## Proposed Township: Rietspruit

(Proposed New Mixed Land Use Development to be situated on Portion 8 of the Farm Rietspruit 152-IR)

TRAFFIC IMPACT ASSESSMENT

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| :--- | :--- |
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## 1. Introduction

Dhubecon Consulting Engineers (Pty) Ltd have been appointed to undertake this Traffic Impact Assessment (TIA) as part of the township application for a proposed new mixed land-use development, which is to be situated on Portion 8 of the Farm Rietspruit 152-IR. The proposed new township will be known as Rietspruit. The site location is shown in Figure 1 and Figure 2 and falls under the jurisdiction of Midvaal Local Municipality.

The subject site, as a whole, is approximately 163ha in extent. With reference to the Town Planner's proposed Township Layout Plan in Annexure A, Rietspruit will be a mixed land-use development and will comprise a total of 3,782 single residential erven ('Residential $1^{\prime}$ ). Provision is also made for 'Institutional' land uses in the form of two new public primary schools and one new public secondary school, given the large extent of the residential component. The proposed township layout also makes provision for erven with 'Community Facility' and 'Utilities' zonings, as well as ample public open spaces/ parks. It can be noted that the subject site is bordered by the Watervalspruit Townships (also known as Sky City) to the north-west, which has the same developer as the proposed development. Similar to these neighbouring Watervalspruit Townships, the proposed development is expected to mostly cater for lower income households and it is anticipated that a similar housing product will be developed, with erf sizes ranging between $155 \mathrm{~m}^{2}$ and $202 \mathrm{~m}^{2}$. The proposed development is not planned to be security controlled at this stage. These houses on the single residential stands are typically known as "charter housing", which is the lowest level where households qualify for a home loan.

This study investigates the impact of the additional traffic to be generated by the proposed development of Rietspruit onto the immediate surrounding road network and determines whether it is necessary to implement any road and/ or intersection improvements to mitigate the anticipated traffic impact. New traffic counts had been undertaken at identified key intersections in the study area in order to quantify and assess the traffic flow operations. The study also investigates the proposed site layout, the site access arrangements and provides comments with respect to non-motorised and public transport.

## 2. Site Location \& Surrounding Road Network

### 2.1 SITE LOCATION

With reference to Figures 1 and 2, the subject site is situated approximately 1.5 km south-east of the existing intersection between Heidelberg Road (R550/ Future K154) and the K91, which does not currently have another name. The site itself falls just within the borders of the Midvaal Local Municipality, however, the primary roads that will be utilized to provide access to the site falls within the jurisdiction of the City of Ekurhuleni (CoE), Southern Region. The subject site is bordered by an existing Transnet Freight Rail (TFR) railway line to the south and will be bordered by the future Watervalspruit Townships (also known as Sky City) to the north. It can also be seen that the Rietspruit River traverses the southern portion of the site.

The following existing and planned future roads are relevant and key to the study area:

### 2.2 EXISTING ROAD NETWORK

Heidelberg Road (R550 / K154/ Road D64): This is an existing east-west Class 2 provincial road (major arterial), which is located about 650 m north of the closest corner of the subject site. Currently this road comprises a 2-lane single carriageway road in the vicinity of the site, with additional turning lanes at most of its intersections, most notably in this case with the K91 and Kingfish Street / Garthview Street. Further east of the site, Heidelberg Road forms an access interchange with the N3-freeway and travels to areas such as Tsakane and Nigel, while further to the west of the site, Heidelberg Road forms an access interchange with the R59-freeway. According to the recent surveys, the traffic volumes along the section of Heidelberg Road directly north of the subject site are in the order of 600vph and 710 vph (total both directions) during the weekday AM and PM peak hours, respectively.

Road K91: is an existing Class 2 provincial road (major arterial), which runs north-south and connects areas such as Palm Ridge with Heidelberg Road. The road is currently a 2-lane single carriageway road along the majority of its length, with additional turning lanes at its T-intersection with Cosmopolitan Drive. The K91 currently forms a 4-legged, priority stop controlled intersection with Heidelberg Road about 1.5 km north-west of the subject site. The southern leg of this intersection, which is also currently known as the K91, forms a T-intersection with Edge Road, which is a local collector road for the surrounding plot erven in the area. In the vicinity of the above-mentioned intersection with Heidelberg Road, the current traffic volumes on the K91 are in the order of 810 vph and 860 vph (total both directions) during the weekday AM and PM peak hours, respectively.

Cosmopolitan Drive: is a Class 3 minor arterial road that intersects with the K91 about 1.8 km north of the subject site and runs parallel to Heidelberg Road (i.e. east-west). This road was constructed as part of the first phases of the neighbouring Watervalspruit Townships and currently serves as the primary east-west distributor road in these townships. It is a single carriageway (2-lanes undivided) along its length and connects the K91 with Kingfish Street. The extension of this road to the east of the K91 was only recently completed. A number of traffic circle controlled intersections are formed with this road along its length, including one with Kingfish Street. The current traffic volumes on this road, in the vicinity of its intersection with the K91, are in the order of 780vph and 1,020vph (total both directions) during the weekday AM and PM peak hours, respectively. These volumes have increased considerably over the years as a result of the ongoing development of the neighbouring Watervalspruit Townships.

Kingfish Street: is also a Class 3 minor arterial road, which intersects with Heidelberg Road approximately 2.2 km north-west of the subject site. This road directly connects above-mentioned Cosmopolitan Drive with Heidelberg Road. It was also constructed as part of the first phases of the Watervalspruit Townships and is currently the primary north-south distributor road in these townships. This road is a single carriageway (2-lanes undivided) along its length, with an additional turning lane at
its 4 -legged, signalised intersection with Heidelberg Road and Garthview Street. In the vicinity of this intersection, the current traffic volumes on Kingfish Street are in the order of 910 vph and 620 vph (total both directions) during the weekday AM and PM peak hours, respectively. These volumes have also increased considerably over the years as a result of the ongoing development of the neighbouring Watervalspruit Townships.

### 2.3 PLANNED FUTURE ROAD NETWORK

### 2.3.1 Provincial Road Network

An extract of Gautrans' Strategic Major Road Network (2007) is shown in Figure 3, which indicates several planned future K-routes in the vicinity of the site. The most relevant ones are:
\# Future K154: This road will follow the existing alignment of Heidelberg Road (R550 or D64). Along its length, this road is primarily still a single carriageway; the future upgrade to full K-route standards would imply doubling of the existing 2-lane road to a 4-lane dual carriageway road. It must be noted that there are preliminary designs/ basic planning for the relevant section of this road in the vicinity of the site, which have been accepted by the MEC of the Gauteng Department of Roads and Transport (GPDRT).
\# Future K91: This road is currently a single carriageway past the neighbouring Watervalspruit Townships and will also be upgraded in future to a 4-lane dual carriageway road, when the demand arises. The current road is already constructed in the correct position and will become an important future north-south carriageway. The portion of future road to the south of its existing intersection with Heidelberg Road (K154) is yet to be constructed and is expected to be triggered with increased development to the south of Heidelberg Road. It must be noted that there are preliminary designs/ basic planning for the relevant section of this road in the vicinity of the site, which have also been accepted by the MEC of GPDRT.
\# Future PWV18: This future east-west Class 1 road/ free-way is planned to traverse the subject site more or less through the middle and will subsequently split the site into a northern and southern portion. This road is planned to extend further west of the site, past the R59freeway and further to the east of the site, past the N3-freeway.

It must be noted that this planned future route is still in its Route Determination phase, i.e. no basic/ preliminary designs are in place for this route as yet. Given the significant impact of this planned future route on the subject site, Dhubecon was tasked to undertake a first preliminary design for this route, with specific focus on the section of the PWV18 extending between the future K91 and the future K154 (see Figure 3). This was necessary to determine the horizontal and vertical alignment of the future PWV18 through the subject site, which in turn determines the necessary road reserves that must be accommodated. It is confirmed that meetings and discussions were held with Gautrans in this regard and the preliminary design has subsequently been accepted by Gautrans. This will be addressed in more detail in a separate Section 7 report, which will be submitted to Gautrans for approval in due course.
It can be seen that the proposed Township Layout Plan, as enclosed in Annexure A, has taken full account of the future PWV18, based on the preliminary design undertaken by Dhubecon, and has accommodated the necessary road reserves accordingly.

At this stage it is not known when future routes K154 and K91 will be upgraded to full K-route standards. Sections of the K154 and K91 are anticipated to become important in about 5-10 years' time and it is recommended that Gautrans undertake the necessary budget planning to implement the upgrades by then. The PWV18 is not expected to be implemented in the foreseeable future, but possibly only in the much longer term.

### 2.3.2 Local Road Network

With regards to the local road network, it can be mentioned that both the City of Ekurhuleni and the Midvaal Local Municipality have no formal local road master planning in the study area, which lies to the south of Heidelberg Road (R550/ future K154) and to the east of the K91. In this particular case, the road network is largely determined by the approved townships of the neighbouring Watervalspruit Townships (i.e. Sky City), as well as the Palm Ridge Townships to the north of the subject site.
Given the lack of proper local road master planning in the study area, accessibility to the subject site becomes an issue. Dhubecon were therefore requested by the client/ developer to investigate a proposed local road master planning that will allow for feasible accesses to the subject site, integrate with existing and planned future provincial roads and also enable access to surrounding properties in future. Our proposed road master plan is shown conceptually in attached Figure 4 and some of the key aspects of this proposal are briefly discussed below:
\# It can be seen that access to the subject site will have to be provided via the internal road network of the future phase of the Watervalspruit Townships to the south of Heidelberg Road, which will border the subject site to the north-west. It must be noted that there is already a Township Layout Plan in place for this future phase adjacent to the subject site, but which has not been proclaimed yet and will be amended to accommodate the proposed road network, as per Figure 4. This is also indicated on the township layout in Annexure A.
\# With further reference to Figure 4 and Annexure A, there are a number of constraints in the study area that had to be taken into account during the compilation of the proposed road master plan. These include the Rietspruit River, which traverses the southern portion of the site, the existing Transnet Freight Rail (TFR) railway line directly south of the site, a northsouth TFR railway servitude that traverses the north-western corner of the subject site and the future planned PWV18, which runs through the middle of the site in an east-west direction, as discussed in Section 2.3.1 above. It is confirmed that all of these factors have been accommodated and that the proposed township layout, as enclosed in Annexure A, has also made provision for the relevant TFR railway servitudes and the wetland buffers and flood lines of the Rietspruit River.
\# It is proposed that a Class 3 road, within a 30 m road reserve, should travel through the middle of the site, as per Figure 4 and Annexure A, which will serve as the main internal collector and distributor road of the proposed township and which can be extend further to the south in future in order to become an important minor arterial in the study area. For the purposes of this TIA, this Class 3 road will be referred to as 'Road A', given that there is no official street name as yet. The alignment of this road, through the middle of the site, is ideal given for the predominantly residential development proposed and will also enable an easier conversion to security controlled complexes in future, if/ when the need arises.

It can be seen that this proposed Class 3 road will not only be beneficial to the proposed development itself, but will also integrate effectively with the rest of the proposed road master plan, while allowing for ample future access opportunities to adjacent properties via its planned intersections with east-west Class 4 collector roads (refer to Figure 4 and Annexure A).
\# Although some of the proposed new roads are more indicative than others, it is evident that the proposed road master plan will integrate with existing local and provincial roads, as well as planned future provincial roads. It will also integrate with Dhubecon's proposed road master planning to the north of Heidelberg Road, which is also indicated on Figure 4 and which has been accepted by the City of Ekurhuleni in principle. Furthermore, access can be provided to all surrounding properties in the relevant study area, even when taking into account the constraints posed by the rivers and railway lines, as the proposed planning allows for easy integration when more new roads need to be determined in the study area in future.

It is confirmed that the proposed local road master plan, as per Figure 4, has been discussed with the relevant official(s) at the Midvaal Local Municipality, who confirmed their support of the proposal in principle.

## 3. Proposed Development \& Site Access

### 3.1 PROPOSED DEVELOPMENT

The subject site for the proposed new township is situated on Portion 8 of the Farm Rietspruit 152-IR and extends a total of approximately 172 ha . The proposed new township will be known as Rietspruit. The site location is shown in Figure 1 and Figure 2 and falls under the jurisdiction of Midvaal Local Municipality.

With reference to the Town Planner's proposed Township Layout Plan in Annexure A, Rietspruit will be a mixed land-use development and will comprise a total of $\mathbf{3 , 7 8 2}$ single residential erven (zoned 'Residential $1^{\prime}$ '. Provision is also made for 'Institutional' land uses in the form of two new public primary schools and one new public secondary school, given the large extent of the residential component. Without the necessary details with regards to the sizes of the proposed schools at this stage, it was assumed in this study that the proposed public primary schools would each have a capacity of 800 students (thus 1,600 students in total), while the proposed public secondary school would have a capacity of 1,200 students. The proposed township layout also makes provision for a 'Community Facility' erf, which will mostly be utilized as an informal trade area and also make provision for erven with 'Utilities' zonings, which will accommodate engineering services (given the shortage thereof in the vicinity of the subject site). Provision has furthermore been made for ample erven with 'Public Open Space' zonings, which include the Rietspruit River (and it buffer area) that traverses the subject site. The existing cemeteries located on the subject site have also been protected and accommodated on the proposed township layout.

It can be noted that the subject site is bordered by the Watervalspruit Townships (also known as Sky City) to the north-west, which has the same developer as the proposed development. Similar to these neighbouring Watervalspruit Townships, the proposed development is expected to mostly cater for lower income households and it is anticipated that a similar housing product will be developed, with erf sizes ranging between $155 \mathrm{~m}^{2}$ and $202 \mathrm{~m}^{2}$. The proposed development is not planned to be security controlled at this stage. These houses on the single residential stands are typically known as "charter housing", which is the lowest level where households qualify for a home loan.

### 3.2 PROPOSED SITE ACCESS INTERSECTIONS

Given the lack of proper (formal/ paved) roads in the study area, it is proposed that the subject township gain access via the future internal road network of the neighbouring Watervalspruit Townships (as mentioned in Section 2.3.2), which border the subject site to the north-west. Access to these townships, and therefore the subject townships, will be provided via two (2) new access intersections with Heidelberg Road (R550/ future K154), as indicated in attached Figure 2. The positions of the proposed site access intersections are also reflected on the proposed local road master plan in Figure 4.

The proposed access roads that will intersect with Heidelberg Road will be known as Silver Dory Street and Yellow Jack Street, respectively, with Silver Dory Street being the road closest to the K91. The main north-south collector and distributor road through the subject township, which will essentially be the future extension of Yellow Jack Street, is referred to as 'Road A' for now in this TIA (as mentioned in Section 2.3.2).

It is confirmed that the locations of the proposed two site access intersections with Heidelberg Road, as mentioned above, are in line with the location on Gautrans' latest preliminary design of the future K154, past the site, which has been accepted by the MEC of GPDRT (as mentioned in Section 2.3.1). The proposed Township Layout Plan for the neighbouring Watervalspruit Townships has taken full cognisance of the road reserve of the future K154, including the necessary splays for these proposed site access intersections. However, it must be noted that the internal layout of the neighbouring

Watervalspruit Townships to the south of Heidelberg Road (i.e. bordering the subject site) is not fixed yet and will be adjusted to accommodate the proposed internal road network of the subject township, as indicated in Annexure A.

### 3.3 INTERNAL TOWNSHIP LAYOUT \& ROAD NETWORK

Given the fairly large extent of the subject township, this study focusses on access provision at a township level, instead of at a micro level for individual erven. For the other uses, such as the schools, separate Site Development Plans (SDP's) will be submitted for each site at a later stage, which will provide the necessary access details of those developments. Should it be necessary, the Traffic Engineer will provide more inputs and also liaise with the relevant council officials at that stage.

