# 8.8 Surface Water Assessment

Jones & Wagener (Pty) Ltd

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# NEMA Appendix 6 requirements

Regulation: GNR 326	Description	Section in the Report
	Specialist Report	
Appendix 6 (a)	A specialist report prepared in terms of these Regulations must contain— details of— the specialist who prepared the report; and the expertise of that specialist to compile a specialist report including a curriculum vitae;	Appendix B
Appendix 6 (b)	A declaration that the specialist is independent in a form as may be specified by the competent authority;	Appendix A
Appendix 6 (c)	An indication of the scope of, and the purpose for which, the report was prepared;	Section1.2
Appendix 6 (cA)	An indication of the quality and age of base data used for the specialist report;	Section 5.6
Appendix 6 (cB)	A description of existing impacts on the site, cumulative impacts of the proposed development and levels of acceptable change;	Section 8
Appendix 6 (d)	The duration, date and season of the site investigation and the relevance of the season to the outcome of the assessment;	N/A
Appendix 6 (e)	A description of the methodology adopted in preparing the report or carrying out the specialised process inclusive of equipment and modelling used;	Section1.4
Appendix 6 (f)	Details of an assessment of the specific identified sensitivity of the site related to the proposed activity or activities and its associated structures and infrastructure, inclusive of a, site plan identifying site alternatives;	Section 7 and 8
Appendix 6 (g)	An identification of any areas to be avoided, including buffers;	Section5.5.5
Appendix 6 (h)	A map superimposing the activity including the associated structures and infrastructure on the environmental sensitivities of the site including areas to be avoided, including buffers;	Section5.5.5
Appendix 6 (i)	A description of any assumptions made and any uncertainties or gaps in knowledge;	Section 10
Appendix 6 (j)	A description of the findings and potential implications of such findings on the impact of the proposed activity or activities;	Section 8
Appendix 6 (k)	Any mitigation measures for inclusion in the EMPr;	Section 8
Appendix 6 (I)	Any conditions for inclusion in the environmental authorisation;	Section 8
Appendix 6 (m)	Any monitoring requirements for inclusion in the EMPr or environmental authorisation;	Section 11
Appendix 6 (n)	A reasoned opinion— whether the proposed activity, activities or portions thereof should be authorised;	Section 13
	(iA) regarding the acceptability of the proposed activity or activities; and if the opinion is that the proposed activity, activities or portions thereof should be authorised, any avoidance, management and mitigation measures that should be included in the EMPr, and where applicable, the closure plan;	
Appendix 6 (o)	A description of any consultation process that was undertaken during the course of preparing the specialist report;	Section5.10

Regulation: GNR 326	Description	Section in the Report
Appendix 6 (p)	A summary and copies of any comments received during any consultation process and where applicable all responses thereto; and	Section5.10
Appendix 6 (q)	Any other information requested by the competent authority.	N/A

# SPECIALIST DECLARATION

I, Malini Veeragaloo, hereby declare that:

- I act as the independent specialist in this application.
- I will perform the work relating to the application in an objective manner, even if this results in views and findings that are not favourable to the applicant.
- I declare that there are no circumstances that may compromise my objectivity in performing such work.
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act, Regulations and any guidelines that have relevance to the proposed activity.
- I will comply with the Act, Regulations and all other applicable legislation.
- I have not, and will not engage in, conflicting interests in the undertaking of the activity.
- I undertake to disclose to the applicant and the competent authority all material information in my possession that reasonably has or may have the potential of influencing - any decision to be taken with respect to the application by the competent authority; and - the objectivity of any report, plan or document to be prepared by myself for submission to the competent authority.
- All the particulars furnished by me in this form are true and correct.
- I realise that a false declaration is an offence in terms of regulation 48 and is punishable in terms of section 24F of the Act.

A detailed CV of the author included in **Appendix A**.

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MA Veeragaloo Pr Eng

### SYNOPSIS

South32 SA Coal Holdings (Pty) Ltd (South32) is the holder of an amended mining right for the Wolvekrans Colliery. The mine is located between the towns of eMalahleni and Kriel in the Nkangala District Municipality of the Mpumalanga Province.

The VDDC area of the Wolvekrans Colliery area falls within the footprint of historic underground mining operations known as Douglas Colliery. The Environmental Management Programme Report (EMPR) for the Douglas Colliery operations was amended and approved in 2007, to allow the opencast mining of the remaining coal reserves (extraction of remaining pillars, roof and floor) via opencast mining.

The mine has an original Environmental Authorisation (EA) (previously referred to as an approved Environmental Management Programme Report (EMPR)) dated February 2006 for opencast mining operations on the farms Steenkoolspruit 18 IS, Kleinkopje 15 IS and Vandyksdrift 19 IS. Applications for the dewatering of the flooded No. 2 seam workings were compiled and submitted in August 2016. Additional infrastructure is required in support of opencast mining of the pillars at the Vandyksdrift Central (VDDC) section of the Wolvekrans Colliery. However, planning for this infrastructure had not yet been undertaken, and it was therefore not included in the applications at the time.

Jones & Wagener Engineering and Environmental Consultants (J&W) was appointed by South32 as an independent Environmental Assessment Practitioner (EAP) to undertake an Integrated Regulatory Process (IRP) to obtain the required approvals/authorisations for the proposed infrastructure and mining development at the VDDC section.

Various specialist studies are required to support the regulatory process. One of the required studies is a surface water specialist study.

#### Study Approach

This surface water study entails a review characterising the surface water regime at the site and the catchment in which it resides, in terms of surface water quality and quantity.

It is important to note that Golder Associates updated the overall water balance for Wolvekrans Colliery to include the VDDC infrastructure and mining project (including areas that are authorised but does not form part of this environmental application process) (please refer to Report : "Inclusion of VDDC water management into Wolvekrans site wide water management plan", July 2019, Report number 19124625-327233-1). Input, in terms of the pit water make and surface runoff from the proposed infrastructure and mining areas were provided by J&W to Golder Associates.

An assessment of the impacts of the project on surface water, in terms of both quality and quantity, was conducted, as well as an assessment of the mitigation of the impacts. The method by which the impacts are quantified is to first assess the impact assuming no mitigation measures are applied, in order to provide a "worst case" scenario, thereafter the mitigation measures are evaluated and the residual impact indicated.

#### Study Area

The VDDC infrastructure development project is a brownfields project within the greater Wolvekrans Colliery mining right area. Wolvekrans Colliery is located between the towns of eMalahleni and Kriel, within the jurisdictional area of the eMalahleni Local Municipality (ELM) and the Nkangala District Municipality (NDM) of the Mpumalanga Province. The mine is situated approximately 30 km south-east of the town of eMalahleni, in close proximity to the Duvha Power Station.

VDDC is located on the western boundary of Wolvekrans Colliery. The Olifants River forms the southern boundary of this mining section.

### Proposed Infrastructure

The new infrastructure to be developed (and which will be the subject of the IRP) includes:

- Topsoil dumps.
- Overburden dumps.
- ROM stockpiles and mixed ROM coal and slurry stockpile areas.
- The existing explosives magazine will be relocated to the north of Pit 4.
- New roads required for the VDDC project include:
  - Temporary high wall roads and dragline walkways which will be re-established as mining progresses;
  - Earth Moving Equipment (EME) haul roads (40 m width) from the bottom of box cut ramps to the existing haul roads;
  - Additional maintenance/service and access roads within the VDDC project area from the existing infrastructure to the box-cut;
  - New haul road to the No. 4 seam and No. 5 seam stockpiles.
- EME hard park and brake test ramp.
- Access control and security fencing
- Access control will be through the existing control measures.
- Triple security fencing will be provided at the explosives magazine. Triple fencing includes a triple barrier of 2.4 m high clear mesh, electric and normal security fencing. Electric fencing is connected to the local security system (South32, 2017b).
- Equipment, including water bowsers for dust suppression.
- Other infrastructure would include:
  - Opencast pit areas not previously authorised.
  - In pit sumps.
  - Proposed modular Water Treatment Plant (WTP).
  - Mechanical evaporators. The evaporators will be operated at 30 % efficiency.
  - Clean and dirty water canals and pipelines.
  - Future coal plant infrastructure area.

The existing PSS and LAC dumps are currently reclaimed and processed within the existing VDD processing plant. As mining progresses, this plant will need to be relocated. An area has been allocated for this purpose and is situated to the south of the proposed new overburden dump in the south-eastern corner of the VDDC area.

- The remainder of the supporting infrastructure is mostly catered for by the existing SKS complex facilities. Existing change houses, stores facilities, office facilities, tracked vehicle workshops, LDV workshops will be used.
- No additional fuel or lube storage area, servicing bays or tyre bays are required.

#### Baseline Assessment

Information for the baseline assessment was abstracted from the November 2013 Surface Water Impact Study compiled by SRK for the VDDC Dewatering Project (Report Number 449019) as well as the 2004 Surface Water Study carried out by J&W for the Douglas Pillar Project EMPR (Report Number JW188/04/9347).

In terms of surface water quantity, the above information remains valid and is sufficient for the purposes of the baseline update. The floodlines for the area is more than 5 years old and South32 is in the process of updating these at the time of writing. However, it is not anticipated that the VDDC pit will encroach on the updated floodline and therefore the impacts assessed in this report will still remain relevant.

In terms of surface water quality within the study area there are visible impacts associated with mining activities both upstream and downstream of VDDC.

#### Water balance

The old 2 Seam underground workings have filled with water. This area will need to be dewatered prior to mining the VDDC pit and is therefore a key to the success of the proposed project.

The current plan is to make extensive use of mechanical evaporators to manage the pit water make and dewatering water from VDDC. The VDDC pit water balance as well as the estimated surface runoff, that can be expected from the proposed infrastructure areas was computed by J&W as input to the overall site wide water balance compiled by Golder Associates.

The water management plan for VDDC impacts on the site wide water balance as some of the infrastructure and mine workings such as Vleishaft Dam and Steenkoolspruit are planned to be used to manage the VDDC mine water make.

The total water make to be managed for the pit is estimated as follows:

- VDDC Opencast area:
  - Average water make over LOM =  $4 760 \text{ m}^3/\text{day}$ ;
  - Peak summer water make =  $12\,950$  m<sup>3</sup>/day.

As mentioned above, Golder Associates were appointed to update the site wide water management model for the Wolvekrans Colliery to include the mine plan and catchment areas from the VDDC feasibility study with the above input provided by J&W.

- The following conclusions have been extracted from the Golder Associates report:
  - The dewatering rates during 2020 and 2021 are estimated to be about 27 000 m<sup>3</sup>/d. During this period the site wide water balance model showed that the planned installed evaporator capacity will be insufficient to manage the water. South32 should consider installing the 8 evaporators at SKS by November 2019.
  - The extensive use of the evaporators will result in salt buildup in the water bodies over which the evaporators are spraying. Therefore, monitoring of salination of water due to brine evaporation will need to be undertaken and corrective action carried out if need be.
  - Vleishaft Dam is expected to spill during the period 2020 to 2022 which is during the initial VDDC dewatering period. The spills will report to the SKS pit. During this initial dewatering period, Golder Associate's model estimates that the SKS pit will decant into the adjacent Glencore workings. Therefore, the evaporators at SKS pit should be installed earlier than the planned implementation date of May 2020. After 2029, the 18 000 m<sup>3</sup>/d of evaporator capacity installed at SKS pit will draw down the water level in the pit.

# Impact Assessment

Location	Catchment area (km²)	MAR Pre- Construction (x10 <sup>6</sup> m <sup>3</sup> )	MAR during operations (x10 <sup>6</sup> m <sup>3</sup> )	Percentage reduction (%)
VDDC opencast pit	11.4	0.36	0	100
New proposed infrastructure	1.6	0.05	0	100
Extension/replacem ent of existing infrastructure	1.4	0.04	0	100
VDDC Infrastructure and mining project in total	14.5	0.45	0	100
Olifants River Downstream of the mine property	3309	188.1	187.65	0.24
Witbank Dam	579	190	189.5	0.24*

The loss of yield is quantified in the following table:

\* Note: The runoff calculations are not accurate to three decimal places. However, the values remain indicative of the magnitude of the impact.

It is evident from the table above that the impact in surface water yield to the most downstream watercourse and Witbank Dam is <u>LOW</u>.

Impact on water quality with the mitigation measures described in the impact assessment, is considered to be **HIGH** to **LOW** in relation to the anticipated future activities in the area.

The surrounding and downstream surface water resources, namely the Olifants River, are considered stressed water resources in terms of both the quantity of water in the system and the quality of the water. The Olifants River also forms part of the water supply for irrigation water further downstream (from the Witbank Dam). Any impact on the quantity or quality of water in the system has the potential to affect the quality and assurance of supply to the community and agriculture.

The cumulative impact of the VDDC mining operation extension, with the mitigation measures described in the impact assessment, is considered to be **MEDIUM** to **HIGH** in relation to the current and anticipated future activities in the area, as the catchment is already impacted by mining activities.

# SOUTH32 SA COAL HOLDINGS (PTY) LTD

# VANDYKSDRIF CENTRAL (VDDC) MINING: INFRASTRUCTURE DEVELOPMENT SPECIALIST SURFACE WATER STUDY <u>REPORT NO: JW188/18/G535</u> – Rev <u>1</u>

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# Abbreviations used

BEEH	Bio-resources Engineering and Environmental Hydrology
BPG	Best Practise Guidelines
DMR	Department of Mineral Resources
DWA	Department of Water Affairs
DWAF	Department of Water Affairs and Forestry
DWS	Department of Water and Sanitation
DWF	Dry Weather Flow
EA	Environmental Authorisation
EAP	Environmental Assessment Practitioner
EC	Electrical Conductivity
EIA	Environmental Impact Assessment
EIAR	Environmental Impact Assessment Report
EMPr	Environmental Management Programme
EMPR	Environmental Management Program Report
GN	Government Notice
GNR	Government Notice Regulation
ICFR	Institute for Commercial Forestry Research
IRP	Integrated Regulatory Process
IUA	Integrated Unit of Analysis
IWULA	Integrated Water Use Licence Application
IWWMP	Integrated Water and Waste Management Plan
J&W	Jones & Wagener
LoM	Life of Mine
mamsl	<b>m</b> etres <b>a</b> bove <b>m</b> ean <b>s</b> ea level
MAP	Mean Annual Precipitation
MAR	Mean Annual Runoff
NEMA	National Environmental Management Act
NEM:WA	National Environmental Management: Waste Act
NWA	National Water Act, 1998 (Act 36 of 1998)
PCD	Pollution Control Dam
RMF	Regional Maximum Flood
ROM	Run Of Mine
RQO	Resource Quality Objectives
SANCOLD	South African National Commission on Large Dams
SANS	South African National Standard
SAWS	South African Weather Service
SCS	Soil Conservation Services
SDF	Standard Design Flood
I	

South32	South32 SA Coal Holdings (Pty) Ltd
SS	Suspended Solids
SKS	Steenkoolspruit
TDS	Total Dissolved Solids
TWQG	Target Water Quality Guidelines
WR05	Surface Water Resources of South Africa 2005
WR90	Surface Water Resources of South Africa 1990
WRC	Water Resource Commission
WTP	Water Treatment Plant



# SOUTH32 SA COAL HOLDINGS (PTY) LTD

VANDYKSDRIF CENTRAL (VDDC) MINING: INFRASTRUCTURE DEVELOPMENT SPECIALIST SURFACE WATER STUDY REPORT NO: JW188/18/G535 - Rev 1

#### 1. INTRODUCTION

#### 1.1 Background

South32 SA Coal Holdings (Pty) Ltd (South32), is the holder of an amended mining right for coal, granted by the Minister of Mineral Resources, in terms of the Mineral and Petroleum Resources Development Act (MPRDA) and notarially executed on the 21 May 2015 under DMR reference MP30/5/1/2/2/379MR, in respect of its Wolvekrans – Ifalethu Colliery. This mining right comprises of the following areas:

- Ifalethu Colliery (previously referred to as Wolvekrans North Section<sup>1</sup>) consisting of the Hartbeestfontein, Bankfontein (mining ceased), Goedehoop, Klipfontein sections and the North Processing Plant; and
- Wolvekrans Colliery (previously referred to as the Wolvekrans South Section) Wolvekrans, Vlaklaagte consisting of the (mining ceased), Driefontein, Boschmanskrans, Vandyksdrift, Albion and Steenkoolspruit sections, as well as the South Processing Plants (Eskom and Export). Some of these areas were previously known as Douglas Colliery.

The Vandyksdrift Central (VDDC) area falls within the footprint of historic underground mining operations at the old Douglas Colliery. In 2007, an amendment of the Environmental Management Programme Report (EMPR) for the Douglas Colliery operations was approved, to allow pillar mining (opencast) of the area previously mined by underground bord and pillar mining. Authorisation of the VDDC mining project included the following:

- Opencast operation on the farm Kleinkopje 15 IS;
- Opencast operation on the farm Steenkoolspruit 18 IS;
- Pillar extraction operation on the farm Vandyksdrift 19 IS;
- Reclamation of existing slurry ponds; and
- Rewashing of existing discard dumps (PHD, 2006).



<sup>&</sup>lt;sup>1</sup> This was previously referred to as Middelburg Colliery

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The water uses associated with the opencast mining have been authorised in terms of Water Use Licence (WUL) number 24084535 dated 10 October 2008, issued to Douglas Colliery Services Limited.

The No. 2 seam workings are flooded with water and must be dewatered to enable the open pit development to proceed. A dewatering strategy has therefore been developed and an application for Environmental Authorisation (EA) of the dewatering activities was submitted to the Department of Mineral Resources (DMR) (Jaco-K Consulting, 2016(a)); a decision in this regard is pending. The water use activities associated with this upfront dewatering strategy have been authorised by WUL number 06/B11F/GCIJ/7943 dated 19 July 2018.

The 2007 approved EMPR Amendment included limited additional infrastructure in support of the opencast mining operations, as it was assumed at that stage that existing infrastructure will be used. In addition, the applications for authorisation of the activities associated with the dewatering strategy, were limited to the infrastructure to facilitate dewatering (i.e. dewatering boreholes, pumps, pipelines, storage tanks, mechanical evaporators, roads and power lines).

A pre-feasibility investigation has since been conducted, and the need to develop additional infrastructure to support the proposed opencast mining was identified. The additional infrastructure includes the following:

- Storm water management structures (drains and berms);
- Water management measures for the management of mine impacted water;
- Overburden dumps;
- Run of Mine (ROM) coal stockpile areas;
- Mixed ROM coal and slurry stockpile areas;
- Topsoil stockpiles following clearance of vegetation;
- Pipelines for the conveyance of water;
- Hard park area and brake test ramp; and
- Haul roads and service roads.

The proposed VDDC opencast pit boundary as determined through the pre-feasibility investigation also differs from the mining area approved in the 2007 EMPR amendment. An area of approximately 196 hectares in the latest mine lay-out was not included in the previous mine lay-out and is therefore not approved to be opencast mined.

Jones & Wagener Engineering and Environmental Consultants (J&W) was appointed by South32 as an independent Environmental Assessment Practitioner (EAP) to undertake an Integrated Regulatory Process (IRP) to obtain the required approvals/authorisations for the proposed infrastructure and mining development at the VDDC section.

Various specialist studies are required to support the regulatory process, one of which is a specialist surface water study.

#### 1.2 Terms of reference

The terms of reference for the specialist surface water study are summarised below. Specific components to be addressed include the following:

#### 1.2.1 **Baseline** assessment

The objective of the baseline study is to characterise the surface water regime at the site and the catchments in which it resides in terms of surface water quantity and quality.

Information for the baseline assessment was abstracted from the November 2013 Surface Water Impact Study compiled by SRK for the VDDC Dewatering Project (Report Number 449019) as well as the 2004 Surface Water Study carried out by J&W for the Douglas Pillar Project EMPR (Report Number JW188/04/9347). In terms of surface water quantity, the above information remains valid and is sufficient for the purposes of the baseline update, with the exception of additional surface water quality information, which was made available by South32. In addition to the above the floodlines for the area is more than 5 years old and South32 is in the process of updating these at the time of writing.

Please note that the surface water study does not include the delineation of sensitive areas such as pans and wetlands, or the assessment of aquatic ecology. Information regarding the aquatic ecology, pans and wetlands is included in separate specialist studies.

#### 1.2.2 Site water management

This includes the compilation of a conceptual surface water management plan to mitigate the identified impacts, as well as the development of a surface water monitoring protocol. This includes the provision of information on the management of surface water around the planned activities, as well as the identification of pollution point sources.

The objective is to ensure compliance with legislation in terms of the management of both storm water and water affected by planned activities. The separation of clean and dirty water, with the diversion of clean water around dirty areas and the containment of dirty water on site, is necessary in order to achieve compliance.

#### 1.2.3 Mine water balance

This includes the compilation of a site water balance in GoldSim and water flow diagrams for the proposed VDDC infrastructure areas only. The water balance was therefore limited to the proposed activities at VDDC.

It is important to note that Golder Associates has updated the overall water balance for Wolvekrans Colliery to incorporate the VDDC mining and infrastructure project. Input, in terms of the pit water make and surface runoff from the proposed infrastructure areas, was conducted by J&W and provided to Golder Associates.

The objective of the water balance is to quantify the water make over the life of the mine, during operations and post closure.

#### 1.2.4 Impact assessment

This includes an assessment of the impact of the project and its components on surface water in the study area, in terms of both water quality and water quantity.



In addition, this includes the formulation of proposed mitigation measures for significant impacts, as well as monitoring required to measure the success of the mitigation measures, once implemented. The residual impact after implementation of the mitigation measures was also quantified.

# 1.3 Study area

The VDDC infrastructure development project is a brownfields project within the greater Wolvekrans Colliery mining right area. Wolvekrans Colliery is located between the towns of eMalahleni and Kriel, within the jurisdictional area of the eMalahleni Local Municipality (ELM) and the Nkangala District Municipality (NDM) of the Mpumalanga Province. The mine is situated approximately 30 km south-east of the town of eMalahleni, in close proximity to the Duvha Power Station. Locality plan given in **Figure 1.1.a** above.

VDDC is located on the western boundary of Wolvekrans Colliery. The Olifants River forms the southern boundary of this mining section.

The proposed infrastructure and mining development will take place on the farms Kleinkopje 15 IS, Vandyksdrift 19 IS, Wolvekrans 17 IS and Steenkoolspruit 18 IS.

# 1.4 Approach and methodology

The following actions were taken as part of the surface water specialist study for this project:

Information received from South32 as well as the design engineers (i.e. Worley), was reviewed and relevant issues were noted.

- Rainfall data was obtained from the Institute for Commercial Forestry Research (ICFR) database and the South African Weather Service (SAWS) and will be processed for use in the water balance modelling. In addition to this Golder Associates provided the critical stochastically generated rainfall for the water balance.
- Topographical maps and satellite imagery (Google Earth) were reviewed to assess the study area.
- Peak flood flows at relevant locations within the study area were extracted from previous studies undertaken in the area.
- Water quality data received from South32 was reviewed, collated and assessed.
- A site-specific water balance model was developed for the VDDC infrastructure areas. The water balance modelled the VDDC pit water balance (i.e. estimated pit water make over the Life of Mine (LOM)), as well as the estimated surface runoff, that can be expected from the proposed infrastructure areas, for the proposed VDDC infrastructure development project.
- Sketches and a description of the pollution control strategies around the various point sources was compiled using the storm water management proposed by the design engineers, Worley.
- The potential impacts associated with the proposed mining and related activities will be assessed according to the methodology stipulated by the lead environmental consultant (J&W). Impacts will be assessed for the construction, operational, decommissioning and post closure phases. Potential impacts will be detailed, then mitigation measures described, with residual impacts then being assessed.



# 2. LEGISLATIVE ASPECTS

# 2.1 Regulatory Requirements

The Acts and Regulations that pertain to the surface water for mining projects include:

- The Constitution of the Republic of South Africa, 1996 (Act 108 of 1996).
- The Mineral and Petroleum Resources Development Act, 2002 (Act 28 of 2002).
- The Mineral and Petroleum Resources Development Amendment Act, 2008 (Act 49 of 2008).
- The National Water Act, 1998 (Act 36 of 1998) (hereafter referred to as NWA).
- The National Environmental Management Act, 1998 (Act 107 of 1998) (hereafter referred to as NEMA).
- National Environmental Management: Waste Act, 2008 (Act 59 of 2008) (NEM:WA).
- Government Notice (GN) R704 of 4 June 1999: Regulation on use of water for mining and related activities aimed at the protection of water resources (hereafter referred to as GN R704).
- GN R139 of 24 February 2012: Regulations regarding the safety of dams in terms of Section 123(1) of the NWA.
- GN R991 of 18 May 1984: Requirements for the purification of waste water or effluent.
- GN 399 dated 26 March 2004: General Authorisations in terms of Section 39 of the NWA: S21(a) and (b) water uses, as extended in GN 970 dated 30 November 2012: Extension of time period for General Authorisations in terms of Section 39 of the NWA: S21(a) and (b) water uses – until withdrawn by Notice in the Government Gazette.
- GN 509 dated 27 July 2016: General Authorisation in terms of Section 39 of the NWA for water uses as defined in S21(c) or section 21(i).
- GN R324 to 327 of April 2017: NEMA EIA Regulations 2014, as amended.
- GN R636 of August 2013: National norms and standards for disposal of waste to landfill, in terms of NEM:WA.
- GN 466 of April 2016: Classes and Resource Quality Objectives for water resources in the catchment of the Olifants River, in terms of S13(4) of the NWA.

# 2.2 Applicable policies and/or guidelines

The following DWAF Best Practice Guideline (BPG) documents are relevant to this project:

- BPG for Water Resource Protection in the SA Mining Industry, Series A: Best Practice Guideline A2: Water Management for Mine Residue Deposits, July 2008
- BPG for Water Resource Protection in the SA Mining Industry, Series A: Best Practice Guideline A4: Pollution Control Dams, August 2007
- BPG for Water Resource Protection in the SA Mining Industry, Series A: Best Practice Guideline A6: Water Management for Underground Mines, July 2008
- BPG for Water Resource Protection in the SA Mining Industry, Series G: Best Practice Guideline G1: Storm Water Management, August 2006
- BPG for Water Resource Protection in the SA Mining Industry, Series G: Best Practice Guideline G2: Water and Salt Balances, August 2006



- BPG for Water Resource Protection in the SA Mining Industry, Series G: Best Practice Guideline G3: Water Monitoring Systems, July 2007
- BPG for Water Resource Protection in the SA Mining Industry, Series G: Best Practice Guideline G4: Impact Prediction, December 2008
- BPG for Water Resource Protection in the SA Mining Industry, Series G: Best Practice Guideline G5: Water Management Aspects for Mine Closure, December 2008
- BPG for Water Resource Protection in the SA Mining Industry, Series H: Best Practice Guideline H1: Integrated Mine Water Management, December 2008
- BPG for Water Resource Protection in the SA Mining Industry, Series H: Best Practice Guideline H2: Pollution Prevention and Minimization of Impacts, July 2008
- BPG for Water Resource Protection in the SA Mining Industry, Series H: Best Practice Guideline H3: Water Reuse and Reclamation, June 2006.

# 3. <u>DETAILS OF THE APPLICANT AND ENVIRONMENTAL ASSESSMENT</u> <u>PRACTITIONER</u>

# 3.1 Details of the Applicant

**Table 3.1.a** below provides the details for the applicant responsible for the environmental applications for the proposed project.

# Table 3.1.a:Applicant details.

Project applicant:	South32 SA Coal Holdings (Pty) Ltd: Wolvekrans Colliery		
Trading name (if any):	South32 SA Coal Holdings (Pty) Ltd		
Contact person:	Thembani Mashamba		
Postal address:	P.O Box 61820, Marshalltown, 2107		
Email:	thembani.mashamba@south32.net	Tel:	011 376 2705

# 3.2 Details of the environmental consultant

The details of the EAP responsible for the IWULA in respect of this project are provided in **Table 3.2.a** below.

# Table 3.2.a:Environmental consultant details.

Environmental consultant	Jones & Wagener (Pty) Ltd				
Contact person:	Tolmay Hopkins				
Postal address:	PO Box 1434, Rivonia, 2128				
Email:	tolmay@jaws.co.za	Tel:	011 519 0200	Fax:	011 519 0201

# 3.3 Details of the surface water specialists

The details of the Surface Water Specialist responsible for the Specialist Surface Water Study in respect of this project are provided in **Table 3.3.a** below. Details of the J&W project team members and their relevant experience are provided in **Table 3.3.b**.

# Table 3.3.a:Specialist consultant contact details

Specialist consultant	Jones & Wagener (Pty) Ltd				
Contact person:	Malini Veeragaloo				
Postal address:	PO Box 1434, Rivonia, 2128				
Email:	moodley@jaws.co.za	Tel:	011 519 0200	Fax:	011 519 0201



Name	Email address	Experience	Responsibility
Malini Veeragaloo	moodley@jaws.co.za	BSc (Eng) 10 years experience	Water Balance and Surface Water Specialist Report
Michael Palmer	palmer@jaws.co.za	Pr Eng, MSc Eng Civil 20 years experience	Project Director Review of: Surface Water Specialist Report



# 4. DESCRIPTION OF THE PROJECT

# 4.1 **Project location**

Project location is given in section 1.3 above.

# 4.2 General description

The VDDC area was identified as the most likely coal source to replace the Steenkoolspruit (SKS) operations, and to fulfil the current contracts and market obligations of the mining complex (South32, 2017a).

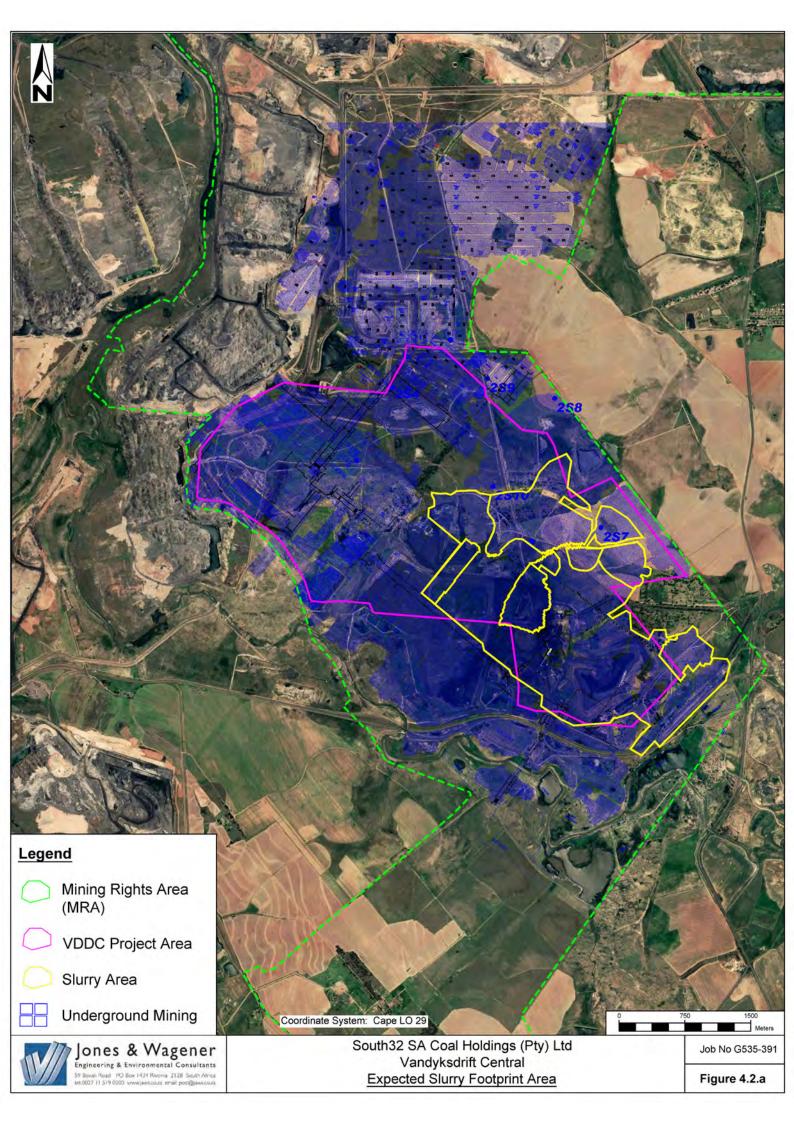
Coal produced will be mainly exported through the Richards Bay coal terminal.

