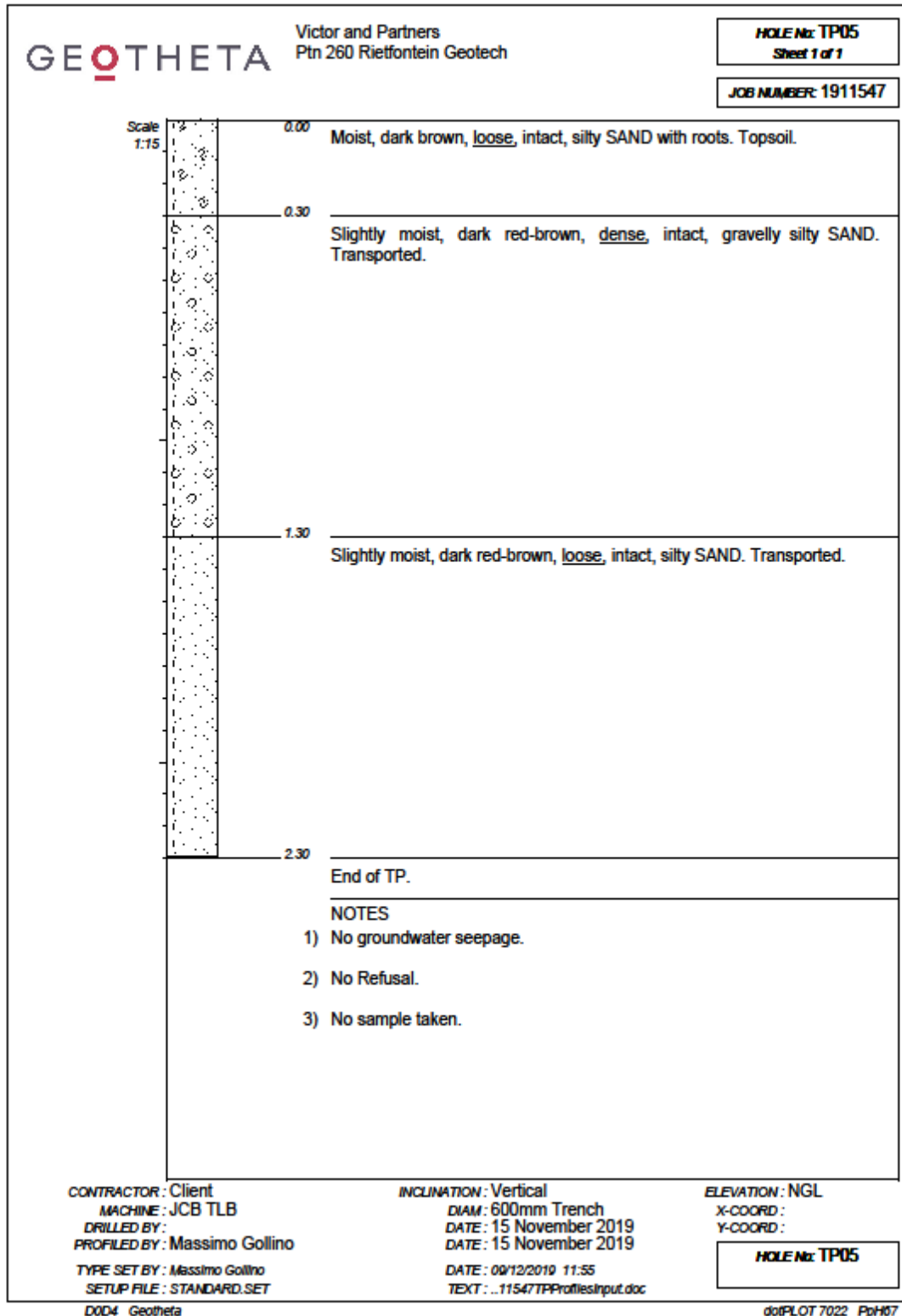


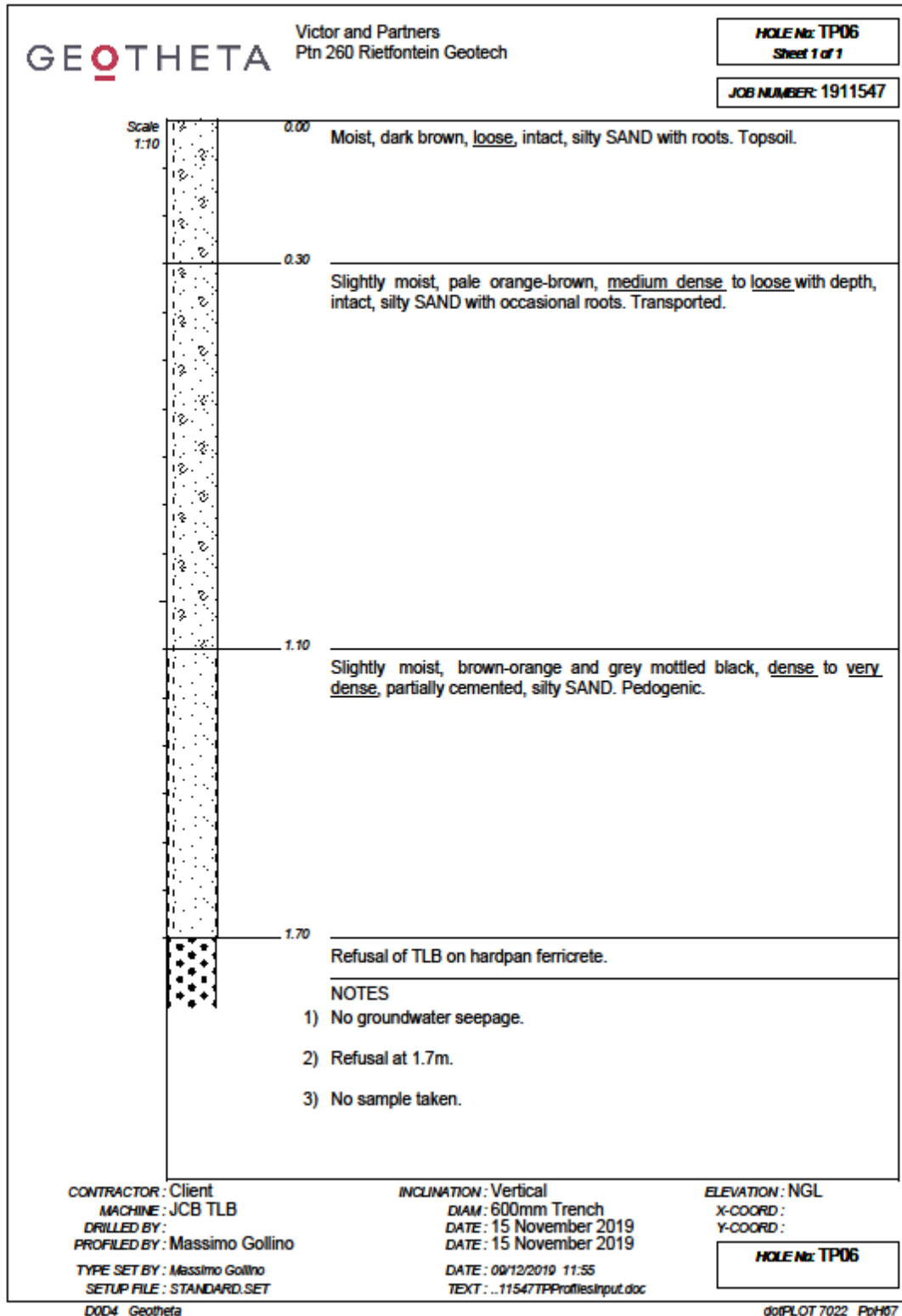


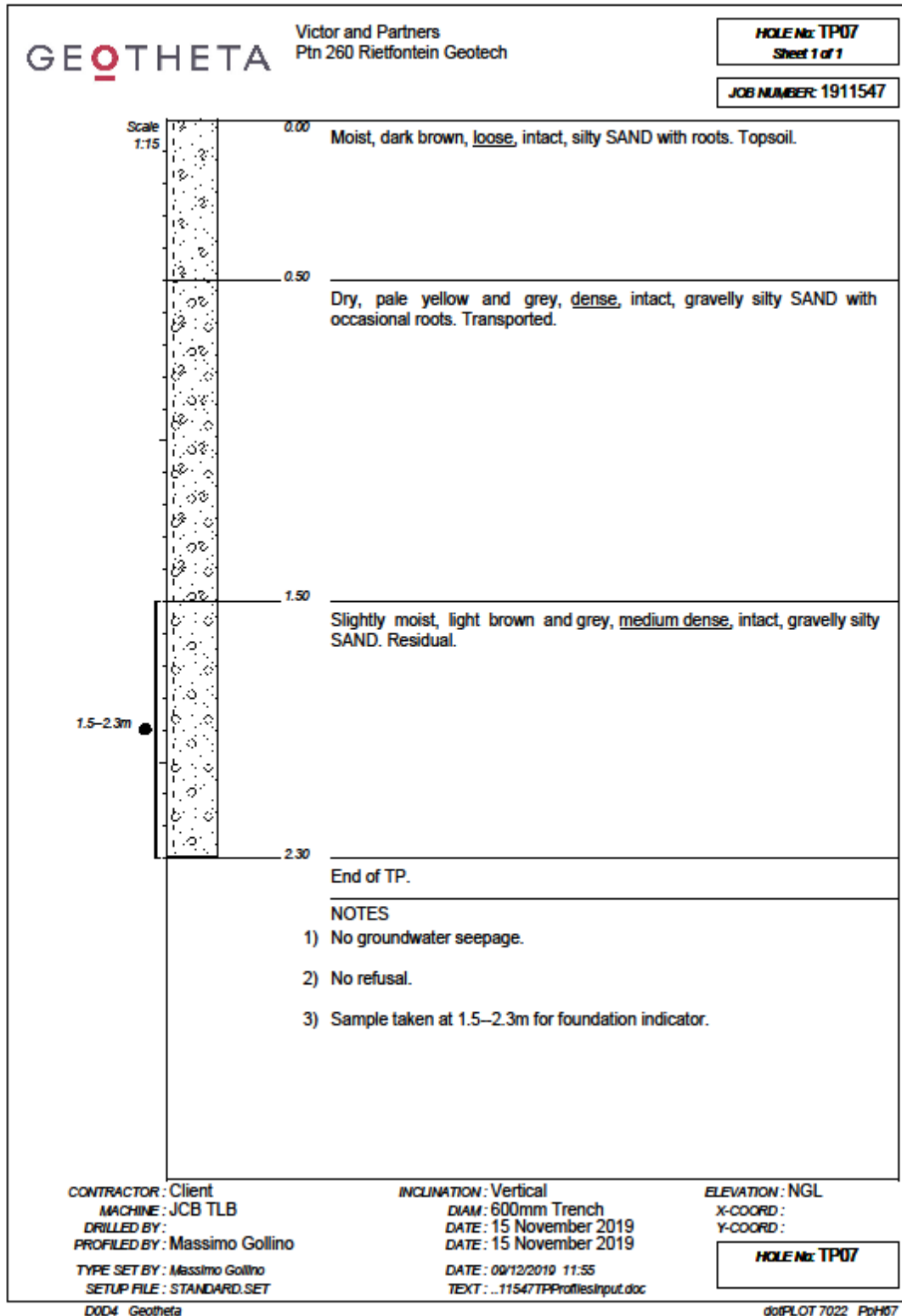












<p><b>GEOTHETA</b></p>	<p>Victor and Partners Ptn 260 Rietfontein Geotech</p>	<div style="border: 1px solid black; padding: 2px; text-align: center;"> <b>LEGEND</b> Sheet 1 of 1         </div> <div style="border: 1px solid black; padding: 2px; text-align: center; margin-top: 5px;"> <b>JOB NUMBER: 1911547</b> </div>
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<p>D0D4 Geotheta</p>		<p>dotPLOT 7022 PpH67</p>