As can be noted from Annexure A, a complete new network of local Class 3, 4 and 5 public roads and access streets are proposed as part of the township development, in order to provide vehicular access to all individual stands. The following comments are relevant:

* Minor Arterial Road (Class 3): These are typically all proposed roads within $25-32 \mathrm{~m}$ wide road reserves; in this case 'Road $A$ ' is the only major north-south collector street that will have a Class 3 status, within a proposed 30 m road reserve. This road will traverse the entire site from north-south and provide a link between the development portions north and south of the future PWV18. This road is also planned to bridge over the existing railway line along the southern border of the subject site and will therefore serve as a minor arterial for surrounding areas in future as well. It can be seen in Annexure A that the proposed Township Layout Plan has made provision for the necessary bridge sections (including batters) over the future PWV18 and the TFR railway line south of the site. Generally, no direct accesses to individual erven will be allowed off this road; it will only serve as the main collector and distributor for the subject township. In order to discourage speeding along 'Road A', traffic circles can be implemented at the intersections as traffic calming measures. This road will also serve as the primary public transport route through the proposed township (see Section 7).
* Major Collector Streets (Class 4a): These are typically all the proposed roads with 25 m wide road reserves; in this case the portion of proposed 'Road $\mathrm{C}^{\prime}$ to east of the proposed secondary school is the only collector street that will have a Class 4a status. 'Road B' is one of four proposed east-west Class 4 roads that will intersect with 'Road A' (see also Figure 2). To note is that no direct access to individual residential erven is allowed off this road. In order to discourage speeding along 'Road $\mathrm{B}^{\prime}$, speed humps (where necessary) and roundabouts can be implemented, but which will only be necessary in future if/ when this road is extended further to the east.
* Minor Collector Streets (Class 4b): These are typically all the proposed roads with 20 m wide road reserves; in this case they are 'Roads B, D and E' (see also Figure 2). These are all east-west Class 4 b roads that will intersect with 'Road $A$ ', as mentioned above. Direct access off these roads will be provided to the proposed school erven and possibly some residential erven - note that direct access to individual properties are allowed off Class 4 b roads, which are in line with the UTG 5 guidelines for urban collector streets. In order to discourage speeding along the Class 4 b roads, speed humps and mini roundabouts can be considered.
* Access Streets (Class 5): All other streets in the township will be Class 5 local access streets with road reserve widths typically ranging between $10 \mathrm{~m}, 13 \mathrm{~m}$ and 16 m . These roads will provide direct access to all single residential erven of the proposed townships.

It is confirmed that, from a traffic engineering point of view, inputs have already been provided with regards to the proposed township layout in Annexure A. It is therefore confirmed that the proposed internal road network of the subject township is supported in this TIA. Where necessary or requested, continued input will be provided to the township layout.

To that is that the proposed township is not planned to be security controlled upon completion and therefore stacking distance requirements become less relevant at this stage. It can be noted, however, that the proposed township layout makes provision for the implementation of security control in future, if required.

## 4. Traffic Flows \& Development Trip Generation

### 4.1 EXISTING TRAFFIC FLOWS \& OPERATION

Given the location and extent of the proposed development, new detailed traffic surveys were carried out at identified key intersections during the critical peak periods, namely the weekday AM and PM peak hour periods, on 23, 24 and 26 August 2021. The surveys comprised manual traffic counts at the nearby key intersections listed below. Note that for ease of reference and consistency, the intersection numbers given below correspond with those numbers of the previously approved Master TIA of the neighbouring Watervalspruit Townships (May 2015).
\# Heidelberg Road (R550/K154) \& K91 [Intersection 5];
\# Heidelberg Road (R550/K154) / Kingfish Street / Garthview Street [Intersection 12];
\# K91 / Cosmopolitan Drive [Intersection 13]; and
\# New traffic counts were also carried out at identified key intersections within the neighbouring Watervalspruit Townships, in order to estimate the actual trip generations of these neighbouring townships. Given that the subject township will cater for the same income market as the neighbouring Watervalspruit Townships (i.e. similar products to be developed), this will provide useful data that can be compared with the (theoretical) trip rates that are normally applied in the study area.

Classified traffic counts were conducted at the latter two intersections (i.e. 12 and 13), in order to also quantify public transport availability in the vicinity of the site. The current 2021 weekday morning (AM) and afternoon (PM) peak hour traffic volumes at this intersection are summarised in Figure 5. The respective peak hours occurred at 06:30-07:30 and 16:30-17:30.

From a traffic engineering perspective, it is acknowledged that the Covid-19 pandemic has also had an impact on the traffic volumes on the roads in general, with the Covid-19 lockdown regulations resulting in less traffic overall on the roads. However, at the time these traffic surveys were conducted, the majority of industries, businesses and schools had been fully operational again, with the resultant effect that the traffic volumes were considered sufficiently representative for this study. These traffic counts had also been compared to previous traffic counts that were conducted at the same $3 x$ intersections in 2019 and February 2020, before the Covid-19 lockdown, and it is confirmed that the latest 2021 traffic counts indicated considerable traffic growth overall at these key intersections.

### 4.2 FUTURE BACKGROUND TRAFFIC FLOWS

Apart from the current 2021 traffic flows, two future base traffic flow scenarios have been considered in this report, namely future 2026 and 2031. These future scenarios are in line with the proposed 'Service Plan Stages' of the neighbouring Watervalspruit Townships, which have been included as latent rights in this report (see Section 4.2.2). These future scenarios comprise different escalations of the existing 2021 peak hour traffic flows, at the different growth rates discussed in Section 4.2.1 below.

### 4.2.1 Traffic Growth

The THM16, Volume 1, South African Traffic Impact and Site Traffic Assessment Manual (Committee Draft, October 2019) suggests that for developments which generate more than 50 peak hour trips, it is necessary to undertake a full traffic impact assessment which must also include traffic growth and/ or the potential traffic generations of other nearby approved developments that still need to realise.

In order to make provision for other developments in the area and increases in traffic along the main routes, traffic growth is added. In this case the traffic growth makes provision for those other developments not accounted for in Section 4.2.2 below.

For the purposes of this study, it has been assumed that the background traffic would increase at the rate of $2.5 \%$ per annum for 5 years to 2026 and $2 \%$ per annum for 10 years to 2031. These growth rates are considered reasonable and typical to that used in most traffic studies in Gauteng and is also in line with was applied in the approved Master TIA of the neighbouring Watervalspruit Townships (May 2015). It can be added that the traffic growth is applied in addition to the extensive latent rights/ other developments which have been included in this study, as discussed below.

### 4.2.2 Trip Generations from 'Other Developments' (Latent Rights)

As indicated in attached Figure 2, three (3) other nearby developments in this case have been included as latent rights developments, which are discussed below:
\# Palm Ridge Extensions 10, 12 and 13. This is a low-cost, RDP housing development which is located about 1 km north of the subject site (this development is located directly north-east of the neighbouring Watervalspruit Townships). To note is that this is a Ministerial Project, which is overseen by the City of Ekurhuleni and the Gauteng Department of Human Settlements (DHS). Although the development mainly comprises RDP housing, it will also comprise educational facilities, social nodes and public open spaces. The breakdown of the land use rights, quantities and trip generation data for this development was obtained from the approved TIA conducted by MPA Consulting Engineers (Pty) Ltd in March 2016, entitled Palm Ridge Ext. 10, 12 \& 13, Ekurhuleni RDP Housing Development. Based on this TIA, the development, as a whole, will comprise a total of 6,063 'Residential 1' erven, 886 'Residential 4 ' units and 220 duplex dwelling units/row housing. It was also conservatively assumed that the schools would have 2,000 primary school students and 1,000 secondary school students between them. With regards to trip generations, it was estimated in the TIA that the Palm Ridge development, as a whole, would generate approximately 2,262 trips during the weekday AM and PM peaks.
To date, approximately 4,000 'Residential 1 ' erven have been constructed and occupied. The trips that are generated by these occupied units are already included in the existing 2021 traffic counts. For latent rights purposes, only the remaining trips during the weekday AM and PM peak were therefore considered, and added to the road network. Attached Figure 6a indicates the expected trips to be generated by the remainder of the Palm Ridge development through the subject study area, during the weekday AM and PM peak hours.
\# Watervalspruit Ext. 54. This proposed township is situated on Portion 43 of the Farm Waterval No. 150-IR, approximately 3.5 km north-west of the subject site. The breakdown of the land use rights, quantities and trip generation data for this development was obtained from the approved TIA conducted by Dhubecon Consulting Engineers in July 2020. Based on this TIA, the proposed township will be a mixed land-use development that will comprise of a total of 1,529 single residential stands ('Residential 1'). Provision is also made for two new public schools, a community facility and ample public open spaces. Without the necessary details with regards to the proposed new schools, it was assumed in this study that the schools would be combined primary and secondary public schools, with the two schools having a combined capacity of approximately 2,000 learners.
With regards to trip generations, it was estimated in the TIA that Watervalspruit Ext. 54, as a whole, would generate approximately 604 trips and 514 trips during the weekday AM and PM peak hours, respectively. No development has occurred to date and therefore the full trips have been taken into account in this TIA as part of latent rights. Attached Figure $\mathbf{6 e}$ indicates the estimated total trips to be generated by Watervalspruit Ext. 54 through the subject study area, during the weekday AM and PM peak hours.
\# Remainder of Watervalspruit Townships (Sky City): The remaining extent of the neighbouring Watervalspruit Townships development, which border the subject site directly to the north-west, has also been included as latent rights in this report (see Figure 2). It can be noted
that Dhubecon undertook a full Master TIA for the Watervalspruit Townships (dated May 2015), which had been approved by the City of Ekurhuleni (CoE) and Gautrans (GPDRT). Given the large extent of this development as a whole, the townships were grouped together into six (6) 'Service Plan Nodes' in the approved Master TIA. Those 6 'Service Plan Nodes' were then further grouped into three (3) 'Service Plan Stages' in order to split the development as a whole into three main parts. To note is that considerable development has taken place since the approved Master TIA of 2015 and the extents of the service nodes have changed over time, however, the same principle was applied for the purposes of this TIA.
Table 1 below provides the composition of the updated 'Service Plan Nodes' and 'Service Plan Stages' used in this TIA, for the purposes of latent rights. Note that the remaining extents/ quantities are indicated for 'Service Plan Nodes 1-3', since the majority of construction has already taken place in these Nodes. It is then further assumed that the three 'Service Plan Stages' will each take approximately 5 years to develop. Since 'Service Plan Stage $1^{\prime}$ (Node 1 and 2 ) is close to completion, 2021 was selected as the year when it will be fully operational / completed. This TIA therefore uses two horizon stages when the two (2) remaining 'Service Plan Stages' of the neighbouring Watervalspruit Townships will be operational, namely at 2026 and 2031.

Table 1: Neighbouring Watervalspruit Townships - Service Plan Nodes (Latent Rights)

| Service Plan Node | Watervalspruit Townships (Sky City) | Service Plan Stage (For Roads) | Residential <br> (Res 2 \& 4) | Business/ <br> Retail/ <br> Special | Educational |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1* | Watervalspruit Proper <br> Watervalspruit Ext. 1 <br> Watervalspruit Ext. 9 | 1 | 91 Erven | $19,009 \mathrm{~m}^{2} \text { GLA }$ <br> (Shopping Centre) <br> 13,532 m² GLA <br> (Big Box Retail) | $2 \times$ Primary <br> School |
| 2* | Watervalspruit Ext. 10-13, 21, 27 and 28 |  |  |  |  |
| 3* | Watervalspruit Ext. 16-20 | 2 | 2,931 Erven <br> 1,845 Units | $5,387 \mathrm{~m}^{2} \mathrm{GLA}$ <br> (Convenience Retail) <br> Filling Station $11,803 \mathrm{~m}^{2} \text { GLA }$ <br> (Special) | 4 x Primary School |
| 4 | Watervalspruit Ext. $\begin{gathered} 35,37,38,47,48, \\ 50,51 \& 55 \end{gathered}$ |  |  |  |  |
|  | Palm Ridge Ext. 3133 |  |  |  |  |
| Future | Watervalspruit Ext. $14,15,22-26,31-33$ <br> and 39-46 | 3 | 5,976 Erven <br> 1,040 Units | - | $4 \times$ Primary <br> School <br>  <br> Secondary <br> School <br> Combined |
| TOTAL |  |  | 8,998 Erven <br> 2,885 Units | 49,731 m² GLA (Retail \& Special) | $12 \times$ schools |

*The remaining development extents are indicated, since construction and occupation is already far along for these Nodes.

Attached Figures 6b-d shows the expected trips to be generated by 'Service Plan Stage 1, 2 and 3', respectively, of the neighbouring Watervalspruit Townships, through the key intersections during the weekday AM and PM peaks. Note that the 'Service Plan Stage 2' trips (as per Figure 6c) include the 'Service Plan Stage 1' trips (as per Figure 6b), while the 'Service Plan Stage 3' trips (as per Figure 6d) represent the total trips that will be generated by the Watervalspruit Townships (as a whole) and therefore includes the 'Service Plan Stage 1 and 2' trips (as per Figure 6c).
Given all of the above-mentioned developments that have been included as latent rights in this TIA, the following must be noted:
\# The Watervalspruit Townships (i.e. Sky City) will have to be fully developed before Watervalspruit Ext. 54 and the subject township can be developed, given that the accessibility of these two townships will be dependent on the future road network of the Watervalspruit Townships. For the purposes of this TIA, it was assumed that the Watervalspruit Townships would be fully developed by 2026 (along with the Palm Ridge Townships), while Watervalspruit Ext. 54 and the subject township would be fully developed by 2031.
\# Therefore, the total future 2026 background traffic presented and investigated in this TIA, as summarised in Figure 7, comprises of three components, namely the background traffic growth over 5 years (at $2.5 \%$ p.a.), the total latent rights trips from Palm Ridge Ext. 10, 12 and 13 (Figure 6a) and the neighbouring Watervalspruit Townships (i.e. 'Service Plan Stage 3'), as per Figure 6d.
\# Similarly, the total future 2031 background traffic presented and investigated in this TIA, as summarised in Figure 8, comprises of three components, namely the background traffic growth over 10 years (at $2.0 \%$ p.a.), the total latent rights trips from Palm Ridge Ext. 10, 12 and 13 (Figure 6a) and the neighbouring Watervalspruit Townships (i.e. 'Service Plan Stage $\mathbf{3}^{\prime}$ ), as per Figure 6d, as well as the total latent rights trips from Watervalspruit Ext. 54 (Figure 6e).

### 4.3 DEVELOPMENT TRIP GENERATION

In order to determine the expected trip generations of the proposed development, the latest and most relevant guideline, entitled TMH 17 Volume 1, South African Trip Data Manual (Committee Draft 2.0, May 2018) was used as a basis, which is based on a more comprehensive data base and which makes provision for the different types of residential developments, as well different income levels of developments, vehicle ownership and availability of public transport services.

Since Rietspruit is a proposed mixed land use development is was necessary to consider each of the different (primary) land uses separately, allowing for the necessary adjustments of each land use and then add all the separate land uses together.

### 4.3.1 Residential Trip Generation

Given the type of development proposed (as per Section 3.1), the lower income market is being targeted, which is generally synonymous with a lower vehicle ownership and consequently the trip generation characteristics are different. Apart from a lower vehicle ownership itself, many of these residents still find it more affordable to use public transport for commuting instead of their own private vehicles.

The Trip Data Manual allows for 'Single Dwelling Units' ('Residential 1'), with adjustments in terms of vehicle ownership and the availability of public transport. As noted in Section 3.1 of this report and the proposed township layout in Annexure A, the majority of the proposed township will comprise of single residential erven (i.e. 'Residential $1^{\prime}$ ').