Limited opencast mining was done before 1990 in the top shallower No. 5 seam. The No. 4L, No. 2, No. 2A and No. 1 coal seams were exploited in the past by means of underground mining. All underground operations were terminated during October 2008. The No. 2 Seam is the principal seam in the project area and its thickness can exceed 9 m, but only the lower select horizon of higher quality 2.5 m – 4.5 m was previously extracted. The targeted mineable seams are the No. 5, No. S4UA, No. S4L, No. S2RP, No. S2A and No. S1 seams respectively (Southt32, 2017a).

As a result of the previous mining of the No. 2 Seam horizon by bord and pillar means, the following has resulted:

- The majority of the underground No. 2 seam workings are flooded because of water ingress from both surface and underground aquifers. A dewatering programme will be implemented before opencast mining operations commence.
- An area of the No. 2 Seam was historically used for placement of slurry from the processing plant. It is believed to be contained in the southeast portion of the deposit by underground seals and barrier pillars (the expected slurry footprint is indicated in Figure 4.2.a).





# 4.3 Surface infrastructure

4.3.1 Existing infrastructure

Existing infrastructure in the VDDC area is shown on **Figure 4.3.1.a** and includes the following:

Access, transport and logistics

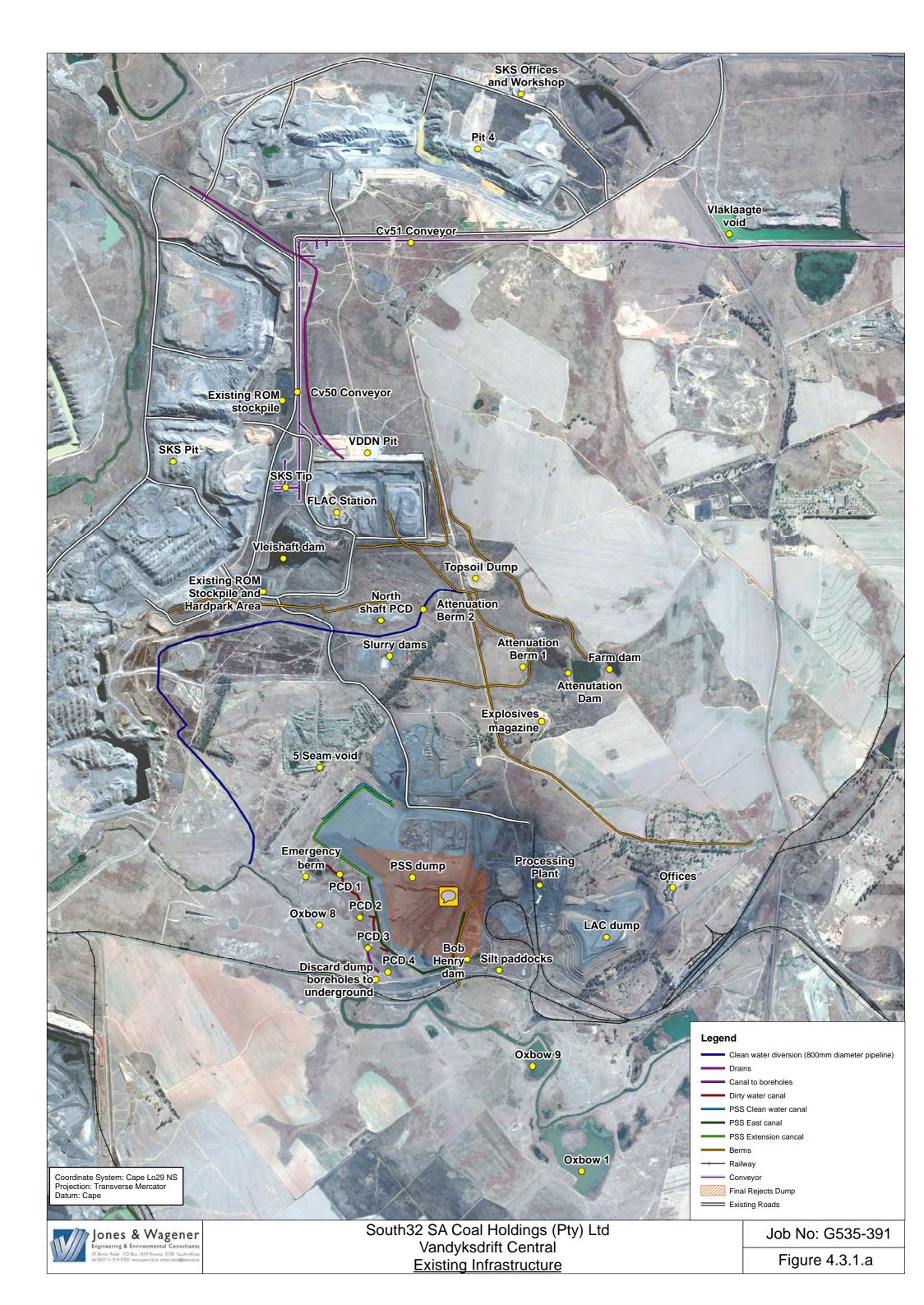
Access to the VDDC project area is via one of three existing approaches, depending on the size of the transport, namely:

- Current SKS main entrance: All personnel transport, light delivery vehicles and heavy delivery vehicles up to 10 t single body trucks;
- Current Wolvekrans main entrance (via Boschmanskrans (BMK) workshops): Heavy delivery vehicles and lowbeds; and
- Current VDD main entrance (opposite Springbok village): Heavy delivery vehicles and lowbeds.
- Existing haul roads;
- Existing personnel vehicle parking;
- Existing bus turnaround;
- Existing facilities at the SKS operations:
  - o ROM tip and the overland conveyor system to the South Export Plant;
  - The SKS complex offices, warehouse, change houses, workshops, wash bays, laydown areas, a sewage treatment plant and fuelling facilities.
  - The southern SKS facilities currently in use by the Vandyksdrift North (VDDN) operation include contractors' offices, laydown areas, as well as a fuel, lube, air and coolant (FLAC) station.
- Existing topsoil dump is located on the north-eastern boundary of the VDDC section;
- Existing surface dumps:

Surface discard dumps exist on the southern portion of the VDDC resource area, namely the PSS and LAC dumps. These dumps are in the process of being reclaimed and it is expected that approximately 40% of the material will be recovered. Final rejects from the reclamation process is disposed of on the southern portion of the PSS dump on the Final Rejects Dump.

- Two existing ROM coal stockpiles have been developed:
  - A ROM coal pad located between the SKS void and the haul road, from where it is taken to the South Export Processing Plant via conveyors from the SKS crushing plant;
  - A ROM stockpile area to the south of the Vleishaft Dam, of which a portion is currently used as a hard park area.





• Existing power supply:

The VDDC section is supplied from Eskom's Klein 132 kV Substation, which feeds the DMO Klein Olifant 132 kV Substation. The voltage is stepped down to 22 kV via two 20 MVA power transformers feeding the 22 kV switchgear located in the Klein Olifant Substation (South32, 2017b).

The existing electricity infrastructure is shown on Figure 4.3.1.b.

A section of the Klein-Kromfontein 132 kV powerline must be relocated to allow opencast mining to proceed. This is the subject of a separate application that is undertaken by South32 in terms of a self-build agreement with Eskom. The EA for the powerline will be transferred to Eskom on completion of the construction phase.

Upfront dewatering infrastructure

In order to mine the VDDC reserve, the water contained in the underground workings must be removed prior to mining. This will be achieved by drilling a number of boreholes into the old underground workings and to abstract the water via these boreholes.

Water will be pumped from the boreholes accessing different underground compartments and will be transferred via borehole connector pipelines to the Vleishaft Dam and/or directly to the evaporation tanks that will be located at the evaporation sites where water will be evaporated using mechanical evaporators. Three evaporators sites have been identified, namely No. 5 Seam void, Vleishaft Dam and Vlaklaagte Void.

In addition, some water will be pumped and stored in the SKS Pit void (Jaco-K Consulting, 2016(b)).

A summary of the evaporator system is given in **Table 4.3.1.a** below.

Number of Evaporators	Location	Time Period	Capacity (m <sup>3</sup> /d)			
8 – 2000 m³/d each	Vleishaft Dam	Currently operating	4800			
20 - 2000 m³/d each	Vlaklaagte South	Currently operating	12000			
12 - 3000 m³/d each	5 Seam opencast	Installed in November 2019	10800			
8 - 3000 m³/d each	Steenkoolspruit pit	Installed in May 2020	7200			
20 - 3000 m³/d each	Steenkoolspruit pit	12 evaporators moved from 5 Seam to SKS in 2023. 20 operating at SKS by June 2024	18000			

# Table 4.3:Summary of evaporators (Taken from Golder Associates Water balance<br/>Report, page 8, Table 4)

#### 4.3.2 Proposed infrastructure

The new infrastructure to be developed (and which will be the subject of the IRP) is shown on a **Figure 4 3.2.a** and includes:

- Topsoil dumps.
- Overburden dumps.
- ROM stockpiles and mixed ROM coal and slurry stockpile areas.
- The existing explosives magazine will be relocated to the north of Pit 4.
- New roads required for the VDDC project include:
  - Temporary high wall roads and dragline walkways which will be re-established as mining progresses;
  - Earth Moving Equipment (EME) haul roads (40 m width) from the bottom of box cut ramps to the existing haul roads;
  - Additional maintenance/service and access roads within the VDDC project area from the existing infrastructure to the box-cut;
  - New haul road to the No. 4 seam and No. 5 seam stockpiles.
- EME hard park and brake test ramp.
- Access control and security fencing

Access control will be through the existing control measures.

Triple security fencing will be provided at the explosives magazine. Triple fencing includes a triple barrier of 2.4 m high clear mesh, electric and normal security fencing. Electric fencing is connected to the local security system (South32, 2017b).

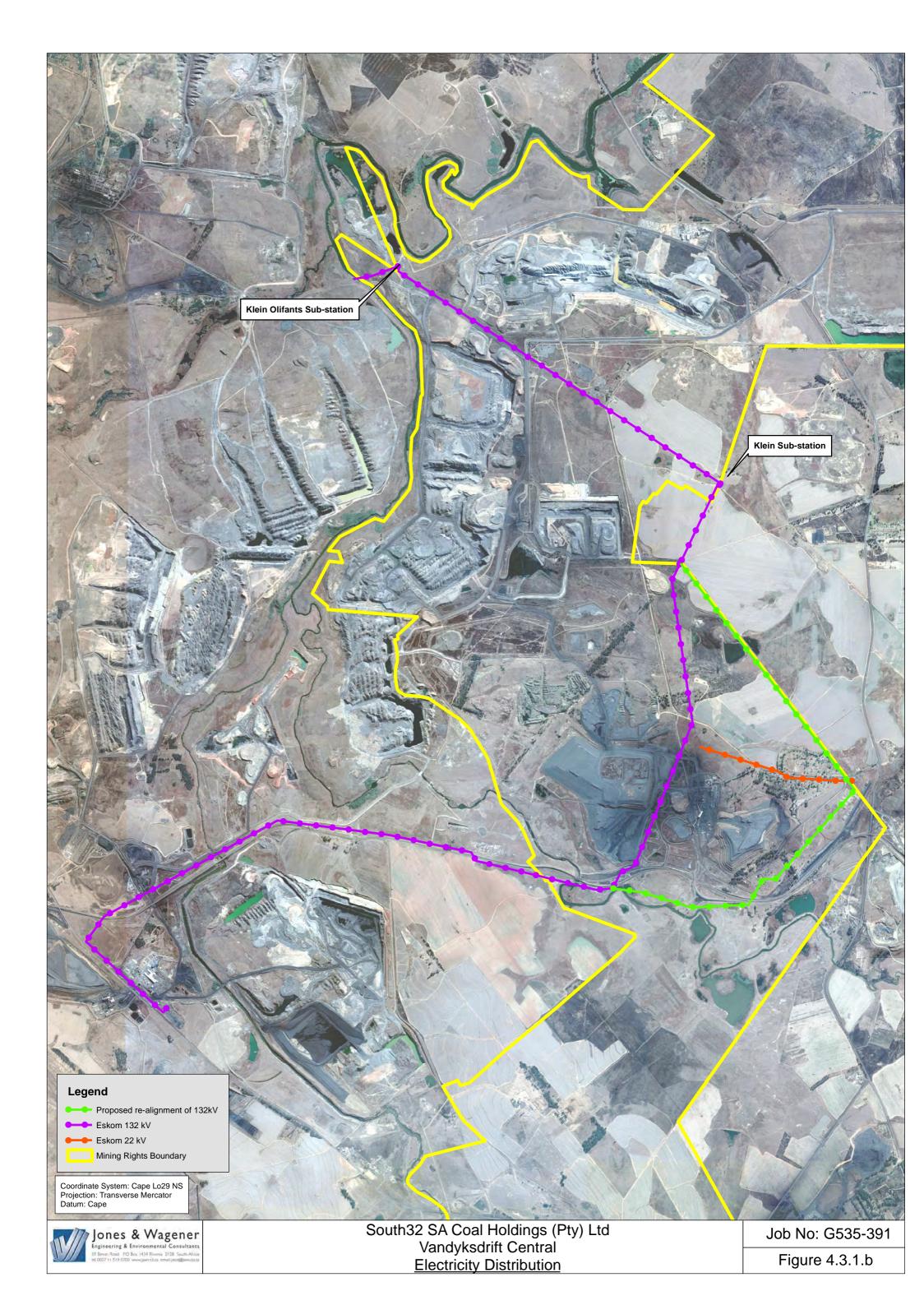
- Equipment, including water bowsers for dust suppression.
- Other infrastructure would include:
  - Opencast pit.
  - In pit sumps.
  - Proposed modular Water Treatment Plant (WTP).
  - Mechanical evaporators as detailed in **Table 4.3.1**.a above. The evaporators will be operated at 30 % efficiency.
- Clean and dirty water canals and pipelines.
- Future coal plant infrastructure area

As indicated earlier, the PSS and LAC dumps are currently reclaimed and processed within the existing VDD processing plant. As mining progresses, this plant will need to be relocated. An area has been allocated for this purpose and is situated to the south of the proposed new overburden dump in the south-eastern corner of the VDDC area.

The remainder of the supporting infrastructure is mostly catered for by the existing SKS complex facilities. Existing change houses, stores facilities, office facilities, tracked vehicle workshops, LDV workshops will be used.

No additional fuel or lube storage area, servicing bays or tyre bays are required.





#### Legend

#### Drains Culverts

- Dirty Water Pipelilne to Water Treatment Plant
- Dirty Water Pipeline to Vleishaft Dam
- Pipes Clean
  - Proposed 450 clean Water Pipeline
- Treated Water Pipeline (Existing Pipeline)
- ----- Contractors Laydown Area
- Dirty Water Drains
- Mine Haul Truck Park
- Proposed Box Cut
- Proposed EME Hard Park Terrace and Brake TES Ramp
- ----- Proposed Evaporators
- Proposed Haul Roads
- Service Roads
- Servitude
- Stormwater Drains & Berms
- Water Management
- 4 Seam Stockpile
- 5 Seam Stockpile
- Future Coal Plant Infrastructure Area
- Overburden Dump Mixed ROM-Slurry Stockpile areas
- Dragline Spoils
- Proposed Box Cut
- Proposed Evaporators
- Proposed Explosives Magazine
- Proposed Modular Water Treatment Plant
- Topsoil Dumps
- Transfer Tanks

Existing road to be upgraded



### 4.4 Sources of water

#### 4.4.1 Water consumption requirements

The water consumption requirements for the VDDC mining project is as follows:

- Potable water for human consumption or use in restrooms will be adequately catered for by the existing potable water supply existing at the SKS complex;
- Wash water for wash-down, either of vehicles, workshops or conveyor bunds. The water make from the upfront No. 2 Seam dewatering makes this a water positive operation. Therefore, the required volumes of process water and service water are adequately catered for.;
- Water for dust suppression on bulk materials handling systems which will be sourced from mine impacted water, i.e. the Vleishaft Dam;
- Water for dust suppression on haul roads which will be sourced from pit water;
- Fire water supplies are required at the new workshops at the SKS complex and will be taken from the existing fire water network.

#### 4.5 Solid waste management

Solid waste has the potential to impact on surface water through contaminated runoff and seepage. The waste management proposed for the site is discussed below. It is anticipated that both hazardous and general waste will be produced.

#### 4.5.1 Disposal of general waste

For this project VDDC will follow what is currently done at Wolvekrans Colliery. Wolvekrans Colliery disposes its general waste at the Middelburg municipal landfill site. This landfill site is licensed and after each disposal the mine receives a safe disposal certificate.

#### 4.5.2 Disposal of industrial waste

All industrial waste, including wood, rubber, paper and refurbishable waste (i.e. pumps, valves etc.) will be sorted and stored in designated areas. Materials that can be recycled will be re-claimed, re-used or sold to scrap metal dealers as far as possible. Items such as used tyres and oil will be returned to suppliers for re-use.

Wood may be taken to an area outside the shaft area for use by the community. Plastic waste (i.e. PVC, HDP, plastic containers, electrical cables) that will be generated will be removed by a licenced waste removing contractor for recycling.

#### 4.5.3 Disposal of hazardous waste

For this project VDDC will follow what is currently done at Wolvekrans Colliery. Wolvekrans Colliery contracts a registered waste removing company to remove and dispose of hazardous waste generated at the mine complex. The waste is taken to the Holfontein Hazardous waste site, a licensed waste facility, and safe disposal certificates are received for each waste disposal.

#### 4.5.4 Disposal of healthcare risk waste

There will be no new clinics developed. All healthcare risk waste, including bandages, used dressings, urine cups, used HIV kits, used needles and syringes and used urines teat strips etc. will be placed in a designated container, at the existing Clinic known as Naledi Village Clinic, for disposal until collected and removed by an external registered medical waste company/contractor employed by the mine.

# 4.5.5 Disposal of mine residue

An area of the underground No. 2 Seam was historically used for disposal of slurry from the processing plant. It is believed to be contained in the southeast portion of the deposit by underground seals and barrier pillars.

Slurry will be mined together with the ROM coal and the blended coal and slurry will be transferred to the mixed ROM coal and slurry stockpile areas, located to the south of the Vleishaft Dam. The mixed material will be allowed to dewater for a period, before it is removed via trucks to the existing SKS tip, from where it will be taken to the South Export Processing Plant using an overland conveyor. Water will be collected and conveyed via a silt trap to the Vleishaft Dam.

ROM coal from the No. 4 and No. 5 seams will be placed on transfer stockpiles. These stockpiles will be located on a partially reclaimed area of the PSS dump footprint. The stockpile positions will be moved as mining progresses but will remain within the footprint of the existing PSS dump or other previously mined out or disturbed areas.

The boxcut will be done using a combination of dragline and truck and shovel. Overburden from the boxcut will be placed on four overburden dumps located in between the proposed ramps.

In addition, provision has been made for two overburden dumps. A new overburden dump will be developed in the south-east of the project area and the existing overburden dump at the SKS pit will also be used.

All overburden dumps will be mined through", with the exception of the south east overburden dump. The material from this dump will be removed and used in the concurrent rehabilitation of the opencast pit. The dump footprint will be rehabilitated.

The topsoil excavated from the box cut areas and areas cleared for the development of infrastructure will be placed in the designated topsoil stockpile area to be located adjacent to the existing topsoil stockpile in the east of the project area. In addition, provision has been made for a topsoil stockpile area in between the ramps. The box cut topsoil will be stockpiled due to the lack of direct placement option at the start of the opencast mining operations.

# 4.5.6 Disposal of waste from the water treatment plant

Mine impacted water will be pumped to the Vleishaft Dam and thereafter, to the evaporator sites, or to the proposed modular WTP or to Vlaklaagte void.

A summary of the mechanical evaporator sites is provided in **Table 4.3.1.a** above.

Surplus water which cannot be handled through the evaporation system, will be conveyed to a mobile, modular WTP with a maximum treatment capacity of 20 Ml/day. Brine from the WTP will be collected in existing tanks before being conveyed to the evaporators at the SKS void.

# 4.6 Liquid waste water management

4.6.1 Disposal of process effluent

It is not expected that the VDDC operation will produce any process effluent, with process water being recycled within the operations as far as is practicable. Any spills of process water during upset conditions will report via the dirty storm water system via a silt trap to the Vleishaft Dam and thereafter, to one of the evaporator sites, or to the proposed modular WTP.

4.6.2 Disposal of domestic waste water management

The disposal of domestic sewage is described in Section 4.7.1 below.

4.6.3 Disposal of treated mine water

Effluent from the WTP (i.e. treated mine water) will be conveyed via an existing mine water pipeline to the existing northern clean water canal, from where it will discharge via a wetland area into the Olifants River. Water will be treated to comply with Resource Quality Objectives for the Olifants River catchment as published in GN 466 in April 2016.

# 4.7 Water pollution management facilities

4.7.1 Domestic waste water management

During construction, chemical toilets will be used by the contractors. These will be emptied regularly for disposal at an authorised off-site sewage treatment plant.

Once operational, the existing facilities at the SKS complex will be used.

4.7.2 Storm water management

# 4.7.2.1. Background

An effective surface water management system will be essential to ensure efficient mining and to protect the natural water resource during the construction, operation and post closure phases of the mine. This will entail management of dirty water generated through the mining process (including the mine water make and run-off from mine infrastructure areas), as well as handling of clean water flowing towards the mining area.

Water management measures that are required will include the diversion of clean runoff from upstream of the mining areas around the site, and the containment of dirty runoff from the site in Vleishaft Dam, being the main pollution control dam (PCD) to which all surplus dirty water is pumped and thereafter, to one of the evaporator sites, or to the proposed modular WTP. These measures need to be designed to accommodate events up to at least the 1:50 year event, in line with GN R704.

Storm water that is generated around the mining area consists of clean and dirty runoff. This includes:

• Clean runoff from clean catchments draining towards the mining activities and infrastructure. Measures will be implemented to ensure that significant clean

catchments are diverted away from the workings. Clean water diversions and flood protection measures will be designed to accommodate at least the 1:50 year event.

Dirty runoff will be generated in the opencast and proposed infrastructure. Measures will be implemented to contain this runoff by directing it to the pollution control dam. At the proposed pit extension area, dirty runoff reporting to the pit will be collected in an in-pit sump from where it will be pumped to the Vleishaft Dam and thereafter, to one of the evaporator sites, to the proposed modular WTP or to Vlaklaagte void. The dirty water management system, including the pollution control dams, needs to be designed in accordance with GN R704 to accommodate the 1:50 year event as a minimum (i.e. 2% risk of spillage) with a minimum of 800 mm freeboard.

Storm water management measures are discussed in more detail below.

Layouts of the existing and proposed surface water management infrastructure are shown in **Figures 4.8.2.a** and **b** and are discussed in more detail below.

### 4.7.2.2. Storm water management in clean areas

In line with best practice and the requirements of the NWA, contaminated storm water runoff volumes will be minimised by preventing runoff from clean areas from entering the dirty areas. This will be achieved by means of clean water diversion canals that will collect clean runoff and divert it around the dirty areas.

All clean water diversions will be designed to accommodate the peak flow expected for at least a 1:50 year event.

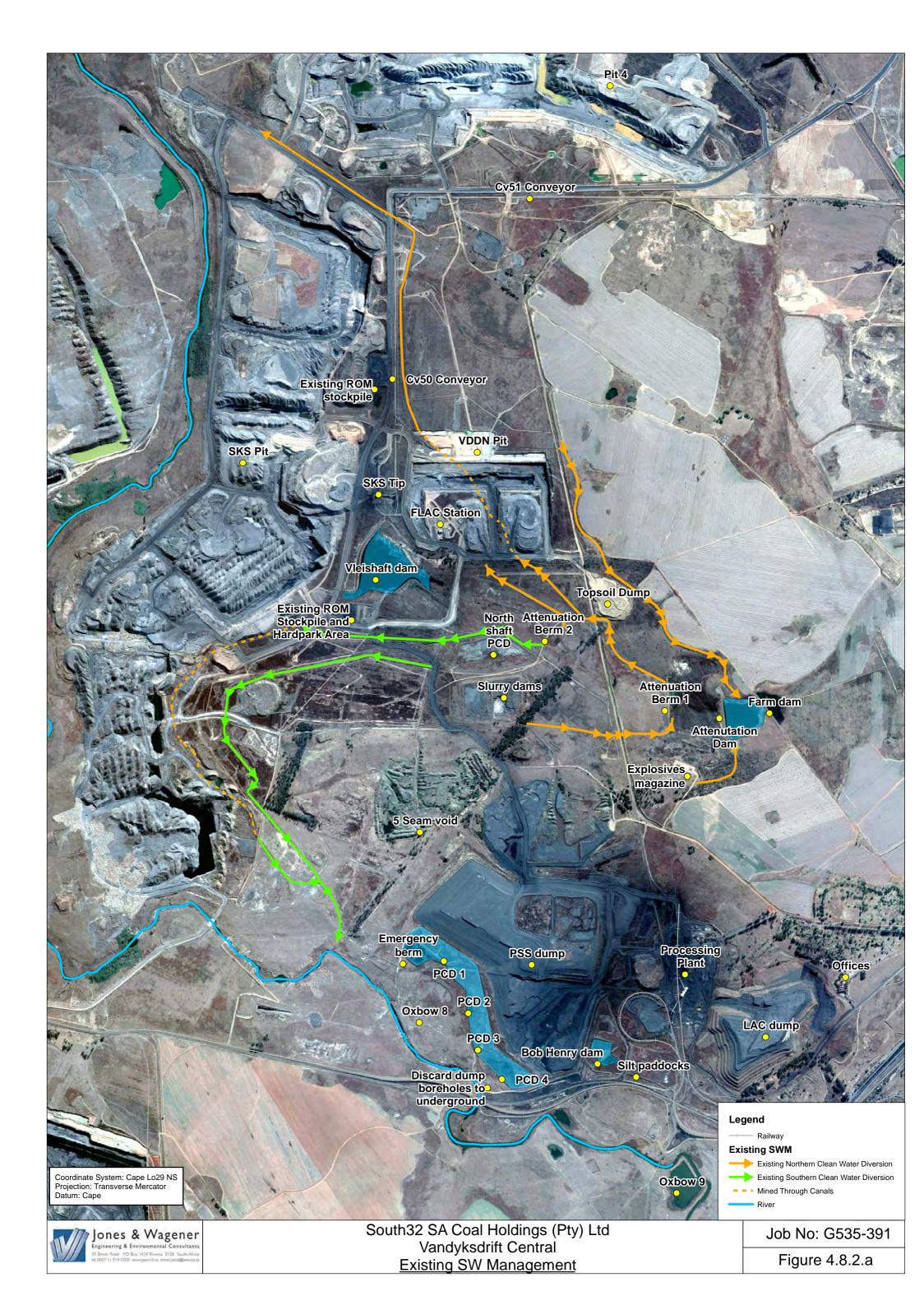
In terms of clean water management, VDDC is an existing mine and has existing infrastructure including existing water management infrastructure. There are several existing clean water canals in the area. These are indicated in **Figure 4.8.2.a**.

As indicated in **Figure 4.8.2.a** there are several existing clean water canals that divert the clean upslope catchment from the north east and south west, as described below:

### Clean upslope catchment from the north and north east

Prior to mining of the SKS pit as well as the VDD North area in the north west and north respectively, the clean upslope catchment to the east and north east was diverted by means of a series of clean water canal, berm and dam systems, discharging clean water into the Olifants River in the north west. Since the mining of SKS Pit and VDD North area, a portion of these canals have been mined through.





All Existing Canals within the Study Area to become Future Mined-Out Canals

WWW I



The clean water dams, namely Attenuation Berm 1 and 2 and Attenuation Dam 1 (indicated as Attenuation Dam in the figure), lie within the Vleishaft tributary of the Olifants River and are utilised as clean water dams. Vleishaft Dam serves as the main PCD for the VDDC area. Due to the proposed infrastructure development, Attenuation Berm 1 and 2 will now be mined through, along with a portion of the existing clean water canals. This leaves Attenuation Dam 1 (indicated as Attenuation Dam in the figure), as the only clean water dam near the proposed mining area. This dam is located directly upstream of the proposed VDDC boxcut area and poses a potential risk to mining in this area as the stability of the dam wall is uncertain.

The current plan is to construct a pump and pipeline system to pump clean water from this dam to the Olifants River via an existing clean water canal, operating the dam as empty as possible at all times. However, it was recognised by South32 that the dam wall needs to be inspected to determine the status and any remedial or improvement work needed on the dam itself. There is also a farm dam, as indicated on **Figure 4.8.2.a**, that is upstream of Attenuation Dam 1 (indicated as Attenuation Dam in the figure), which needs to be taken into account in the above planning.

A storm water management plan and in particular the diversion of clean water, has been developed for the VDD North area by Golder Associates. The clean water diversion canals proposed for the VDDC area will need to tie into this proposed clean water system. This is proposed to be done as follows:

- The clean upslope catchment approaching from the east of the VDDC infrastructure area will be diverted via a canal and berm system towards Attenuation Dam 1. The VDD North clean water canal in the north will tie into this proposed canal.
- From Attenuation Dam 1 water will be pumped via two 450 mm diameter clean water diversion pipelines to the existing northern canal at VDD North, from where water will be discharged via a wetland area into the Olifants River.
- The treated effluent from the proposed WTP will be pumped via a separate pipeline which will then discharge into the northern canal.

### Clean upslope catchment from the west and south west

Clean upslope catchment approaching from the west and south west is diverted by a series of canal and berm systems (to the south west of Vleishaft Dam) to the Olifants River in the south. Due to the proposed infrastructure and pit development, as part of the VDDC Infrastructure development project, the majority of these canal sections will be mined through. A portion of the existing canal to the north west of the PSS dumps will remain temporarily as the pit progresses and will eventually be mined through. A strip of clean upslope catchment from the south west will be diverted via new proposed clean water canals and berms to a proposed silt trap before discharging to the Olifants River.