## **Appendix B: Test Pit Photos**



**TP 1**



**TP 2**



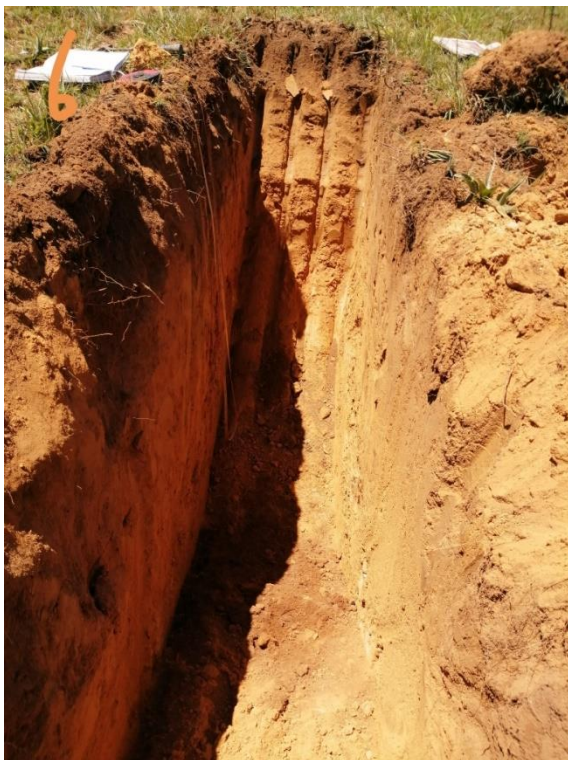
**TP 3**



**TP 4**



**TP 5**



**TP 6**



**TP7**

## **Appendix C: Laboratory Results**

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 Tel: +27 (0)11 835 3117 • Fax: +27 (0)11 835 2503



E-mail: info@civilab.co.za • Website: www.civilab.co.za

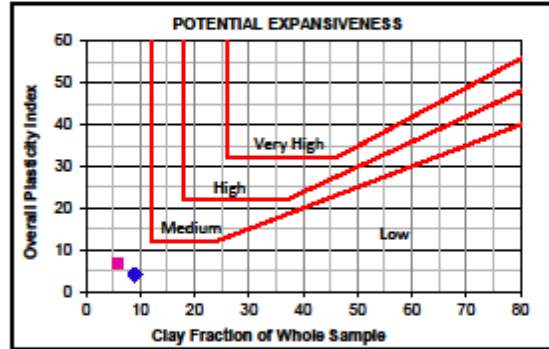
Civil Engineering Testing Laboratories

Client : GEOTHETA (PTY) LTD  
 Project : Ptn 260 Rietfontein  
 Project No : 2019-B-1948

Date Received: 15/11/2019  
 Date Reported: 06/12/2019  
 Page No. : 2 of 4

**FOUNDATION INDICATOR**

Laboratory Number	1	2
Field Number	TP2	TP7
Client Reference		
Depth (m)	1.2-2.4	1.5-2.3
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		



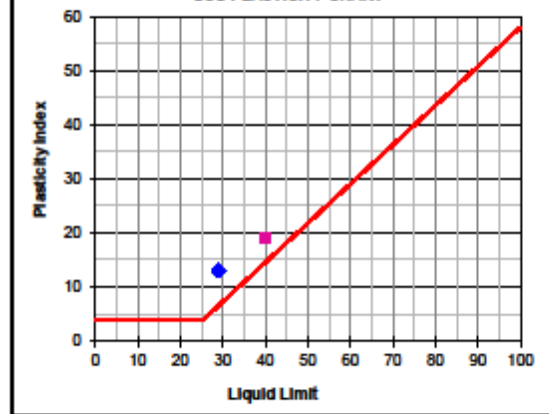
Moisture Content & Relative Density SANS 3001 GR30

Moisture Content (%)		
Relative Density (S.G.)		

Sieve Analysis (Wet Prep) SANS 3001 GR1

Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	100	100
	28 mm	100	100
	20 mm	100	100
	14 mm	100	100
	5 mm	82	98
	2 mm	59	85
	1 mm	40	65
	0.425 mm	28	37
	0.250 mm	28	37
0.150 mm	24	35	
0.075 mm	22	32	
Grading Modulus	1.91	1.46	

USC PLASTICITY CHART



Hydrometer Analysis SANS 3001 GR3

Percentage Passing	0.080 mm	19	28
	0.040 mm	15	21
	0.020 mm	13	16
	0.008 mm	10	9
	0.002 mm	9	6
Gravel	%	41	15
Sand	%	40	59
Silt	%	10	20
Clay	%	9	6