The following assumptions and notes are relevant with respect to the trip generation calculations:

* Standard trip rate for 'Single Dwelling Units' is 1.00 trips/ unit during the weekday AM and PM peaks;
* 'Single Dwelling Unit' adjustment factor allowed for low vehicle ownership is $40 \%$ and that for very low vehicle ownership is $70 \%$ - in this case $60 \%$ had been applied;
* For 'Transit Nodes or Corridors' (i.e. availability of public transport) a maximum adjustment of $15 \%$ is allowed. In this instance the maximum value of $15 \%$ had been applied, given the significant public transport availability and usage in the study area; and
* For 'Mixed Land Use' a maximum adjustment of $10 \%$ is allowed for 'Single Dwelling Units'. However, since the residential component is viewed as the main land use, no such reduction had been applied in this case.
With the above assumptions, the reduced trip rate has been calculated as follows: - 'Residential 1 ' $1.00 \times 0.40 \times 0.85=\mathbf{0 . 3 4 0}$ trips/unit

To note is that the above residential trip rate is slightly more conservative than the trip rate that was applied in the approved Master TIA for the neighbouring Watervalspruit Townships (May 2015), as well as in the approved TIA for Watervalspruit Ext. 54 (July 2020), which have been approved by both CoE and Gautrans. It is also slightly more conservative than trip rates that were applied in the previously approved TIA for Palm Ridge Ext. $10,12 \& 13$, which is included as latent rights in this study.
By applying the above calculated trip rate to the total number of erven proposed, the maximum number of peak hour trips is estimated at:

- For 3,782 single residential erven ('Residential 1') = 1,286 trips

The estimated residential trips during the weekday AM and PM peak hours for the proposed township are summarised in Table 2 below, given the directional splits (IN:OUT) of 25:75 and 70:30 for the weekday AM and PM peaks, respectively.
Table 2: Estimated Development Trips - Residential

| Peak | Development Trips (vph) |  |  |
| :--- | :---: | :---: | :---: |
|  | IN | OUT | TOTAL |
| Weekday AM Peak hr | 322 | 964 | $\mathbf{1 , 2 8 6}$ |
| Weekday PM Peak hr | 900 | 386 | $\mathbf{1 , 2 8 6}$ |

### 4.3.2 Educational Trip Generation

It can be argued that the proposed schools are a direct result of the dominantly large residential component. With the development catering for the lower income market, it is expected that learners would typically walk to and from school. In the case of some vehicle trips, most of those would be internal trips (i.e. parents dropping children off at school), except for some students and teachers from outside the area that may use private vehicle transport. It is also expected that minibus taxis and buses will be utilized to drop off and pick up students at the proposed schools.

As mentioned in Section 3.1 of this TIA, it was assumed in this study that the proposed public primary schools would each have a capacity of 800 students (thus 1,600 students in total), while the proposed public secondary school would have a capacity of 1,200 students. Similar to the residential component, the following additional assumptions and notes are relevant with respect to the trip generation rate calculations:

For the proposed public primary and secondary schools, the following average base trip rates are recommended in the TMH 17 Volume 1 (Committee Draft 2.0, May 2018):

- Public Primary School - 0.85 trips/ student and 0.30 trips/ student for the weekday AM and PM peak hours, respectively; and
- Public Secondary School - 0.75 trips/ student and 0.25 trips/ student for the weekday AM and PM peak hours, respectively
* Since this is a mixed land use development, of which the largest overall component by far is residential, it would be reasonable to assume that the proposed school would, to a large extent, be dependent on the proposed residential component. Therefore a 'Mixed-use Development' reduction was applied which accounts for internal trips, i.e. trips made by vehicles originating from inside the proposed township. In this study $50 \%$ had been applied;
* The maximum adjustment factor allowed for 'Very Low Vehicle Ownership' is $80 \%$. In this instance the maximum value of $80 \%$ had been applied; and
* For 'Transit nodes or Corridors' (i.e. availability of public transport) a maximum adjustment of $15 \%$ is allowed. The considerable existing public transport presence in the vicinity of the site justifies an adjustment factor and in this case the maximum $15 \%$ had been applied.
Based on the above assumptions, the estimated (reduced) trip rates for the different school types during the weekday AM and PM peak hours are summarised in Table 3 below:
Table 3: Estimated School Trip Rates

| Proposed School Type | Trips Generated (per Student) |  |
| :--- | :---: | :---: |
|  | Weekday AM Peak hr | Weekday PM Peak hr |
| Public Primary | 0.072 | 0.026 |
| Public Secondary | 0.064 | 0.021 |

To note is that the above trip rates are in line with the trip rates which were applied in the previously approved Master TIA of the neighbouring Watervalspruit Townships (May 2015), given the similar nature of the subject development.

Based on the above trip rates, it is estimated that the proposed three schools will generate a combined total of about 192 trips and 66 trips during the weekday AM and PM peak hours, respectively. Using directional splits (IN:OUT) of 50:50 for the weekday AM and PM peaks, the estimated educational trips are summarised below in Table 4.

Table 4: Estimated Development Trips - Educational

| 寝 Peak | Development Trips (vph) |  |  |
| :--- | :---: | :---: | :---: |
|  | IN | OUT | TOTAL |
| Weekday AM Peak hr | 96 | 96 | $\mathbf{1 9 2}$ |
| Weekday PM Peak hr | 33 | 33 | $\mathbf{6 6}$ |

### 4.3.3 Other Land Use Trip Generations

The other proposed land uses such as the community facilities, utilities erven and public open spaces are viewed as ancillary to the main residential and institutional land uses, with trip generations resulting from these land uses expected to be mostly internal. For the purposes of this document, the trip
generations of these land uses are therefore viewed as negligible and have been discarded from the traffic projections and analyses.

### 4.3.4 TOTAL Development Trips

The total (combined) development trips during the weekday AM and PM peak hours, which consist of the primary trips to be generated by the proposed township, as a whole, are summarised in Table 5 below.

Table 5: Estimated TOTAL Development Trips - Proposed Township: Rietspruit

| Land Use | AM Peak Hour (vph) |  |  | PM Peak Hour (vph) |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN | OUT | TOTAL |  | IN | OUT | TOTAL |
| Residential | 322 | 964 | 1,286 |  | 900 | 386 | 1,286 |
| Educational | 96 | 96 | 192 |  |  |  |  |
| TOTAL | $\mathbf{4 1 8}$ | $\mathbf{1 , 0 6 0}$ | $\mathbf{1 , 4 7 8}$ |  |  |  |  |

It is confirmed that the theoretical trip generations of the neighbouring Watervalspruit Townships (based on the trip rates applied in the approved TIA) had been compared with the actual trip generations (based on the traffic counts mentioned in Section 4.1), given the existing overall development extent, which had been confirmed by the client/ developer. It was found that, overall, the theoretical and actual trip generations are very similar and given that a slightly more conservative residential trip rate had been applied in this TIA, the estimation of the total trips that will be generated by the subject township, as a whole, is viewed as representative/ adequate.

### 4.4 TRIP DISTRIBUTION \& ASSIGNMENT

Assumptions on the expected trip distribution were based on the location of the proposed site access intersections in relation to the surrounding road network, existing traffic volumes and patterns in the study area, the type of development in relation to employment as well as our knowledge of the area and involvement in other surrounding developments.

Attached Figures 9a-b depict the expected trip distributions of the residential and educational components (i.e. main land uses) of the proposed township.

Given the above distributions, Figures 10a-b summarise the corresponding development trips at the key intersections for the proposed township and Figure 11 indicates the estimated TOTAL development weekday AM and PM peak hour trips at the key intersections.

### 4.5 ASSESSMENT TRAFFIC FLOWS WITH DEVELOPMENT

Figure 12 shows the projected future 2031 base traffic volumes with the estimated traffic generations of the proposed development (as a whole), plus the total latent rights trips from Palm Ridge Ext. 10, 12 and 13 , 'Service Plan Stage 3 ' of the neighbouring Watervalspruit Townships and Watervalspruit Ext. 54 (i.e. total latent rights trips). This figure represents the summation of Figures $\mathbf{8}$ and $\mathbf{1 1}$.

In this report Figures 5, 7, $\mathbf{8}$ and $\mathbf{1 2}$ had been used for assessing the current traffic conditions, as well as the traffic impact of the proposed development, other nearby developments (i.e. latent rights) and future background traffic growth, onto the surrounding road network (see Section 5 on the following page).

## 5. Road / Intersection Capacity

Capacity analyses had been undertaken in order to quantify the anticipated traffic impact of the proposed development rights. For this purpose, PTV Vistro 2020 and SIDRA Intersection 9 traffic engineering software had been used to undertake capacity analyses at the various key intersections.

With reference to the analyses of various scenarios, this section comments on the current traffic operations without the additional development traffic, as well as the likely traffic flow conditions with the additional development traffic. Where necessary and feasible, intersection improvements have identified that would mitigate the likely traffic impact and/or improve current traffic flow conditions.

The following key intersections have been analysed for potential traffic impact, namely:

1. Heidelberg Road (R550/K154) \& K91 [Intersection 5];
2. Heidelberg Road (R550/K154) / Kingfish Street / Garthview Street [Intersection 12];
3. K91 / Cosmopolitan Drive [Intersection 13];
4. Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street [Intersection 14];
5. Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15];

Note that for ease of reference, the relevant intersection numbers have also been indicated, as per the approved Master TIA of the neighbouring Watervalspruit Townships (May 2015).

The following scenarios were analysed, namely:
> Scenario 1: Existing 2021 weekday AM and PM peak hour traffic volumes without the proposed development (as per Figure 5);
> Scenario 2: Future 2026 base weekday AM and PM peak hour traffic volumes PLUS Palm Ridge Ext. 10, 12 \& 13 latent rights trips PLUS Watervalspruit 'Service Plan Stage 3' latent rights trips, but WITHOUT the proposed development (as per Figure 7);
> Scenario 3: Future 2031 base weekday AM and PM peak hour traffic volumes PLUS Palm Ridge Ext. 10, 12 \& 13 latent rights trips PLUS Watervalspruit 'Service Plan Stage 3' latent rights trips PLUS Watervalspruit Ext. 54 latent rights trips, but WITHOUT the proposed development (as per Figure 8);
> Scenario 4: Future 2031 base weekday AM and PM peak hour traffic volumes PLUS Palm Ridge Ext. 10, 12 \& 13 latent rights trips PLUS Watervalspruit 'Service Plan Stage 3' latent rights trips PLUS Watervalspruit Ext. 54 latent rights trips PLUS total development trips (as per Figure 13);

Results of the SIDRA Intersection 9capacity analyses at the various intersections are discussed in the following sub sections, with the details of the outputs enclosed in Annexure B. It must be noted that for all signalized intersections, optimised traffic signal phasing had been used during the traffic analyses.

### 5.1 HEIDELBERG ROAD (R550/K154) \& K91 [INTERSECTION 5]

## Existing Geometry \& Control:

- 4-Legged;
- Priority stop controlled intersection with freeflow conditions prevailing along Heidelberg Road;
- North: One shared through, left-turning and right-turning lane (single lane approach);
- East: One through lane, one short rightturning lane and one short left-turning lane;
- South: One shared through, left turning and right turning lane (single lane approach); and
- West: One through lane, one short rightturning lane and one short left-turning slip lane.


Analysis Results \& Conclusion Intersection: Heidelberg Road \& K91
Detailed Results: Annexures B1.1 to B1.12

| Scenario |  <br> Control | Peak | 'Worst Case' Stop / Overall |  | Comment |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :--- |
|  |  |  | Delay(s) | $\mathbf{v} / \mathbf{c}_{\text {max }}$ |  |  |
| Scenario 1 | Existing geometry | AM | F | $>200$ | 1.214 | Very poor level of operation |
| Scenario 2 | Upgraded geometry | AM | F | 124 | 1.295 | Very poor overall level of operation |
| Scenario 2 | Phase 1 geometry | AM | C | 32 | 0.875 | Acceptable overall level of operation |
| Scenario 3 | Phase 1 geometry | AM | D | 35 | 0.921 | Acceptable overall level of operation |
| Scenario 4 | Phase 1 geometry | AM | F | 171 | 1.409 | Very poor overall level of operation |
| Scenario 4 | Phase 2 geometry | AM | D | 38 | 0.904 | Acceptable overall level of operation |
| Scenario 1 | Existing geometry | PM | F | $>200$ | 1.292 | Very poor level of operation |
| Scenario 2 | Upgraded geometry | PM | D | 41 | 1.024 | Poor overall level of operation |
| Scenario 2 | Phase 1 geometry | PM | C | 21 | 0.844 | Acceptable overall level of operation |
| Scenario 3 | Phase 1 geometry | PM | C | 22 | 0.862 | Acceptable overall level of operation |
| Scenario 4 | Phase 1 geometry | PM | F | 189 | 1.083 | Very poor overall level of operation |
| Scenario 4 | Phase 2 geometry | PM | C | 25 | 0.896 | Acceptable overall level of operation |


|  | This intersection already operates over capacity during the weekday AM and PM <br> peak hours and is set to be upgraded in due course (discussed in more detail in <br> Section 0. However, by the time the full extent of the neighbouring Watervalspruit <br> Townships has realized, additional upgrades will be required to this intersection and <br> these form part of the first phase of upgrades identified in this TIA. These <br> upgrades are represented by Phase 1 geometry above. Further upgrades will also <br> be required as part of the proposed development and is represented by Phase 2 <br> geometry above. The primary reason for the above upgrades is to mitigate the <br> conflicting movement between the large through volumes along Heidelberg Road <br> and the large turning volumes on the K91 northern approach. |
| :--- | :--- |
| Conclusion: | Yes, as per Drawing No. 0573/CL/01/01a - 01c |
| Upgrade Required: | Developer - to be split proportionally between the subject development (Rietspruit) <br> and the neighbouring Watervalspruit Townships (Sky City). |
| Upgrade Responsibility: |  |

### 5.2 HEIDELBERG ROAD (R550/K154) / KINGFISH STREET / GARTHVIEW STREET [INTERSECTION 12]

## Existing Geometry \& Control:

- 4-Legged;
- Signalised Intersection;
- North: One shared through and rightturning lane and one short left-turning lane;
- East: One through lane, one short rightturning lane and one short left-turning lane;
- South: One shared through, left turning and right turning lane (single lane approach); and
- West: One through lane, one short rightturning lane and one short left-turning slip lane.