### VDDC Opencast pit

Runoff from clean catchments from the east draining towards the VDDC pit area will be diverted around the mining area, minimising clean runoff into the opencast workings and onto the mine infrastructure areas. These will be in the form of clean water cut-off canals and berms. Clean water diversions and flood protection measures will be designed to

accommodate at least the 1:50 year event within the excavated canal with flood events of at least the 1:100 year being accommodated on the flood protection berm.

High wall drains will be installed to divert clean water away from the mining area where practical. These drains will move as mining progresses.

### New proposed hard park area

The new proposed hard park area will be located within the designated dirty water footprint.

#### **Overburden dumps**

The overburden material has the potential to contain carbonaceous material and therefore potential to generate poor quality runoff due to contact of the water with carbonaceous material.

Overburden from the boxcut will be placed on four overburden dumps located in between the proposed ramps. In addition, provision has been made for one new overburden dump and the extension of an existing overburden dump. The new overburden dump will be developed in the south-east of the project area and the existing overburden dump at the SKS pit will be extended.

The existing overburden dump at the SKS pit as well as the four dumps between the ramps are located within the dirty water footprint. Runoff from clean catchments draining towards the overburden dump to the south-east of the project area will be diverted around the dumps by means of a diversion berm.

### Topsoil stockpiles

Topsoil is considered clean. However, all proposed topsoil stockpiles are located within the dirty area. Clean runoff draining towards the stockpile area from the south and east will be diverted by means of clean water diversion canals and berms.

In addition to the canal/berm system, the design engineers have indicated that adequate energy dissipation and erosion protection will be provided at the discharge points.( Please refer to Worley's "The Mine Water Management Report", Section 7, Report/Document Number: C00820-000-CI-REP-0001, August 2019)

#### ROM stockpiles and mixed ROM coal and slurry stockpiles

These stockpiles will all be located within the designated dirty footprint. Clean runoff draining towards the stockpile areas from the south and east will be diverted by means of clean water diversion canals and berms.

In addition to the canal/berm system, the design engineers have indicated that adequate energy dissipation and erosion protection will be provided at the discharge points.

### 4.7.2.3. Storm water management in dirty areas

The dirty water containment facilities will be designed to ensure a risk of spill of dirty water to the environment of not more than once in 50 years (a 2% or lower risk in any one year). Infrastructure that will be provided to ensure the containment of contaminated water is described in the sections that follow, and is illustrated in **Figure 4.8.2.b**.

A number of dirty water canals drain dirty runoff to dirty water facilities. The Vleishaft Dam is an existing PCD that forms the main PCD for the VDDC Infrastructure Development project.

The North Shaft PCD is located to the south east of the Vleishaft Dam, but is not currently in use.

Dirty runoff from the discard reclamation and processing plant drains to the Bob Henry dam and silt paddocks.

Existing water management measures at the PSS dump comprise a clean water canal which collects clean water west of the PSS Dump Extension, as well as a system of unlined canals which collects dirty runoff from the PSS Dump and conveys the water to four PCDs. Excess water from the PCDs is pumped to the underground workings via a borehole. Water is abstracted from the workings via boreholes for re-use in the South Export processing plant.

### VDDC Opencast pit

In order to manage the inflow of water into the mining operations, sumps will be constructed in the pit floor where the water will be collected at the bottom of the pit (at lowest points) and pumped out of the pit. These temporary sumps will be situated at the bottom of each access ramp and the piping routed in a berm servitude on the side of the access ramp, up to transfer tanks situated at the top of the ramp. Once the water reaches the transfer tanks, it will join the polluted water management system. Water will be pumped from the pit with self-priming diesel driven pumps mounted on trailers or skids to allow for easy movement (South32, 2017a). Water will be pumped to the Vleishaft Dam and from there, to one of the evaporator sites, to the proposed modular WTP or to Vlaklaagte void.

The 4 and 5 seam coal stockpiles will move as the mining of the pit progresses and all runoff will drain to the Pit.

### New proposed hard park area

The new proposed hard park area will be located within the designated dirty water footprint.

All dirty runoff will drain to SKS void.

### Overburden dumps

The overburden dumps located at the SKS void will drain to the void and no additional measures are foreseen.

Pollution control measures will be required at the new overburden dump located on the south-eastern boundary to collect dirty runoff and seepage. Runoff from this dump will be diverted via a canal and berm system to silt traps and a set of boreholes which will take all runoff into the underground workings. This will allow the water to be temporarily stored until it can be pumped via the mine dewatering system to the PCD (Veishaft dam).

### Topsoil stockpiles

All topsoil stockpiles are located within the dirty area. Runoff generated from the topsoil stockpiles will drain via gravity to Vleishaft Dam.

### ROM stockpiles and mixed ROM coal and slurry stockpiles

Mine impacted water from the Mixed ROM coal and slurry stockpile areas will be collected and conveyed to the Vleishaft Dam via silt traps.

### Pollution control dams

There are no new PCDs proposed for the VDDC infrastructure development project, as all dirty water generated in the opencast pit, as well as runoff generated from the infrastructure areas will be pumped to the existing PCD (i.e. Vleishaft Dam).

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### 4.7.3 Mine water management

The proposed mining operations require the management of mine impacted water. Dirty areas that have been identified and included in the water management strategy are:

- Opencast pit;
- Mixed ROM coal and slurry stockpile areas;
- Overburden dumps;
- ROM stockpiles; and
- Hard park area.

Surface runoff generated from various proposed and existing infrastructure that need to be considered include:

- Existing hard park area, which drains to Vleishaft Dam;
- New proposed hard park area, which drains to SKS void;
- Topsoil stockpile within dirty area, which drains to Vleishaft Dam;
- Overburden dump, which drains to old underground workings via boreholes;
- Overburden dump at SKS pit, which drains to SKS void;
- Existing ROM stockpile to the north, which drains to SKS void;
- Existing ROM stockpile to the south, which drains to Vleishaft Dam;
- Mixed ROM coal and slurry stockpiles, which drains to Vleishaft Dam;
- Dirty water management area, which drains to which drains to old underground workings via boreholes;
- 4 and 5 seam coal stockpiles, which drains to the VDDC Pit.

Mine impacted water will be pumped to the Vleishaft Dam and thereafter, to one of the evaporator sites, or to the proposed modular WTP.

Surplus water which cannot be managed through the evaporation system, will be conveyed to a mobile, modular WTP with a maximum treatment capacity of 20 Mł/day. Brine from the WTP will be collected in existing tanks before being conveyed to the evaporators at the SKS void.

Effluent from the WTP (i.e. treated mine water) will be conveyed via an existing mine water pipeline to the existing northern clean water canal, from where it will discharge via a wetland area into the Olifants River. Water will be treated to comply with Resource Quality Objectives for the Olifants River catchment, as published in GN 466 in April 2016.

- 4.7.4 Water storage facilities
- 4.7.4.1. General description of dams

### Existing dams

The Vleishaft Dam is an existing PCD with a capacity of 600 000 m<sup>3</sup>, that has been authorised for the disposal of mine impacted water in terms of WULs issued to the mine.

### **Proposed dams**

No new surface water dams are proposed as part of the VDDC Infrastructure Development project.

- 4.7.5 Polluted water treatment facilities
- 4.7.5.1. Mine water treatment

Mine water treatment is discussed in detail under Section 4.5.6 and 4.6.3 above.

### 4.8 Watercourse alterations

The mining area is located adjacent to the Olifants River. The proposed WTP will discharge into an existing clean water canal (the northern canal). Therefore, alteration of flow in the Olifants River due to excess treated water from the WTP, being discharged into existing clean water canal prior to discharge to the Olifants River.



### 5. BASELINE ENVIRONMENTAL DESCRIPTION

The baseline environmental information is important for several reasons. This data forms the basis of the assessment of possible impacts, and the setting of objectives for closure. For surface water it is important that the mine is able to identify point sources that may be impacting on surface water so that the origin of any future impacts can be identified.

### 5.1 Regional Climate

The VDDC infrastructure and mining development project is located in the Mpumalanga Highveld region where the climate is characterised as generally dry. Summers are warm to hot with an average daily high temperature of approximately 27°C (with occasional extremes up to 35°C). Winters range from mild to cold with an average daily high of approximately 15°C (with occasional extreme minima as low as -10°C). Frost and mist are frequently experienced during the winter months on the Mpumalanga Highveld.

### 5.2 Catchment description

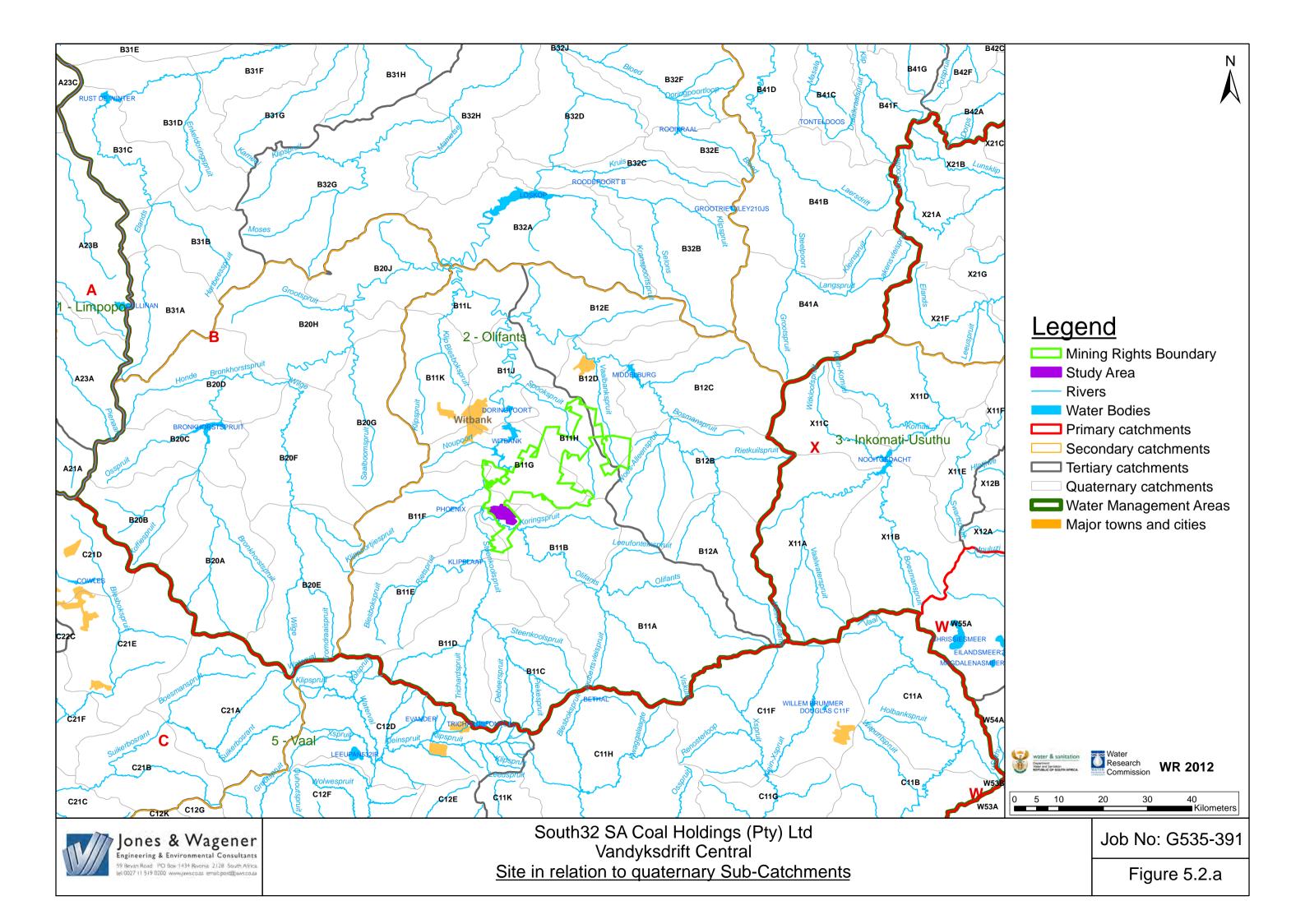
### 5.2.1 General description

The VDDC infrastructure and mining development project is situated within the catchment area of the Olifants River. This catchment makes up part of the Witbank and Loskop Dam catchment. The proposed project is largely situated within quaternary sub-catchment B11F and B11B with some infrastructure components located within B11G of the Limpopo-Olifants primary drainage region, as indicted in **Figure 5.2.a** taken from "Surface Water Resources of South Africa – 2012" (Midgley, Pitman & Middleton, 2012) (WR2012)).

The proposed infrastructure and mining development area drains towards the Olifants River. Prior to mining that took place in 2004, the drainage of the northern portion of the proposed infrastructure development area previously drained via the Vleishaft tributary (which was diverted then to facilitate future mining, with the Vleishaft Dam being used as a PCD) which flowed through the mine's property.

Downstream of the mine, the river flows to the Witbank Dam, then to the Loskop Dam and through the central part of the Kruger National Park to Mozambique. It joins the Limpopo River and discharges to the Indian Ocean on the east African coastline.

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### 5.3 Receiving water body

In terms of the catchment description, the receiving water body is an important concept. The receiving water body is the point below which the mine's impact on the catchment is considered to be negligible. This implies that aspects such as surface water users need only be defined down to the receiving water body.

The receiving water body for the assessment of potential surface water quality impacts of the VDDC Infrastructure and mining development project is taken as the Witbank Dam.

The use of this dam is motivated on the basis that:

- The Witbank Dam has been selected as it is located downstream of the proposed development within the Olifants River catchment area.
- Beyond the Witbank Dam, the potential impacts become extremely small due to the water volumes in the catchment and dilution effects.
- Further, by the time the water reaches the Witbank Dam, it is required to be suitable for use for all of the expected uses (drinking water, agricultural, industrial and aquatic ecosystems). Thus, by achieving compliance in terms of these, no additional impacts are expected downstream of the Witbank Dam. The receiving water body is relevant only in so far as it defines the aerial extent of the catchment to be considered in the impact assessment and described in the baseline study.
- The use of the Witbank Dam is based on the relatively small size of the disturbed areas compared to the catchment for the dam.
- The catchment for the Witbank Dam is reported as 579 km<sup>2</sup>. The proposed VDDC infrastructure development area covers approximately 14.5 km<sup>2</sup>. The mine area thus totals approximately 2.5% of the Witbank Dam catchment.
- The mean annual runoff (MAR) for Witbank Dam is 190 x 10<sup>6</sup> m<sup>3</sup>, while the MAR for the proposed mining area is estimated at 0.45 x 10<sup>6</sup> m<sup>3</sup>.

### 5.4 Rainfall and evaporation

#### 5.4.1 Rainfall data

The Daily Rainfall Extraction Utility, developed by the Institute for Commercial Forestry Research (ICFR) in conjunction with the School of Bio-resources Engineering and Environmental Hydrology (BEEH) at the University of KwaZulu-Natal, Pietermaritzburg, was used to obtain summary data for all rainfall stations within the vicinity of the site. This data was assessed in terms of length of record, completeness of the data set, mean annual precipitation (MAP) and location of the rainfall station with respect to the site and the catchment. Key data extracted from the database for the five most reliable stations is shown in **Table 5.4.1.a**. The ICFR database contains daily patched rainfall data for all official SAWS stations, and includes data up to August 2000.

After an assessment of the length of the record, MAP and the reliability of the data for the five rainfall stations, the Witbank, EDE and Blinkpan rainfall stations were disregarded. This was due to the limited length of the records and low reliability of the data sets. To further assess the two remaining rainfall stations, and select an appropriate and representative station for the site, each of the records were assessed to determine whether the records contained events exceeding the 1:50 year event.

Station number	Station name	Reliable (%)	MAP (mm)	Length of record (years)
0515826_W	Middelburg (TNK)	51.9	643	96 (1903 – 1999)
0516201_W	EDE	42.2	643	90 (1903 – 1993)
0515412_W	Witbank (MUN)	37.1	641	44 (1956 – 2000)
0478546_W	Vandyksdrift	59.8	686	82 (1928 – 2010)
0478786	Blinkpan	25	643	13 (1987 – 2000)

 Table 5.4.1.a:
 Key data for selected rainfall stations (ICFR database)

The top 100 ranked peaks from the two rainfall records were plotted along with the rainfall depths relating to various recurrence intervals, extracted from the SAWS design rainfall depths manual. For both rainfall stations it was found that only one event exceeded the 1:50 year event. Therefore, the Vandyksdrift rainfall station was selected as being the representative rainfall data set for the site. The Vandyksdrift rainfall station was found to have the most reliable data set with a high MAP.

It was found that, although data was available for the Vandyksdrift station after 1998, this data was not completely intact, with data missing and inconsistencies. Therefore, only data up until 1998 was considered for the station. A mass plot was produced for the record and is shown in **Figure 5.4.1.a.** A mass plot is a graph showing the cumulative rainfall depth with time for the full rainfall record. It is good indication of the reliability of the data set. A good mass plot will produce a straight line, with slight oscillations for seasonality. Any changes in the slope indicate a potential problem in the data set.

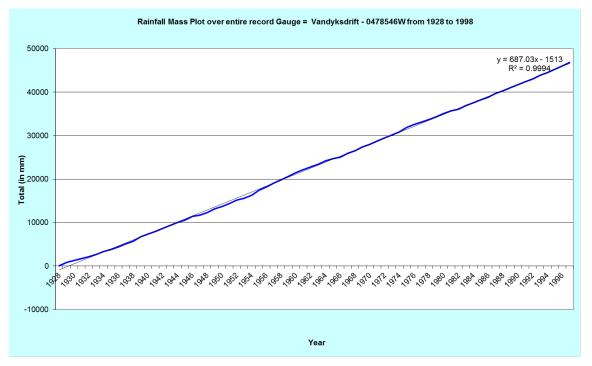


Figure 5.4.1.a: Rainfall mass plot for the rainfall record

46

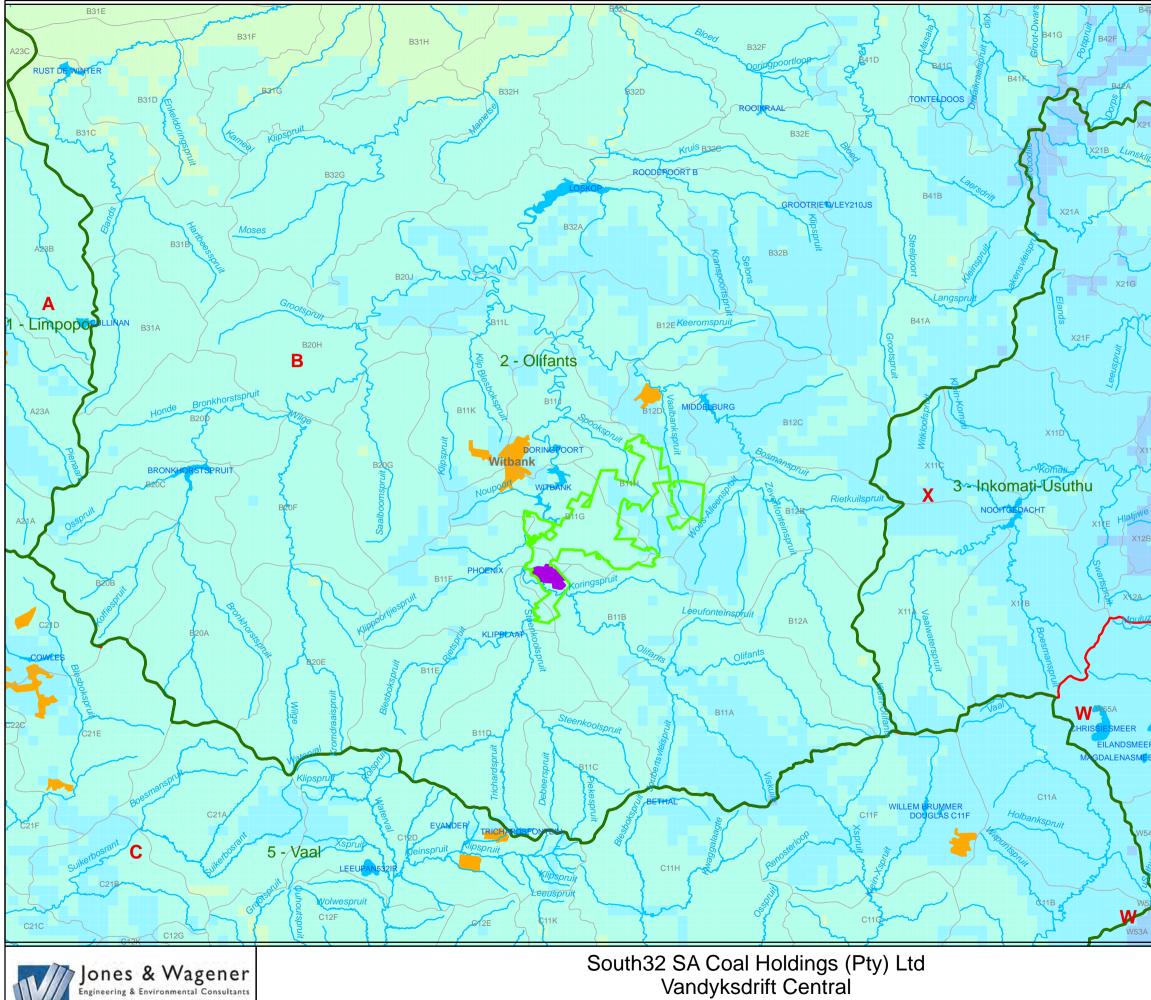


The mass plot for the rainfall record is considered to be acceptable. The record has therefore been selected as being a representative rainfall data set for the site for the hydrological assessment.

The average monthly rainfall depths are presented in **Table 5.4.1.a.** The rainfall record is presented graphically in **Figure 5.4.1.a**. The entire rainfall record is presented graphically in **Figure 5.4.1.a**. Mean monthly rainfall is shown graphically, together with mean monthly evaporation, in **Figure 5.4.1.c**.

The site in relation to the regional MAP for the area, taken from WR2012 can be seen in **Figure 5.4.1.b**.





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Vandyksdrift Central Mean Annual Precipitation



## Legend

Mining Rights Boundary Study Area Water Management Areas Rivers Water Bodies Primary catchments Quaternary catchments Major towns and cities

### **Mean Annual Precipitation**

0-100 mm
100-200 mm
200-300 mm
300-400 mm
400-500 mm
500-600 mm
600-700 mm
700-800 mm
800-1000 mm
1000-1500 mm

>1500 mm



0 5 10

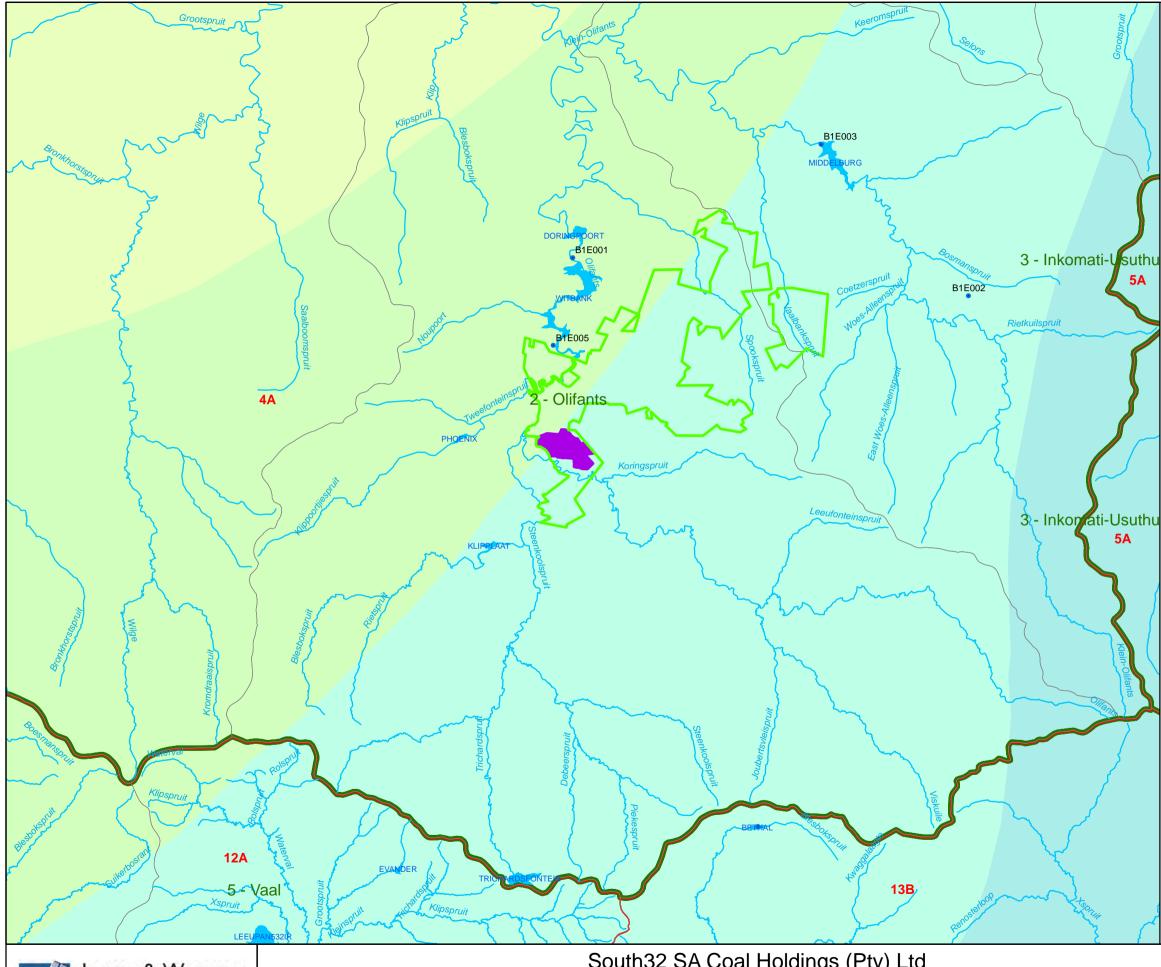


20



40 Kilometers

### Job No: G535-391 Figure 5.4.1.b



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South32 SA Coal Holdings (Pty) Ltd Vandyksdrift Central Mean Annual Evaporation (S-Pan)



## Legend

Mining Rights Boundary
Study Area
<ul> <li>Evaporation stations WR90</li> </ul>
—— Rivers
International boundary
Quaternary catchments
Impoundments
Evaporation zones
Mater Management Areas

Water Management Areas

### Mean Annual Evaporation S-Pan

< 1200 mm
1200-1300 mm
1300-1400 mm
1400-1500 mm
1500-1600 mm
1600-1700 mm
1700-1800 mm
1800-2000 mm
2000-2200 mm
2200-2600 mm

> 2600 mm



0 3 6



12



18

# Job No: G535-391

### Figure 5.4.1.c

24 Kilometers

### 5.4.2 Evaporation data

Evaporation data was taken from the evaporation station for Witbank Dam (B1E001). Monthly data for this station was only available for the period 1964 to 2009. Over the periods for which there was no monthly evaporation data, average evaporation depth, taken directly from the *WR90 report* for the Evaporation Zone into which the site falls. The Evaporation Zone is 4A. The Mean Annual Evaporation for this zone is 1600 mm. The average monthly evaporation depths are presented in **Table 5.4.2.a** and **Figure 5.4.2.b**. The site in relation to the regional MAE for the area, taken from WR2012 can be seen in **Figure 5.4.1.c**.

### Table 5.4.2.a:Average monthly rainfall depth for the Vandyksdrift rainfall record<br/>(0478546\_W) and evaporation depths (from WR90)

Month	Average rainfall (mm)	Average evaporation (mm)
October	70	176
November	108	147
December	109	145
January	109	111
February	94	94
March	72	76
April	42	83
Мау	17	110
June	8	143
July	7	172
August	7	163
September	24	179
Annual Total	669	1600

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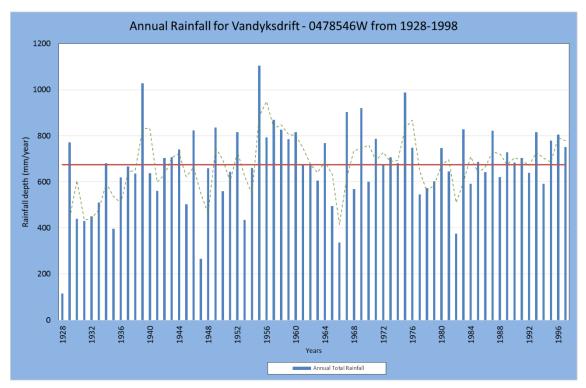


Figure 5.4.2.a: Rainfall record for Vandyksdrift

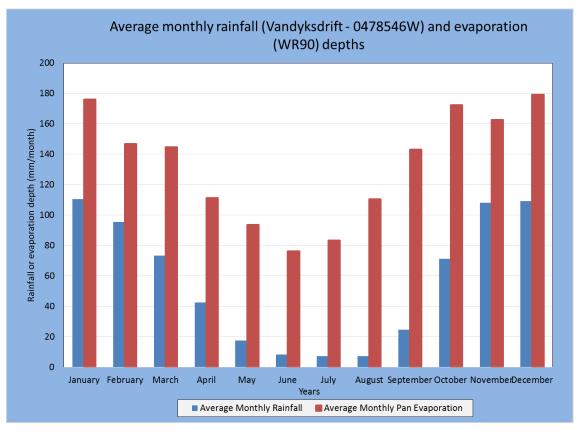


Figure 5.4.2.b: Mean monthly rainfall and evaporation for Vandyksdrift

### 5.4.3 Maximum rainfall intensities

#### 5.4.3.1. Rainfall extremes

Apart from the normal criteria of being statistically consistent, normally measured by considering the mass plot and ensuring that it is linear, it is also important that the rain gauge have a long record, and within that record that it contain rainfall events that correspond to at least the 1:50 year event, since the legal requirement is that a mine should not spill dirty water to the environment more than once in 50 years (a 2% risk of spilling in any one year). The duration of the event can vary, and in most of the larger mines, the critical event is not the 24 hour event, but rather above average rainfall over a period of several months, typically with several extreme rainfall events occurring during a wetter than average period.

Statistical rainfall extremes corresponding to various recurrence intervals where extracted from the Design Rainfall Depths of SAWS Rainfall Stations (Smithers and Schulze, WRC Project No K5/1060). These are shown in **Table 5.4.3.a**.

### Table 5.4.3.a: Statistical rainfall extremes for Vandyksdrift rainfall station (from WRC K5/1060)

Event	Rainfall depth (mm)						
Event	1:2         1:5         1:10         120         1:50         1:100         1:200						1:200
1 day	54	72	85	99	117	132	148

**Figure 5.4.3.a** illustrates the top 100 one day ranked rainfall peaks, along with the statistical rainfall extremes for Vandyksdrift, from the WRC. It is evident that, for the Vandyksdrift station, there are no events that has been recorded at the station, which are in excess of the 1:50 year event, making this record unsuitable for the water balance assessment. However, the rainfall record is still suitable for the hydrological assessment. Therefore, for the water balance modelling Langsloot/Secunda gauge will be used and further detail is given in Section 6.





Figure 5.4.3.a: Top 100 one day ranked rainfall peaks



### 5.5 Surface water quantity

This section details the baseline surface water information related to water quantity, such as flood events and stream flow (in essence the hydrology).