Laboratory Number 1 2

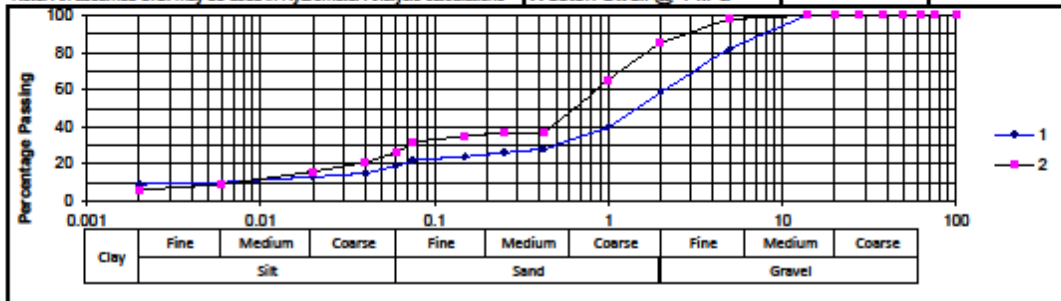
Atterberg Limits -425µ SANS 3001 GR10

Liquid Limit	%	29	40
Plasticity Index	%	13	19
Linear Shrinkage	%	6.0	8.0
Overall PI	%	4	7

Classifications

HRB (AASHTO)	A-2-6(0)	A-2-6(2)
Unified (ASTM D2487)	SC	SC
Weston Swell @ 1 kPa		

Note: An assumed S.G. may be used in Hydrometer Analysis calculations



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**Civil Engineering Testing Laboratories**

Client :	GEOETHETA (PTY) LTD	Date Received:	15/11/2019
Project :	Ptn 260 Rietfontein	Date Reported:	06/12/2019
Project No:	2019-B-1946	Page No. :	3 of 4

**MOISTURE DENSITY RELATIONSHIP**

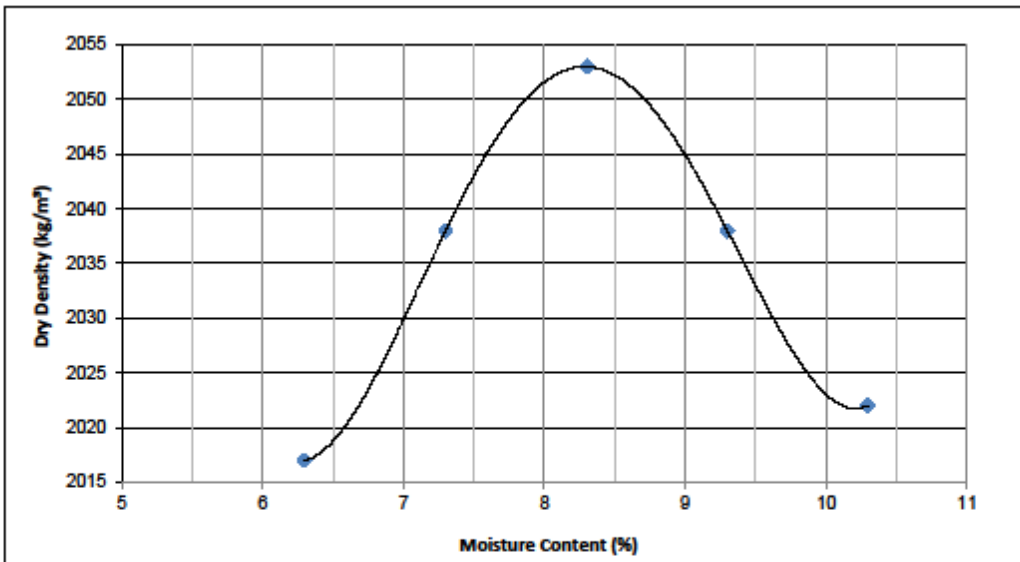
Laboratory Number	1	
Field Number	TP2	
Client Reference		
Depth (m)	1.2-2.4	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

**Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30**

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m <sup>3</sup>	2017	2038	2053	2038	2022	
Moisture Content	%	6.3	7.3	8.3	9.3	10.3	