Analysis Results \& Conclusion Intersection: Heidelberg Rd/Kingfish St / Garthview St
Detailed Results: Annexures B2.1 to B2.12

| Scenario | Geometry \& Control | Peak | Overall |  |  | Comment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Delay(s) | v/c ${ }_{\text {max }}$ |  |
| Scenario 1 | Existing geometry | AM | D | 53 | 0.967 | Acceptable overall level of operation |
| Scenario 2 | Existing geometry | AM | F | >200 | 1.897 | Very poor overall level of operation |
| Scenario 2 | Phase 1 geometry | AM | D | 40 | 0.919 | Acceptable overall level of operation |
| Scenario 3 | Phase 1 geometry | AM | E | 65 | 1.006 | Poor overall level of operation |
| Scenario 4 | Phase 1 geometry | AM | F | 114 | 1.109 | Very poor overall level of operation |
| Scenario 4 | Phase 2 geometry | AM | D | 40 | 0.907 | Acceptable overall level of operation |
| Scenario 1 | Existing geometry | PM | B | 11 | 0.519 | Good overall level of operation |
| Scenario 2 | Existing geometry | PM | F | 106 | 1.280 | Very poor overall level of operation |
| Scenario 2 | Phase 1 geometry | PM | B | 16 | 0.819 | Good overall level of operation |
| Scenario 3 | Phase 1 geometry | PM | C | 22 | 0.846 | Acceptable overall level of operation |
| Scenario 4 | Phase 1 geometry | PM | D | 41 | 1.003 | Poor overall level of operation |
| Scenario 4 | Phase 2 geometry | PM | B | 19 | 0.773 | Good overall level of operation |


|  | This intersection currently operates adequately during the weekday AM and PM <br> peak hours, but by the time the full extent of the neighbouring Watervalspruit <br> Townships has realized, additional upgrades will be required to this intersection and <br> these form part of the first phase of upgrades identified in this TIA. Further <br> upgrades will also be required as part of the proposed development and these form <br> part of the second phase of upgrades identified in this TIA. Both phases of the <br> proposed upgrades to this intersection are discussed in more detail in Section 6. |
| :--- | :--- |
| Conclusion: | Yes, as per Drawing No. 0573/CL/01/02a - 02b |
| Upgrade Required: | Developer - to be split proportionally between the subject development (Rietspruit) <br> and the neighbouring Watervalspruit Townships (Sky City). |
| Upgrade Responsibility: |  |

### 5.3 K91 / COSMOPOLITAN DRIVE [INTERSECTION 13]

## Existing Geometry \& Control:

- 4-Legged;
- Allow stop controlled intersection (to be signalized in future);
- North-East: One through lane, one short right-turning lane and one short left-turning slip lane;
- South-West: One through lane, one short right-turning lane and one short left-turning slip lane;
- North-West: One through lane, one short right-turning lane and one short left-turning slip lane; and
- South-East: One through lane, one short right-turning lane and one short left-turning slip lane.


| Analysis Results \& Conclusion |  |  | Intersection: K91 / Cosmopolitan Dr |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detailed Results: Annexures B3.1 to B3.10 |  |  |  |  |  |  |
| Scenario | Geometry \& Control | Peak | Overall |  |  | Comment |
|  |  |  | LOS | Delay(s) | v/c $\mathrm{m}_{\text {max }}$ |  |
| Scenario 1 | Existing geometry | AM | B | 11 | 0.331 | Good overall level of operation |
| Scenario 2 | Signalized | AM | F | 145 | 1.394 | Very poor overall level of operation |
| Scenario 2 | Phase 1 geometry | AM | C | 24 | 0.864 | Acceptable overall level of operation |
| Scenario 3 | Phase 1 geometry | AM | C | 26 | 0.858 | Acceptable overall level of operation |
| Scenario 4 | Phase 2 geometry | AM | D | 42 | 0.964 | Acceptable overall level of operation |
| Scenario 1 | Existing geometry | PM | B | 15 | 0.602 | Good overall level of operation |
| Scenario 2 | Signalized | PM | F | 153 | 1.500 | Very poor overall level of operation |
| Scenario 2 | Phase 1 geometry | PM | C | 25 | 0.918 | Acceptable overall level of operation |
| Scenario 3 | Phase 1 geometry | PM | E | 73 | 1.158 | Poor overall level of operation |
| Scenario 4 | Phase 2 geometry | PM | D | 42 | 0.975 | Acceptable overall level of operation |

$\left.\begin{array}{|l|l|}\hline \text { Conclusion: } & \begin{array}{l}\text { This intersection currently operates adequately during the weekday AM and PM } \\ \text { peak hours, but by the time the full extent of the neighbouring Watervalspruit }\end{array} \\ \text { Townships has realized, additional upgrades will be required to this intersection and } \\ \text { these form part of the first phase of upgrades identified in this TIA. Further } \\ \text { upgrades will also be required as part of the proposed development and these form } \\ \text { part of the second phase of upgrades identified in this TIA. Both phases of the } \\ \text { proposed upgrades to this intersection are discussed in more detail in Section 6. }\end{array}\right\}$

### 5.4 HEIDELBERG ROAD (R550/K154) / SILVER DORY STREET / SALAMANDERFISH STREET [INTERSECTION 14]

## Proposed Geometry \& Control:

- Note: For PHASE 1 upgrades;
- 4-Legged;
- Signalized;
- North: One through lane, one short rightturning lane and one short left-turning slip lane;
- South: One through lane, one short rightturning lane and one short left-turning slip lane;
- East: One through lane, one short rightturning lane and one short left-turning slip lane; and
- West: One through lane, one short rightturning lane and one short left-turning slip lane.


Analysis Results \& Conclusion Intersection: Heidelberg Rd / Silver Dory St / Salamanderfish St

Detailed Results: Annexures B4.1 to B4.8

| Scenario |  <br> Control | Peak | Overall |  |  | Comment |
| :--- | :--- | :---: | :---: | :---: | :---: | :--- |
|  |  |  | Delay(s) | $\mathbf{v / c}_{\mathbf{m a x}}$ |  |  |
| Scenario 2 | Phase 1 geometry | AM | B | 14 | 0.791 | Good overall level of operation |
| Scenario 3 | Phase 1 geometry | AM | B | 16 | 0.842 | Good overall level of operation |
| Scenario 4 | Phase 1 geometry | AM | F | 154 | 1.244 | Very poor overall level of operation |
| Scenario 4 | Phase 2 geometry | AM | B | 18 | 0.805 | Good overall level of operation |
| Scenario 1 | Phase 1 geometry | PM | B | 13 | 0.820 | Good overall level of operation |
| Scenario 2 | Phase 1 geometry | PM | B | 14 | 0.838 | Good overall level of operation |
| Scenario 3 | Phase 1 geometry | PM | F | 153 | 1.243 | Very poor overall level of operation |
| Scenario 5 | Phase 2 geometry | PM | B | 16 | 0.792 | Good overall level of operation |


| Conclusion: | The proposed geometry for this intersection, as depicted above, forms part of the <br> first phase of upgrades identified in this TIA, which will be required by the time the <br> full extent of the neighbouring Watervalspruit Townships has realized. Further <br> upgrades will also be required as part of the proposed development and these form <br> part of the second phase of upgrades identified in this TIA. Both phases of the <br> proposed upgrades to this intersection are discussed in more detail in Section 6. |
| :--- | :--- |
| Upgrade Required: | Yes, as per Drawing No. 0573/CL/01/04a - 04b |
| Upgrade Responsibility: | Developer - to be split proportionally between the subject development (Rietspruit) <br> and the neighbouring Watervalspruit Townships (Sky City). |

### 5.5 HEIDELBERG ROAD (R550/K154) / YELLOW JACK STREET [INTERSECTION 15]

## Proposed Geometry \& Control:

- Note: For PHASE 1 upgrades;
- 3-Legged (T-intersection);
- Signalized;
- South: One short right-turning lane and one short left-turning slip lane;
- East: One through lane and one short left-turning lane; and
- West: One through lane and one short right-turning lane.


Analysis Results \& Conclusion Intersection: Heidelberg Rd/Yellow Jack St

## Detailed Results: Annexures B5.1 to B5.8

| Scenario |  <br> Control | Peak | Overall |  |  | Comment |
| :--- | :--- | :---: | :---: | :---: | :---: | :--- |
|  |  |  | Delay(s) | $\mathbf{v} / \mathbf{c}_{\text {max }}$ |  |  |
| Scenario 2 | Phase 1 geometry | AM | A |  | 0.580 | Very good overall level of operation |
| Scenario 3 | Phase 1 geometry | AM | A | 8 | 0.643 | Very good overall level of operation |
| Scenario 4 | Phase 1 geometry | AM | F | 94 | 1.210 | Very poor overall level of operation |
| Scenario 4 | Phase 2 geometry | AM | B | 20 | 0.869 | Good overall level of operation |
| Scenario 1 | Phase 1 geometry | PM | A | 9 | 0.625 | Very good overall level of operation |
| Scenario 2 | Phase 1 geometry | PM | A | 9 | 0.656 | Very good overall level of operation |
| Scenario 3 | Phase 1 geometry | PM | F | 106 | 1.287 | Very poor overall level of operation |
| Scenario 5 | Phase 2 geometry | PM | B | 19 | 0.755 | Good overall level of operation |


| Conclusion: | The proposed geometry for this intersection, as depicted above, forms part of the <br> first phase of upgrades identified in this TIA, which will be required by the time the <br> full extent of the neighbouring Watervalspruit Townships has realized. Further <br> upgrades will also be required as part of the proposed development and these form <br> part of the second phase of upgrades identified in this TIA. Both phases of the <br> proposed upgrades to this intersection are discussed in more detail in Section 6. |
| :--- | :--- |
| Upgrade Required: | Yes, as per Drawing No. 0573/CL/01/05a - 05b |
| Upgrade Responsibility: | Developer - to be split proportionally between subject development (Rietspruit) and <br> the neighbouring Watervalspruit Townships (Sky City) development. |

## 6. Road and/or Intersection Upgrades

Based on the estimated additional traffic generations of the proposed development (as a whole) and the projected trip distribution onto the surrounding road network during the weekday AM and PM peak hours, the impact of other nearby developments (i.e. latent rights), the capacity analyses in Section 5 as well as on-site observations during the peaks, the road/ intersection upgrades as outlined in this section are proposed.

Important to note is that all of the required upgrades at the external key intersections have been split into two (2) phases, as indicated in Section 5 above. The first phase of upgrades will be required as part of the complete development of the neighbouring Watervalspruit Townships, i.e. when the total trips from these townships have realized. The second phase of upgrades will be required as part of the development of the proposed Rietspruit Township, which is only expected to happen after the neighbouring Watervalspruit Townships have been completed. Therefore, the first phase of upgrades are based on the traffic volumes summarized in Figure 7 (or Scenario 2 in Section 5), while the second phase of upgrades are based on the traffic volumes summarized in Figure $\mathbf{1 2}$ (or Scenario 4 in Section 5). The external intersection upgrades required as part of the Watervalspruit Ext. 54 Township have also been taken into account; however, the majority of these upgrades are expected to already be catered for by the time the neighbouring Watervalspruit Townships have been fully developed. These upgrades are therefore not shown/ highlighted individually.

It must further be mentioned that the Heidelberg Road (R550 / K154) and K91 intersection is due for the upgrades shown separately in Drawing No. 0573/CL/01a. These upgrades have been approved by the relevant road authorities and a Wayleave is already in place for construction to commence in due course. Therefore, the proposed first and second phase upgrades (as mentioned above) are taken as additional upgrades to these upgrades that will be implemented in the near future.

The proposed road and intersection upgrades for each of the two phases are summarized below. All of the proposed upgrades on Heidelberg Road (future K154) and the K91 are to be implemented to Gautrans' minimum design standards.

### 6.1 EXTERNAL ROAD \& INTERSECTION UPGRADES

### 6.1.1 Phase 1 Upgrades

(Required as part of the neighbouring Watervalspruit Townships)

## \# Heidelberg Road (R550/ K154) / K91 [Intersection 5]:

Refer to Drawing No. 0573/CL/01b

- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road;
- Additional short right turning lane to be added on the northern approach of the K91;
- The short, shared through and left turning slip lane on the northern approach of the K91 (as per Drawing No. 0573/CL/01a) to be upgraded to a short through lane with a separate short left turning slip lane; and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/K154) / Kingfish Street / Garthview Street [Intersection 12]:


## Refer to Drawing No. 0573/CL/02a

- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road;
- Existing shared through and right turning lane on the Kingfish Street approach to be converted to a dedicated right turning lane;
- Additional short right turning lane to be added on the Kingfish Street approach;
- Existing short left turning lane on the Kingfish Street approach to be extended and upgraded to a short, shared through and left turning slip lane;
- Additional short right turning lane to be added on the Garthview Street approach, with the existing approach lane to be converted to a shared through and left turning lane only; and
- Updated signal layout and signal timing plans.


## \# K91 / Cosmopolitan Drive [Intersection 13]:

## Refer to Drawing No. 0573/CL/03a

- Additional through lane to be added on the south-western approach of the K91;
- Additional receiving lane to be added on the north-eastern leg of the K91;
- Additional short right turning lane to be added on the north-eastern approach of the K91;
- Additional short receiving lane to be added on the north-western leg of Cosmopolitan Drive;
- Existing left turning slip lane (with yield control) on the north-western approach of Cosmopolitan Drive to be upgraded to a continuous slip lane with a short receiving lane on the K91 (north-eastern leg); and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street [Intersection 141:


## Refer to Drawing No. 0573/CL/04a

- Proposed new 4-legged intersection with separate short right turning and left turning slip lanes on all 4 approaches; and
- Signalization of the intersection, when warranted.
\# Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15]: Refer to Drawing No. 0573/CL/05a
- Proposed new T-intersection with separate turning lanes on the eastern and western approaches of Heidelberg Road;
- Southern approach of Yellow Jack Street to comprise a dedicated left turning slip lane and a short right turning lane; and
- Signalization of the intersection, when warranted.


### 6.1.2 Phase 2 Upgrades

(Required as part of the proposed Rietspruit Township)

## \# Heidelberg Road (R550/ K154) / K91 [Intersection 5]: Refer to Drawing No. 0573/CL/01c

- Additional through lane to be added on the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road;
- Additional short right turning lane to be added on the eastern approach of Heidelberg Road and the existing short right turning lane to be extended;
- Additional receiving lane to be added on the northern leg of the K91; and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/ K154) / Kingfish Street / Garthview Street [Intersection 12]:
Refer to Drawing No. 0573/CL/02b
- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road; and
- Updated signal layout and signal timing plans.
\# K91 / Cosmopolitan Drive [Intersection 13]:


## Refer to Drawing No. 0573/CL/03b

- Additional through lane to be added on the north-eastern approach of the K91;
- Additional receiving lane to be added on the south-western leg of the K91; and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street [Intersection 14]:


## Refer to Drawing No. 0573/CL/04b

- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road; and
- Updated signal layout and signal timing plans.
\# Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15]:
Refer to Drawing No. 0573/CL/05b
- Additional short right turning lane to be added on the western approach of Heidelberg Road;
- Additional short receiving lane to be added on Yellow Jack Street;
- Additional through lane to be added on the eastern approach of Heidelberg Road;
- Additional receiving lane on the western leg of Heidelberg Road; and
- Updated signal layout and signal timing plans.


### 6.2 INTERNAL ROAD \& INTERSECTION UPGRADES

All of the proposed upgrades outlined below are required as part of the proposed Rietspruit Township and are shown in attached Drawing No. 0573/CL/06.
\# 'Road A' (Extension of Yellow Jack Street):

- New Class 3 public road of approximately $2150 \mathrm{~m}(2.15 \mathrm{~km})$ in length.
\# 'Road A' / 'Road B' Intersection:
- Proposed new traffic circle (approximately 18 m inscribed diameter) with a single circulating lane and painted splitter islands.


## \# 'Road A' / 'Road C' Intersection:

- Proposed new traffic circle (approximately 20 m inscribed diameter) with a single circulating lane and painted splitter islands.


## \# 'Road A' / 'Road D' Intersection:

- Proposed new traffic circle (approximately 18 m inscribed diameter) with a single circulating lane and painted splitter islands.
\# 'Road A' / 'Road E' Intersection:
- Proposed new 4-legged priority stop controlled intersection, with free-flow conditions prevailing along 'Road $\mathrm{A}^{\prime}$.

In the event of bulk engineering contributions payable with respect to roads and stormwater, it is recommended that at least part of the contribution be off-set against the proposed road and intersection upgrades, as outlined above, since the upgrades will also benefit other future developments and the relevant road authorities. It is acknowledged that the off-setting of costs against provincial roads could be a problem in terms of the legislation, but it is recommended that the CoE, Midvaal Local Municipality and Gautrans come to some agreement in this respect.

## 7. Non-Motorised \& Public Transport

### 7.1 AVAILABILITY OF SERVICES \& FACILITIES

On-site observations revealed that Heidelberg Road (R550/K154) and Road K91, which are both located in close proximity to the subject site, are popular public transport routes for minibus-taxis and buses. These roads are serving and connecting several low income townships to the north of Heidelberg Road such as Vosloorus, Katlehong, Thokoza and Palm Ridge. To note is that there are several bus stops along these routes and their intersections. Cosmopolitan Drive and Kingfish Street, which had been constructed as part of the neighbouring Watervalspruit Townships, have also become popular public transport routes in recent years.