### 5.5.1 Map of the catchment

The Witbank Dam catchment is shown in **Figure 5.2.a** above. Catchment areas upstream, downstream and within the project area are given in **Table 5.5.1.a** below.

### Table 5.5.1.a:Catchment areas

River	Measured at	Catchment (km²)	
Olifants River	Upstream of Vandyksdrift (Entrance of mine property)	1350	
Olifants River	Downstream of mine property	3309	

### 5.5.2 Mean Annual Runoff (MAR)

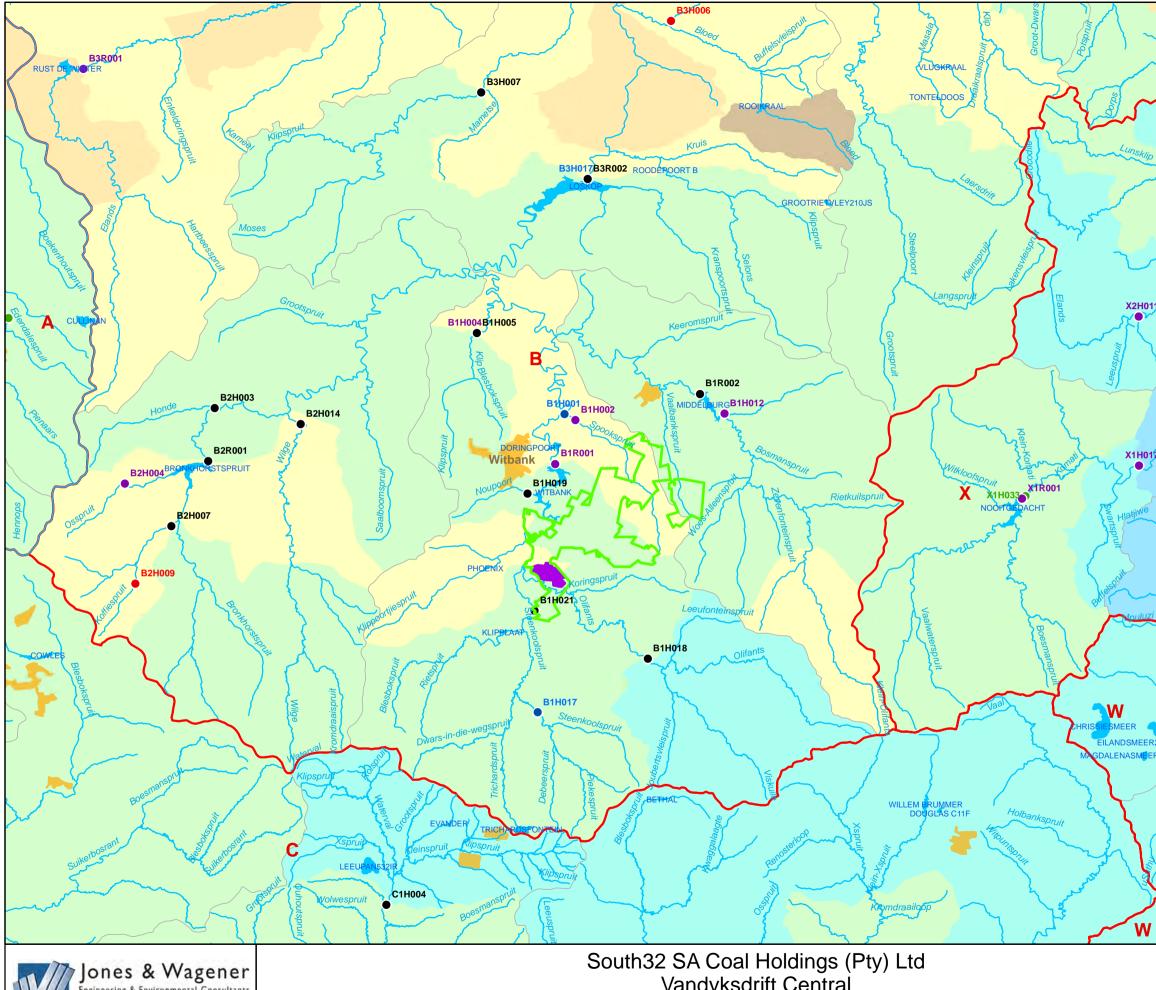
The WRSM2012 synthetic generation model was used to obtain simulated monthly flow records at various points within the mine property. The rainfall input to the model was an averaged historical record of several rain gauges in the vicinity. The MAR is given in **Table 5.5.2.a**. The site in relation to the regional MAR for the area, taken from WR2012 can be seen in **Figure 5.5.2.a**.

Table 5.5.2.a:Computed MAR

River	Measured at	MAR (x106m³)	Percentage of MAR at Witbank Dam
Olifants River	Entrance to mine	59.5	46
Steenkoolspruit	Immediately before confluence with Olifants River	52.0	40
Olifants River	Exit from mine property	188.1	99
Witbank Dam	At dam	190	100

**Note:** Varying values on the MAR for Witbank Dam were found in the literature. This value of  $190 \times 10^6 \text{ m}^3$  is derived from the runoff values given for various measuring points in the Surface Water Resources of South Africa – 1990





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South32 SA Coal Holdings (Pty) Ltd Vandyksdrift Central Mean Annual Runoff



### Legend

Mining Rights Boundary Study Area

Stream flow gauges

	o apparent problems				
	utliers				
• In sa	balance among records on me river or catchment				
-	ero or near-zero annual ws				
• So	ome data problems				
Ri	vers				
Se	econdary rivers				
W	ater Bodies				
Pi	imary catchments				
Q	Quaternary catchments				
W	ater Management Areas				
	ajor towns and cities				
Mean annual	-				
	2.5 mm				
2.	5-5 mm				
5-	10 mm				
10	0-20 mm				
20	0-50 mm				
	0-100 mm				
	100-200 mm				
20	200-500 mm				
>5	>500 mm				
water & sanitation	Water Research WD 2012				
Water & sanitation Degeneration Reposite of Bourn Arrica	₩ater				
Department Venue and Samateon REPUBLIC OF SOUTH AFRICA	Water Research Commission WR 2012				
	Water Research WD 2012				
Department Venue and Samateon REPUBLIC OF SOUTH AFRICA	Water Research Commission WR 2012 20 30 40				
Department Venue and Samateon REPUBLIC OF SOUTH AFRICA	Water Research Commission WR 2012				

### 5.5.3 Dry Weather Flow

A simulated stream flow record was generated (as described in **Section 5.5.2** above) at the downstream boundary of the mine. A flow-duration curve was then constructed for the simulated stream flow record. Based on the criterion that the dry weather flow is the flow in the stream that is equalled or exceeded 70% of the time, this flow was computed and corresponds to the flow during the winter months, shown for key points in **Table 5.5.3.a**.

River	Measured at	Dry weather flow (m³/s)	Nature of stream flow
Olifants River	Entrance to mine property	0.3	Perennial
Steenkoolspruit	Immediately before confluence with Olifants River	0.34	Perennial
Olifants River	Exit from mine property	0.71	Perennial

### Table 5.5.3.a: Dry weather flows

#### 5.5.4 Flood Peaks and Volumes

The flood peaks for the 1:20, 1:50 and 1:100 year recurrence intervals were computed using the Rational Method (DWA implementation and Alternative implementation) and Unit Hydrograph techniques. Use was also made of the Regional Maximum Flood.

The volumes of the floods were based on the simplified hydrograph proposed by Kovacs, and the relationship between the Regional Maximum Flood and Mean Annual Runoff as derived from the measurement of various extreme flood events across South Africa documented in various Department of Water Affairs and Forestry (DWAF) publications.

**Table 5.5.4.a** lists these flood peaks and the Regional Maximum Flood together with the corresponding flood volumes on the Olifants River and Steenkoolspruit.

## Table 5.5.4.a:Computed flood peaks and volumes in the Olifants River, Steenkoolspruit<br/>and their tributaries affected by mining

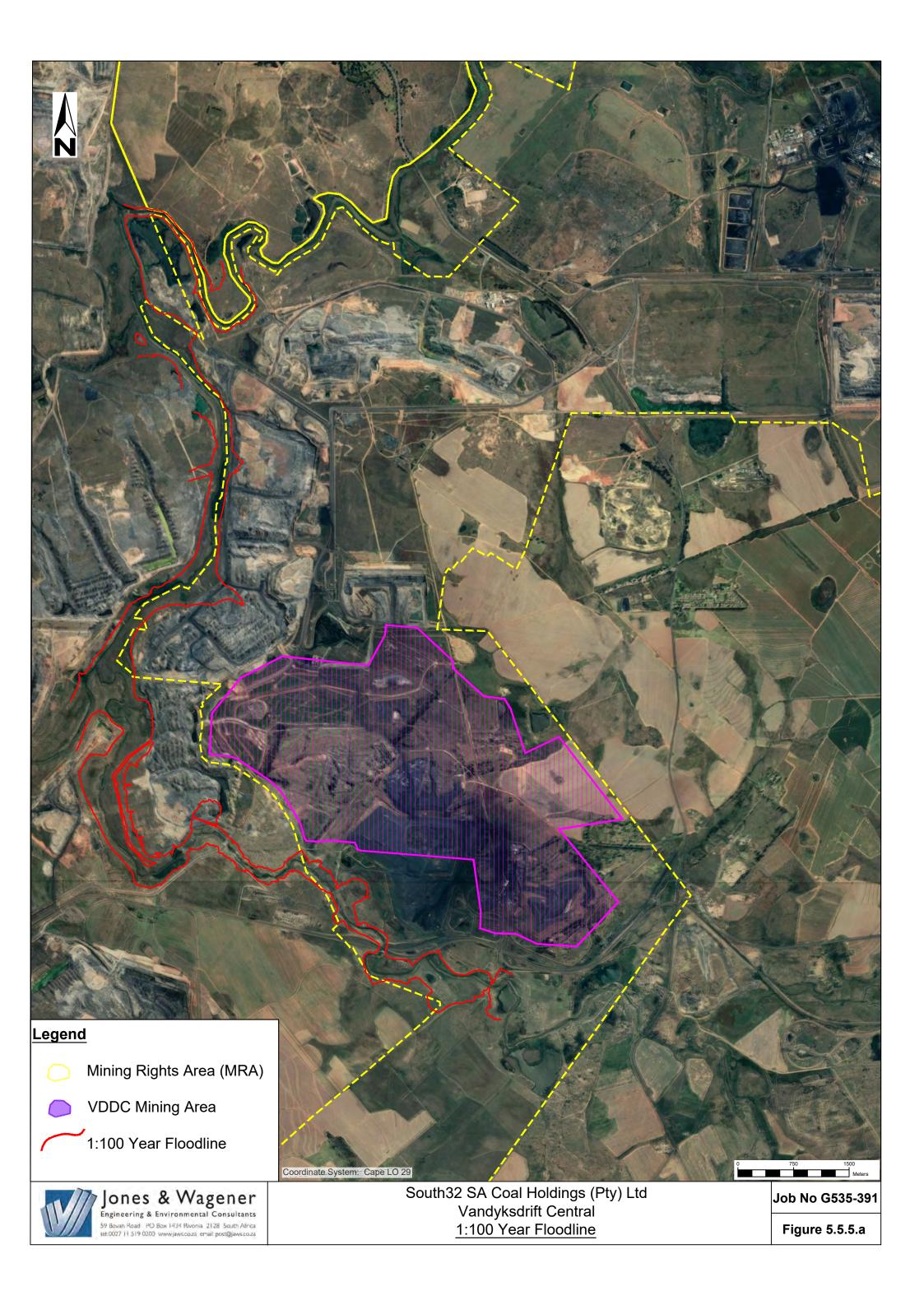
River	Measured at	Recurrence Interval	Flood Peak (m³/s)	Flood Volume (x10 <sup>6</sup> m <sup>3</sup> )
Olifants River	Entrance to mine	20 year	480	26
	property	50 year	760	41
		100 year	1150	58
		RMF	350	196
Olifants River	Immediately before	20 year	490	27
	confluence with Steenkoolspruit	50 year	780	3
		100 year	1200	60
		RMF	240	203

River	Measured at	Recurrence Interval	Flood Peak (m³/s)	Flood Volume (x10 <sup>6</sup> m <sup>3</sup> )
Steenkoolspruit	Immediately before	20 year	515	26
	confluence with Olifants River	50 year	810	42
		100 year	1250	58
		RMF	2402	199
Olifants River	Exit from mine	20 year	823	51
p	property	50 year	1292	80
		100 year	1837	112
		RMF	3810	380

### 5.5.5 Floodlines

The 1:100 year recurrence interval pre-mining floodlines are shown on in **Figure 5.5.5.a**, taken from J&W 2004 report – "Surface Water Inputs to Douglas Pillar Project EMPR"-Report Number JW188/04/9347).





### 5.6 Surface water quality

This section details sampling locations and water quality objectives, with respect to surface water and provides an assessment of the surface water quality and the impact of mining on the surrounding watercourses and catchments.

Wolvekrans Colliery is an existing mine and has a monitoring programme in place and therefore the available surface water quality data was used. Water quality data, for several locations around the site, extending from September to October 2012, July 2015 to November 2017 and January to February 2018, was received from South32.

This section details sampling locations and water quality objectives, with respect to surface water and provides an assessment of the surface water quality and the impact of mining on the surrounding watercourses and catchments.

### 5.6.1 Surface water quality monitoring locations

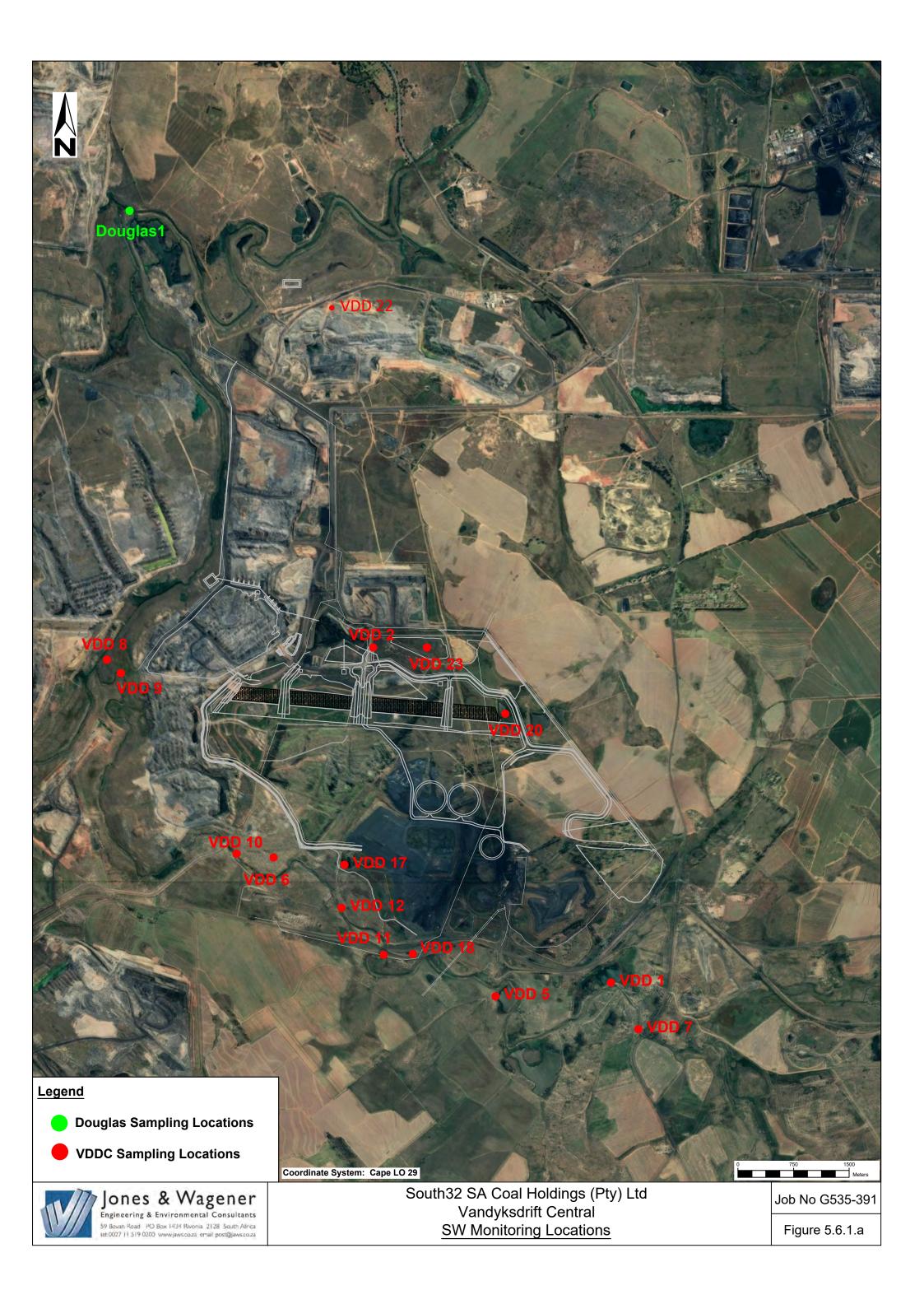
The surface water monitoring locations are illustrated in

Figure 5.6.1.a and the coordinates of these points are given in Table 5.6.1.a.

Table 5.6.1.a: List of surface water monitoring locations

Sampling Location	Description	Coorc	linates
VDD 1	2538 V01 Springbokspruit @ entrance to mine property	S26°06.043'	E29°19.148'
VDD 2	2542 U/s of vlei shaft & V7 con. belt	S26°03.599'	E29°17.218'
VDD 5	2545 V09 Oxbow 9 ponded water	S26°06.146'	E29°18.214'
VDD 6	2551 V16 Olifants D/S of PSS discard dump	S26°05.135'	E29°16.416'
VDD 7	V 22 Douglas Upstream Betal Bridge	S26°06.383'	E29°19.371'
VDD 8	2555 V30 Olifants D/S of confluence with Steenkoolspruit	S26°03.40.7	E29°15.03.8'
VDD 9	2556 V31 Olifants U/S Steenkoolspruit confluence D/S pit	S26°03.791'	E29°15.177'
VDD 10	2557 V32 Olifants D/S tributary near defunct pit U/S pit	S26°05.108'	E29°16.116'
VDD 11	2558 V40 Plant water u/g railway boreholes @ small bridge	S26°05.844'	E29°17.308'
VDD 12	2547 V11 Olifants @ DWAF Weir U/S PSS discard dump	S26°05.502"	E29°16.967'
VDD 18	2569 VW Olifants tributary from PSS dump pollution control dam	S26°05.838	E29°17.544
VDD 20	2603 Attenuation dam1	S26°04.081'	E29°18.287'
VDD 21	2604 Outlet of the Southern Canal	S26°05.109'	E29°16.629'
VDD22	2606 Exit of the Northern canal	S26°01.119'	E29°16.877'
VDD 23	Attenuation Berm 2	S26°03.599'	E29°17.653'
Douglas 1	Douglas 1-2571 W02 Olifants River at Wolwekrans Weir.	S26°00.413'	E29°15.240'





5.6.2 Surface water quality objectives

> There are various standards and objectives in terms of surface water quality, depending on what the end use is to be. Some of these include the DWS South African Target Water Quality Guidelines (TWQG) for different uses (e.g. Aquatic Ecosystems and Agricultural use) that were published in 1996 and the SANS 241 Drinking Water Quality Standard (2015).

> In some cases, however, there are more specific standards in terms of the catchment itself, as determined by the Catchment Management Agency. The DWS published in 2016 Classes and Resource Quality Objectives of water resources for the Olifants River catchment. One of the key elements of this document is Resource Quality Objectives (RQO) in the Olifants River catchment. In this document the catchment is divided into various Integrated Unit of Analysis (IUA) areas and Resource Units. Each IUA has a set of water quality constituents for which limits have been set. The proposed VDDC project is located within IUA 1, which is referred to as the Upper Olifants River catchment and within Resource Unit 11.

> A summary of the different standards, guidelines and objectives is provided in Table 5.6.2.a.

For the purpose of this assessment, the 2016 RQO was used to describe the current status of the water resources in the catchment, since this is the most recent objectives set specifically for the catchment. Where no limits are provided for a specific constituent, the SANS 241 standards were used as a guideline to indicate the level of impact.

Although the TWQO were also considered, these were not used in the assessment of the current water quality status in the catchment. The guidelines provide target water quality objectives for the specific water use and is more stringent in most cases than the SANS 241 Drinking Water Quality Standard. The aquatic ecosystem is always present as a potential water user. In the case of VDDC, although some agriculture is practiced in the larger catchment area, the area immediately downstream of the VDDC section, is mining.

Table 5.6.2.a:	Standards, objectives	and	guidelines	considered	for	the	baseline
	assessment						

Constituent	Unit	TWQG Agricultural Use: Irrigation (DWS, 1996)	TWQG Aquatic Ecosystems (DWS, 1996)	SANS 241: 2015 Drinking Water Standard	RQO for Olifants River IUA 1, Resource Unit 11 (2016)
Physical					
Electrical conductivity (EC) @ 25°C	mS/m			170	111
Chemical Oxygen Demand (COD)	mg/ <b>ℓ</b>				-
рН	-	6.5-8.4	Background +/-0.50 pH units	5 to 9.7	-
Chemical, Inorganic					
Alkalinity	mg CaCO₃/ ℓ				-

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Constituent	Unit	TWQG Agricultural Use: Irrigation (DWS, 1996)	TWQG Aquatic Ecosystems (DWS, 1996)	SANS 241: 2015 Drinking Water Standard	RQO for Olifants River IUA 1, Resource Unit
		( · · )		Stanuaru	11 (2016)
Boron (B)	mg/ <b>ł</b>	≤ 0.5		2.4	-
Calcium (Ca)	mg/ <b>ł</b>				-
Chloride (Cl)	mg/ <b>ł</b>	≤ 100		300	-
Fluoride (F)	mg/ <b>ł</b>	≤ 2	≤ 0.75	1.5	-
Magnesium (Mg)	mg/ℓ				-
Potassium (K)	mg/ℓ				-
Sodium (Na)	mg/ℓ	≤ 70		200	-
Sulphate (SO <sub>4</sub> )	mg/ <b>ℓ</b>			500	500
Total Dissolved Solids (TDS)	mg/ <b>ł</b>	≤ 40	Background +/-10%	1 200	-
Metals, Dissolved					
Iron (Fe)	mg/ <b>ℓ</b>	<= 5	Background +/-10%	2	-
Aluminium (Al)	mg/ℓ	≤ 5	≤ 0.005 for pH<6.5 and ≤ 0.01 for pH>6.5		-
Manganese (Mn)	mg/ℓ	≤ 0.02	≤ 0.18	0.40	-
Chromium VI (Cr VI)	mg/ℓ	≤ 0.1	≤ 0.007		-
Plant Nutrients					
Nitrate (NO <sub>3</sub> )	mg/ℓ as N			11	4
Ammonium (NH4)	mg/ <b>ℓ</b> as N		≤ 0.007	1.5	0.1
Phosphate (PO <sub>4</sub> )	mg/ <b>ℓ</b> as P				0.125
Nickel (Ni)	mg/ <b>ł</b>	≤ 0.2		0.07	-
Arsenic (As)	mg/ℓ	≤ 0.1	≤ 0.01	0.010	-
Antimony (Sb)	mg/ℓ			0.020	-
Barium (Ba)	mg/ℓ			0.70	-
Beryllium (Be)	mg/ℓ	≤ 0.1			-
Cadmium (Cd)	mg/ℓ	≤ 0.01		0.0030	-
Total Chrome (Total Cr)	mg/ℓ			0.050	-
Cobalt (Co)	mg/ℓ	≤ 0.05		0.50	-
Copper (Cu)	mg/ <b>ł</b>	≤ 0.2		2.0	-
Lead (Pb)	mg/ <b>ł</b>	≤ 0.2		0.010	-
Mercury (Hg)	mg/ <b>ł</b>		≤ 4x10 <sup>-5</sup>	0.006	-
Molybdenum (Mo)	mg/ <b>ℓ</b>				-
Selenium (Se)	mg/ℓ	≤ 0.02	≤ 0.002	0.010	-

Constituent	Unit	TWQG Agricultural Use: Irrigation (DWS, 1996)	TWQG Aquatic Ecosystems (DWS, 1996)	SANS 241: 2015 Drinking Water Standard	RQO for Olifants River IUA 1, Resource Unit 11 (2016)
Tin (Sn)	mg/ <b>ł</b>				-
Vanadium (V)	mg/ <b>ℓ</b>	≤ 0.1		0.20	-
Zinc (Zn)	mg/ℓ	≤1	≤ 0.002	5.0	-

### 5.6.3 Baseline water quality analysis

The summarised baseline water quality results, for the data provided by South32 for periods indicated in section 5.6 is shown in **Table 5.6.3.a**, where the average, maximum and minimum concentrations are presented, together with the coefficient of variation. It is important to note that the 2016 RQO do not provide limits for all constituents and therefore the SANS 241 guidelines were used in such cases. However, there are certain constituents for which no limitations are specified.

For **Table 5.6.3.a**, values in highlighted in red indicate where the RQO for the Olifants River catchments or the SANS 241 guidelines are exceeded.



### Table 5.6.3.a: Water quality monitoring results

		RQO and SANS		EC	TDS	ss	Fe		Са	СІ	Mg	NO <sub>3</sub>	PO₄	к	Na	SO₄	AI	F	м
		Guidelines	рН	mS/m	mg/ℓ	mg/ℓ	mg/ℓ	TALK	mg/ℓ	mg/ℓ	mg/ℓ	mg/ℓ	mg/ℓ	mg/ℓ	mg/ℓ	mg/ℓ	mg/ℓ	mg/ℓ	mg
		SANS 241 2015	5-9.7	170	1200	-	2	-	-	300	-	11	-	-	200	500	-	1.5	0.
		Olifants IUA 1		111	-	-	-	-	-	-	-	4	0.125	-	-	500			
Mine	Sample Location																		
WITTE	VDD1	Average	7.71	121.59	999.33	24.61	0.08	87.50	108.02	23.11	85.78	0.16	0.00	9.43	49.27	581.80	0.08	0.91	0.
		Maximum	8.80	268.00	2444.00	252.00	0.37	142.00	269.00	61.00	210.00	0.42	0.00	14.40	176.00	1481.00	0.20	1.37	1.
		Minimum	6.05	42.40	326.00	3.60	0.01	17.00	39.00	8.13	25.50	0.00	0.00	6.15	15.90	187.00	0.02	0.60	0
		Coeff of Variation %	8.66	34.96	39.74	188.37	102.87	47.86	38.61	41.59	42.05	64.26		17.00	57.94	40.12	63.94	27.60	16
	VDD2	Average	7.71	325.45	3069.52	380.10	0.20	172.14	302.41	27.61	194.93	0.85		10.76	299.55	1900.83	0.09	0.61	1
		Maximum	8.23	523.00	5088.00	7900.00	1.86	316.00	516.00	53.50	340.00	5.68	0.00	31.00	542.00	3172.00	0.19	0.94	g
		Minimum	7.02	189.00	1548.00	4.00	0.02	57.00	150.00	3.50	87.10	0.10	0.00	1.85	112.00	895.00	0.01	0.34	0
		Coeff of Variation%	4.41	24.64	29.24	382.37	189.14	36.70	29.16	37.60	29.38	214.94		47.50	31.26	32.11	58.54	26.14	17
	VDD5	Average	8.05	90.21	674.87	26.84	0.08	115.53	72.38	24.51	50.39	0.15	0.10	9.12	54.92	342.48	0.13	0.69	
		Maximum Minimum	8.74 6.99	175.00 39.60	1524.00 280.00	91.20 0.40	0.21	155.00 60.00	149.00 28.90	50.50 12.50	139.00 16.80	0.24	0.10	13.00 6.11	110.00 24.50	863.00 95.90	0.50 0.01	1.10 0.49	(
		Coeff of Variation%	4.61	39.60	46.26	74.25	71.79	22.35	44.61	37.26	59.82	40.77	0.10	18.88	24.50 39.15	95.90 57.17	96.43	22.63	1
	VDD6	Average	7.47	132.66	1097.11	754.44	0.31	137.33	122.56	42.48	82.91	0.25	0.32	23.29	65.15	581.52	0.19	0.63	İ
	1220	Maximum	8.31	295.00	2506.00	10450.00	1.31	297.00	266.00	136.00	221.00	0.88	0.38	186.00	147.00	1439.00	1.13	1.36	1
		Minimum	6.48	26.60	182.00	1.60	0.01	32.00	18.20	9.66	9.30	0.10	0.23	4.88	10.60	63.80	0.01	0.47	
		Coeff of Variation%	6.45	59.85	65.54	330.16	107.64	49.81	57.81	79.31	74.48	94.59	25.19	187.13	65.47	70.80	141.59	30.74	1(
	VDD7	Average	7.90	209.01	2070.13	22.67	0.23	120.07	215.58	25.53	177.13	1.93		14.47	97.61	1288.03	0.52	0.66	2
		Maximum	8.44	478.00	5406.00	64.40	1.04	163.00	569.00	38.80	504.00	5.24	0.00	43.70	241.00	3480.00	9.08	0.96	1
		Minimum	7.43	32.60	230.00	2.80	0.01	69.00	23.40	11.80	13.40	0.17	0.00	5.35	21.40	60.00	0.01	0.43	(
		Coeff of Variation%	3.31	80.55	93.56	76.77	104.45	23.41	89.12	32.85	100.94	78.60		67.06	68.30	100.98	319.32	25.45	1:
	VDD8	Average	7.85	51.76	373.10	43.78	0.29	99.00	39.27	20.07	25.63	0.93	0.14	6.88	33.97	152.21	0.41	0.41	(
		Maximum Minimum	8.90 7.32	113.40 31.10	842.00 208.00	82.00 14.40	1.42 0.02	149.00 68.00	99.20 20.40	37.60 14.10	64.50 13.10	3.18 0.10	0.21 0.10	10.30 5.06	62.10 22.80	436.00 59.10	2.32 0.02	0.63 0.25	(
VDDC		Coeff of Variation%	3.85	41.54	46.72	45.78	101.19	19.80	51.00	28.04	59.79	85.19	43.45	21.61	32.44	70.37	118.22	24.37	1:
													40.40						
	VDD9	Average	7.96	74.41	565.20	24.97	0.25	110.90	60.62	22.75	40.87	0.46		8.06	45.95	269.03	0.29	0.51	
		Maximum	8.53	158.00	1410.00	54.40	0.93	158.00	150.00	46.20	115.00	1.06	0.00	13.60	98.70	780.00	1.63	0.74	
		Minimum	7.35	30.30	240.00	1.60	0.02	61.00	25.30	12.40	14.50	0.20	0.00	5.74	21.60	90.00	0.01	0.32	
		Coeff of Variation%	3.49	41.88	49.35	67.18	100.47	21.24	51.81	32.04	59.89	48.01		21.80	39.03	62.06	121.21	17.12	1
	VDD10	Average	7.87	96.47	761.40	33.74	0.23	115.20	81.99	24.31	59.98	0.25		9.80	52.21	400.72	0.21	0.67	
		Maximum	8.58	248.00	2232.00	537.00	0.73	179.00	217.00	72.00	206.00	0.41	0.00	17.00	165.00	1284.00	0.77	1.12	
		Minimum	6.53	31.30	248.00	0.80	0.01	60.00	25.40	9.76	14.80	0.10	0.00	5.71	12.00	80.10	0.01	0.39	
		Coeff of Variation%	6.53	56.70	65.31	285.22	100.97	31.65	59.11	50.76	77.87	49.49		28.55	61.04	75.02	117.26	29.94	18
	VDD11	Average	7.87 8.50	107.67 231.00	873.72 2058.00	13.30 41.20	0.23	121.69 175.00	92.54 223.00	26.92 61.70	64.28 167.00	1.05 8.50	0.00	9.63 15.90	66.07 146.00	457.89 1210.00	0.24	0.59 0.83	
		Maximum Minimum	6.78	31.20	2058.00	0.80	0.92	63.00	223.00	12.80	167.00	0.00	0.00	5.68	22.40	76.10	0.01	0.83	
		Coeff of Variation%	4.78	51.73	59.03	86.29	110.38	25.88	57.87	46.23	64.31	250.95	0.00	26.62	54.28	67.34	135.13	18.36	2
	VDD12	Average	8.14	101.19	797.33	25.55	0.33	112.04	78.44	26.67	60.93	0.24	8.96	10.85	71.85	412.65	0.18	0.65	(
		Maximum	9.04	195.40	1590.00	246.00	3.00	182.00	132.00	44.50	143.00	0.57	8.96	34.30	246.00	939.00	0.64	0.92	(
		Minimum	7.12	31.10	248.00	1.20	0.01	63.00	25.10	13.20	14.40	0.10	8.96	5.76	21.60	0.05	0.01	0.41	(
		Coeff of Variation%	5.97	47.80	52.78	186.92	186.54	25.13	46.74	39.02	61.42	68.01		50.28	65.81	65.37	107.70	23.34	1(
	VDD18	Average	6.51	29.78	217.43	69.78	1.23	35.44	22.25	7.44	12.10	1.48		6.10	17.55	110.98	0.15	0.44	(
		Maximum	7.72	74.50	614.00	320.00	4.90	187.00	70.80	28.10	31.90	4.28	0.00	20.60	41.70	347.00	1.16	0.65	3
		Minimum	4.69	5.57	36.00	1.60	0.02	5.00	2.57	1.90	1.17	0.10	0.00	1.17	1.11	14.50	0.02	0.23	0
		Coeff of Variation%	13.26	62.85	67.07	144.92	131.63	157.31	79.54	79.58	74.08	128.16		74.87	54.46	81.19	166.20	28.45	17