Max. Dry Density	kg/m <sup>3</sup>	2053
Optimum Moisture	%	8.3





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**Civil Engineering Testing Laboratories**

Client : GEOTHETA (PTY) LTD

Date Received : 15/11/2019

Project : Ptn 280 Rietfontein

Date Reported : 08/12/2019

Project No. : 2019-B-1948

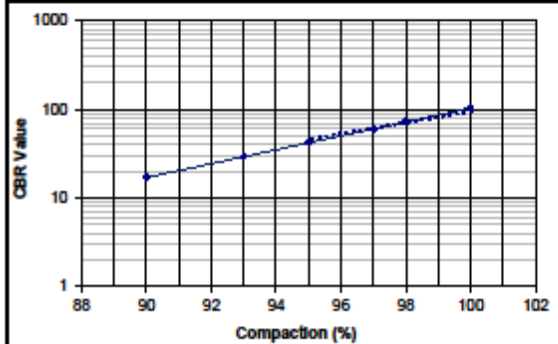
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**CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT**

Laboratory No.	1
Field Number	TP2
Client Reference	
Depth (m)	1.2-2.4
Position	
Coordinates	X Y
Description	
Additional information	
Calcrete/Crushed	
Stabilizing Agent	

Laboratory No.	1
Maximum Dry Density & Optimum Moisture Content	SANS 3001 GR30
MDD	kg/m <sup>3</sup> 2053
OMC	% 8.3
California Bearing Ratio	SANS 3001 GR40
Compaction Data	
Moisture	% 8.3
Dry Density	kg/m <sup>3</sup> 2083 1978 1874
Compaction	% 100.0 95.0 90.0
Penetration Data	
CBR at	2.50 mm 94 46 17 5.00 mm 95 43 16 7.50 mm 88 39 15
Swell	% 0.1 0.2 0.3
Final Moisture (%)	10.5 12.3 15.5

Sieve Analysis (Wet preparation)		SANS 3001 GR1
Percentage Passing		
100 mm	100	
75 mm	100	
63 mm	100	
50 mm	100	
37.5 mm	100	
28 mm	100	
20 mm	100	
14 mm	100	
5 mm	82	
2 mm	59	
1 mm	40	
0.425 mm	28	
0.250 mm	26	
0.150 mm	24	
0.075 mm	22	
Grading Modulus	1.9	

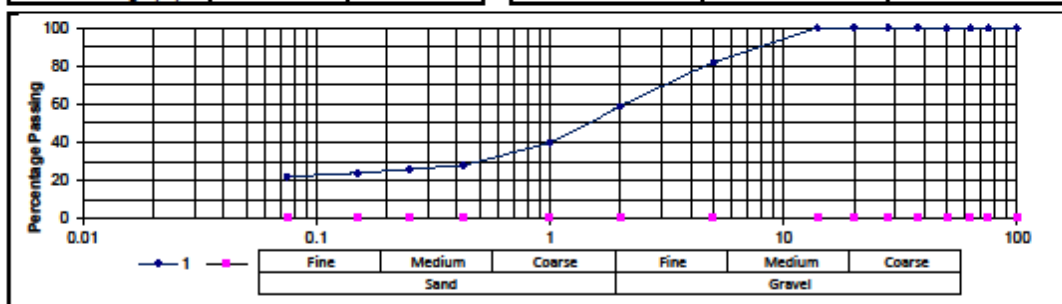


Soil Mortar Analysis	
Coarse Sand	53
Coarse Fine Sand	3
Medium Fine Sand	4
Fine Fine Sand	4
Silt and Clay	37

Interpolated CBR Data	
CBR	100% 104
	98% 73
	97% 61
	95% 42
	93% 29
	90% 17
	SANS3001 Midpoint 66

Atterberg Limits		SANS 3001 GR10
Liquid Limit (%)	29	
Plasticity Index (%)	13	
Linear Shrinkage (%)	6.0	

Classifications	
HRB (AASHTO)	A-2-6(0)
COLTO	G7
TRH14	G6



## Geotheta Report Distribution Record

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Robert Victor	Victor and Partners	Electronic	Dec '19	Ian Hammond

Approval Signature:



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