The classified traffic counts undertaken at the Cosmopolitan Drive / K91 intersection indicated that of all vehicles at this intersection during the weekday AM and PM peak hours, approximately $16 \%$ and $11 \%$, respectively, were minibus-taxis. Similar counts at the Heidelberg Road (R550) / Kingfish Street / Garthview Street intersection confirmed percentages of about $8 \%$ and $6 \%$ during the weekday AM and PM peaks, respectively. Buses accounted for about 1-2\% of all vehicles at these intersections during the weekday AM and PM peaks. Considering the traffic volumes at these intersections (refer to Figure 5), these percentages suggest a considerable public transport presence in the study area.

Given the undeveloped status of the subject site and surrounding properties, the site itself is not currently served by public transport services, nor is there any proper public transport facilities in place (such as walkway and laybys). However, the implementation of the proposed new public roads will connect the subject site to such services and facilities and it is expected that the proposed development, together with other developments such as the neighbouring Watervalspruit Townships and the Palm Ridge Townships, will further stimulate the demand for public transport services as they develop over time and it is expected that particularly minibus taxis would respond to this demand by providing more services. It is also expected that 'Road A ' will become an important north-south public road in future, while Heidelberg Road (K154) and Road K91 are expected to become even more popular public transport routes in the future.

It can therefore be concluded that the subject site will be well located with respect to the availability of public transport facilities and -services in future.

### 7.2 PROPOSED FACILITIES

In order to make provision for the users of public transport that will be generated by the proposed development, the following facilities are proposed:

1. Public Transport Laybys: Since a notable number of residents and employees associated with the proposed development (e.g. domestic workers and maintenance personnel) are expected to make use of public transport services, it is suggested that public transport laybys be constructed at the following locations:

- Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street Intersection: A set of Gautrans standard bus laybys along Heidelberg Road, upstream and downstream of the intersection, as per Drawing No. 0573/CL/04a \& 04b
- Heidelberg Road (R550/K154) / Yellow Jack Street Intersection: A set of Gautrans standard bus laybys along Heidelberg Road, upstream and downstream of the intersection, as per Drawing No. 0573/CL/05a \& 05b

In addition, public transport laybys are also proposed at the following locations inside the subject township development:

- 'Road A' / 'Road B' Intersection: A set of laybys along 'Road A', upstream and downstream of the intersection, as per Drawing No. 0573/CL/06
- 'Road $\mathrm{A}^{\prime} /$ 'Road $\mathrm{C}^{\prime}$ Intersection: A set of laybys along 'Road $\mathrm{A}^{\prime}$, upstream and downstream of the intersection, as per Drawing No. 0573/CL/06
- 'Road A' / 'Road D' Intersection: A set of laybys along 'Road A', upstream and downstream of the intersection, as per Drawing No. 0573/CL/06

The final location of these laybys can be discussed with Midvaal Local Municipality at design stage.
2. Paved Sidewalks: In order to ease and formalize the movement of pedestrians to and from the subject township, it is proposed to construct paved pedestrian sidewalks of at least 1.8 m wide along both sides of 'Road A', as indicated in Drawing No. 0573/CL/06.
More details of the above would be submitted as part of the final Site Development Plans (where relevant) and/or detail designs of the external road and intersection upgrades.

## 8. Summary, Conclusions \& Recommendations

Based on the content of this document, the following key conclusions and recommendations are relevant:

1. This Traffic Impact Assessment (TIA) has been undertaken as part of the township application for a proposed new mixed land-use development, which is to be situated on Portion 8 of the Farm Rietspruit 152-IR. The proposed new township will be known as Rietspruit. The site location is shown in Figure 1 and Figure 2 and falls under the jurisdiction of Midvaal Local Municipality.
2. The subject site, as a whole, is approximately 163 ha in extent. With reference to the Town Planner's proposed Township Layout Plan in Annexure A, Rietspruit will be a mixed land-use development and will comprise a total of 3,782 single residential erven (zoned 'Residential $1^{\prime}$ ). Provision is also made for 'Institutional' land uses in the form of two new public primary schools and one new public secondary school, given the large extent of the residential component. Without the necessary details with regards to the sizes of the proposed schools at this stage, it was assumed in this study that the proposed public primary schools would each have a capacity of 800 students (thus 1,600 students in total), while the proposed public secondary school would have a capacity of 1,200 students. The proposed township layout also makes provision for erven with 'Community Facility' and 'Utilities' zonings, as well as ample public open spaces/ parks.
3. It can be noted that the subject site is bordered by the Watervalspruit Townships (also known as Sky City) to the north-west, which has the same developer as the proposed development. Similar to these neighbouring Watervalspruit Townships, the proposed development is expected to mostly cater for lower income households and it is anticipated that a similar housing product will be developed, with erf sizes ranging between $155 \mathrm{~m}^{2}$ and $202 \mathrm{~m}^{2}$. The proposed development is not planned to be security controlled at this stage. These houses on the single residential stands are typically known as "charter housing", which is the lowest level where households qualify for a home loan.
4. PROPOSED SITE ACCESS INTERSECTIONS: Given the lack of proper (formal/ paved) roads in the study area, it is proposed that the subject township gain access via the future internal road network of the neighbouring Watervalspruit Townships, which border the subject site to the north-west. Access to these townships, and therefore the subject townships, will be provided via two (2) new access intersections with Heidelberg Road (R550/ future K154), as indicated in attached Figure 2. The positions of the proposed site access intersections are also reflected on the proposed local road master plan in Figure 4, which has been accepted by Midvaal Local Municipality in principle. The proposed access roads that will intersect with Heidelberg Road will be known as Silver Dory Street and Yellow Jack Street, respectively. The main north-south collector and distributor road through the subject township, which will essentially be the future extension of Yellow Jack Street, is referred to as 'Road $A^{\prime}$ for now in this TIA.

It is confirmed that the locations of the proposed two site access intersections with Heidelberg Road, as mentioned above, are in line with the location on Gautrans' latest preliminary design of the future K154, past the site, which has been accepted by the MEC of GPDRT. The proposed Township Layout Plan for the neighbouring Watervalspruit Townships has taken full cognisance of the road reserve of the future K154, including the necessary splays for these proposed site access intersections. However, it must be noted that the internal layout of the neighbouring Watervalspruit Townships to the south of Heidelberg Road (i.e. bordering the subject site) is not fixed yet and will be adjusted to accommodate the proposed internal road network of the subject township, as indicated in Annexure A.
5. INTERNAL TOWNSHIP LAYOUT \& ROAD NETWORK: Given the fairly large extent of the subject township, this study focusses on access provision at a township level, instead of at a micro level for individual erven. As can be noted from Annexure A, a complete new network of local Class 3, 4 and 5 public roads and access streets are proposed as part of the township development, in order to provide vehicular access to all individual stands.

It is confirmed that, from a traffic engineering point of view, inputs have already been provided with regards to the proposed township layout in Annexure A. It is therefore confirmed that the proposed internal road network of the subject townships is supported in this TIA. Where necessary or requested, continued input will be provided to the township layout. To that is that the proposed township is not planned to be security controlled upon completion and therefore stacking distance requirements become less relevant at this stage. It can be noted, however, that the proposed township layout makes provision for the implementation of security control in future, if required.
6. DEVELOPMENT TRIP GENERATION: It is estimated that the proposed development of Rietspruit, as a whole, will generate a total of approximately $\mathbf{1 , 4 7 8}$ and $\mathbf{1 , 3 5 2}$ new trips (total IN plus OUT) during the weekday AM and PM peak hours, respectively.
It is confirmed that the theoretical trip generations of the neighbouring Watervalspruit Townships (based on the trip rates applied in the approved TIA) had been compared with the actual trip generations (based on the recent traffic counts), given the existing overall development extent, which had been confirmed by the client/ developer. It was found that, overall, the theoretical and actual trip generations are very similar and given that a slightly more conservative residential trip rate had been applied in this TIA, the estimation of the total trips that will be generated by the subject township, as a whole, is viewed as representative/ adequate.
7. PROPOSED ROAD \& INTERSECTION UPGRADES: Based on the estimated additional traffic generations of the proposed development (as a whole) and the projected trip distribution onto the surrounding road network during the weekday AM and PM peak hours, the impact of other nearby developments (i.e. latent rights), the capacity analyses as well as on-site observations during the peaks, the road/ intersection upgrades as discussed further below are proposed. Important to note is that all of the required upgrades at the external key intersections have been split into two (2) phases. The first phase of upgrades will be required as part of the complete development of the neighbouring Watervalspruit Townships. The second phase of upgrades will be required as part of the development of the proposed Rietspruit Township, which is only expected to happen after the neighbouring Watervalspruit Townships have been completed. The external intersection upgrades required as part of the Watervalspruit Ext. 54 Township have also been taken into account.

It must further be mentioned that the Heidelberg Road (R550 / K154) and K91 intersection is due for the upgrades shown separately in Drawing No. 0573/CL/01a. These upgrades have been approved by the relevant road authorities and a Wayleave is already in place for construction to commence in due course. Therefore, the proposed first and second phase upgrades (as mentioned above) are taken as additional upgrades to these upgrades that will be implemented in the near future. All of the proposed upgrades on Heidelberg Road (future K154) and the K91 are to be implemented to Gautrans' minimum design standards.

PHASE 1 UPGRADES: Required as part of the neighbouring Watervalspruit Townships
\# Heidelberg Road (R550/ K154) / K91 [Intersection 5]:
Refer to Drawing No. 0573/CL/01b

- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road;
- Additional short right turning lane to be added on the northern approach of the K91;
- The short, shared through and left turning slip lane on the northern approach of the K91 (as per Drawing No. 0573/CL/01a) to be upgraded to a short through lane with a separate short left turning slip lane; and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/ K154) / Kingfish Street / Garthview Street [Intersection 12]:


## Refer to Drawing No. 0573/CL/02a

- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road;
- Existing shared through and right turning lane on the Kingfish Street approach to be converted to a dedicated right turning lane;
- Additional short right turning lane to be added on the Kingfish Street approach;
- Existing short left turning lane on the Kingfish Street approach to be extended and upgraded to a short, shared through and left turning slip lane;
- Additional short right turning lane to be added on the Garthview Street approach, with the existing approach lane to be converted to a shared through and left turning lane only; and
- Updated signal layout and signal timing plans.


## \# K91 / Cosmopolitan Drive [Intersection 13]:

## Refer to Drawing No. 0573/CL/03a

- Additional through lane to be added on the south-western approach of the K91;
- Additional receiving lane to be added on the north-eastern leg of the K91;
- Additional short right turning lane to be added on the north-eastern approach of the K91;
- Additional short receiving lane to be added on the north-western leg of Cosmopolitan Drive;
- Existing left turning slip lane (with yield control) on the north-western approach of Cosmopolitan Drive to be upgraded to a continuous slip lane with a short receiving lane on the K91 (north-eastern leg); and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street [Intersection 14]:


## Refer to Drawing No. 0573/CL/04a

- Proposed new 4-legged intersection with separate short right turning and left turning slip lanes on all 4 approaches; and
- Signalization of the intersection, when warranted.
\# Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15]:


## Refer to Drawing No. 0573/CL/05a

- Proposed new T-intersection with separate turning lanes on the eastern and western approaches of Heidelberg Road;
- Southern approach of Yellow Jack Street to comprise a dedicated left turning slip lane and a short right turning lane; and
- Signalization of the intersection, when warranted.

PHASE 2 UPGRADES: Required as part of the proposed Rietspruit Township)

## \# Heidelberg Road (R550/ K154) / K91 [Intersection 5]:

## Refer to Drawing No. 0573/CL/01c

- Additional through lane to be added on the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road;
- Additional short right turning lane to be added on the eastern approach of Heidelberg Road and the existing short right turning lane to be extended;
- Additional receiving lane to be added on the northern leg of the K91; and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/ K154) / Kingfish Street / Garthview Street [Intersection 12]:


## Refer to Drawing No. 0573/CL/02b

- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road; and
- Updated signal layout and signal timing plans.
\# K91 / Cosmopolitan Drive [Intersection 13]:


## Refer to Drawing No. 0573/CL/03b

- Additional through lane to be added on the north-eastern approach of the K91;
- Additional receiving lane to be added on the south-western leg of the K91; and
- Updated traffic signal layout and signal timing plans.
\# Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street
[Intersection 14]:


## Refer to Drawing No. 0573/CL/04b

- Additional through lane to be added on both the eastern and western approaches of Heidelberg Road;
- Additional receiving lane to be added on the eastern and western legs of Heidelberg Road; and
- Updated signal layout and signal timing plans.
\# Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15]:


## Refer to Drawing No. 0573/CL/05b

- Additional short right turning lane to be added on the western approach of Heidelberg Road;
- Additional short receiving lane on Yellow Jack Street;
- Additional short through lane to be added on the eastern approach of Heidelberg Road;
- Additional receiving lane on the western leg of Heidelberg Road; and
- Updated signal layout and signal timing plans.

INTERNAL ROAD \& INTERSECTION UPGRADES: All of the proposed upgrades outlined below are required as part of the proposed Rietspruit Township and are shown in attached Drawing No. 0573/CL/06.
\# 'Road A' (Extension of Yellow Jack Street):

- New Class 3 public road of approximately 2150 m (2.15km) in length.
\#
'Road A' / 'Road B' Intersection:
- Proposed new traffic circle (approximately 18 m inscribed diameter) with a single circulating lane and painted splitter islands.
\# 'Road A' / 'Road C' Intersection:
- Proposed new traffic circle (approximately 20 m inscribed diameter) with a single circulating lane and painted splitter islands.
\# 'Road A' / 'Road D' Intersection:
- Proposed new traffic circle (approximately 18 m inscribed diameter) with a single circulating lane and painted splitter islands.


## \# <br> 'Road A' / 'Road E' Intersection: <br> - Proposed new 4-legged priority stop controlled intersection.

8. In the event of bulk engineering contributions payable with respect to roads and stormwater, it is recommended that at least part of the contribution be off-set against the proposed road and intersection upgrades, as outlined above, since the upgrades will also benefit other future developments and the relevant road authorities. It is acknowledged that the off-setting of costs against provincial roads could be a problem in terms of the legislation, but it is recommended that the CoE, Midvaal Local Municipality and Gautrans come to some agreement in this respect.
9. NON-MOTORISED \& PUBLIC TRANSPORT: Heidelberg Road (R550/K154) and Road K91, which are both located in close proximity to the subject site, are known to be very popular public transport routes for minibus-taxis and buses. Cosmopolitan Drive and Kingfish Street, which had been constructed as part of the neighbouring Watervalspruit Townships, have also become popular public transport routes in recent years. Given the undeveloped status of the subject site and surrounding properties, the site itself is not currently served by public transport services, nor is there any proper public transport facilities in place (such as walkway and laybys). However, the implementation of the proposed new public roads will connect the subject site to such services and facilities and it is expected that the proposed development, together with other developments in the area, will further stimulate the demand for public transport services as they develop over time and it is expected that particularly minibus taxis would respond to this demand by providing more services. It is also expected that 'Road $A^{\prime}$ will become an important north-south public road in future, while Heidelberg Road (K154) and Road K91 are expected to become even more popular public transport routes in the future. It can therefore be concluded that the subject site will be well located with respect to the availability of public transport facilities and -services in future.
10. In order to make provision for the users of public transport that will be generated by the proposed development, the following facilities are proposed:
\# Public Transport Laybys: Since a notable number of residents and employees associated with the proposed development are expected to make use of public transport services, it is suggested that public transport laybys be constructed at the following locations:

- Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street Intersection: A set of Gautrans standard bus laybys along Heidelberg Road, upstream and downstream of the intersection, as per Drawing No. 0573/CL/04a \& 04b
- Heidelberg Road (R550/K154) / Yellow Jack Street Intersection: A set of Gautrans standard bus laybys along Heidelberg Road, upstream and downstream of the intersection, as per Drawing No. 0573/CL/05a \& 05b
In addition, public transport laybys are also proposed at the following locations inside the subject township development:
- 'Road A' / 'Road B' Intersection: A set of laybys along 'Road A', upstream and downstream of the intersection, as per Drawing No. 0573/CL/06
- 'Road A' / 'Road C' Intersection: A set of laybys along 'Road A', upstream and downstream of the intersection, as per Drawing No. 0573/CL/06
- 'Road A' / 'Road D' Intersection: A set of laybys along 'Road A', upstream and downstream of the intersection, as per Drawing No. 0573/CL/06
The final location of these laybys can be discussed with Midvaal Local Municipality at design stage.
\# Paved Sidewalks: In order to ease and formalize the movement of pedestrians to and from the subject township, it is proposed to construct paved pedestrian sidewalks of at least 1.8 m wide along both sides of 'Road A', as per Drawing No. 0573/CL/06.
More details of the above would be submitted as part of the final Site Development Plans (where relevant) and/or detail designs of the external road and intersection upgrades.