		RQO and SANS Guidelines SANS 241 2015 Olifants IUA 1	рН 5-9.7	EC mS/m 170 111	TDS mg/ℓ 1200	<u>SS</u> -	Fe mg/ℓ 2	TALK -	Ca mg/ℓ -	Cl mg/ℓ 300	Mg mg/ℓ -	NO <sub>3</sub> mg/ℓ 11	PO₄ mg/ℓ - 0.125	K mg/ℓ -	Na mg/ℓ 200	SO₄ mg/ℓ 500	Al mg/ℓ -	F mg/ℓ 1.5	Mn mg/୧ 0.4
Mine	Sample Location																		
	VDD20	Average	7.82	48.66	339.19	814.15	0.63	101.07	27.74	24.83	15.86	0.41	0.31	11.49	52.22	114.71	0.37	1.42	0.66
		Maximum	9.75	131.00	856.00	8264.00	1.91	424.00	125.00	130.00	42.40	1.55	0.76	28.50	251.00	412.00	3.24	6.54	3.21
		Minimum	6.36	6.09	52.00	0.40	0.06	6.00	3.31	2.92	1.02	0.12	0.00	3.40	3.20	4.39	0.01	0.43	0.01
		Coeff of Variation%	10.43	79.84	83.74	214.13	76.37	84.40	98.74	105.14	74.61	98.62	130.65	68.85	111.83	140.07	169.67	82.04	157.00
	VDD21	Average	8.05	261.64	2370.00	74.46	0.15	112.57	248.21	93.71	204.29	0.17		14.39	173.10	1500.71	0.08	0.56	0.17
		Maximum	8.59	552.00	4840.00	590.00	0.55	202.00	503.00	338.00	559.00	0.31	0.00	53.80	644.00	4118.00	0.54	1.36	1.28
		Minimum	7.06	168.00	1322.00	3.20	0.01	16.00	145.00	31.50	101.00	0.00	0.00	7.85	72.60	762.00	0.02	0.31	0.01
		Coeff of Variation%	5.14	36.89	38.16	205.82	118.56	46.71	38.49	79.70	56.89	76.39		81.74	82.26	54.47	165.44	47.92	230.24
	VDD22	Average	7.26	59.70	496.50	976.90	0.21	46.75	48.53	16.57	39.80			4.57	31.60	286.45	0.12	0.73	0.65
VDDC		Maximum	8.31	168.00	1456.00	3685.00	0.39	119.00	145.00	31.50	126.00	0.00	0.00	11.50	72.60	881.00	0.27	1.36	2.21
		Minimum	6.57	20.40	150.00	4.80	0.07	11.00	15.60	9.20	9.89	0.00	0.00	1.30	11.60	60.00	0.05	0.39	0.01
		Coeff of Variation%	10.24	121.00	128.89	185.07	77.96	104.62	132.55	62.95	144.42			105.09	87.95	138.55	87.73	59.94	162.41
	VDD23	Average	7.44	182.67	1654.56	126.02	0.20	155.56	167.32	23.87	94.80	0.33	0.26	12.17	166.74	942.44	0.09	0.89	1.03
		Maximum	8.34	433.00	4482.00	1245.00	1.07	381.00	516.00	48.90	293.00	0.98	0.35	53.40	418.00	2839.00	0.33	1.94	8.00
		Minimum	6.20	35.40	256.00	10.80	0.02	10.00	30.60	5.56 53.72	17.50	0.11	0.12	0.30	23.60	70.20	0.01	0.33	0.01
	Develop 4	Coeff of Variation%	6.28	80.06	89.35	209.30	129.45	56.12	87.60		87.50	77.42	38.22	92.64	89.02	101.80	84.58	37.63	228.71
	Douglas 1	Average Maximum	7.80 8.23	47.01 69.80	340.13 526.00	42.19 178.00	0.36	85.63 113.00	34.04 45.60	18.13 23.80	21.77 32.70	0.64	0.00	6.62 8.83	31.74 61.90	140.74 229.00	0.31 1.65	0.45 0.60	0.06
		Maximum Minimum	8.23 7.49	28.30	224.00	4.80	0.02	65.00	45.60 22.90	13.20	32.70 13.70	0.21	0.00	8.83 5.24	22.10	75.90	0.03	0.60	0.43
		Coeff of Variation%	2.70	22.01	224.00	4.00	131.92	13.72	22.90	13.20	26.72	45.93	0.00	14.93	30.33	32.94	137.12	18.52	223.21



**Figure 5.6.3.a to Figure 5.6.3.b** indicate the average and maximum concentrations measured at each monitoring location, in terms of compliance with the RQO or SANS 241, for pH, sulphate ( $SO_4$ ) and electrical conductivity (EC) respectively.

5.6.4 Baseline water quality interpretation

The values for various constituents measured around the proposed VDDC infrastructure and development area were compared to the RQO for the Olifants and SANS 241 guidelines; pH, SO<sub>4</sub>, EC, Iron (Fe), Aluminium (AI) and Manganese (Mn) are discussed below:

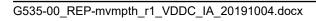
### 5.6.4.1. pH

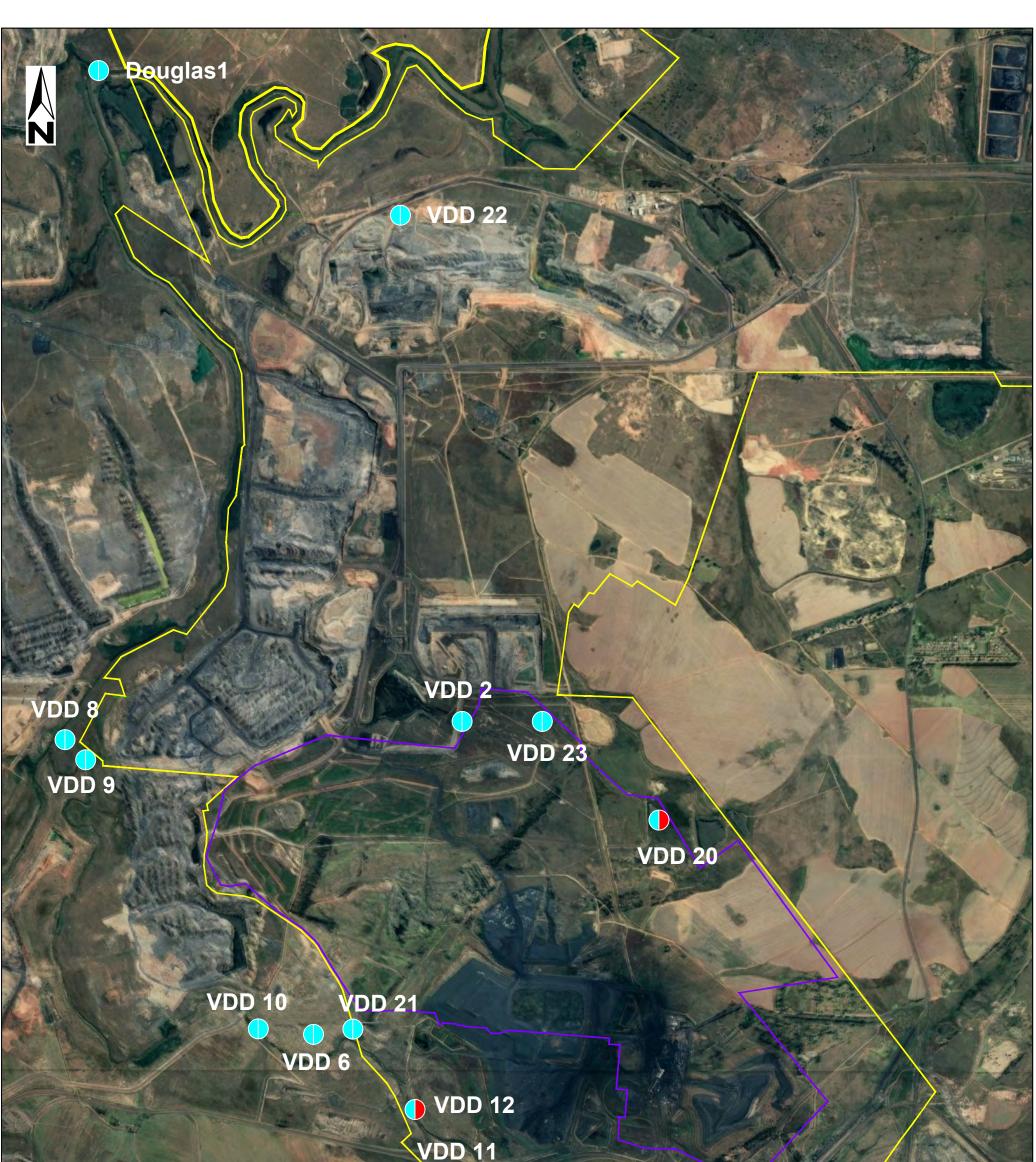
The pH of natural waters is a measurement of the acidity/alkalinity and is the result of complex acid-base equilibrium of various dissolved compounds. The pH of most raw water sources is within the range of 6.5 to 8.5 (DWAF, 1996). A decrease in the pH of water in a mining area will be an indication of acid mine drainage (AMD).

The results in **Table 5.6.3.a** indicate the following:

- On average, all of the monitoring points are within the required pH range of 5 to 9.7.
- Minimum recorded levels of pH which fell out of the required pH range, and lower than the required 5.0 was at monitoring point VDD18 – 2569 VW Olifants tributary from PSS dump pollution control dam. A decrease in the pH level may be due to mining activities.
- Maximum recorded levels of pH which fell out of the required pH range, and higher than the required 9.7 was at monitoring point VDD20 – 2603 Attenuation dam1 which may be due to agricultural activities.

pH levels are indicated in Figure 5.6.4.a





<u>pH</u> ● 5 - 9.7 (SANS 241) ● <5 or >9.7 Average - Out of Range	VDD 11 VDD 18 VDD 5 VDD 5	
<ul> <li>Mining Rights Area (MRA)</li> <li>VDDC Opencast Area</li> </ul>	Coordinate System: Cape LO 29	YAN
Jones & Wagener Engineering & Environmental Consultants 59 Bevan Road PO Box 1434 Rivonia 2128 South Africa tet:0027 11 519 0200 vww.javsco.za email: post@javsco.za	South32 SA Coal Holdings (Pty) Ltd VDDC Project <u>pH Levels</u>	Job No G535-391 Figure 5.6.4.a

### 5.6.4.2. Sulphate (SO<sub>4</sub>)

The concentration of sulphates in natural surface water is typically low (~5mg/ $\ell$ ), although concentrations of several hundred mg/ $\ell$  may occur where dissolution of sulphate minerals or discharge of sulphate-rich effluents takes place (DWAF, 1996). AMD decanting or seeping from mining areas can increase the sulphate in surface water significantly. Chemical fall-out during rain events in areas where coal burning takes place can also increase the sulphate content of surface water bodies.

Sulphate is a key indicator of water affected by coal mining. The results in **Table 5.6.3.a** indicate that for maximum recorded sulphate concentrations, all of the monitoring points exceed the required SO<sub>4</sub> concentration limit of 500mg/l with the exception of VDD8 - 2555 V30 Olifants D/S of confluence with Steenkoolspruit, VDD20 - 2603 Attenuation dam1, VDD18 2569 VW Olifants tributary from PSS dump pollution control dam and Douglas1- 2571 W02 Olifants River at Wolwekrans Weir.

On average, the majority of the monitoring points exceed the required SO<sub>4</sub> concentration limit, with the exception of VDD5 -2545 V09 Oxbow 9 ponded water, VDD9- 2556 V31 Olifants U/S Steenkoolspruit confluence D/S pit, VDD10- 2557 V32 Olifants D/S tributary near defunct pit U/S pit, VDD11-2558 V40 Plant water u/g railway boreholes @ small bridge, VDD12- 2547 V11 Olifants @ DWAF Weir U/S PSS discard dump and VDD 22-2606 Exit of the Northern canal Douglas 1.

The monitoring data indicates that the water upstream of the VDDC mining section shows an impact as a result of the land use activities. The elevated sulphate concentrations at these locations may be attributed to mining activities in the area.

SO<sub>4</sub> concentrations are indicated in **Figure 5.6.4.b**.

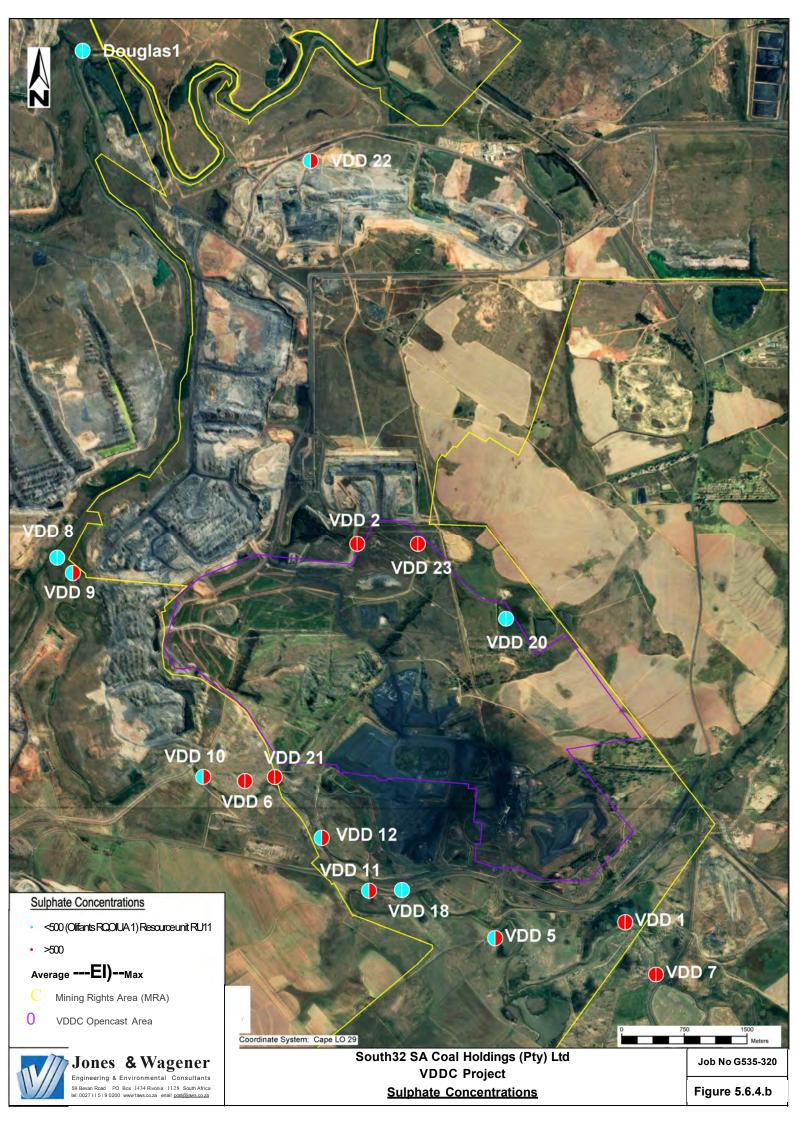
5.6.4.3. Electrical Conductivity (EC)

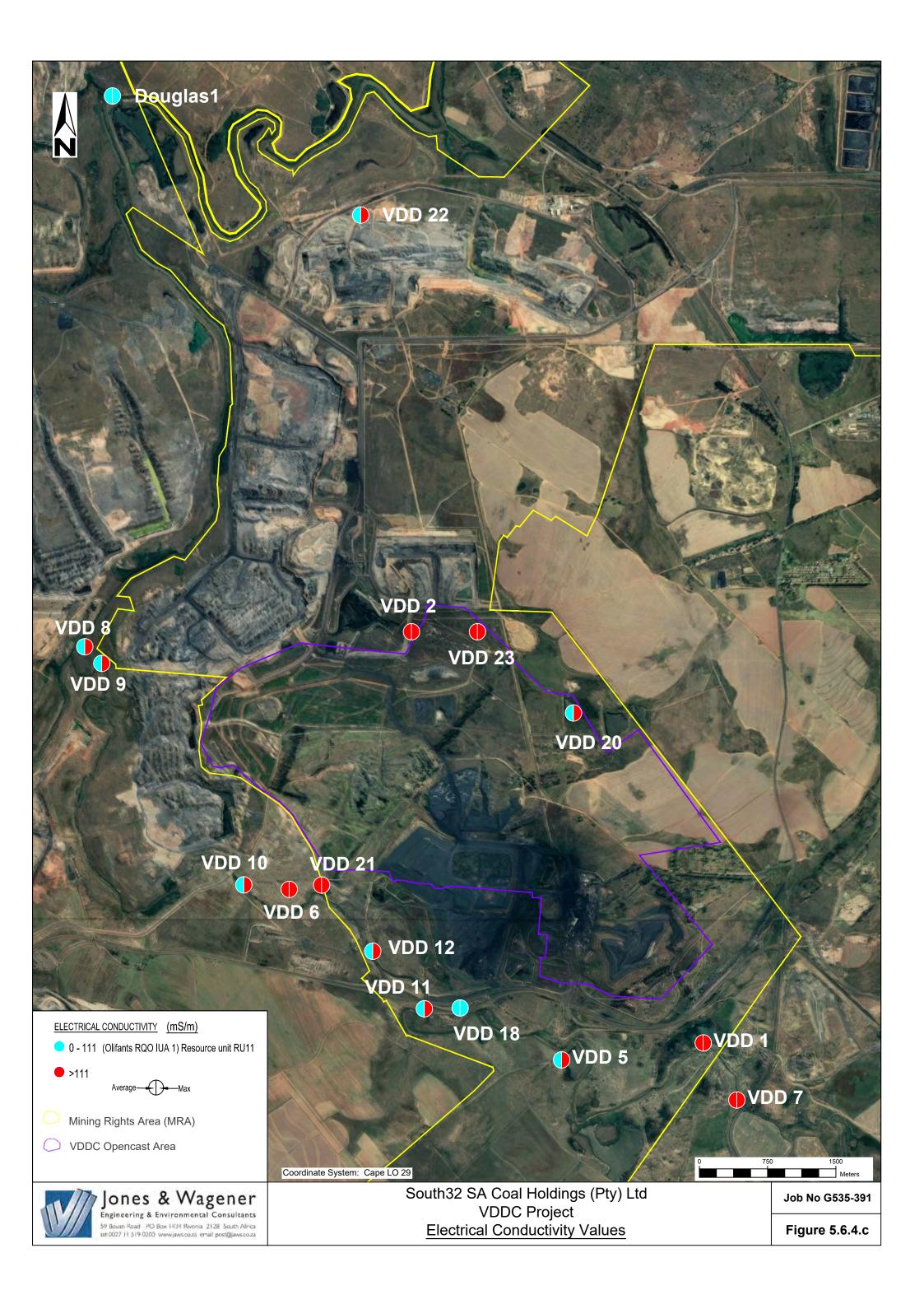
Electrical conductivity (EC) is a measure of the ability of water to conduct an electrical current, which is as a result of the presence of charged ions such as carbonate, bicarbonate, chloride, sulphate, nitrate, potassium, calcium and magnesium (DWAF, 1996). It is therefore an indicator of the salinity, or total salt content, of water. Accumulation of salts can influence the potential to use the water downstream by water users.

The results in **Table 5.6.3.a** indicate that on average, elevated EC levels were noted at monitoring locations VDD1-2538 V01 Springbokspruit @ entrance to mine property,VDD2-2542 U/s of vlei shaft & V7 con. Belt, VDD6-2551 V16 Olifants D/S of PSS discard dump, VDD7- V 22 Douglas Upstream Betal Bridge, VDD21-2604 Outlet of the Southern Canal and VDD23- Attenuation Berm 2. Elevated EC for these locations may be attributed existing mining activities in the area.

EC levels are indicated in **Figure 5.6.4.b**. The monitoring data shows an impact on the water resources upstream of the VDDC mining area as a result of the land use activities.







### 5.6.4.1. Iron (Fe)

Iron (Fe) is the fourth most abundant element, constitutes 5% of the earth's crust and is found in many minerals. An important mineral in the context of this investigation is pyrite (FeS), which is often associated with coal formations. Iron can be present in water as dissolved ferric iron (Fe III), as ferrous iron (Fe II) or as suspended iron hydroxides. The concentration of dissolved iron in unpolluted surface water is typically in the range of 0.001 - 0.5 mg/ $\ell$  (DWAF, 1996). There are no limits provided in the RQO for iron. The SANS 241 guidelines for iron is set as 2 mg/ $\ell$ .

The results in **Table 5.6.3.a** indicate on average, iron concentrations for all monitoring locations are within the guideline limits. Maximum recorded iron concentrations which were marginally elevated were noted at VDD12- 2547 V11 Olifants @ DWAF Weir U/S PSS discard dump and VDD18 2569 VW Olifants tributary from PSS dump pollution control dam. Elevated iron concentrations may be due to mining and/or agricultural activities in the surrounding area.

### 5.6.4.2. <u>Aluminium</u>

Aluminium occurs in water either as suspended aluminium minerals or as dissolved aluminium species. The concentration of dissolved aluminium in unpolluted water at neutral pH is typically 0.005 mg/ $\ell$  or less. In water with a low pH, or where soluble aluminium complexes are present, the dissolved aluminium concentration can rise to high values (DWAF, 1996).

There are no limits set for AI in the SANS 241 guidelines or the RQO for the catchment. Therefore, the TWQO for irrigation and aquatic ecosystems was used to assess AI and are not displayed in **Table 5.6.3.a**.

The TWQO for irrigation for AI is 5 mg/*l* or less and the TWQO for aquatic ecosystems are as follows:

- For pH <6.5 the AI concentration limit is 0.005 mg/*l* or less.
- For pH >6.5 the AI concentration limit is 0.01 mg/ℓ or less.

On average, all monitoring locations are within the TWQO for irrigation, with a maximum recorded AI concentration of 9 mg/ $\ell$  noted at VDD 7-V 22 Douglas Upstream Bethal Bridge.

On average all monitoring locations have a pH > 6.5, and all monitoring locations exceed the TWQO for aquatic ecosystems of 0.01 mg/ $\ell$  or less.

Elevated aluminium concentrations may be due to agricultural activities in the surrounding area.

### 5.6.4.3. Manganese

Manganese (Mn) is a relatively abundant element which constitutes 0.1% of the earth's crust. The median concentration in fresh water is 8  $\mu$ g/ $\ell$ , with a range of 0.02 to 130  $\mu$ g/ $\ell$  (DWAF, 1996).

The results are indicated in **Table 5.6.3.a**. On average, elevated manganese concentrations were noted at the following monitoring locations:

- VDD2 2542 U/s of vlei shaft & V7 con. Belt
- VDD6-2551 V16 Olifants D/S of PSS discard dump
- VDD7 V22 Douglas Upstream Betal Bridge
- VDD18 2569 VW Olifants tributary from PSS dump pollution control dam



- VDD20 2603 Attenuation dam1
- VDD 22- 2606 Exit of the Northern canal Douglas 1
- VDD23- Attenuation Berm 2

Elevated manganese concentrations may be due to agricultural activities and mining activities in the surrounding area.

#### 5.6.4.4. Other constituents

Analysis of the other constituents in **Table 5.6.3.a** indicates the following:

- On average the TDS levels at the majority of monitoring points was highly elevated when compared to the SANS 241 guidelines, which can be attributed to mining in the area.
- On average the Na concentrations at majority of locations was within range when compared to the SANS241 guidelines, with the exception of VDD2 - 2542 U/s of vlei shaft & V7 con. belt, which can be attributed to mining in the area.
- The maximum recorded Nitrate (NO<sub>3</sub>) concentrations were elevated at monitoring points VDD2-2542 U/s of vlei shaft & V7 con. belt, VDD7-V 22 Douglas Upstream Betal Bridge,VDD11-2558 V40 Plant water u/g railway boreholes @ small bridge and VDD18 2569 VW Olifants tributary from PSS dump pollution control dam, when compared to the RQOs, which may be attributed mining activities in the area.
- Phosphate (PO<sub>4</sub>) concentrations on average as well as maximum recorded at monitoring points VDD6-2551 V16 Olifants D/S of PSS discard dump, VDD8-2555 V30 Olifants D/S of confluence with Steenkoolspruit, VDD12-2547 V11 Olifants @ DWAF Weir U/S PSS discard dump, VDD20 - 2603 Attenuation dam1 and VDD23-Attenuation Berm 2 was elevated when compared to the RQOs, which may be attributed to farming and mining activities in the area.
- Although there are no guideline limitations provided for suspended solids, several points show on average elevated suspended solids and highly elevated suspended solids for the maximum recorded at the monitoring points VDD2, VDD6, VDD20, VDD22 and VDD23. These are all within the mining area and therefore may be attributed to mining in the area.

Therefore, in terms of surface water quality within the study area there are visible impacts associated with mining activities both upstream and downstream of VDDC.

### 5.7 Biomonitoring

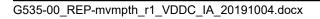
Biomonitoring is addressed in a separate specialist report .

### 5.8 Water authority

The water authority is the Department of Water and Sanitation, Mpumalanga Region.

### 5.9 Wetlands

The delineation of sensitive areas such as wetlands is addressed in a separate specialist report as part of this Scoping/EIA process.



### 5.10 Surface water use

The VDDC Project area is situated in a farming district, where water from the Olifants River and the Steenkoolspruit upstream of the mining area is used for irrigation, formal and informal domestic usage, as well as livestock watering. Other uses include domestic supply to villages and other amenities in the area.

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The Witbank Dam is located downstream of the mining area and is used for municipal and industrial water supply, as well as recreational activities such as fishing and boating.

The aquatic ecosystem is also present as a downstream user.

## 6. WATER BALANCE

The objective of the water balance modelling was to estimate the volumes of water that will be generated by the proposed activities, including effluent water and surface runoff from the dirty areas. This was assessed together with the water demands on the site to determine whether the site will operate with a water surplus or deficit and to determine the storage/treatment capacity required to ensure legal compliance, in terms of prevention of spills from the site. The water balance modelling is therefore a key input to the overall water management strategy for the site.

It is important to note that Golder Associates updated the overall water balance for Wolvekrans Colliery to include the VDDC infrastructure and mining project (including areas that are authorised but does not form part of this environmental application process) (please refer to Report : "Inclusion of VDDC water management into Wolvekrans site wide water management plan", July 2019, Report number 19124625-327233-1). Input, in terms of the pit water make and surface runoff from the proposed infrastructure and mining areas were provided by J&W to Golder and Associates.

Therefore, the following section details the VDDC pit water balance (i.e. estimated pit water make over the LOM), as well as the estimated surface runoff, that can be expected from the proposed infrastructure areas. For the detailed overall water balance please refer to the Golder Associates water balance update.

### 6.1 Computational methodology

Daily rainfall data from the SAWS rainfall stations 0478292 Langsloot and 0478303 Secunda, together with monthly evaporation data estimated from the "Surface Water Resources of South Africa 2012", also known as *WR2012*, were inputs to a hydrological model based on the Soil Conservation Services (SCS) method to determine runoff on a daily basis using antecedent conditions. The method (as adapted to South African conditions by Schmidt & Schulze) is believed to be highly suitable for the site, having been developed in catchments with areas of approximately 8 km<sup>2</sup>, and smaller.

The underground water inflows were derived by the J&W geohydrological team, taking into account the upfront pre-mining dewatering required for the purposes of opencast mining.

Recharge and dewatering through fracturing of strata have been taken into account using the above information received from the J&W geohydrological team. These rates of inflow were then brought into the J&W surface model, where rainfall impacts and surface water make was subsequently assessed.

The surface runoff areas were measured from Block Plan (i.e. Rev1) layout drawings prepared by the design engineers (i.e. Worley). This data was entered into the pit water balance and runoff model.

The estimated VDDC pit water make and runoff volumes were subsequently calculated.

## 6.2 Assumptions, information used and limitations

### 6.2.1 Assumptions and information used

The overall schematic flow diagram showing the water make and surface runoff volumes, over the LOM for VDDC, is presented in **Figure 6.3.3.a** (which can be found in **Section 6.3.3** below). This figure indicates the average pit water make and surface runoff over the LOM.

The following activities have been included:

- Mining will commence in 2022 and end in 2043;
- Surface runoff from the following areas (as per the Block Plan received. Refer to Table 6.2.a for the relevant numbering on the Block Plan. Note that existing areas are not included in the table):
  - Existing hard park area, which drains to Vleishaft Dam;
  - o New proposed hard park area, which drains to SKS void;
  - Topsoil dump within dirty area, which drains to Vleishaft Dam;
  - o Overburden dump, which drains to old underground workings via boreholes;
  - o Overburden dump at SKS pit, which drains to SKS void;
  - o Existing ROM stockpile to the north, which drains to SKS void;
  - Existing ROM stockpile to the south, which drains to Vleishaft Dam;
  - Mixed ROM coal and slurry stockpiles, which drains to Vleishaft Dam;
  - o Dirty water management area, to old underground workings via boreholes;
  - 4 and 5 seam coal stockpiles, which drains to the VDDC Pit.