From a traffic engineering perspective, the proposed new mixed land-use township known as Rietspruit is supported, provided that the proposed site access intersections and internal roads, external roadand intersection upgrades and public transport- and non-motorized facilities as proposed in this TIA are implemented to the relevant design standards of the Midvaal Local Municipality, the City of Ekurhuleni (COE) and Gautrans.

## Figures

Figure 1 Locality Plan
Figure 2 Site Aerial View \& Key Plan
Figure 3 Extract of Gautrans' Strategic Major Road Network (2007)
Figure 4 Proposed Local Road Master Planning
Figure 5 Existing 2021 Peak Hour Traffic Volumes
Figure 6a Latent Rights: Palm Ridge Ext. 10, 12 \& 13 Trips
Figure 6b Latent Rights: Watervalspruit Townships - Service Plan Stage 1 Remaining Trips

Figure 6c Latent Rights: Watervalspruit Townships - Service Plan Stage 2 Remaining Trips
Figure 6d Latent Rights: Watervalspruit Townships - Service Plan Stage 3 Trips
Figure 6 e Latent Rights: Watervalspruit Ext. 54 Trips
Figure 7 Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Service Plan Stage 3 Trips
Figure 8 Future 2031 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Service Plan Stage 3 Trips + Watervalspruit Ext. 54 Trips

Figure 9a Expected Trip Distribution: Residential
Figure 9b Expected Trip Distribution: Educational
Figure 10a Estimated Development Trips: Residential
Figure 10b Estimated Development Trips: Educational
Figure 11 Estimated Total Development Trips
Figure 12 Future 2031 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Service Plan Stage 3 Trips + Watervalspruit Ext. 54 Trips + Estimated Total Development Trips


| Project Name | Proposed Township: Rietspruit | Proj Ref. <br> P0573 |
| :--- | :---: | :--- |
| Description | Pocality Plan | Figure |
|  |  | $\mathbf{1}$ |




## Proposed Township: Rietspruit

P0573



| Froset tane | Proposed Township: Rietspruit | ${ }^{\text {Pop Refef }}$ P0573 |
| :---: | :---: | :---: |
| Spion | Existing 2021 Peak Hour Traffic Volumes | 5 |






Project Name $\quad$ Proposed Township: Rietspruit



| Proposed Township: Reitspruit | P0573 |
| :---: | :---: |
| Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Service Plan Stage 3 Trips | 7 |



| Project Name | Proposed Township: Rietspruit | ${ }^{\text {Proj Ref. }}$ P0573 |
| :---: | :---: | :---: |
| Description | Future 2031 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips <br> + Watervalspruit Service Plan Stage 3 Trips + Watervalspruit Ext. 54 Trips | ${ }^{\text {Figue }} 8$ |


$\square$
Project Name $\quad$ Proposed Township: Rietspruit


Projet Name $\quad$ Proposed Township: Rietspruit

dhubecon $\square$

| Project Name |
| :--- |
| Descinion |


| Estimated Development Trips: Residential |
| :---: | :---: |



| Project Name | Proposed Township: Rietspruit |
| :--- | :--- |
| Descrition |  |


| Doscrivion | Proposed Township: Rietspruit |
| :---: | :---: |
|  | Estimated Development Trips: Educational |

$\square$

$\square$ Project Name $\quad$ Proposed Township: Rietspruit
 + Watervalspruit Service Plan Stage 3 Trips + Watervalspruit Ext. 54 Trips + Estimated Total Development Trips

## Drawings

Drawing No. 0573/CL/01a
Drawing No. 0573/CL/01b
Drawing No. 0573/CL/01c
Drawing No. 0573/CL/02a

Drawing No. 0573/CL/02b

Drawing No. 0573/CL/03a

Drawing No. 0573/CL/03b

Drawing No. 0573/CL/04a

Drawing No. 0573/CL/04b

Drawing No. 0573/CL/05a

Drawing No. 0573/CL/05b

Drawing No. 0573/CL/06

Approved Intersection Upgrade: Heidelberg Road (R550/K154) / K91 [Intersection 5]

Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / K91 [Intersection 5]: PHASE 1

Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / K91 [Intersection 5]: PHASE 2

Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / Kingfish Street / Garthview Street [Intersection 12]: PHASE 1

Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / Kingfish Street / Garthview Street [Intersection 12]: PHASE 2

Proposed Intersection Upgrade: K91 / Cosmopolitan Drive [Intersection 13]: PHASE 1

Proposed Intersection Upgrade: K91 / Cosmopolitan Drive [Intersection 13]: PHASE 2

Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street [Intersection 14]: PHASE 1

Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street [Intersection 14]: PHASE 2

Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15]: PHASE 1
Proposed Intersection Upgrade: Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15]: PHASE 2

Proposed Internal Road Network Layout













## Annexures

| Annexure A | Town Planner's Proposed Township Layout Plan |
| :--- | :--- |
| Annexure B | Relevant Outputs of the SIDRA Intersection 9 Capacity <br> Analyses |

## Annexure A

Town Planner's Proposed Township Layout Plan


## Annexure B

## Relevant Outputs of the SIDRA Intersection 9 Capacity Analyses:

B1 Heidelberg Road (R550/K154) \& K91 [Intersection 5]
B2 Heidelberg Road (R550/K154) / Kingfish Street / Garthview Street [Intersection 12]

B3 K91 / Cosmopolitan Drive [Intersection 13]
B4 Heidelberg Road (R550/K154) / Silver Dory Street / Salamanderfish Street [Intersection 14]

B5 Heidelberg Road (R550/K154) / Yellow Jack Street [Intersection 15]

ANNEXURE B1: SITE LAYOUT

## Existing Intersection Geometry

New Site
Site Category: (None)
Stop (Two-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## ANNEXURE B1.1: MOVEMENT SUMMARY

## (10) Site: [Scenario 1 AM (Site <br> Folder: Existing Intersection Geometry)]

New Site
Site Category: (None)
Stop (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { WND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service | $\begin{gathered} \text { 95\% BA } \\ \text { QUE } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 21 | 0.0 | 22 | 0.0 | 0.036 | 9.6 | LOS A | 0.1 | 0.9 | 0.42 | 0.88 | 0.42 | 50.6 |
| 2 T1 | 2 | 0.0 | 2 | 0.0 | 0.036 | 15.6 | LOS C | 0.1 | 0.9 | 0.42 | 0.88 | 0.42 | 50.6 |
| 3 R2 | 1 | 0.0 | 1 | 0.0 | 0.036 | 20.0 | LOS C | 0.1 | 0.9 | 0.42 | 0.88 | 0.42 | 50.7 |
| Approach | 24 | 0.0 | 25 | 0.0 | 0.036 | 10.5 | LOS B | 0.1 | 0.9 | 0.42 | 0.88 | 0.42 | 50.6 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 7 | 0.0 | 7 | 0.0 | 0.004 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.6 |
| 5 T1 | 287 | 0.0 | 302 | 0.0 | 0.147 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 6 R2 | 38 | 0.0 | 40 | 0.0 | 0.027 | 6.0 | LOSA | 0.1 | 0.8 | 0.30 | 0.56 | 0.30 | 52.4 |
| Approach | 332 | 0.0 | 349 | 0.0 | 0.147 | 0.8 | NA | 0.1 | 0.8 | 0.03 | 0.08 | 0.03 | 58.8 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 78 | 0.0 | 82 | 0.0 | 1.214 | 205.4 | LOS F | 73.3 | 513.1 | 1.00 | 4.45 | 12.67 | 13.8 |
| 8 T1 | 23 | 0.0 | 24 | 0.0 | 1.214 | 241.4 | LOS F | 73.3 | 513.1 | 1.00 | 4.45 | 12.67 | 13.8 |
| 9 R2 | 472 | 0.0 | 497 | 0.0 | 1.214 | 201.6 | LOS F | 73.3 | 513.1 | 1.00 | 4.45 | 12.67 | 13.8 |
| Approach | 573 | 0.0 | 603 | 0.0 | 1.214 | 203.7 | LOS F | 73.3 | 513.1 | 1.00 | 4.45 | 12.67 | 13.8 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 162 | 0.0 | 171 | 0.0 | 0.108 | 5.7 | LOS A | 0.5 | 3.2 | 0.12 | 0.52 | 0.12 | 53.9 |
| 11 T1 | 189 | 0.0 | 199 | 0.0 | 0.096 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 60.0 |
| 12 R2 | 5 | 0.0 | 5 | 0.0 | 0.005 | 6.7 | LOSA | 0.0 | 0.1 | 0.37 | 0.57 | 0.37 | 52.2 |
| Approach | 356 | 0.0 | 375 | 0.0 | 0.108 | 2.7 | LOS A | 0.5 | 3.2 | 0.06 | 0.24 | 0.06 | 56.9 |
| All <br> Vehicles | 1285 | 0.0 | 1353 | 0.0 | 1.214 | 92.0 | NA | 73.3 | 513.1 | 0.48 | 2.09 | 5.68 | 23.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Minor Road Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## ANNEXURE B1.2: MOVEMENT SUMMARY

## (4i0) Site: [Scenario 1 PM (Site <br> Folder: Existing Intersection Geometry)]

New Site
Site Category: (None)
Stop (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { JT } \\ \text { UES } \\ \text { HV ] } \\ \% \end{gathered}$ | $\begin{aligned} & \text { DEM } \\ & \text { FLOO } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service |  | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 12 | 0.0 | 13 | 0.0 | 0.120 | 8.9 | LOSA | 0.4 | 2.9 | 0.56 | 0.93 | 0.56 | 46.3 |
| 2 T1 | 19 | 0.0 | 20 | 0.0 | 0.120 | 19.9 | LOS C | 0.4 | 2.9 | 0.56 | 0.93 | 0.56 | 46.4 |
| 3 R2 | 6 | 0.0 | 6 | 0.0 | 0.120 | 26.7 | LOS D | 0.4 | 2.9 | 0.56 | 0.93 | 0.56 | 46.5 |
| Approach | 37 | 0.0 | 39 | 0.0 | 0.120 | 17.4 | LOS C | 0.4 | 2.9 | 0.56 | 0.93 | 0.56 | 46.4 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 2 | 0.0 | 2 | 0.0 | 0.001 | 5.5 | LOSA | 0.0 | 0.0 | 0.00 | 0.58 | 0.00 | 53.6 |
| 5 T1 | 174 | 0.0 | 183 | 0.0 | 0.089 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 60.0 |
| 6 R2 | 106 | 0.0 | 112 | 0.0 | 0.089 | 6.8 | LOSA | 0.4 | 2.7 | 0.44 | 0.64 | 0.44 | 52.0 |
| Approach | 282 | 0.0 | 297 | 0.0 | 0.089 | 2.6 | NA | 0.4 | 2.7 | 0.16 | 0.25 | 0.16 | 56.6 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 69 | 0.0 | 73 | 0.0 | 1.292 | 291.8 | LOS F | 47.3 | 331.1 | 1.00 | 3.83 | 11.00 | 9.9 |
| 8 T1 | 25 | 0.0 | 26 | 0.0 | 1.292 | 311.5 | LOS F | 47.3 | 331.1 | 1.00 | 3.83 | 11.00 | 9.9 |
| 9 R2 | 169 | 0.0 | 178 | 0.0 | 1.292 | 309.8 | LOS F | 47.3 | 331.1 | 1.00 | 3.83 | 11.00 | 9.9 |
| Approach | 263 | 0.0 | 277 | 0.0 | 1.292 | 305.3 | LOS F | 47.3 | 331.1 | 1.00 | 3.83 | 11.00 | 9.9 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 417 | 0.0 | 439 | 0.0 | 0.300 | 6.1 | LOS A | 1.5 | 10.6 | 0.28 | 0.55 | 0.28 | 53.3 |
| 11 T1 | 353 | 0.0 | 372 | 0.0 | 0.180 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 59.9 |
| 12 R 2 | 33 | 0.0 | 35 | 0.0 | 0.029 | 6.2 | LOSA | 0.1 | 0.8 | 0.29 | 0.57 | 0.29 | 52.4 |
| Approach | 803 | 0.0 | 845 | 0.0 | 0.300 | 3.5 | LOS A | 1.5 | 10.6 | 0.16 | 0.31 | 0.16 | 56.0 |
| All <br> Vehicles | 1385 | 0.0 | 1458 | 0.0 | 1.292 | 61.0 | NA | 47.3 | 331.1 | 0.33 | 0.98 | 2.23 | 29.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Minor Road Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## ANNEXURE B1: SITE LAYOUT <br> Upgraded Intersection Geometry (Approved \& to be Constructed in Due Course)

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated
Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## ANNEXURE B1.3: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: <br> Upgraded Intersection Geometry (Approved \& to be <br> Constructed in Due Course))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 85 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | UT MES HV ] \% |  | ND VS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | CK OF UE Dist $]$ m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 29 | 0.0 | 29 | 0.0 | 0.149 | 24.8 | LOS C | 0.9 | 6.0 | 0.92 | 0.70 | 0.92 | 43.0 |
| 2 T1 | 10 | 0.0 | 10 | 0.0 | 0.149 | 19.2 | LOS B | 0.9 | 6.0 | 0.92 | 0.70 | 0.92 | 43.4 |
| 3 R2 | 8 | 0.0 | 8 | 0.0 | 0.013 | 22.5 | LOS C | 0.2 | 1.4 | 0.63 | 0.65 | 0.63 | 43.1 |
| Approach | 47 | 0.0 | 47 | 0.0 | 0.149 | 23.2 | LOS C | 0.9 | 6.0 | 0.87 | 0.69 | 0.87 | 43.1 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 27 | 0.0 | 27 | 0.0 | 0.029 | 19.4 | LOS B | 0.6 | 4.3 | 0.58 | 0.67 | 0.58 | 44.5 |
| 5 T1 | 913 | 0.0 | 913 | 0.0 | 0.951 | 48.6 | LOS D | 51.0 | 357.2 | 1.00 | 1.21 | 1.38 | 33.3 |
| 6 R2 | 610 | 0.0 | 610 | 0.0 | *1.295 | 303.5 | LOS F | 80.2 | 561.5 | 1.00 | 1.88 | 3.68 | 9.4 |
| Approach | 1550 | 0.0 | 1550 | 0.0 | 1.295 | 148.4 | LOS F | 80.2 | 561.5 | 0.99 | 1.46 | 2.27 | 16.7 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 375 | 0.0 | 375 | 0.0 | 0.346 | 9.2 | LOSA | 5.2 | 36.5 | 0.39 | 0.63 | 0.39 | 51.8 |
| 8 T1 | 39 | 0.0 | 39 | 0.0 | 0.346 | 3.6 | LOSA | 5.2 | 36.5 | 0.39 | 0.63 | 0.39 | 52.5 |
| 9 R2 | 877 | 0.0 | 877 | 0.0 | *1.123 | 167.6 | LOS F | 89.1 | 623.7 | 1.00 | 1.55 | 2.52 | 15.7 |
| Approach | 1291 | 0.0 | 1291 | 0.0 | 1.123 | 116.6 | LOS F | 89.1 | 623.7 | 0.80 | 1.25 | 1.83 | 20.2 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 346 | 0.0 | 346 | 0.0 | 0.253 | 9.8 | LOS A | 4.4 | 31.1 | 0.45 | 0.69 | 0.45 | 51.1 |
| 11 T1 | 538 | 0.0 | 538 | 0.0 | * 1.111 | 153.8 | LOS F | 51.1 | 357.8 | 1.00 | 1.84 | 2.50 | 16.7 |
| 12 R 2 | 22 | 0.0 | 22 | 0.0 | 0.199 | 50.5 | LOS D | 0.9 | 6.6 | 0.99 | 0.69 | 0.99 | 32.2 |
| Approach | 906 | 0.0 | 906 | 0.0 | 1.111 | 96.3 | LOS F | 51.1 | 357.8 | 0.79 | 1.37 | 1.68 | 22.9 |
| All <br> Vehicles | 3794 | 0.0 | 3794 | 0.0 | 1.295 | 123.6 | LOS F | 89.1 | 623.7 | 0.88 | 1.36 | 1.96 | 19.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.3: PHASING SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder:

Upgraded Intersection Geometry (Approved \& to be
Constructed in Due Course))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 85 seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase A
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

## Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 23 | 63 |
| Green Time (sec) | 19 | 33 | 15 |
| Phase Time (sec) | 26 | 40 | 19 |
| Phase Split | $31 \%$ | $47 \%$ | $22 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.

Output Phase Sequence


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

## ANNEXURE B1.4: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: <br> Upgraded Intersection Geometry (Approved \& to be <br> Constructed in Due Course))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 105 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { vOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | MES HV ] \% |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \hline \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay sec | Level of Service | $\begin{gathered} 95 \% \text { E } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \end{aligned}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \end{aligned}$ | Aver. Speed km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 30 | 0.0 | 30 | 0.0 | 0.250 | 33.1 | LOS C | 2.4 | 17.0 | 0.89 | 0.71 | 0.89 | 39.9 |
| 2 T 1 | 38 | 0.0 | 38 | 0.0 | 0.250 | 27.5 | LOS C | 2.4 | 17.0 | 0.89 | 0.71 | 0.89 | 40.3 |
| 3 R2 | 24 | 0.0 | 24 | 0.0 | 0.067 | 41.5 | LOS D | 1.0 | 6.9 | 0.83 | 0.70 | 0.83 | 35.2 |
| Approach | 92 | 0.0 | 92 | 0.0 | 0.250 | 33.0 | LOS C | 2.4 | 17.0 | 0.88 | 0.71 | 0.88 | 38.7 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 10 | 0.0 | 10 | 0.0 | 0.007 | 12.3 | LOS B | 0.2 | 1.2 | 0.37 | 0.62 | 0.37 | 48.8 |
| 5 T1 | 520 | 0.0 | 520 | 0.0 | 0.370 | 9.0 | LOS A | 12.1 | 84.6 | 0.50 | 0.44 | 0.50 | 52.2 |
| 6 R2 | 391 | 0.0 | 391 | 0.0 | * 1.024 | 88.5 | LOS F | 23.5 | 164.6 | 1.00 | 1.17 | 1.83 | 20.7 |
| Approach | 921 | 0.0 | 921 | 0.0 | 1.024 | 42.8 | LOS D | 23.5 | 164.6 | 0.71 | 0.75 | 1.06 | 31.7 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 563 | 0.0 | 563 | 0.0 | 0.742 | 28.8 | LOS C | 18.6 | 130.4 | 0.86 | 0.97 | 0.86 | 40.6 |
| 8 T1 | 38 | 0.0 | 38 | 0.0 | 0.742 | 23.2 | LOS C | 18.6 | 130.4 | 0.86 | 0.97 | 0.86 | 41.0 |
| 9 R2 | 399 | 0.0 | 399 | 0.0 | * 0.974 | 83.1 | LOS F | 28.3 | 198.0 | 1.00 | 1.10 | 1.57 | 25.1 |
| Approach | 1000 | 0.0 | 1000 | 0.0 | 0.974 | 50.2 | LOS D | 28.3 | 198.0 | 0.92 | 1.02 | 1.15 | 32.7 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 825 | 0.0 | 825 | 0.0 | 0.598 | 11.3 | LOS B | 15.3 | 107.2 | 0.60 | 0.76 | 0.60 | 50.1 |
| 11 T1 | 937 | 0.0 | 937 | 0.0 | * 0.962 | 56.2 | LOS E | 61.9 | 433.0 | 1.00 | 1.18 | 1.33 | 31.2 |
| 12 R 2 | 44 | 0.0 | 44 | 0.0 | 0.094 | 21.8 | LOS C | 1.2 | 8.7 | 0.58 | 0.70 | 0.58 | 43.2 |
| Approach | 1806 | 0.0 | 1806 | 0.0 | 0.962 | 34.9 | LOS C | 61.9 | 433.0 | 0.81 | 0.98 | 0.98 | 38.0 |
| All <br> Vehicles | 3819 | 0.0 | 3819 | 0.0 | 1.024 | 40.8 | LOS D | 61.9 | 433.0 | 0.81 | 0.93 | 1.04 | 34.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.4: PHASING SUMMARY

## 自 Site: [Scenario 2 PM (Site Folder:

Upgraded Intersection Geometry (Approved \& to be
Constructed in Due Course))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase A
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

## Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 54 | 84 |
| Green Time (sec) | 50 | 23 | 14 |
| Phase Time (sec) | 57 | 30 | 18 |
| Phase Split | $54 \%$ | $29 \%$ | $17 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.

Output Phase Sequence


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running

## ANNEXURE B1: SITE LAYOUT <br> Upgraded Intersection Geometry (PHASE 1)

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings
1 N


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## ANNEXURE B1.5: MOVEMENT SUMMARY

## 目ite: [Scenario 2 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 95 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT <br> MES <br> HV ] <br> \% | $\begin{array}{r} \text { DEN } \\ \text { FL( } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L 2 | 29 | 0.0 | 29 | 0.0 | 0.093 | 21.3 | LOS C | 0.8 | 5.5 | 0.80 | 0.68 | 0.80 | 44.9 |
| 2 T1 | 10 | 0.0 | 10 | 0.0 | * 0.093 | 15.7 | LOS B | 0.8 | 5.5 | 0.80 | 0.68 | 0.80 | 45.3 |
| 3 R 2 | 8 | 0.0 | 8 | 0.0 | 0.051 | 51.1 | LOS D | 0.4 | 2.5 | 0.95 | 0.66 | 0.95 | 32.4 |
| Approach | 47 | 0.0 | 47 | 0.0 | 0.093 | 25.2 | LOS C | 0.8 | 5.5 | 0.83 | 0.67 | 0.83 | 42.2 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 27 | 0.0 | 27 | 0.0 | 0.018 | 6.3 | LOS A | 0.1 | 0.7 | 0.18 | 0.58 | 0.18 | 53.7 |
| 5 T1 | 913 | 0.0 | 913 | 0.0 | 0.425 | 16.3 | LOS B | 13.4 | 93.7 | 0.69 | 0.60 | 0.69 | 47.4 |
| 6 R2 | 610 | 0.0 | 610 | 0.0 | * 0.871 | 38.3 | LOS D | 26.4 | 184.8 | 1.00 | 0.97 | 1.18 | 36.6 |
| Approach | 1550 | 0.0 | 1550 | 0.0 | 0.871 | 24.8 | LOS C | 26.4 | 184.8 | 0.80 | 0.75 | 0.87 | 42.5 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 375 | 0.0 | 375 | 0.0 | 0.267 | 8.8 | LOS A | 3.8 | 26.6 | 0.30 | 0.64 | 0.30 | 52.5 |
| 8 T1 | 39 | 0.0 | 39 | 0.0 | 0.050 | 21.1 | LOS C | 1.2 | 8.1 | 0.68 | 0.51 | 0.68 | 44.7 |
| 9 R 2 | 877 | 0.0 | 877 | 0.0 | * 0.875 | 52.3 | LOS D | 22.7 | 159.2 | 1.00 | 0.97 | 1.25 | 32.0 |
| Approach | 1291 | 0.0 | 1291 | 0.0 | 0.875 | 38.7 | LOS D | 22.7 | 159.2 | 0.79 | 0.86 | 0.96 | 36.5 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 346 | 0.0 | 346 | 0.0 | 0.382 | 13.1 | LOS B | 5.6 | 39.5 | 0.63 | 0.74 | 0.63 | 48.9 |
| 11 T1 | 538 | 0.0 | 538 | 0.0 | * 0.853 | 46.9 | LOS D | 14.9 | 104.4 | 1.00 | 0.93 | 1.18 | 34.1 |
| 12 R 2 | 22 | 0.0 | 22 | 0.0 | 0.135 | 44.5 | LOS D | 0.9 | 6.5 | 0.89 | 0.72 | 0.89 | 34.2 |
| Approach | 906 | 0.0 | 906 | 0.0 | 0.853 | 34.0 | LOS C | 14.9 | 104.4 | 0.86 | 0.86 | 0.96 | 38.6 |
| All <br> Vehicles | 3794 | 0.0 | 3794 | 0.0 | 0.875 | 31.7 | LOS C | 26.4 | 184.8 | 0.81 | 0.81 | 0.92 | 39.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.5: PHASING SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=95$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 35 | 54 | 84 |
| Green Time (sec) | 28 | 15 | 23 | 7 |
| Phase Time (sec) | 32 | 22 | 27 | 14 |
| Phase Split | $34 \%$ | $23 \%$ | $28 \%$ | $15 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B1.6: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 70 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 30 | 0.0 | 30 | 0.0 | 0.219 | 22.0 | Los C | 1.5 | 10.2 | 0.90 | 0.70 | 0.90 | 45.4 |
| 2 T1 | 38 | 0.0 | 38 | 0.0 | * 0.219 | 16.4 | LOS B | 1.5 | 10.2 | 0.90 | 0.70 | 0.90 | 45.9 |
| 3 R 2 | 24 | 0.0 | 24 | 0.0 | 0.112 | 37.8 | LOS D | 0.8 | 5.5 | 0.94 | 0.70 | 0.94 | 36.7 |
| Approach | 92 | 0.0 | 92 | 0.0 | 0.219 | 23.8 | LOS C | 1.5 | 10.2 | 0.91 | 0.70 | 0.91 | 42.9 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 10 | 0.0 | 10 | 0.0 | 0.007 | 6.5 | LOSA | 0.0 | 0.3 | 0.22 | 0.58 | 0.22 | 53.5 |
| 5 T1 | 520 | 0.0 | 520 | 0.0 | 0.226 | 9.4 | LOS A | 4.7 | 33.0 | 0.57 | 0.48 | 0.57 | 52.0 |
| 6 R2 | 391 | 0.0 | 391 | 0.0 | * 0.745 | 22.0 | LOS C | 8.7 | 60.8 | 0.97 | 0.87 | 1.07 | 43.7 |
| Approach | 921 | 0.0 | 921 | 0.0 | 0.745 | 14.7 | LOS B | 8.7 | 60.8 | 0.74 | 0.65 | 0.78 | 48.1 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 563 | 0.0 | 563 | 0.0 | 0.495 | 16.1 | LOS B | 7.4 | 51.9 | 0.57 | 0.76 | 0.57 | 50.0 |
| 8 T1 | 38 | 0.0 | 38 | 0.0 | 0.064 | 20.4 | LOS C | 1.0 | 6.8 | 0.77 | 0.57 | 0.77 | 45.0 |
| 9 R2 | 399 | 0.0 | 399 | 0.0 | * 0.844 | 45.2 | LOS D | 7.8 | 54.3 | 1.00 | 0.98 | 1.40 | 34.2 |
| Approach | 1000 | 0.0 | 1000 | 0.0 | 0.844 | 27.9 | LOS C | 7.8 | 54.3 | 0.75 | 0.84 | 0.91 | 42.0 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 825 | 0.0 | 825 | 0.0 | 0.643 | 9.6 | LOS A | 10.9 | 76.2 | 0.62 | 0.76 | 0.62 | 51.2 |
| 11 T1 | 937 | 0.0 | 937 | 0.0 | * 0.821 | 29.7 | LOS C | 18.3 | 128.4 | 0.97 | 0.91 | 1.08 | 41.4 |
| 12 R 2 | 44 | 0.0 | 44 | 0.0 | 0.126 | 26.1 | LOS C | 1.1 | 8.0 | 0.77 | 0.72 | 0.77 | 41.2 |
| Approach | 1806 | 0.0 | 1806 | 0.0 | 0.821 | 20.4 | LOS C | 18.3 | 128.4 | 0.81 | 0.84 | 0.86 | 45.3 |
| All <br> Vehicles | 3819 | 0.0 | 3819 | 0.0 | 0.844 | 21.1 | LOS C | 18.3 | 128.4 | 0.78 | 0.79 | 0.85 | 45.0 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.6: PHASING SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=70$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 20 | 44 | 59 |
| Green Time (sec) | 13 | 20 | 8 | 7 |
| Phase Time (sec) | 17 | 27 | 12 | 14 |
| Phase Split | $24 \%$ | $39 \%$ | $17 \%$ | $20 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B1.7: MOVEMENT SUMMARY