The following key assumptions and information have been used:

- The mining areas used for the modelling are based on the LOM plans (File name: "StripAdvancepitFloor.dwg") provided to J&W by South32;
- The surface runoff areas are based on the Block Plan provided by Worley (File name: C0082005AADAL0001001Rev1.dwg/pdf);
- As per email correspondence with South32 the following was confirmed and incorporated into the model:
  - A slope of 37° for all dumps/stockpiles were used to compute runoff from side slopes;
  - Pit ramps may vary in length from 500 m to 1000 m as the pit advances with an average of approximately 700 m over life of ramp, before being rehabilitated. Therefore, it was assumed that there will be 4 ramps, each 700 m long;
  - o There will be a pre-mining dewatering of old underground workings;
  - Assumed that all water make will collect in the pit during mining of the pit, as well as the old underground recharge;
  - In terms of pre-strip, spoils and levelled spoils and rehab areas, the total disturbed length excluding the active face will be 522 m, sub-divided as follows:

	Meters					
Active face	<b>150 172 200</b>					
	Pre-strip Spoils and levelled spoils Rehab					
		522				

- For the potable water use, as per email correspondence with South32 on 11 June 2019, the potable water use at VDDC is as follows:
  - Existing water treatment plant (i.e. Middelburg Water Reclamation Plant (MWRP)) will supply 5 000 m<sup>3</sup>/month for potable use;



- Of the 5 000 m<sup>3</sup>/month, 2 682 m<sup>3</sup>/month will be for domestic use, of which 70% will report to Sewage Treatment Plant and 30% will be consumed;
- The remaining 2 318 m<sup>3</sup>/month will be used for vehicle washing, which will report to Pit 4A;
- Stochastically generated rainfall data (spanning 2019 to 2069) was supplied by Golder Associates.

A list of drawings from which information for the water balance was obtained is provided in **Table 6.2.b**.

 Table 6.2.a:
 Infrastructure areas for which runoff has been computed

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Surface Area Description	No. as per Block Plan
New Proposed Hard Park Area	12, 3, 4
Topsoil Dump Within Dirty Area	27A, B and C
Overburden Dump 1	51
Overburden Dump At SKS Pit	7
Mixed ROM coal and slurry stockpiles	39
Dirty Water Management Area	25 and 28
4 and 5 seam coal stockpile	49 and 50

## Table 6.2.bList of Drawings received from Worley and South32

Drawing No.	File name/Details
StripAdvancepitFloor.dwg	Life of Mine
C0082005AADAL0001001Rev1.dwg	Block Plan

### 6.2.2 Limitations

By their nature, models are theoretical estimates of natural phenomena that are too complex to be derived exactly. It is inevitable that there will be variations in the actual flows when compared to the predicted flows. This can only be addressed by the recalibration of modelled data with measured data, from which more reliable estimates of extreme and average water make and runoff volumes can be developed.

### 6.3 Pit water make and surface runoff volumes

### 6.3.1 Water make

The total mining water make is expected to be as follows:

- VDDC Opencast area:
  - Average water make over LOM =  $4 760 \text{ m}^3/\text{day}$ ;
- Peak summer water make =  $12 950 \text{ m}^3/\text{day}$ .
- The 2 seam underground workings:
  - Average pre-mining upfront dewatering required over two years prior to mining the VDDC opencast pit = 25 300 m<sup>3</sup>/day;
  - $\circ$  Average recharge to the opencast pit as mining progresses = 2 100 m<sup>3</sup>/day.

## 6.3.2 Surface runoff

As mentioned previously, surface runoff was required to be computed for the following areas:

- Existing hard park area;
- New proposed hard park area;
- Topsoil dump within dirty area;
- Topsoil dump to north and north east of VDDC;
- Overburden dump 1;
- Overburden dump at SKS pit;
- Existing ROM stockpile to the north;
- Existing ROM stockpile to the south;
- Mixed ROM coal and slurry stockpiles;
- Dirty water management area;
- 4 and 5 seam coal stockpiles.

## 6.3.2.1. SCS runoff estimation

Surface runoff volumes over the LOM can be seen in **Figure 6.3.3.a.** 

The SCS runoff estimation typically requires historical daily rainfall data from a gauge in close proximity to the site. However, for this simulation, stochastically generated rainfall data was supplied by Golder Associates and subsequently utilised for the SCS runoff modelling.

The estimated SCS runoff depths computed for each surface runoff area (i.e. infrastructure area), was then multiplied by the delineated catchment area to determine the anticipated flow volume for each surface runoff area.

Computational parameters required for SCS runoff estimation include:

- Daily rainfall data as received from Golder Associates;
- Evaporation data taken directly from the WR90 report, with a Mean Annual Evaporation of 1 600 mm (Symons Pan);
- SCS curve number a value of 75 has been used;
- Crop factor for evaporation.

## 6.3.2.2. Daily rainfall data



This data was provided by Golder Associates. Rainfall data was received in the form of a stochastically generated daily rainfall depth from 2019 till 2069 (i.e. beyond the extent of the modelling period).

#### 6.3.2.3. Evaporation data

Monthly evaporation data was taken directly from the WR90 report for the Evaporation Zone into which the site falls. The Evaporation Zone is 4A. The Mean Annual Evaporation for this zone is 1600 mm. The average monthly evaporation depths are presented in Table 1.3.2(a) below.

#### Table 6.3.2.a: Average monthly evaporation depths (from *WR90*)

Month	Average evaporation (mm)
October	176
November	147
December	145
January	111
February	94
March	76
April	83
Мау	110
June	143
July	172
August	163
September	179
Annual Total	1600

#### 6.3.2.4. SCS curve number

The SCS runoff curve number is a catchment response index to rainfall. This curve number gives indicative conditions for the site based on soil and vegetation types and ensures the potential maximum retention of the soil is within reasonable limits for the anticipated conditions. The higher the curve number the higher the runoff response will be.

For this runoff estimation, the anticipated soil zones were determined from the South African Atlas of Agro-hydrology and Climatology (Reference: R.E Schulze, "South African Atlas of Agrohydology and Climatology, 1997)\_ and were translated into hydrological soil groupings based on data provided by Schmidt and Schulze (1987), and subsequently an applicable curve number for veld runoff (i.e. 75).



Runoff was either calculated based on a percentage of veld runoff or as a percentage of rainfall. The area and runoff factors for each surface infrastructure area documented below in **Table 6.3.2.b** 

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Surface Area	Area (ha)	Runoff as % of veld runoff	Runoff as % of rainfall
Existing Hard Park area	4.10	N/A	90%
New Proposed Hard Park area	5.30	N/A	90%
Topsoil dump within dirty area	14.30	90%	N/A
Topsoil dump within dirty area	47.20	90%	N/A
Overburden dump 1	21.10	90%	N/A
Overburden dump at SKS pit	135.70	90%	N/A
Existing ROM stockpile to the north	3.00	90%	N/A
Existing ROM stockpile to the south	4.50	90%	N/A
Mixed ROM coal and slurry stockpiles	25.90	90%	N/A
Dirty water management area	54.00	N/A	90%
4 and 5 seam coal stockpiles	31.20	90%	N/A

 Table 6.3.2.b:
 Surface areas and runoff

### 6.3.2.5. Crop factors

Crop factors were used in the model to modify evapotranspiration rates in order to vary antecedent moisture conditions for the soil. A higher evapotranspiration rate will translate to lower antecedent moisture conditions and therefore higher infiltration and lower runoff.

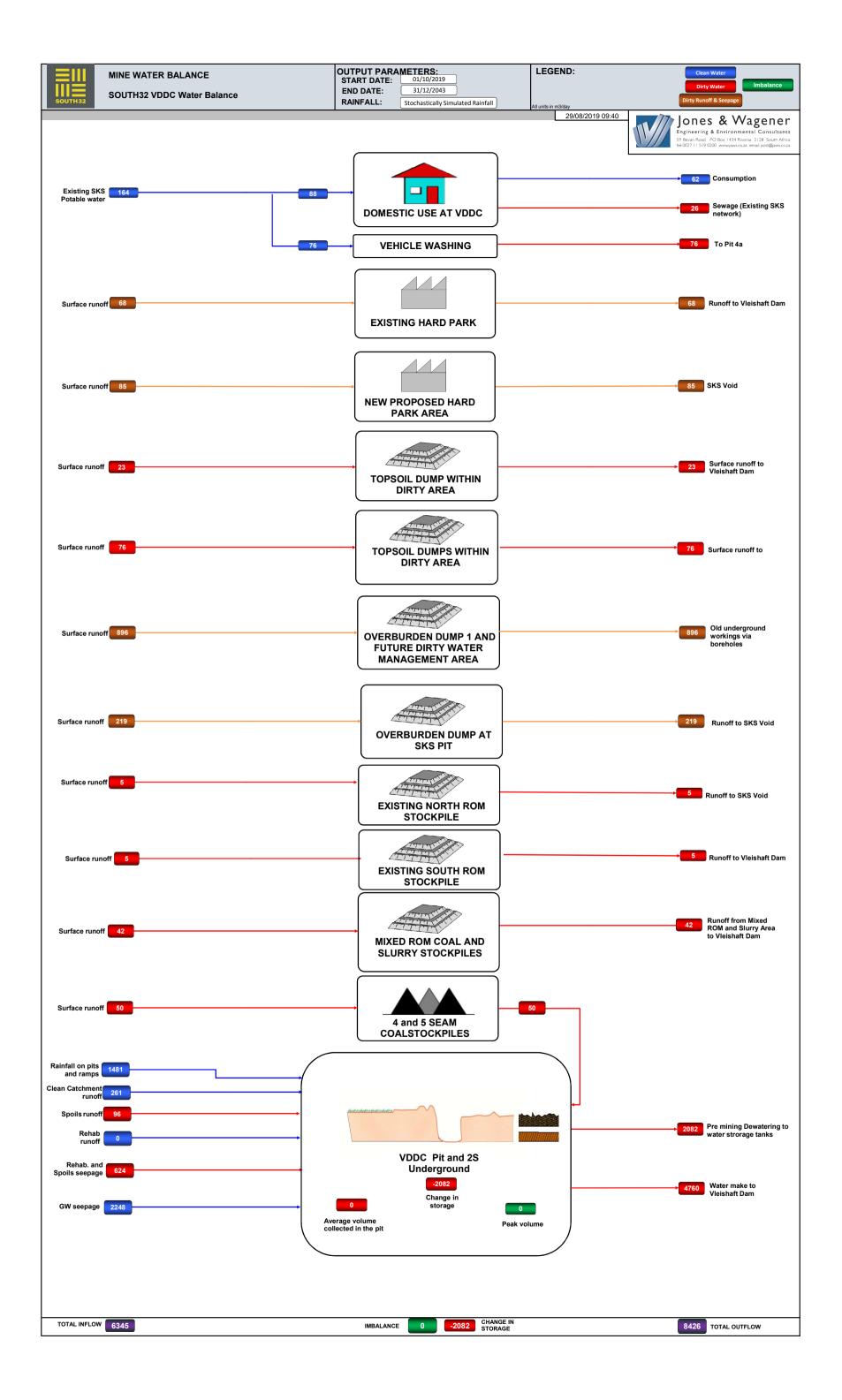
For this analysis crop factors were obtained from the WR90 report for Karoo and Karroid and used in the runoff estimation.

### 6.3.3 Schematic water balance diagram

The schematic water balance diagram is presented in **Figure 6.3.3.a** for the average water flows over the life of mine and over the operational period for the opencast workings (2022 to 2043).

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### 6.4 Conclusions

The old 2 Seam underground workings have filled with water. This area will need to be dewatered prior to mining the VDDC pit and is therefore a key to the success of the proposed project.

The current plan is to make extensive use of mechanical evaporators to manage the pit water make and dewatering water from VDDC. Timing and location of the mechanical evaporators are provided in Table 4.3.1.a. The VDDC pit water balance as well as the estimated surface runoff, that can be expected from the proposed infrastructure areas was computed by J&W as input to the overall site wide water balance compiled by Golder Associates.

The water management plan for VDDC impacts on the site wide water balance as some of the infrastructure and mine workings such as Vleishaft Dam and Steenkoolspruit are planned to be used to manage the VDDC mine water make.

The total water make to be managed for the pit is estimated as follows:

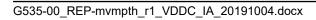
VDDC Opencast area:

0	Average water make over LOM	= 4 760	) m³/day;
0	Peak summer water make	= 12 950	) m <sup>3</sup> /day.

As mentioned above, Golder Associates were appointed to update the site wide water management model for the Wolvekrans Colliery to include the mine plan and catchment areas from the VDDC feasibility study with the above input provided by J&W.

The following conclusions have been extracted from the Golder Associates report:

- The dewatering rates during 2020 and 2021 are estimated to be about 27 000 m<sup>3</sup>/d. During this period the site wide water balance model showed that the planned installed evaporator capacity will be insufficient to manage the water. South32 should consider installing the 8 evaporators at SKS by November 2019.
- The extensive use of the evaporators will result in salt buildup in the water bodies over which the evaporators are spraying. Therefore, monitoring of salination of water due to brine evaporation will need to be undertaken and corrective action carried out if need be.
- Vleishaft Dam is expected to spill during the period 2020 to 2022 which is during the initial VDDC dewatering period. The spills will report to the SKS pit. During this initial dewatering period, Golder Associate's model estimates that the SKS pit will decant into the adjacent Glencore workings. Therefore, the evaporators at SKS pit should be installed earlier than the planned implementation date of May 2020. After 2029, the 18 000 m<sup>3</sup>/d of evaporator capacity installed at SKS pit will draw down the water level in the pit.



# 7. CONSIDERATION OF ALTERNATIVES

Various alternatives were evaluated in terms of the overall water management, including the following issues:

### 7.1 Clean water management

In so far as is practically possible all clean catchment draining towards the dirty areas at VDDC will be diverted around the dirty areas, in order to minimise the generation of contaminated water, as well as maximise the clean runoff draining to the natural system, thereby minimising the impact on catchment yield.

### 7.2 Minimising the generation of dirty water make

All storm water generated on the site is considered dirty and will be contained in the opencast pit or old underground workings before being directed to the Vleishaft Dam and from there, to one of the evaporator sites, or to the proposed modular WTP or to Vlaklaagte void.

The mixing of clean and dirty water will be avoided, and the footprint of the dirty water areas have been minimised as far as is practically possible.

### 7.3 Maximising the reuse of dirty water

Dirty water will be collected and stored at Vleishaft Dam. Surplus water will be pumped from Vleishaft Dam, to one of the evaporator sites, or to the proposed modular WTP or to Vlaklaagte void.

### 7.4 Implementing treatment where required

Surplus water which cannot be handled through the evaporation system, will be conveyed to a mobile, modular WTP with a maximum treatment capacity of 20 Ml/day.

Brine from the WTP will be collected in existing tanks and before being conveyed to the evaporators at the SKS void.

Effluent from the WTP (i.e. treated mine water) will be conveyed via an existing mine water pipeline to the existing northern clean water canal, from where it will discharge via a wetland area into the Olifants River.

## 7.5 Alternatives in terms of process development

These are detailed in the main EMPr document.



# 8. ENVIRONMENTAL IMPACT ASSESSMENT AND MITIGATION MEASURES

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In order to quantify the potential impacts, the general format of the assessment is to first assess the impact assuming no mitigation measures are applied. In some instances, these impacts could not result without extreme or unlawful practices, such as discharging all of the affected water from the mining facilities into the river system. However, this provides a basis for the "worst case" scenario, from which mitigation measures can be evaluated (such as containment or treatment for example). The residual impact after implementation of the mitigation measures is then assessed and indicated.

Cumulative impacts are also assessed as and where this is practical.

The format of the impact assessment is as follows:

- Section 8.1: The impact assessment methodology and rating system is described.
- Section 8.2: The nature of the various activities is described in terms of the phases of the project, from construction through to post closure.
- Section 8.3: The activities are assessed, detailing the potential impacts, proposed mitigation and residual impact over the full life cycle of the project.
- Section 8.4: The proposed mitigations are summarised to form a summarised water management plan.

A summarised water management plan is provided in Section 10.

### 8.1 Impact assessment methodology and rating system

The rating of impacts was undertaken according to the impact rating and assessment process outlined in **Appendix B**.

# 8.2 Activities to be undertaken at the Vandyksdrift Central (VDDC) area that could potentially affect surface water

There are five main phases within the proposed project, namely:

- Planning Phase.
- Construction Phase.
- Operational Phase.
- Decommissioning Phase.
- Closure Phase.

Each of these phases is outlined below.

#### 8.2.1 Planning Phase

During the planning phase, the proposed project is conceptualised. This includes undertaking preliminary/ conceptual and detailed designs of the proposed infrastructure development and opencast mining, environmental screening, specialist environmental baseline investigations and the application for the required Integrated Environmental Authorisation and WUL.

### 8.2.2 Construction phase

Once the relevant authorisations have been received, construction activities will commence. This involves the establishment of the facilities and infrastructure as specified in Section 4 above.

Activities to be undertaken that may potentially impact on surface water include the following:

- General construction activities:
  - Civil works.
  - Movement of materials and equipment.
  - Servicing of construction vehicles and equipment.
- Construction of mine surface infrastructure
- Construction of the pit:
  - Earthworks, access roads and ramps.
  - Excavation and stockpile waste material.
  - Concrete and steel work.
- Construction of water management infrastructure:
  - Clean and dirty water canals.
  - Sediment traps.
  - Pump stations and pipelines.
- Construction of roads:
  - Access and internal roads.
- Construction of a WTP

Rehabilitation of any surrounding areas impacted by the construction of infrastructure components must occur immediately after the construction thereof except if there are plans to mine in these areas in the near future.

### 8.2.3 Operational Phase

The infrastructure will be utilised during this phase when mining commences. Topsoil stripping will be conducted, and topsoil stockpiles will be placed separately for use during rehabilitation. Boxcut spoils dumps will be established, and overburden will be stripped and stockpiled following blasting. Coal will be extracted and transported to the No. 4 and No. 5 seam stockpiles or to the mixed ROM coal and slurry stockpile areas. Mine-affected water will be collected and managed as described above.

The "roll-over" mining method will be used for the opencast operations, whereby mining and rehabilitation will be undertaken concurrently. As part of the ongoing mining operations the rehabilitation process will already start with topsoil stripping ahead of the mining operation. After the removal of the coal, the overburden will be levelled and the topsoil replaced and re-vegetated.

The operational phase ends when the last reserves have been extracted.

The activities that can impact on surface water include the following:

- Opencast mining operation.
- Alteration of flows in watercourse due to WTP treated effluent discharges.



- WTP operation.
- Transport of coal to the existing crushing and screening plant
- Loading and unloading of coal.
- Operation and maintenance of the water management system around the opencast operations.
- Cleaning, repair and maintenance activities along roads.
- Dust and fire suppression water management.
- Operation of the water management system, including sediment management and management of the water levels in the PCD and the pumping systems.
- Stockpiling of mine residues and ROM coal.

### 8.2.4 Decommissioning Phase

This is the period directly after cessation of operational activities. It includes the removal of all operation-related equipment that has no beneficial re-use potential, as well as reclamation, rehabilitation and/or restoration of any final remaining areas (e.g. backfilling of final ramps and voids, landform shaping, topsoiling and seeding).

### 8.2.5 Closure Phase

The point in time when all decommissioning and rehabilitation activities have ceased, monitoring has been completed and the mine applies for a closure certificate.

### 8.3 Surface water impact assessment and mitigation measures

The impacts are described in terms of the nature of the activity that could potentially impact on surface water, the nature of the impact if not mitigated, possible mitigation measures and the long-term impact.

Cumulative impacts are not addressed in the tables in **Section 8.3**, but are noted in **Section 8.4**.

### 8.3.1 Construction Phase

8.3.1.1. Impact on surface water quality

The construction phase impacts on surface water quality are detailed in **Impact Tables** C1 to C3

8.3.1.2. Impact on surface water quantity – catchment yield and flow rates

The construction phase impacts on surface water quantity are detailed in **Impact Table C4**.

### 8.3.2 Operational Phase

8.3.2.1. Impact on surface water quality

The operational phase impacts on surface water quality are detailed in **Impact Tables O1** to **O4**, **O6** to **O9**, **O11**.

#### 8.3.2.2. Impact on surface water quantity – catchment yield

The operational phase impacts on surface water quantity are detailed in **Impact Tables O5** and **O10** to **O11**.

#### 8.3.3 Decommissioning and Closure Phases

#### Impact on surface water quality 8.3.3.1.

The decommissioning and closure phase impacts on surface water quality are detailed in Impact Tables D1, D2 and PC1.

#### 8.3.3.2. Impact on surface water quantity – catchment yield

During decommissioning and closure the affected areas will be rehabilitated to generate clean runoff and will be restored to free draining conditions. Until the water management infrastructure is decommissioned the impact on catchment yield will remain as per the Operational Phase.

#### 8.3.4 Post Closure Residual Impacts

#### 8.3.4.1. Impact on surface water quality

Post closure the site will be rehabilitated, grassed and made free draining. All of the contaminated materials will have been removed from the site.

The impact on water quality is detailed in Impact Table PC1

#### 8.3.4.2. Impact on surface water quantity – catchment yield

Post closure all areas, including the shaft area, will be rehabilitated and made free draining. There will therefore be no long-term impact on catchment yield.

### 8.4 Cumulative impacts

The Wolvekrans Colliery and Ifalethu Colliery within the mining right area, form a large portion of surface disturbance in relation to the other activities in the area that could potentially impact on surface water. The VDDC area is small in relation to the existing Wolvekrans and Ifalethu Collieries mining area. However, it does add to the surface disturbance of Wolvekrans Colliery as a whole.

There are other existing coal mining operations in the region, Kleinkopje in the west, Black Wattle Colliery to the north, as well as Mavela Colliery and Muhanga Mine on the banks of the Spookspruit downstream of the Middelburg Water Reclamation Plant located at Ifalethu Colliery, but these are small in relation to Wolwekrans and Ifalethu Colliery and iMpunzi Complex..

In addition, there are numerous coal mines in the Olifants River catchment, both upstream and downstream of the mine, as well as surrounding agricultural activities, power stations and industrial areas that also potentially impact on the water quality and quantity in the catchment. Wolvekrans Colliery does form a large portion of this area.

The cumulative impact of the VDDC mining operation extension, with the mitigation measures described in the impact assessment, is considered to be medium to high in relation to the current and anticipated future activities in the area, as the catchment is already impacted by mining activities. The cumulative impact of all of the coal mines in the area has resulted in deterioration of water quality and quantity in the region. Every

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new mine contributes to the further reduction and / or deterioration of the water resources in the Mpumalanga region and in particular the Olifants River catchment. It is essential that good water management be implemented at VDDC to limit further contributions to the existing impacts in the catchment.



CONSTRUCTION PHASE		
General mine development		
Construction laydown areas, construction works, movement of materials and construction equipment		
Water Quality – discharge of contaminated water		
Pollution of surface water resources		

# Impact C1 Construction Phase – General mine development – Impact on surface water quality

#### IMPACT DESCRIPTION AND EVALUATION

During the construction phase topsoil will be stripped and civil works, in the form of earthworks and terracing will be undertaken as part of the preparation of the area for the mine and infrastructure development. Impacts may arise from:

- Erosion of soils during rainfall events, with elevated suspended solids in the runoff water.
- Resultant elevated suspended solids in the watercourses, as well as sedimentation in the watercourses.
- Hydrocarbon spillages from fuel storage, servicing areas or construction equipment itself, with resultant elevated hydrocarbon concentrations in runoff water and watercourses.

The surrounding and downstream surface water resources, namely the Olifants River, are considered stressed water resources in terms of both the quantity of water in the system and the quality of the water. The Olifants River also forms part of the water supply for irrigation water further downstream (from the Witbank Dam). Any impact on the quantity or quality of water in the system has the potential to affect the quality and assurance of supply to the community and agriculture.

IMPACT BE	IMPACT BEFORE MANAGEMENT								
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Low	Local	Short- term	Very Likely	LOW	2	Probable			
2	3	2	4	1.87					
MANAGEME									

#### MANAGEMENT MEASURES

The following mitigation measures will be implemented:

- The footprint of disturbed areas will be minimised.
- "No-go" zones will be delineated for construction plant and personnel where they are in close proximity to the Olifants River.
- Diversion of clean upslope runoff away from the new proposed pit to be constructed first before establishment of box-cuts.
- The construction area will largely be within the existing dirty water management area of the mine. Stormwater will be managed in terms of the existing system..
- Surface water management infrastructure, such as storm water canals, sediment traps and sumps are to be constructed first at the south east overburden stockpiles and dirty water management infrastructure area to ensure that contaminated runoff and dirty water spills are contained.
- Servicing of construction vehicles will take place only in dedicated areas that are equipped with drip trays.
- Bunded containment and settlement facilities will be provided for hazardous materials, such as fuel and oil.
- Spill-sorb or a similar product will be kept on site, and used to clean up hydrocarbon spills in the event that they should occur.
- Erosion protection measures will be implemented at steep areas.
- A waste management plan will be developed for the construction phase.
- Appropriate sewage management will be implemented during the construction phase that would tie into the existing sewage management strategy at Wolvekrans Colliery, which will entail the use of portable chemical toilets.
- Existing water quality monitoring will continue downstream of the construction areas, before and during construction where practical, in order to detect any increase in suspended solids or turbidity.

PHASE		CONSTR	CONSTRUCTION PHASE				
		General	General mine development				
ACTIVITY			Construction laydown areas, construction works, movement of materials and construction equipment				
ASPECT		Water Q	uality – discharge	of contaminated w	ater		
IMPACT DEI		Pollution	of surface water r	esources			
			uction areas will be		ease in suspended	Solius, Waler	
	ement arour	nd the constru			ease in suspended		
manag	ement arour	nd the constru			Impact Class	Confidence	
manag IMPACT AF	ement arour	GEMENT	uction areas will be	e reviewed.			

#### Construction Phase - Removal of material from the initial boxcuts -Impact C2 Impact on surface water quality

PHASE	CONSTRUCTION PHASE	
ACTIVITY	Initial boxcut	
ACTIVITY	Removal of material from the boxcut	
ASPECT	Water Quality – discharge of contaminated water	
IMPACT DEFINITION	Pollution of surface water resources	

#### IMPACT DESCRIPTION AND EVALUATION

The construction phase is considered to end once carbonaceous material, in the form of the coal seam, is exposed within the boxcut. However, much of the overburden removed prior to the exposing of coal has the potential to contain some carbonaceous material.

The boxcut will be done using a combination of dragline and truck and shovel. Overburden from the boxcut will be placed on four overburden dumps located in between the proposed ramps.

In addition, provision has been made for one new overburden dump to be developed in the south-east of the project area and an extension of an existing overburden dump at the SKS pit.

All overburden dumps will be mined through with the exception of the south east overburden dump. The material from this dump will be removed and used in the concurrent rehabilitation of the opencast pit. The dump footprint will be rehabilitated.

Impacts may arise from:

- Erosion during rainfall events, resulting in increased turbidity and suspended solids in the runoff water, reporting to the local watercourses.
- Deposition of sediments in the local watercourses, impacting on the aquatic ecology.
- Overburden stockpiles will potentially contain carbonaceous material, with the potential to affect downstream watercourses by increasing sulphate and TDS concentrations.
- Increase in turbidity and suspended solids.

IMPACT BEFORE MANAGEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence	
Moderate	Local	Medium term	Very Likely	MODERATE	3	Definite	
3	3	3	4	2.4			

#### MANAGEMENT MEASURES

The following mitigation measures will be implemented:

- Runoff and seepage from the overburden dumps located in between the proposed ramps will be directed to Vleishaft Dam.
- Runoff and seepage from the overburden dumps located at the SKS pit will drain to the SKS void.
- Runoff and seepage from the overburden dumps in the south-east of the project area will be diverted via a canal and berm system to silt traps and a set of boreholes which will take all runoff into the underground workings. This will allow the water to be temporarily stored until it can be pumped via the mine dewatering system to the PCD (Veishaft dam).
- Existing monitoring of the water gualities will continue in the streams downstream of the boxcuts and overburden dumps will be undertaken, in order to identify the potential impacts on water quality.

IMPACT AFTER MANAGEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence	
Very Low	Local	Medium term	Unlikely	VERY LOW	2	Definite	
1	3	3	2	0.93			



PHASE	CONSTRUCTION PHASE		
ACTIVITY	Initial boxcut		
ACTIVITY	Removal of material from the boxcut		
ASPECT	Water Quality – discharge of contaminated water		
IMPACT DEFINITION Pollution of surface water resources			

# Impact C3 Construction Phase – Dewatering of water ingress to boxcut – Impact on surface water quality

PHASE	CONSTRUCTION PHASE			
ACTIVITY	Initial boxcut			
ACTIVITY	Dewatering of water ingress to boxcut			
ASPECT	SPECT Water Quality – discharge of contaminated water			
IMPACT DEFINITION	PACT DEFINITION Pollution of surface water resources			
IMPACT DESCRIPTION AND EVALUATION				

In order to mine the VDDC reserve, the water contained in the old underground workings must be removed prior to mining. This will be achieved by drilling a number of boreholes into the old underground workings and to abstract the water via these boreholes.

Water will be pumped from the boreholes accessing different underground compartments and will be transferred via borehole connector pipelines to the Vleishaft Dam and/or directly to the evaporation tanks that will be located at the evaporation sites where water will be evaporated using mechanical evaporators. This has been authorised.

Water that enters the boxcut, both from groundwater seepage from the headwalls of the pit, recharge from the old underground workings and direct rainfall, is expected to be largely clean. However, there is a possibility that this water will make contact with carbonaceous and pyritic materials. The water quality from the boxcut is therefore likely to be slightly to moderately impacted in terms of sulphate, TDS and suspended solids.

Impacts may arise from:

- Deposition of sediments in the local watercourses, impacting on the aquatic ecology.
- Discharge of the potentially impacted water to the environment, with a resultant increase in sulphate and TDS concentrations in the natural watercourses.

IMPACT BEI	FORE MAN	AGEMENT				
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence
Moderate	Local	Medium term	Very Likely	MODERATE	3	Definite
3	3	3	4	2.4		

#### MANAGEMENT MEASURES

The following mitigation measures will be implemented:

- The water will be contained at the site, at in-pit sumps and pumped from here to either Vleishaft Dam for reuse in the existing mining operations or pumped to existing mechanical evaporators for disposal.
- Surface water management measures, such as clean upslope diversion canals and berms to divert clean catchment away from mine workings, will be implemented.
- A Water Use Licence for the dewatering of groundwater encountered during mining has been issued.

IMPACT AFTER MANAGEMENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence
Low	Local	Short term	Unlikely	VERY LOW	2	Definite
2	3	2	2	0.93		
		•				

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Impact C4	Construction Phase – mine surface infrastructure, and boxcut area –
	Impact on surface water quantity

PHASE	CONSTRUCTION PHASE			
	Mine surface infrastructure, and boxcut areas			
ACTIVITY	Construction Laydown areas, construction works, movement of materials and construction equipment, excavation of boxcut and incline shaft			
ASPECT Water Quantity – containment of runoff from the site				
IMPACT DEFINITION Reduction in catchment yield				
IMPACT DESCRIPTION AND EVALUATION				

During construction, surface runoff will not ne released to the catchment., as all proposed activities are within the dirty footprint

All runoff and rainfall in the boxcut pits will be contained in the dirty water system and will therefore be lost to the catchment.

The loss in yield during the construction phase will be significantly lower than during the operational phase, which is quantified in **Table 05** below, and is therefore not quantified individually here, given that the construction of the boxcuts will take place while the rest of the mine is operational.

Impacts may arise from:

• Containment of contaminated runoff water emanating from the site, with no release to the catchment.

Although runoff from dirty areas will be contained (see management measures below) and the probability of impact is definite, its significance has still been assessed as <u>LOW</u> on the basis of the very small volumes of water that will be contained.

#### **IMPACT BEFORE MANAGEMENT**

Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence	
Very Low	Study Area	Medium term	lt's going to happen	LOW	1	Definite	
1	2	3	5	2			

#### MANAGEMENT MEASURES

The following mitigation measures will be implemented:

- The aerial extent of the disturbed and potentially contaminated areas will be kept to a minimum.
- Areas where dirty construction activities are carried out (e.g. servicing areas and workshops, fuel storage areas, waste storage areas) will be minimised and surrounded by bunds.
- Upslope runoff will be diverted around construction activities to minimise the volume of dirty water generated and contained.
- Surplus dirty water will be sent to existing mechanical evaporators for disposal.

IMPACT AFTER MANAGEMENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence
Very Low	Study Area	Short-term	It's going to happen	LOW	1	Definite
1	2	2	5	1.67		
		-			-	

# Impact O1 Operational Phase – Mine water discharge – Impact on surface water quality

PHASE	OPERATIONAL PHASE			
ACTIVITY	Mine water discharge – pit water make			
ACTIVITY	Discharge of mine water to the natural watercourses			
ASPECT	CT Water Quality – discharge of contaminated water			
IMPACT DEFINITION	Pollution of surface water resources			
IMPACT DESCRIPTION AND EVALUATION				

It is important to note that the mine water balance assessment undertaken by Golder (reference "Inclusion of VDDC water management into Wolvekrans site wide water management plan" report 19124625-327233-1, July 2019) is aimed at ensuring that the mine does not spill water during the operational phase, except for extreme events related to rainfall, with a risk of recurrence of 2% or less in any one year. The water management measures detailed in Section 4 and the Golder July 2019 report are mitigation measures, focusing primarily on the storage, reuse and treatment of water.

However, to merely indicate that the mine will not spill dirty water does not allow an assessment of the potential impact of non-compliance with the mitigation measures proposed. In order to assess the impact without mitigation, this impact assessment assumes that all dirty water is discharged to the catchment, where after detail is provided on how this will be prevented, and the impact after management is then assessed.

Impacts may arise from:

- Clean runoff entering the mine affected areas and coming into contact with carbonaceous material, with resultant high salinity, particularly sulphate content.
- Dirty runoff and mine water make discharging to the environment.

The potential impact on aquatic life or downstream users of water within the rivers is highly dependent on the pH of the water discharged. This is because acidic conditions will result in mobilisation of metals, and this would be a major contributing factor to the potential toxicity of the water.

,	5	1	,					
IMPACT BEI	IMPACT BEFORE MANAGEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
High	Regional	Medium to Long term	Very Likely	HIGH	4	Definite		
4	4	4	4	3.2				
MANAGEMENT MEASURES								

The mine water balance will be managed as detailed in Section 4 and the Golder July 2019 water balance report. These measures will include the following:

- Pumping of all dirty water generated at the VDDC workings and proposed infrastructure areas to Vleishaft Dam.
- Reuse of dirty water in the operations at VDDC.
- Treatment of excess dirty water (water pumped from Vleishaft Dam to the mobile water treatment plant or evaporators).
- Provision of water management facilities with a risk of spill that is lower than 2% in any one year as per the Golder water balance.
- A surface water quality monitoring programme will be implemented, as detailed in Section 11, to detect any impacts.
- A water balance monitoring programme will be implemented, as detailed in Section 11, to enable calibration of the water balance.

IMPACT AFTER MANAGEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence	
Moderate	Regional	Medium to Long term	Unlikely	LOW	3	Probable	
3	4	3	2	1.33			



# Impact O2 Operational Phase – Mine development area (infrastructure area) – Impact on surface water quality

PHASE	OPERATIONAL PHASE		
ACTIVITY	Mine development area		
ACTIVITY	Opencast pit and related infrastructure		
ASPECT Water Quality – contaminated runoff			
IMPACT DEFINITION	EFINITION Pollution of surface water resources		

#### IMPACT DESCRIPTION AND EVALUATION

The required surface infrastructure at the pit will be constructed at the start of mining and will remain in place for the duration of mining.

The overburden material has the potential to generate poor quality runoff due to contact of the water with carbonaceous material.

Overburden from the boxcut will be placed on four overburden dumps located in between the proposed ramps. In addition, provision has been made for two overburden dumps. A new overburden dump will be developed in the south-east of the project area and the existing overburden dump at the SKS pit will also be used.

The overburden material has the potential to contain carbonaceous material and therefore potential to generate poor quality runoff due to contact of the water with carbonaceous material.

Impacts associated with the opencast pit are as a result of runoff entering the pits and coming into contact with carbonaceous material.

Impacts may arise from:

- Contaminated storm water runoff, that discharges from the site, with resultant deterioration in water quality within the Olifants River, associated with increased suspended solids, hydrocarbons (oils and greases), siltation of carbonaceous materials, and an increase in salinity and potential decrease in pH in the watercourses.
- Contaminated seepage from the overburden dumps, with potentially elevated sulphate and TDS.
- Leakage of contaminated water from pipelines, poorly maintained storm water channels, sumps, sediment traps and oil skimmers, etc.
- Erosion at the clean canal discharge points could result in the formation of erosion gullies on surface, with elevated suspended solids in the runoff water, potentially impacting on the water quality in the watercourses in terms of suspended solids and deposition of silt.
- Increase in sulphate, turbidity, suspended solids and TDS due to runoff entering the pits and becoming contaminated.

IMPACT BEI	IMPACT BEFORE MANAGEMENT										
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence					
Very High	Regional	Medium term	Very Likely	HIGH	4	Probable					
5	4	3	4	3.2							
MANAGEME	MANAGEMENT MEASURES										

The following mitigation measures will be implemented:

- All proposed infrastructure areas with the potential to generate dirty storm water runoff, washdown water will be located within the designated dirty water areas.
- Clean runoff will be diverted around the designated dirty areas by means of cut-off canals, sized to accommodate at least the 1:50 year peak flow event.
- Adequate erosion protection will be provided at the clean canal discharge locations.
- With regard to general and hazardous wastes, For this project VDDC will follow what is currently done at Wolvekrans Colliery (please refer to Section 4.5).
- All pipeline routes will be inspected regularly to enable early detection of leaks.
- All contaminated storm water generated at the proposed activities will be collected and pumped to Vleishaft Dam.



PHASE	OPERATIONAL PHASE
ACTIVITY	Mine development area
ACTIVITY	Opencast pit and related infrastructure
ASPECT	Water Quality – contaminated runoff
IMPACT DEFINITION	Pollution of surface water resources

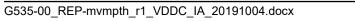
- Runoff from clean catchments draining towards the overburden dumps located in the south east of the project area will be diverted around the dumps.
- An inspection and maintenance plan will be implemented on the storm water system to ensure that all sediment handling facilities are maintained and that storm water canals and pipelines remain unblocked and free flowing monthly inspections will be carried out.
- Spill-sorb or a similar type product must be kept on site and used to clean up hydrocarbon spills in the event that they should occur.
- A surface water quality monitoring programme will be implemented to detect any impacts.
- All overburden dumps will be mined through with the exception of the south east overburden dump. The
  material from this dump will be removed and used in the concurrent rehabilitation of the opencast pit. The
  dump footprint will be rehabilitated.

IMPACT AFTER MANAGEMENT									
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Moderate	Regional	Medium term	Unlikely	LOW	2	Probable			
3	4	3	2	1.33					

# Operational Phase – Dust Suppression with contaminated water – Impact on surface water quality Impact O3

on surface water quality									
PHASE		OPERA	OPERATIONAL PHASE						
Dust Suppression									
ACTIVITY		Dust sup	pression on haul r	oads and stockpile	s				
ASPECT		Water Q	uality – spillage of	contaminated wate	er and coal particul	ates			
IMPACT DE	FINITION	Pollution	of surface water r	esources					
IMPACT DE	SCRIPTION	AND EVALU	JATION						
<ul> <li>Dust suppression will be provided on surface along haul roads and on stockpile areas. This water will become contaminated once it comes into contact with the dirty surface.</li> <li>Impacts may arise from: <ul> <li>Spillage of dust suppression water to the watercourses or associated watercourses, with resultant deterioration in water quality, in terms of elevated salinity, particularly sulphate.</li> <li>General dust suppression water contaminating the surface and washing off during rainfall events, with resultant deterioration in water quality, in terms of elevated salinity, particularly sulphate</li> </ul> </li> </ul>									
	FORE MAN	AGEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Moderate	Local	Medium term	Very Likely	MODERATE	3	Probable			
3	3	3	4	2.4					
MANAGEME	NT MEASU	IRES							
<ul> <li>The following mitigation measures will be implemented:</li> <li>A formal procedure for dust suppression will be developed and implemented. This will ensure that dust suppression application rates are carefully controlled to prevent the application of excessive water and to prevent ponding and runoff of dust suppression water into the watercourses.</li> <li>No dust suppression should be carried out on surfaces that are already moist.</li> <li>Dust suppression with contaminated water should be confined to isolated dirty water management areas.</li> </ul>									
IMPACT AF		GEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Low	Site	Medium term	ledium Unlikely VERY LOW						
2	1	3	2						

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Impact O4	<b>Operational Phase – Transportation of Coal – Impact on surface water</b>
	quality

PHASE		OPERAT	OPERATIONAL PHASE							
		Transpo	ortation of c	oal						
ACTIVITY		Transpo	Transport of coal via haul roads for processing							
ASPECT		Water Q	uality – spilla	age of contamina	ated water	and coa	al particulat	tes		
IMPACT DEF		Pollution	of surface v	vater resources						
IMPACT DESCRIPTION AND EVALUATION										
Transport of coal by road has the potential to impact on watercourses and general runoff quality, primarily due to spillage of coal from overloaded trucks, as well as contaminated water from the load boxes of the trucks on inclines.										
	ssing Plant.			rom the active V tigations are giv		the coa	al processir	ng area at the South		
<ul> <li>Coal spillage, or spillage of water transported from the pit with the coal from the haul trucks onto the haul roads, with resultant contamination of storm water, particularly with elevated salinity and sulphate.</li> <li>Storm water runoff coming into contact with these emissions would suffer a deterioration in water quality, with increased salinity, particularly sulphate.</li> </ul>										
IMPACT BEFORE MANAGEMENT										
Significance	Extent	Dura	ition	Probability	RATING		Impact Class	Confidence		
Low	Local	Med	ium term	Could Happen	LOW		2	Probable		
2	3	3		3	1.6		Z	FIODADIE		
MANAGEME	NT MEASU	RES				-				
<ul> <li>The following mitigation measures will be implemented:</li> <li>The majority of haul roads and haulage of coal will take place within the dedicated dirty water area, with runoff draining either to the opencast pit or to Vleishaft Dam, where it will be contained.</li> <li>All dirty water containment facilities should be designed, operated and maintained to have a risk of spill of 2% or less (1:50 year recurrence interval) in any one year.</li> <li>As far as is practical, ROM coal should be allowed to drain within the pit before being loaded onto the haul trucks, to prevent spillage of water from the haul truck load boxes onto the haul roads.</li> <li>Loading of trucks will be carefully controlled to ensure that overloading will not take place.</li> </ul>										
Significance	Extent	Duration	Probability	RATING	Impact	Class		Confidence		
Very Low	Local	Medium term	Unlikely	VERY LOW	, 1			Probable		
1	3	3	2	0.93						

# Impact O5 Operational Phase – VDDC mining operation – Impact on surface water quantity

PHASE	OPERATIONAL PHASE				
ACTIVITY	VDDC mining operation				
ACTIVITY	Isolation of dirty catchment				
ASPECT	Water Quantity – containment of runoff from the site				
IMPACT DEFINITION Reduction in catchment yield					
IMPACT DESCRIPTION AND EVALUATION					

The loss in yield associated with mining at the VDDC operation will be primarily due to the pit areas and associated infrastructure, which will be isolated from the catchment due to the containment of dirty runoff. Although it is planned to undertake concurrent rehabilitation, so that the dirty water make, as well as the loss of yield to the catchment will be minimised, the assessment below assumes the worst case, being no concurrent rehabilitation, so that the opencast pit, as well as all overburden dumps would be isolated from the clean catchment.

Loss in yield is assessed for Witbank Dam in the area.

The loss of yield is quantified in the following table:

Location	Catchment area (km²)	MAR Pre- Construction (x10 <sup>6</sup> m³)	MAR during operations (x10 <sup>6</sup> m³)	Percentage reduction (%)
VDDC opencast pit	11.4	0.36	0	100
New proposed infrastructure	1.6	0.05	0	100
Extension/replacement of existing infrastructure	1.4	0.04	0	100
VDDC Infrastructure and mining project in total	14.5	0.45	0	100
Olifants River Downstream of the mine property	3309	188.1	187.65	0.24
Witbank Dam	579	190	189.5	0.24*

\* Note: The runoff calculations are not accurate to three decimal places. However, the values remain indicative of the magnitude of the impact.

It is evident from the table above that the impact in surface water yield to the most downstream watercourse and Witbank Dam is <u>LOW</u>.

#### IMPACT ON WATERCOURSES

LOCAL SCALE: Immediately downstream of site and at Witbank Dam

Impact before management									
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Moderate	Regional	Medium term	Unlikely	LOW	2	Probable			
3	4	3	2	1.33	2				

#### Management measures

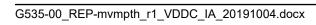
The following mitigation measures will be implemented:

• Concurrent rehabilitation will take place, and the rehabilitation will be shaped to be free draining. Where rehabilitated areas are sloped towards the active opencast pit, berms and canals will be constructed to maximise the area that is free draining.

• The site layout has been designed to minimise the dirty footprint, and therefore to minimise the impact on the catchment yield. No further mitigation is considered necessary.

PHASE		OPERATIONAL PHASE							
		VDDC mining operation							
ACTIVITY		Isolation of dirty cat	chment						
ASPECT		Water Quantity – co	ontainment of run	off from the site					
IMPACT DEFIN	NITION	Reduction in catchn	nent yield						
Impact after management									
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Moderate	Regional	Medium term	Unlikely	LOW	2	Probable			
3	4	3	2	1.33	2				
REGIONAL SC	ALE: Losko	p Dam							
Impact bef	ore manage	ment							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Low	Site	Medium term	Unlikely	VERY LOW		Probable			
2	1	3	2	0.8	1				
Impact afte	r managem	ent							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence			
Low	Site	Medium term	Unlikely	VERY LOW		<b>-</b> · · ·			
2	1	3	2	0.8	1	Probable			
				•					

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# Impact O6 Operational Phase – Operation of a mobile water treatment plant – Impact on surface water quality

PHASE		OPERAT	OPERATIONAL PHASE					
		Mobile v	vater treatment p	lant				
ACTIVITY		Operatio	Operation of the water treatment plant, treatment of contaminated mine water					
ASPECT Water Quality – Runoff from WTP								
IMPACT DEF		Pollution	of surface water r	esources				
IMPACT DES		AND EVALU	JATION					
Mine impacte proposed mo				m and thereafter, to	o one of the evapo	rator sites, or to the		
WTP with a n	naximum tre	eatment capa				a mobile, modular n existing tanks and		
northern clea treated to cor April 2016.	n water can nply with Re	al, from wher	e it will discharge	onveyed via an exis via a wetland area ne Olifants River ca	into the Olifants Ri			
Impacts may								
				n deterioration of w				
	ge of water		•	the form of brine to ge standards, or ur	•	ng upset conditions at		
IMPACT BEF		AGEMENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
High	Regional	Long term	Very Likely	HIGH	4	Droboble		
4	4	4	4	3.2	4	Probable		
MANAGEME	NT MEASU	IRES						
The following	mitigation r	neasures will	be implemented:					
				water area and cor will be directed to		ills from the treatment or SKS Pit.		
				ted bunded areas,				
	ection and r s within spe		plan will be implen	nented to ensure th	hat the water treatr	nent plant always		
•	ge water qu		ontinuously monito	ored for early detec	tion of discharge v	vater quality		
		itions occur, c shaft Dam or		vater quality be de	tected, the WTP di	scharge will be		
IMPACT AFT		GEMENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
Low	Study Area	Long term	Unlikely	LOW	2	Probable		
2	2	4	2	1.06	-			
CUMULATIV	E IMPACT							
Cumulative in	npacts not a	assessed here	e, see Section 8.5.					

# Impact O7 Operational Phase – Handling and storage of waste from water treatment plant – Impact on surface water quality

PHASE		OPERATIO	OPERATIONAL PHASE					
ACTIVITY		Water treatment plant						
		Handling a	nd storage of wa	aste from the WTP				
ASPECT		Water Qua	lity – discharge	of contaminated wa	ater due to contact	with waste products		
IMPACT DEFI	NITION	Pollution o	f surface water r	esources				
IMPACT DESC	CRIPTION A	ND EVALUA	TION					
<ul> <li>The proposed water treatment plant will generate a liquid waste (brine). Brine from the WTP will be collected in existing tanks and before being conveyed to the evaporators at the SKS void.</li> <li>Impacts may arise from: <ul> <li>Spillage of brine onto the ground surface.</li> <li>Inadequate lining systems, or leakage from the liners at the tanks into which the Brine will be pumped.</li> </ul> </li> </ul>								
IMPACT BEFO	ORE MANAG	BEMENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
High	Regional	Long term	Very Likely	HIGH	4	Probable		
4	4	4	4	3.2	4	Flobable		
MANAGEMEN	T MEASUR	ES						
The exist to the Vie	ing closed ta eishaft Dam. ction and ma	anks are loca		signated dirty wate		vill be will be pumped		
IMPACT AFTE	R MANAGE	MENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
Low	Study Area	Long term	Unlikely	LOW	2	Probable		
2	2	4	2	1.06				
CUMULATIVE	IMPACT							
Cumulative impacts not assessed here, see Section 8.5.								

# Operational Phase – Discharge of treated water from the water treatment plant – Impact on surface water quality Impact O8

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PHASE	PHASE OPERATIONAL PHASE							
ACTIVITY		Water tr	Water treatment plant					
		Discharg	Discharge of treated water to the Olifants River					
ASPECT		Water Q	uality – discharge	of treated water				
IMPACT DEI	INITION	Pollution	of surface water r	esources				
IMPACT DESCRIPTION AND EVALUATION								
Effluent from the WTP (i.e. treated mine water) will be conveyed via an existing mine water pipeline to the existing northern clean water canal, from where it will discharge via a wetland area into the Olifants River. Water will be treated to comply with Resource Quality Objectives for the Olifants River catchment as published in GN 466 in April 2016.								
and erosion r				will influence the w	ater quality of the l	receiving resource		
The baseline water quality shows that the Olifants River is already heavily impacted. The quality of water should therefore improve due to dilution effects.								
IMPACT BEI		AGEMENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
High	Regional	Long term	Very Likely	HIGH POSITIVE	4	Possible		
4	4	4	4	3.2				
MANAGEME	NT MEASU	IRES						
<ul> <li>The following mitigation measures will be implemented:</li> <li>Erosion protection measures at the discharge point</li> <li>The quality of the water discharged will be closely monitored to ensure that it complies with the specified RQO at all times.</li> </ul>								
IMPACT AFTER MANAGEMENT								
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
High	Regional	Long term	Very Likely	HIGH POSITIVE	4	Possible		
4	4	4	4	3.2				
CUMULATIVE IMPACT								
Cumulative impacts not assessed here, see Section 8.5.								

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Impact O9	Operational Phase – Discharge of water through forced evaporation–
	Impact on surface water quality

PHASE	OPERATIONAL PHASE							
ACTIVITY	Mechanical Evaporators							
ACTIVITY	Forced evaporation	Forced evaporation						
ASPECT	Water Quality – dischar	Water Quality – discharge of water from the evaporators						
IMPACT DEFINITION	Pollution of surface wat	ter resources						
IMPACT DESCRIPTION AND EVALUATION								
Number of Evaporators	Location	Time Period	Capacity (m³/d)					
8 – 2000 m³/d each	Vleishaft Dam	Currently operating	4800					
20 - 2000 m³/d each	Vlaklaagte South	Currently operating	12000					
12 - 3000 m³/d each	5 Seam opencast	Installed in November 2019	10800					
8 - 3000 m³/d each	Steenkoolspruit pit	Installed in May 2020	7200					
20 - 3000 m³/d each	Steenkoolspruit pit Steenkoolspruit pit Steenkoolspruit pit SKS by June 2024		18000					

Surplus water which cannot be handled through the evaporation system, will be conveyed to a mobile, modular WTP with a maximum treatment capacity of 20 Ml/day. Brine from the WTP will be collected in existing tanks and before being conveyed to the evaporators at the SKS void. The extensive use of the evaporators will result in salt buildup in the water bodies over which the evaporators are spraying.

The release of contaminated water into the catchment will influence the water quality of the receiving resource due to wind-blown contamination. The baseline water quality shows that the Olifants River is already heavily impacted.

IMPACT BEFORE MANAGEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence	
Moderate	Regional	Medium to Long term	Very Likely	MODERATE	3	Possible	
3	4	4	4	2.93			
MANAGEMENT MEASURES							

The following mitigation measures will be implemented:

- Forced evaporation not to happen during high wind conditions. The average daily wind speed during summer months has been around 18 km/h which drops to around 14km/h in winter months. August and September tends to be windier. In recent years the maximum sustained wind speed has reached 65 km/h, that's the equivalent of around 40 mph, or 35 knots. (from <a href="http://www.myweather2.com/City-Town/South-Africa/Witbank/climate-profile.aspx">http://www.myweather2.com/City-Town/South-Africa/Witbank/climate-profile.aspx</a>).
- Ongoing surface water monitoring of surrounding watercourses.
- Where forced evaporation occurs over seeded areas, it is recommended that monitoring of soils by a soils specialist be undertaken. The need for this monitoring is to be assessed by the soils specialist.
- Forced evaporation to spray only over pits and not close to the South32 boundary or over clean areas.
- Forced evaporation not to take place in close proximity to watercourses. Where evaporators are in close proximity to watercourses (i.e. evaporators at SKS void) monitoring at these areas to take place more frequently due to proximity to the Olifants River.



PHASE		OPERAT	OPERATIONAL PHASE					
ACTIVITY		Mechan	Mechanical Evaporators					
		Forced e	Forced evaporation					
ASPECT		Water Q	Water Quality – discharge of water from the evaporators					
IMPACT DEFINITION		Pollution	Pollution of surface water resources					
Need to monitor salination of water due to brine evaporation and corrective action taken if need be.								
IMPACT AFTER MANAGEMENT								
Significance	Extent	Duration	uration Probability RATING Impact Class Confidence					
Low	Regional	Medium to Long term	Could Happen	LOW	2	Possible		
2	4	3	3	1.80				
CUMULATIVE IMPACT								
Cumulative impacts not assessed here, see Section 8.5.								

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# Impact 010 Operational Phase – Discharge of treated water from the water treatment plant – Impact on surface water quantity

plant - impact on Sanace water quantity								
PHASE		OPERA	OPERATIONAL PHASE					
ACTIVITY		Mobile V	Mobile Water Treatment Plant					
		Discharg	Discharge of treated water to the Olifants River					
ASPECT		Water Q	uantity – discharge	e of treated water				
IMPACT DEF	INITION	Pollution	Pollution of surface water resources					
IMPACT DESCRIPTION AND EVALUATION								
The discharge of treated water to the river system will result in a net increase in the flow of water in the Olifants River. While this has a net positive impact on the availability of water in the system as well as assist with the offset in yield loss due to mining as quantified in Table O5, it has the potential to negatively impact on the aquatic ecology by changing the seasonal flow patterns in the river system. This net percentage increase in flow during summer and winter cannot be quantified due to limited information regarding discharge rates to the Olifants River. However, the potential impacts have been assessed below and should be are-assessed once discharge rates are available. The potential impacts to the ecology of the river systems due to the discharge of treated water falls outside the scope of this surface water assessment and will be assessed as part of the aquatic ecology and wetland assessments.								
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
Moderate	Regional	Medium to Long term	Very Likely	MODERATE Positive	3	Possible		
3	4	3	4	2.66				
MANAGEMENT MEASURES								
No mitigation as increase in yield is positive.								
IMPACT AFTER MANAGEMENT								
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence		
Moderate	Regional	Medium to Long term	Very Likely	MODERATE Positive	3	Possible		
3	4	3	4	2.66				
CUMULATIVE IMPACT								
Cumulative impacts not assessed here, see Section 8.5.								

Impact O11	Operational Phase – Consequence of extreme floods – Impact on surface
	water quality and quantity

		OPERA	TIONAL PHASE				
ACTIVITY		VDDC In	nfrastructure Deve	elopment			
ACTIVITY		All activit	All activities				
ASPECT		Flooding	of mine or mine in	nfrastructure during	g extreme flood eve	ents	
IMPACT DEI	INITION	Impact o	n mining operation	ı			
IMPACT DES	SCRIPTION	AND EVALU	JATION				
deposits or d whichever is no mitigation the workings even life if the The propose South32 is in	umps may b the greater. measures a could be floo e flooding in d VDDC pit o the process	e placed with Should mine re implement oded, with co the pit is sev does not ence of updating	hin the 1:100 year to e workings and infr ted, under extreme onsequent contami vere. roach on the 2004, these floodlines as	floodline, or a dist astructure be plac flooding conditior nation of the flood , 1:100 year floodli the available floo	ns in the watercours waters, as well as ne of the Olifants F dlines for the area	any watercourse, signated areas and ses (Olifants River) loss of production or River. However, are more than 5	
years old. However, it is not anticipated that the VDDC pit will encroach on the updated floodline and therefore the impact below will still remain relevant. In addition to the above, Attenuation Dam 1, which is an existing dam, is located directly upstream of the proposed VDDC boxcut area and poses a potential risk to mining in this area, as the stability of the dam wall is uncertain.							
In addition to VDDC boxcu	the above, <i>i</i> t area and p	Attenuation E oses a poten	Dam 1, which is an Itial risk to mining i	existing dam, is lo n this area, as the	cated directly upst stability of the dam	ream of the proposed n wall is uncertain.	
VDDC boxcu It was recogn needed on th	t area and p iised by Sou e dam itself.	oses a poten th32 that the . There is als	itial risk to mining i dam wall needs to o a farm dam, that	n this area, as the b be inspected to d	cated directly upst stability of the dam etermine the status Attenuation Dam	n wall is uncertain. s and any work	
VDDC boxcu It was recogn	t area and p hised by Sou e dam itself. count in the	oses a poten th32 that the . There is als above planni	itial risk to mining i dam wall needs to o a farm dam, that	n this area, as the b be inspected to d	stability of the dam etermine the status	n wall is uncertain. s and any work	
VDDC boxcu It was recogr needed on th taken into ac	t area and p hised by Sou e dam itself. count in the	oses a poten th32 that the . There is als above planni	itial risk to mining i dam wall needs to o a farm dam, that	n this area, as the b be inspected to d	stability of the dam etermine the status	n wall is uncertain. s and any work	
VDDC boxcu It was recogn needed on th taken into ac	t area and p iised by Sou e dam itself. count in the FORE MANA	oses a poten th32 that the . There is als above planni AGEMENT	itial risk to mining i dam wall needs to o a farm dam, that ing.	n this area, as the b be inspected to d is upstream of the	stability of the dam etermine the status Attenuation Dam	n wall is uncertain. s and any work 1 that needs to be	
VDDC boxcu It was recogn needed on th taken into ac IMPACT BEI Significance	t area and p nised by Sou e dam itself. count in the <b>ORE MAN</b> Extent	oses a poten th32 that the . There is als above planni AGEMENT Duration <i>Medium</i>	itial risk to mining i dam wall needs to o a farm dam, that ing. Probability	n this area, as the b be inspected to d is upstream of the <b>RATING</b>	stability of the dam etermine the status Attenuation Dam Impact Class	n wall is uncertain. s and any work 1 that needs to be Confidence	
VDDC boxcu It was recogn needed on th taken into ac IMPACT BEI Significance Moderate	t area and p nised by Sou e dam itself. count in the <b>ORE MAN</b> Extent Regional 4	oses a poten th32 that the . There is als above planni AGEMENT Duration Medium term 3	itial risk to mining i dam wall needs to o a farm dam, that ing. Probability <i>Unlikely</i>	n this area, as the b be inspected to d is upstream of the <b>RATING</b>	stability of the dam etermine the status Attenuation Dam Impact Class	n wall is uncertain. s and any work 1 that needs to be Confidence	
VDDC boxcu It was recogn needed on the taken into ac IMPACT BEI Significance Moderate 3 MANAGEME The following • No min R704 e • Investig	t area and p ised by Sou e dam itself. count in the ORE MAN/ Extent Regional 4 NT MEASU mitigation n ing within th xemptions a gate into upg	oses a poten th32 that the . There is als above planni AGEMENT Duration Medium term 3 RES neasures will ese restricted and Section 2 grading and s	tial risk to mining i dam wall needs to o a farm dam, that ing. Probability Unlikely 2 be implemented: d areas will take pla c1(c) and (i) water of	n this area, as the o be inspected to d is upstream of the <b>RATING</b> <i>LOW</i> <i>1.33</i> ace without the reluse licenses (in ter	stability of the dam etermine the status Attenuation Dam Impact Class 2 evant authorisation	n wall is uncertain. s and any work 1 that needs to be Confidence Probable	
VDDC boxcu It was recogn needed on the taken into ac IMPACT BEI Significance Moderate 3 MANAGEME The following • No min R704 e • Investig	t area and p ised by Sou e dam itself. count in the ORE MAN/ Extent Regional 4 MT MEASU mitigation n ing within th xemptions a gate into upg in this area	oses a poten th32 that the There is als above planni AGEMENT Duration Medium term 3 RES neasures will ese restricted and Section 2 grading and s before mining	tial risk to mining i dam wall needs to o a farm dam, that ing. Probability Unlikely 2 be implemented: d areas will take pla c1(c) and (i) water of stabilise the Attenu	n this area, as the o be inspected to d is upstream of the <b>RATING</b> <i>LOW</i> <i>1.33</i> ace without the reluse licenses (in ter	stability of the dam etermine the status Attenuation Dam Impact Class 2 2 evant authorisation rms of the NWA).	n wall is uncertain. s and any work 1 that needs to be Confidence Probable	
VDDC boxcu It was recogn needed on the taken into ac IMPACT BEI Significance Moderate 3 MANAGEME The following • No min R704 e • Investig mining	t area and p ised by Sou e dam itself. count in the ORE MAN/ Extent Regional 4 MT MEASU mitigation n ing within th xemptions a gate into upg in this area	oses a poten th32 that the There is als above planni AGEMENT Duration Medium term 3 RES neasures will ese restricted and Section 2 grading and s before mining	tial risk to mining i dam wall needs to o a farm dam, that ing. Probability Unlikely 2 be implemented: d areas will take pla c1(c) and (i) water of stabilise the Attenu	n this area, as the o be inspected to d is upstream of the <b>RATING</b> <i>LOW</i> <i>1.33</i> ace without the reluse licenses (in ter	stability of the dam etermine the status Attenuation Dam Impact Class 2 2 evant authorisation rms of the NWA).	n wall is uncertain. s and any work 1 that needs to be Confidence Probable	
VDDC boxcu It was recogn needed on the taken into ac IMPACT BEI Significance Moderate 3 MANAGEME • No min R704 e • Investig mining	t area and p ised by Sou e dam itself. count in the ORE MANA Extent Regional 4 mitigation n ing within th exemptions a gate into upg in this area	oses a poten th32 that the . There is als above planni AGEMENT Duration Medium term 3 RES neasures will ese restricted and Section 2 grading and s before mining	tial risk to mining i dam wall needs to o a farm dam, that ing. Probability Unlikely 2 be implemented: d areas will take pla cl(c) and (i) water to stabilise the Attenu g commences.	n this area, as the b be inspected to d is upstream of the <b>RATING</b> <i>LOW</i> <i>1.33</i> ace without the reluse licenses (in ter ation Dam 1 dam	stability of the dam etermine the status Attenuation Dam Impact Class 2 evant authorisation ms of the NWA). wall, to reduce the	n wall is uncertain. s and any work 1 that needs to be Confidence Probable ns, in terms of GN potential risk to	

# Impact D1 Decommissioning and Closure Phase – General decommissioning and rehabilitation – Impact on surface water quality

PHASE	DECOMMISSIONING AND CLOSURE PHASE					
ACTIVITY	General decommissioning and rehabilitation including water management infrastructure					
ACTIVITY	Demolition camps, demolition works, movement of materials and construction equipment					
ASPECT	ECT Water Quality – discharge of contaminated water					
IMPACT DEFINITION	NITION Pollution of surface water resources					
IMPACT DESCRIPTION A	ND EVALUATION					

Impacts resulting from general rehabilitation and decommissioning works will be similar to those during the construction phase, with earthworks related to rehabilitation and the movement of construction equipment on the site.

The water management berms and canals isolate active areas from the catchment by diverting upslope clean runoff around the active areas and containing runoff generated on the active areas. These can only be removed once the area has been rehabilitated, but may result in increased erosion if not properly planned. Impacts may arise from:

- Erosion of soils during rainfall events, with elevated suspended solids in the runoff water.
- Resultant elevated suspended solids in the watercourses, as well as sedimentation in the watercourses.
- Hydrocarbon spillages from fuel storage, servicing areas or construction equipment itself, with resultant elevated hydrocarbon concentrations in runoff water and watercourses.

These impacts are expected to be relatively small, with the resultant impact post decommissioning being positive in comparison with the operational phase.

Significance         Extent         Duration         Probability         RATING         Impact Class         Confidence           Low         Local         Short-term         Very Likely         LOW         2         Definite	IMPACT BEFORE MANAGEMENT						
	Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence
	Low	Local	Short-term	Very Likely	LOW	2	Dofinito
2 3 2 4 <b>1.87</b> 2 Definite	2	3	2	4	1.87	2	Denimie

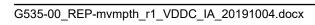
#### MANAGEMENT MEASURES

The following mitigation measures will be implemented:

- The footprint of disturbed areas will be minimised.
- "No-go" zones will be delineated for construction plant and personnel particularly if these are located adjacent to the Olifants River on the western boundary of the site..
- The storm water management infrastructure will be decommissioned last, if at all, to ensure adequate storm water management during the rehabilitation phase.
- Servicing of construction vehicles will take place only in dedicated areas that are equipped with drip trays.
- Bunded containment and settlement facilities will be provided for hazardous materials, such as fuel and oil.
- Spill-sorb or a similar type product will be kept on site and used to clean up hydrocarbon spills in the event that they should occur.
- Erosion protection measures will be implemented at steep areas.
- A waste management plan will be developed for the decommissioning phase, which will include the handling of contaminated materials / soils found on site.
- All traces of hydrocarbons and residual waste will be removed before infrastructure is demolished.
- Contaminated soils will be excavated and placed on the discard facilities prior to their rehabilitation, or removed from site by an appropriately licensed waste contractor.
- An appropriate sewage management strategy will be implemented during the decommissioning phase.
- Water quality monitoring will be undertaken downstream of the decommissioning areas, before and during decommissioning where practical, in order to detect any increase in suspended solids or turbidity.
- If erosion is evident, or the water quality monitoring indicates an increase in suspended solids, water management around the decommissioning areas will be reviewed.



PHASE		DECOM	DECOMMISSIONING AND CLOSURE PHASE				
ΑCTIVITY		General infrastru		g and rehabilitati	on including wate	er management	
			Demolition camps, demolition works, movement of materials and construction equipment				
ASPECT Water Quality – discharge of contaminated water							
IMPACT DEF	INITION	Pollution	Pollution of surface water resources				
IMPACT AFT		GEMENT					
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence	
Very Low	Study Area	Short-term	Unlikely	VERY LOW	1	Definite	
1	1 2		2	0.67	1		



# Impact D2 Decommissioning and Closure Phase – Mine water balance – Impact on surface water quality

PHASE	DECOMMISSIONING AND CLOSURE PHASE			
ACTIVITY	Mine water balance			
ACTIVITY	Recovery of water levels and possible decant			
ASPECT	Water Quality – discharge of contaminated water (mine water decant)			
IMPACT DEFINITION Pollution of surface water resources				
IMPACT DESCRIPTION A	ND EVALUATION			

Once the pit has been backfilled and re-shaped, dewatering will cease and water levels will begin to recover in the workings.

Decant from this mine is expected to take place at the Olifants River tributary to the south-east of the site via subsurface discharge at approximately 1 530 mamsl and approximately 0.5 l/s (please refer to the Groundwater study, JW190/18/G535-04, July 2019). According to Golder Associate's water balance SKS pit will decant into the adjacent Glencore workings.

The predicted time to decant for VDDC pit is within 5 years after mining.

The time to decant at VDDC pit will therefore take place after the decommissioning phase.

Note: Decant elevations and decant times are provisional, and will be confirmed as models are calibrated with actual inflows.

IMPACT BE	FORE MANA	GEMENT				
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence
High	Regional	Long term	It's going to happen	HIGH	4	Definite
4	4	4	5	4.0		
MANAGEME	NT MEASU	RES				
Mitigation me	easures will i	nclude the fo	llowing:			
• The pit v	vill be backfil	led without a	final void, rehabil	itated and made f	free-draining.	
	•		nine and the asso er quality and wate		ty is committed to. T	his will allow both
• The wate	er level in the	workings wi	Il be actively man	aged to ensure it	remains below the de	ecant elevation.
					rkings to the Vleishaf o Vlaklaagte void.	t Dam and
• The treat	ted water wil	l be discharg	ed to the environr	nent.		
A detaile	d decant ma	nagement pl	an will be develop	ed at mine closu	re which will involve p	passive treatment

only.						
IMPACT AFTER MANAGEMENT						
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence
Low	Local	Short term	Very Likely	LOW	2	Definite
2	3	2	4	1.86		

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# Impact PC1 Post Closure – Potential for acid mine drainage (AMD) and poor quality leachate – Impact on surface water quality

PHASE	POST CLOSURE PHASE
ACTIVITY	Potential for decant of AMD
ACTIVITY	Decant of mine water make
ASPECT	Water Quality – discharge of contaminated water
IMPACT DEFINITION	Pollution of surface water resources

#### IMPACT DESCRIPTION AND EVALUATION

Post closure, the infrastructure areas will have been rehabilitated and made free draining. Similarly, the entire opencast will also have been rehabilitated and made free draining.

Two aspects have been considered here, namely the volume of decant that could be generated, and the potential quality of the decant.

If the water levels in the rehabilitated opencast are not controlled, the potential time to decant is estimated to be with 5 years after mining ceases.

If the decant is not managed (as detailed below), there could be an impact on both the downstream catchment. The expected post closure mine water quality for key parameters, is as follows:

• The Sulphate levels are expected to be around 2000 - 3000 mg/l (please refer to the Groundwater study, JW190/18/G535-04, July 2019).

It is considered valuable to assess the potential sulphate loading of the mine on the catchment. This assessment is based on the assumption that the entire water make were to be discharged to the catchment.

The water balance indicates that an average water make in the order of 5 800 m<sup>3</sup>/day can be expected. Based on a sulphate concentration of around 3000 mg/l, this equates to around 17.4 tons SO<sub>4</sub> per day, or around 6351 tons SO<sub>4</sub> per year.

The estimates given above are proposed to be refined over the life of mine as follows:

- On-going sampling and monitoring of parameters important to the final water quality and water volumes
- Quantification and verification of the groundwater model, the water balance model, and the geochemical model
- Evaluation and reassessment of alternative options for the final water use and required associated water quality, together with the technologies required to achieve the required quality.

IMPACT BEFORE MANAGEMENT							
Significance	Extent	Duration	Probability	RATING	Impact Class	Confidence	
High	Regional	Long term	It's going to happen	HIGH	4	Probable	
4	4	4	5	4			
MANAGEME	NT MEASU	RES					
<ul> <li>Mitigation measures will include the following:</li> <li>The pit will be backfilled without a final void, rehabilitated and made free-draining in order to minimise the post closure water make.</li> <li>Monitoring of water levels in the mine and the associated water quality is committed to. This will allow both calibration of the post mining water quality and water volumes.</li> <li>The water level in the workings will be actively managed to ensure it remains below the decant elevation.</li> <li>The post closure mine water make will need to be pumped from the mine workings. A post closure water management plan will need to be developed.</li> <li>Discharge of clean water to the river system.</li> </ul>							
IMPACT AFT	ER MANAG	BEMENT					

 IMPACT AFTER MANAGEMENT

 Significance
 Extent
 Duration
 Probability
 RATING
 Impact Class
 Confidence



ed water	
ed water	
ed water	
2	Probable
2	Probable
V	2

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## 9. FINANCIAL PROVISION

For the operational phase, the water management costs are included in the infrastructure costs in most respects, including pollution control dams and the associated storm water canals, pumps and pipes.

At closure these facilities will be demolished and removed and the area will be rehabilitated. The cost related to this will be included in the overall closure costing.

Post closure the area will be rehabilitated and will not generate dirty runoff. The mine water make will need to be managed. The financial provision required for this will be dependent on the pumping / treatment strategy adopted. South32 water treatment technology post closure will be semi-passive and passive treatment.

The rise of water will be closely monitored (during operations and post closure) to ensure that the environmental safe level is not exceeded and that appropriate management measures, disposal (i.e. via mechanical evaporators) and treatment facilities are constructed in time to treat the surplus water once the environmental safe level is reached. The water will then be actively maintained at or below the environmental safe level.

A detailed decant management plan will be developed at mine closure. Ultimately water treatment solutions, either passive or active, will be implemented.

Monitoring of the water table rebound will continue post-decommissioning phase and the modelling updated to quantify the long-term impacts. If necessary, the management measures should be revised based on the modelling results.

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# 10. SUMMARISED WATER MANAGEMENT PLAN

In **Section 8**, mitigation measures have been indicated to manage the impacts assessed. These measures need to be incorporated into an Integrated Water and Waste Management Plan (IWWMP) that can be used to implement, audit and measure the performance of the water management measures detailed in the EMPr.

This section is intended to only provide inputs on key aspects of the water management plan.

#### **10.1** Construction Phase

- 10.1.1 Key issues and objectives
  - To prevent the contamination of surface water runoff from the cleared construction site areas.
  - To minimise erosion in the construction site areas and to minimise siltation in the adjacent watercourses.
  - To prevent contamination of surface water runoff from the VDDC pit and infrastructure area of construction.
  - To ensure that the required water management infrastructure is constructed timeously.

#### 10.1.2 Key strategies

Areas where impacts in terms of construction activities could occur are listed below:

- Construction of water management infrastructure:
  - The upstream diversion of clean catchments and tying into existing clean water management measures should be constructed first in order to minimise the flow of water across the construction site.
  - The construction of the dirty water management measures at the proposed overburden dump to the south east of the project area.
- Construction of the laydown area.
- Construction of infrastructure.
- The mine infrastructure will be constructed after the water management infrastructure, most notably the clean water diversion and sumps at the VDDC pit area.
- Control of suspended solids. Should wet conditions occur during construction, suspended solids in the watercourses must be monitored and silt traps must be provided on construction areas, should suspended solids be detected.

#### 10.1.3 Monitoring

Monitoring of water quality is undertaken under the mine's current water quality monitoring programme. An assessment of the current status of surface water quality has been included in the baseline surface water assessment. Monitoring will continue throughout the construction and operational phases. A monitoring programme for the proposed activities is detailed in **Section 11**.



### 10.2 Operational Phase

- 10.2.1 Key issues and objectives
  - To minimise the impact of the proposed mining activity on the catchment yield.
  - To identify and control surface runoff that may be affected by the planned activities.
  - To ensure that the risk of spilling this water into the clean catchment is:
    - In line with licensing requirements.
    - In line with legislative requirements.
    - Commensurate with the risks to downstream users associated with any spillage. This is taken currently at a 2% or lower risk in any one year.
  - To prevent clean runoff from upstream / upslope areas from spilling into the dirty water systems for flood events up to at least the 1:50 year recurrence interval.
  - To ensure adequate monitoring so that the objectives of the water management system can be met.

#### 10.2.2 Key strategies

The key management strategy is to keep clean water clean and to minimise the generation of dirty water. This is to be achieved by diverting runoff from clean catchments around the dirty areas and minimising the extent of dirty areas as far as is practicable. Clean and dirty water systems should be designed and managed to have a risk of spill of 2% or less in any one year (1:50 year recurrence interval event). The key strategies include:

Minimising loss of catchment yield:

- The loss in yield is dependent on the on-site management and planning activities, including the following:
- Placement of upstream diversion berms/ canals so that the maximum volume of upstream runoff can be diverted around the dirty areas, back to the receiving environment.
- Investigating and implementing water conservation and demand management, together with maximising recycling and reuse strategies on the site.
- Implementation of a water flow, pumping and dam water level monitoring programme to enable calibration of the water balance model and efficient management of the site water balance.
- Managing the generation of dirty water.
- The dirty water footprint will be minimised by diverting clean runoff around the dirty areas. Clean water cut-off canals, with capacity to accommodate at least the 1:50 year peak flow event, will be provided. Adequate erosion protection will be provided at the canal discharge points.
- Provision has been made to collect, evaporate and treat dirty water generated for discharge. The proponent has committed to having a 2% or lower risk of spilling in any one year.
- The risk of spilling is a function of adequate storage capacity, balanced against the reuse of water in the mining operations, as well as treatment at the mobile WTP.



- In line with best practice, the Vleishaft Dam will be operated as empty as possible at all times to ensure that sufficient storm water retention capacity is available at all times.
- Ongoing calibration of the water balance is required to ensure that the estimates in terms of water make-up, water shortages and storage requirements are evaluated during the life of the mine. Key strategies to address these issues involve:
  - Monitoring of water volumes pumped and stored.
  - Documentation of any problems in reusing dirty water, such as operational difficulties.
  - Ongoing rainfall monitoring.
  - Management of water pumped / draining into the Vleishaft Dam, including documentation of water volumes abstracted for use in the mine.
  - Adjustment for any changes in process or infrastructure layout, where these could affect the water balance.
  - Ongoing monitoring of water levels within Vleishaft Dam, as well as any spillages.
  - Ongoing monitoring of water volumes supplied from the voids, including recycled water.
- These points indicate that the water management will be a dynamic and ongoing process, aimed at ensuring compliance with legal requirements and good environmental practice over the life of mine.

#### 10.2.3 Monitoring

The objective of the surface water monitoring system is to ensure that the water management system performs in accordance with specifications, to act as an early warning system of contaminated surface water, to verify compliance with license requirements, and for reporting purposes. The objective of these systems will be achieved if there is an acceptable impact (attributable to the proposed opencast mining operations) on the receiving environment.

Monitoring requirements are detailed in **Section 11**.

#### 10.3 Decommissioning

- 10.3.1 Key issues and objectives
  - To limit the risk of increased erosion on site and downstream, relating to areas being rehabilitated and consequently impacting on water quality.
  - To ensure that the area is decommissioned and rehabilitated "from the inside out", thereby preventing spillage of any dirty water or waste in the process.
  - To remove all carbonaceous and mining related material on surface at the pits and infrastructure areas.
  - To make the rehabilitated areas free draining.

#### 10.3.2 Key strategies

- Dismantling and removal of the entire mine's surface infrastructure, unless required to remain in place as a result of the post closure land use.
- Removal of all carbonaceous material and other contaminants / waste materials from the site.
- Pits backfilled to ground level by placing the overburden material back into the void. The backfilled pits will be shaped to ensure that they are made free draining, making allowance for future settlement of the backfill.
- Shaping and grassing of the pits and mine surface infrastructure area.
- Erosion protection: The general area is susceptible to erosion. During rehabilitation, the areas where grass has not yet been established will be monitored to ensure that there is not excessive erosion prior to the grass establishing, and where necessary additional erosion protection such as the use of dump rock (non-carbonaceous, from commercial sources) or repair of gullies will be undertaken until such time that the rehabilitated surfaces can be shown to be sustainable.

#### 10.3.3 Monitoring

Monitoring during decommissioning will be based on the operational phase monitoring, adapted to suit the final works to be implemented during this phase. However, in terms of surface water this will be primarily downstream of the area, as for the operational phase.

#### 10.3.4 Knowledge gaps

The final land use for the site has been determined as grazing. This may influence the rehabilitation strategy. The rehabilitation designs indicate that the pit will be backfilled to ground level by placing the overburden material back into the void. The backfilled pit will be shaped to ensure that they are made free draining, making allowance for future settlement of the backfill.

### 10.4 Post Closure

- 10.4.1 Key issues and objectives
  - To manage the post closure water make.
  - To manage the rehabilitated area post closure.

#### 10.4.2 Key strategies

Water management to avoid decant:

- If left to fill with no intervention, it is expected that the water level within the new mine workings will recover over a period of approximately 5 years from the date mining ceases, depending on pit floor elevations, topography and adjacent geological material.
- Water levels in the workings will need to be kept below decant level to prevent decant to the natural watercourses.
- Wolvekrans Colliery is committed to responsible environmental management, which includes containment and treatment of decant water to ensure that there is



no downstream impact on water quality associated with future decant from the mine.

Management of rehabilitated area:

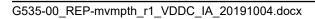
• The key strategy is to ensure that the rehabilitation in terms of shaped land form and vegetation cover is maintained in the long term to ensure long term sustainability of the rehabilitated area.

#### 10.4.3 Monitoring

Monitoring post closure will be undertaken only where required to prove the sustainability of the site. In terms of surface water, this relates primarily to managing the surface topography (monitoring for erosion), and water quality downstream of the site.

#### 10.4.4 Knowledge gaps

The water balance model and final water qualities are conceptual at this stage. These will need to be verified over the life of mine. The final land use for the site is not certain at this stage. The required post closure water management measures and monitoring may be influenced by the final land use.



# 11. MONITORING AND AUDITING

The objective of the surface water monitoring system is to ensure that the water management system performs in accordance with specifications, to act as a pollution early warning system, to check compliance with license requirements and for reporting purposes. The objectives of these systems will be achieved if there is no impact (attributable to the VDDC Infrastructure Development project) on the in-stream and downstream fitness for use criteria.

#### 11.1 Water quality monitoring

#### 11.1.1 Monitoring locations

In order to detect impacts attributable to an activity, water quality monitoring would usually be carried out upstream and downstream of the site.

The proposed monitoring locations for the VDDC Infrastructure and mining project are shown in **Figure 11.1.1.a**. The locations are described in **Table 11.1.1.a**. These locations are to be added to the existing monitoring programme, detailed in Section 6.

Monitoring location	Description	Co-ordinate		
P1	WTP Discharge	S26 01 30.88	E29 16 05.44	
P2	At clean water canal at proposed South East overburden Dump	S26 04 54.72	E29 18 54.69	
P3	At dirty water canal at proposed South East overburden Dump	S26 00 04.36	E29 17 33.15	
P4	Upstream of Discharge of WTP and downstream of Evaporator site	S26 05 17.17	E29 19 23.50	

 Table 11.1.1.a:
 Details of proposed surface water quality monitoring locations

#### 11.1.2 Water quality sampling and analysis

During the Construction and Operational Phases of the VDDC project, rivers and dams should be sampled on a monthly basis.

Monitoring during the Decommissioning Phase will be based on the Operational Phase monitoring, adapted to suit the final works to be implemented during this phase. However, in terms of surface water this will be primarily downstream of the area, as for the Operational Phase.

Monitoring during the Post Closure Phase will be undertaken only where required to prove the sustainability of the site. In terms of surface water, this relates primarily to managing the surface topography (monitoring for settlements), and water quality and levels within the mined out area.

Any infrastructure (PCDs) that will remain on site, post closure, will continue to be included in the surface water monitoring programme and should be monitored in terms of water quality and water levels on a monthly basis. The water quality parameters that are currently being monitored at VDDC project are indicated in **Table 11.1.2.a**.

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Location	Constituent
Location Existing sampling points as detailed in Section 6	Constituent         pH Value at 25°C         Conductivity in mS/m         Total Dissolved Solids         Suspended Solids         Iron as Fe         Total Alkalinity as CaCO3         Calcium as Ca         Chloride as Cl         Magnesium as Mg         Nitrate & Nitrite as N         Ortho Phosphate PO4 as P         Potassium as K
	Sodium as Na Sulphate as SO₄
	Aluminium as Al
	Fluoride as F
	Manganese as Mn

 Table 11.1.2.a: Surface Water Quality monitoring parameters

The recommended frequency of sampling and additional variables to those indicated in **Table 11.1.2.a** to be analysed are detailed in **Table 11.1.2.b**.

Samples will be grab samples, which will include:

- Filtered and unfiltered samples.
- Acid preservation of samples for metals analysis.
- All samples will be analysed by an accredited laboratory.

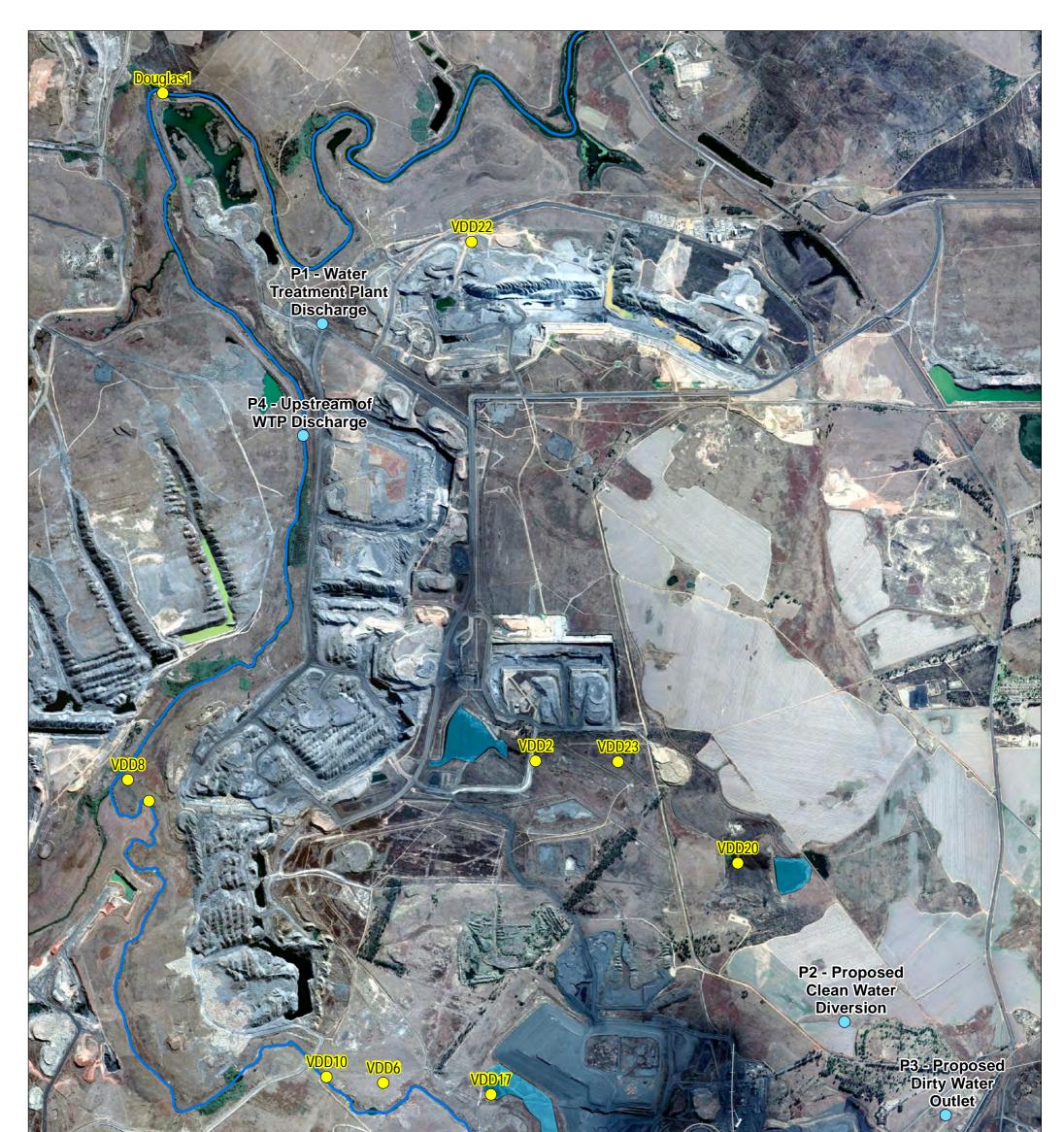
Location	Constituent	Frequency
All existing and proposed monitoring points	Zinc as Zn (total and dissolved) Boron as B (total) Antimony as Sb (total) Molybdenum as Mo (total) Lead as Pb (total) Mercury as Hg (total) Selenium (total) Ammonia as N Aluminum as Al (total and dissolved) Iron as Fe (total and dissolved) Manganese as Mn (total and dissolved)	Monthly
	Bacterial analysis Total Coliforms and E coli	Every six months

# 11.2 Water quantity monitoring (water balance monitoring)

For efficient management of water on the site, a good understanding of the site water balance will be required. To achieve this, the following monitoring will be needed:

- Rainfall to be measured daily on the site.
- Evaporation this is not essential but would be useful for calibration of the water balance model.
- Dam water levels to be measured monthly.
- Flows including the following, to be measured monthly:
  - Mine water make pumped from the opencast workings.
  - Inflows to the Vleishaft Dam.
  - $\circ$  Water pumped from the Pollution Control Dam for reuse in the operations.
  - Water recycled at the Evaporators.
  - Volume treated in the WTP.
  - o Volume of treated water discharged from the WTP.







## 11.3 Data management and reporting

#### 11.3.1 Monthly

The monthly report is an internal environmental data report which is used to keep records of changing water qualities at the site. The report will include:

- Sites that are sampled.
- Water qualities for the relevant constituents.
- Dam levels and flow rates on site.
- Highlight significant issues that require immediate corrective / preventative action.

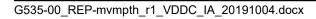
#### 11.3.2 Annually

The water quality annual report consists of all the active environmental components, and for the chapter on surface water, the following components should be included:

- Data audit
  - o Verification of data.
  - Compliance interpretation using RQO and SANS 241 Drinking Water Standard and management unit objectives.
  - Setting of new objectives or recommendation of corrective measures.
  - Comparison of historical and present chemistry assessment
  - Assessment of historical and present pollution sources.
  - Dam level status report.

#### 11.4 Performance assessment/ audit

Annual audits should be carried out to determine the effectiveness of the water management systems that are in place. These should include a combined GN R704 audit as well as an Integrated Water and waste management Plan (IWWMP).



# 12. EMERGENCY AND REMEDIATION PROCEDURE

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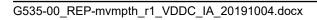
This section is detailed in the main EIAR.



# 13. <u>CONCLUSION</u>

The following conclusions can be drawn from the surface water study:

- The baseline surface water quality assessment within the study area indicate potential impacts associated with mining activities both upstream and downstream of VDDC.
- The old 2 Seam underground workings have filled with water. This area will need to be dewatered prior to mining the VDDC pit and is therefore a key to the success of the proposed project.
- Mine impacted water will be pumped to the Vleishaft Dam and thereafter, to one of the evaporator sites, or to Vlaklaagte void, or to the proposed modular, mobile WTP. Timing and location of the mechanical evaporators are provided in Section 4.3.
- Surplus water which cannot be handled through the evaporation system, will be conveyed to a mobile, modular WTP with a maximum treatment capacity of 20 Ml/day. Brine from the WTP will be collected in existing tanks before being conveyed to the evaporators at the SKS void.
- Effluent from the WTP (i.e. treated mine water) will be conveyed via an existing mine water pipeline to the existing northern clean water canal, from where it will discharge via a wetland area into the Olifants River. Water will be treated to comply with Resource Quality Objectives for the Olifants River catchment as published in GN 466 in April 2016.
- The cumulative impact of the VDDC mining operation extension, with the mitigation measures described in the impact assessment, is considered to be medium to high in relation to the current and anticipated future activities in the area, as the catchment is already impacted by mining activities.
- Surface water impacts from the site can be effectively mitigated by applying best practice water management principles.
- The success of surface water impact management will be judged on the basis of successful prevention of spills from the site.
- The following conclusions were extracted from the site wide water balance modelling carried out by Golder Associates:
  - The dewatering rates during 2020 and 2021 are estimated to be about 27 000 m<sup>3</sup>/d. During this period the site wide water balance model showed that the planned installed evaporator capacity will be insufficient to manage the water. South32 should consider installing the 8 evaporators at SKS by November 2019.
  - The extensive use of the evaporators will result in salt buildup in the water bodies over which the evaporators are spraying. Therefore, monitoring of salination of water due to brine evaporation will need to be undertaken and corrective action carried out if need be.



- 0
- Vleishaft Dam is expected to spill during the period 2020 to 2022 which is 0 during the initial VDDC dewatering period. The spills will report to the SKS pit. During this initial dewatering period, Golder Associate's model estimates that the SKS pit will decant into the adjacent Glencore workings. Therefore, the evaporators at SKS pit should be installed earlier than the planned implementation date of May 2020. After 2029, the 18 000 m<sup>3</sup>/d of evaporator capacity installed at SKS pit will draw down the water level in the pit.

eraanloo

Malini Veeragaloo PrEng

Michael Palmer Pr Eng for Jones & Wagener

5 September 2018

Document source: https://joneswagener.sharepoint.com/JonesWagenerProjects/G535VDDCIRP/Shared Documents/PRJ/REP/SurfaceWater/ImpactAssessment/Rev1/G535-00\_REP-mvmpth\_r1\_VDDC\_IA\_20191004.docx Document template: Normal.dotm

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<u>Report: JW188/18/G535</u> - Rev 1

# **APPENDIX A**

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# **CV OF SPECIALIST**



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# **APPENDIX B**

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# **RISK ASSESSMENT CRITERIA**