## 目ite: [Scenario 3 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=100$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { vOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \hline \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay sec | Level of Service | 95\% B QU [ Veh. veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 31 | 0.0 | 31 | 0.0 | 0.098 | 22.3 | LOS C | 0.9 | 6.2 | 0.81 | 0.68 | 0.81 | 44.3 |
| 2 T1 | 10 | 0.0 | 10 | 0.0 | *0.098 | 16.7 | LOS B | 0.9 | 6.2 | 0.81 | 0.68 | 0.81 | 44.8 |
| 3 R 2 | 8 | 0.0 | 8 | 0.0 | 0.053 | 53.9 | LOS D | 0.4 | 2.6 | 0.96 | 0.66 | 0.96 | 31.6 |
| Approach | 49 | 0.0 | 49 | 0.0 | 0.098 | 26.3 | LOS C | 0.9 | 6.2 | 0.83 | 0.68 | 0.83 | 41.7 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 28 | 0.0 | 28 | 0.0 | 0.019 | 6.4 | LOS A | 0.1 | 0.9 | 0.18 | 0.58 | 0.18 | 53.6 |
| 5 T1 | 973 | 0.0 | 973 | 0.0 | 0.448 | 17.1 | LOS B | 15.1 | 105.7 | 0.69 | 0.61 | 0.69 | 46.9 |
| 6 R2 | 614 | 0.0 | 614 | 0.0 | *0.904 | 46.4 | LOS D | 30.6 | 214.5 | 1.00 | 1.01 | 1.24 | 33.9 |
| Approach | 1615 | 0.0 | 1615 | 0.0 | 0.904 | 28.1 | LOS C | 30.6 | 214.5 | 0.80 | 0.76 | 0.89 | 41.0 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 382 | 0.0 | 382 | 0.0 | 0.276 | 9.7 | LOS A | 4.4 | 30.9 | 0.32 | 0.64 | 0.32 | 52.1 |
| 8 T1 | 41 | 0.0 | 41 | 0.0 | 0.052 | 22.1 | LOS C | 1.3 | 9.0 | 0.68 | 0.51 | 0.68 | 44.1 |
| 9 R2 | 918 | 0.0 | 918 | 0.0 | * 0.887 | 55.4 | LOS E | 25.4 | 177.6 | 1.00 | 0.98 | 1.26 | 31.2 |
| Approach | 1341 | 0.0 | 1341 | 0.0 | 0.887 | 41.4 | LOS D | 25.4 | 177.6 | 0.80 | 0.87 | 0.97 | 35.6 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 361 | 0.0 | 361 | 0.0 | 0.393 | 13.6 | LOS B | 6.4 | 44.9 | 0.63 | 0.75 | 0.63 | 48.6 |
| 11 T1 | 625 | 0.0 | 625 | 0.0 | * 0.921 | 53.9 | LOS D | 20.0 | 139.7 | 1.00 | 1.01 | 1.28 | 32.1 |
| 12 R 2 | 22 | 0.0 | 22 | 0.0 | 0.139 | 45.4 | LOS D | 1.0 | 6.7 | 0.88 | 0.72 | 0.88 | 33.9 |
| Approach | 1008 | 0.0 | 1008 | 0.0 | 0.921 | 39.3 | LOS D | 20.0 | 139.7 | 0.87 | 0.91 | 1.04 | 36.6 |
| All Vehicles | 4013 | 0.0 | 4013 | 0.0 | 0.921 |  | LOS D | 30.6 | 214.5 | 0.82 | 0.83 | 0.95 | 37.9 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.7: PHASING SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=100$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 36 | 57 | 89 |
| Green Time (sec) | 29 | 17 | 25 | 7 |
| Phase Time (sec) | 33 | 24 | 29 | 14 |
| Phase Split | $33 \%$ | $24 \%$ | $29 \%$ | $14 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B1.8: MOVEMENT SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 70 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE <br> [ Veh. Dist] veh <br> m |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 31 | 0.0 | 31 | 0.0 | 0.229 | 21.7 | LOS C | 1.5 | 10.4 | 0.90 | 0.71 | 0.90 | 45.6 |
| 2 T1 | 40 | 0.0 | 40 | 0.0 | * 0.229 | 16.1 | LOS B | 1.5 | 10.4 | 0.90 | 0.71 | 0.90 | 46.1 |
| 3 R2 | 24 | 0.0 | 24 | 0.0 | 0.112 | 37.8 | LOS D | 0.8 | 5.5 | 0.94 | 0.70 | 0.94 | 36.7 |
| Approach | 95 | 0.0 | 95 | 0.0 | 0.229 | 23.4 | LOS C | 1.5 | 10.4 | 0.91 | 0.70 | 0.91 | 43.1 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 10 | 0.0 | 10 | 0.0 | 0.007 | 6.6 | LOS A | 0.0 | 0.3 | 0.24 | 0.58 | 0.24 | 53.4 |
| 5 T1 | 591 | 0.0 | 591 | 0.0 | 0.264 | 10.2 | LOS B | 5.6 | 39.5 | 0.60 | 0.51 | 0.60 | 51.4 |
| 6 R2 | 401 | 0.0 | 401 | 0.0 | * 0.862 | 29.1 | LOS C | 10.9 | 76.4 | 1.00 | 0.98 | 1.31 | 40.3 |
| Approach | 1002 | 0.0 | 1002 | 0.0 | 0.862 | 17.8 | LOS B | 10.9 | 76.4 | 0.76 | 0.70 | 0.88 | 46.3 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 569 | 0.0 | 569 | 0.0 | 0.508 | 18.0 | LOS B | 7.8 | 54.7 | 0.59 | 0.78 | 0.59 | 49.5 |
| 8 T1 | 40 | 0.0 | 40 | 0.0 | 0.064 | 19.6 | LOS B | 1.0 | 7.0 | 0.76 | 0.56 | 0.76 | 45.5 |
| 9 R2 | 414 | 0.0 | 414 | 0.0 | * 0.778 | 41.8 | LOS D | 7.6 | 53.5 | 1.00 | 0.92 | 1.24 | 35.3 |
| Approach | 1023 | 0.0 | 1023 | 0.0 | 0.778 | 27.7 | LOS C | 7.8 | 54.7 | 0.76 | 0.83 | 0.86 | 42.4 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 862 | 0.0 | 862 | 0.0 | 0.649 | 8.9 | LOS A | 9.7 | 67.6 | 0.59 | 0.76 | 0.59 | 51.8 |
| 11 T1 | 995 | 0.0 | 995 | 0.0 | * 0.831 | 29.9 | LOS C | 19.6 | 137.5 | 0.97 | 0.92 | 1.08 | 41.5 |
| 12 R 2 | 47 | 0.0 | 47 | 0.0 | 0.138 | 25.5 | LOS C | 1.2 | 8.5 | 0.76 | 0.72 | 0.76 | 41.6 |
| Approach | 1904 | 0.0 | 1904 | 0.0 | 0.831 | 20.3 | LOS C | 19.6 | 137.5 | 0.79 | 0.84 | 0.85 | 45.6 |
| All <br> Vehicles | 4024 | 0.0 | 4024 | 0.0 | 0.862 | 21.6 | LOS C | 19.6 | 137.5 | 0.78 | 0.80 | 0.86 | 44.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.8: PHASING SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=70$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 18 | 43 | 59 |
| Green Time (sec) | 11 | 21 | 9 | 7 |
| Phase Time (sec) | 15 | 28 | 13 | 14 |
| Phase Split | $21 \%$ | $40 \%$ | $19 \%$ | $20 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B1.9: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 AM (Site <br> Folder: Upgraded Intersection Geometry (PHASE 1))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh <br> veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 31 | 0.0 | 31 | 0.0 | 0.108 | 24.9 | LOS C | 1.0 | 6.8 | 0.83 | 0.69 | 0.83 | 43.0 |
| 2 T1 | 10 | 0.0 | 10 | 0.0 | *0.108 | 19.3 | LOS B | 1.0 | 6.8 | 0.83 | 0.69 | 0.83 | 43.4 |
| 3 R2 | 8 | 0.0 | 8 | 0.0 | 0.059 | 59.4 | LOS E | 0.4 | 2.9 | 0.96 | 0.66 | 0.96 | 30.2 |
| Approach | 49 | 0.0 | 49 | 0.0 | 0.108 | 29.4 | LOS C | 1.0 | 6.8 | 0.85 | 0.68 | 0.85 | 40.3 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 28 | 0.0 | 28 | 0.0 | 0.018 | 6.3 | LOS A | 0.1 | 0.8 | 0.16 | 0.58 | 0.16 | 53.7 |
| 5 T1 | 1374 | 0.0 | 1374 | 0.0 | 0.527 | 13.6 | LOS B | 21.2 | 148.2 | 0.63 | 0.57 | 0.63 | 49.1 |
| 6 R2 | 1063 | 0.0 | 1063 | 0.0 | * 1.409 | 414.8 | LOS F | 184.6 | 1292.3 | 1.00 | 2.01 | 3.54 | 7.4 |
| Approach | 2465 | 0.0 | 2465 | 0.0 | 1.409 | 186.5 | LOS F | 184.6 | 1292.3 | 0.79 | 1.19 | 1.88 | 14.3 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 570 | 0.0 | 570 | 0.0 | 0.416 | 11.3 | LOS B | 6.9 | 48.3 | 0.34 | 0.68 | 0.34 | 51.7 |
| 8 T1 | 41 | 0.0 | 41 | 0.0 | 0.069 | 31.5 | LOS C | 1.6 | 11.3 | 0.77 | 0.58 | 0.77 | 39.7 |
| 9 R2 | 918 | 0.0 | 918 | 0.0 | *1.284 | 316.2 | LOS F | 70.2 | 491.6 | 1.00 | 1.79 | 3.07 | 9.4 |
| Approach | 1529 | 0.0 | 1529 | 0.0 | 1.284 | 194.9 | LOS F | 70.2 | 491.6 | 0.75 | 1.34 | 1.99 | 14.0 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 361 | 0.0 | 361 | 0.0 | 0.394 | 20.1 | LOS C | 10.6 | 74.5 | 0.65 | 0.74 | 0.65 | 44.7 |
| 11 T1 | 765 | 0.0 | 765 | 0.0 | * 1.171 | 155.7 | LOS F | 51.5 | 360.8 | 1.00 | 1.55 | 2.11 | 16.7 |
| 12 R 2 | 22 | 0.0 | 22 | 0.0 | 0.190 | 51.2 | LOS D | 1.1 | 7.6 | 0.90 | 0.73 | 0.90 | 32.1 |
| Approach | 1148 | 0.0 | 1148 | 0.0 | 1.171 | 111.1 | LOS F | 51.5 | 360.8 | 0.89 | 1.28 | 1.63 | 21.1 |
| All Vehicles | 5191 | 0.0 | 5191 | 0.0 | 1.409 | 170.8 | LOS F | 184.6 | 1292.3 | 0.80 | 1.25 | 1.85 | 15.4 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.9: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site <br> Folder: Upgraded Intersection Geometry (PHASE 1))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 51 | 73 | 99 |
| Green Time (sec) | 44 | 18 | 19 | 7 |
| Phase Time (sec) | 48 | 25 | 23 | 14 |
| Phase Split | $44 \%$ | $23 \%$ | $21 \%$ | $13 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.

## Output Phase Sequence



REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B1.10: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: <br> Upgraded Intersection Geometry (PHASE 1))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 90 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|l} \hline \text { Mov Turn } \\ \text { ID } \end{array}$ |  |  |  | ND VS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 31 | 0.0 | 31 | 0.0 | 0.295 | 29.2 | LOS C | 2.1 | 14.6 | 0.94 | 0.73 | 0.94 | 41.7 |
| 2 T1 | 40 | 0.0 | 40 | 0.0 | * 0.295 | 23.6 | LOS C | 2.1 | 14.6 | 0.94 | 0.73 | 0.94 | 42.1 |
| 3 R2 | 24 | 0.0 | 24 | 0.0 | 0.144 | 49.1 | LOS D | 1.0 | 7.2 | 0.96 | 0.70 | 0.96 | 33.0 |
| Approach | 95 | 0.0 | 95 | 0.0 | 0.295 | 31.9 | LOS C | 2.1 | 14.6 | 0.95 | 0.72 | 0.95 | 39.3 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 10 | 0.0 | 10 | 0.0 | 0.007 | 6.6 | LOS A | 0.0 | 0.3 | 0.21 | 0.58 | 0.21 | 53.5 |
| 5 T1 | 750 | 0.0 | 750 | 0.0 | 0.277 | 8.2 | LOSA | 7.4 | 51.7 | 0.49 | 0.42 | 0.49 | 52.9 |
| 6 R2 | 577 | 0.0 | 577 | 0.0 | * 0.990 | 74.2 | LOSE | 34.1 | 238.6 | 1.00 | 1.23 | 1.65 | 27.0 |
| Approach | 1337 | 0.0 | 1337 | 0.0 | 0.990 | 36.7 | LOS D | 34.1 | 238.6 | 0.71 | 0.77 | 0.99 | 37.4 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 954 | 0.0 | 954 | 0.0 | 0.924 | 494.8 | LOS F | 46.4 | 324.5 | 0.98 | 1.12 | 1.22 | 35.2 |
| 8 T1 | 40 | 0.0 | 40 | 0.0 | 0.083 | 29.9 | LOS C | 1.4 | 9.8 | 0.82 | 0.61 | 0.82 | 40.4 |
| 9 R2 | 414 | 0.0 | 414 | 0.0 | * 1.001 | 88.2 | LOS F | 13.5 | 94.5 | 1.00 | 1.23 | 1.94 | 24.4 |
| Approach | 1408 | 0.0 | 1408 | 0.0 | 1.001 | 362.0 | LOS F | 46.4 | 324.5 | 0.98 | 1.13 | 1.42 | 31.2 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 862 | 0.0 | 862 | 0.0 | 0.682 | 14.1 | LOS B | 17.3 | 120.9 | 0.68 | 0.82 | 0.68 | 48.2 |
| 11 T1 | 1363 | 0.0 | 1363 | 0.0 | * 1.083 | 288.0 | LOS F | 72.1 | 504.4 | 0.98 | 1.49 | 1.79 | 23.3 |
| 12 R 2 | 47 | 0.0 | 47 | 0.0 | 0.152 | 28.1 | LOS C | 1.5 | 10.3 | 0.72 | 0.73 | 0.72 | 40.3 |
| Approach | 2272 | 0.0 | 2272 | 0.0 | 1.083 | 178.7 | LOS F | 72.1 | 504.4 | 0.86 | 1.22 | 1.35 | 29.3 |
| All <br> Vehicles | 5112 | 0.0 | 5112 | 0.0 | 1.083 | 189.3 | LOS F | 72.1 | 504.4 | 0.86 | 1.07 | 1.27 | 31.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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# ANNEXURE B1.10: PHASING SUMMARY <br> 目 Site: [Scenario 4 PM (Site Folder: <br> Upgraded Intersection Geometry (PHASE 1))] 

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 28 | 63 | 79 |
| Green Time (sec) | 21 | 31 | 9 | 7 |
| Phase Time (sec) | 25 | 38 | 13 | 14 |
| Phase Split | $28 \%$ | $42 \%$ | $14 \%$ | $16 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.

## Output Phase Sequence



REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B1: SITE LAYOUT <br> Upgraded Intersection Geometry (PHASE 2)

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## ANNEXURE B1.11: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Upgraded Intersection Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 105 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 31 | 0.0 | 31 | 0.0 | 0.104 | 24.8 | LOS C | 1.1 | 7.7 | 0.82 | 0.69 | 0.82 | 43.0 |
| 2 T1 | 10 | 0.0 | 10 | 0.0 | * 0.104 | 19.2 | LOS B | 1.1 | 7.7 | 0.82 | 0.69 | 0.82 | 43.5 |
| 3 R 2 | 8 | 0.0 | 8 | 0.0 | 0.056 | 56.7 | LOS E | 0.4 | 2.8 | 0.96 | 0.66 | 0.96 | 31.0 |
| Approach | 49 | 0.0 | 49 | 0.0 | 0.104 | 28.9 | LOS C | 1.1 | 7.7 | 0.84 | 0.68 | 0.84 | 40.5 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 28 | 0.0 | 28 | 0.0 | 0.019 | 6.3 | LOSA | 0.1 | 0.9 | 0.17 | 0.58 | 0.17 | 53.7 |
| 5 T1 | 1374 | 0.0 | 1374 | 0.0 | 0.602 | 19.0 | LOS B | 24.5 | 171.4 | 0.76 | 0.68 | 0.76 | 45.8 |
| 6 R2 | 1063 | 0.0 | 1063 | 0.0 | * 0.899 | 56.9 | LOS E | 31.1 | 217.9 | 1.00 | 0.99 | 1.25 | 31.0 |
| Approach | 2465 | 0.0 | 2465 | 0.0 | 0.899 | 35.2 | LOS D | 31.1 | 217.9 | 0.86 | 0.82 | 0.96 | 38.0 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 570 | 0.0 | 570 | 0.0 | 0.276 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.9 |
| 8 T1 | 41 | 0.0 | 41 | 0.0 | 0.054 | 23.7 | LOS C | 1.4 | 9.5 | 0.69 | 0.52 | 0.69 | 43.4 |
| 9 R2 | 918 | 0.0 | 918 | 0.0 | *0.904 | 60.3 | LOS E | 27.3 | 191.0 | 1.00 | 1.00 | 1.29 | 30.0 |
| Approach | 1529 | 0.0 | 1529 | 0.0 | 0.904 | 39.4 | LOS D | 27.3 | 191.0 | 0.62 | 0.81 | 0.79 | 36.5 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 361 | 0.0 | 361 | 0.0 | 0.268 | 11.4 | LOS B | 6.7 | 47.2 | 0.42 | 0.67 | 0.42 | 49.9 |
| 11 T1 | 765 | 0.0 | 765 | 0.0 | * 0.903 | 57.2 | LOS E | 22.6 | 158.4 | 1.00 | 1.06 | 1.32 | 31.1 |
| 12 R 2 | 22 | 0.0 | 22 | 0.0 | 0.175 | 46.4 | LOS D | 1.0 | 7.1 | 0.87 | 0.73 | 0.87 | 33.6 |
| Approach | 1148 | 0.0 | 1148 | 0.0 | 0.903 | 42.6 | LOS D | 22.6 | 158.4 | 0.82 | 0.93 | 1.03 | 35.3 |
| All <br> Vehicles | 5191 | 0.0 | 5191 | 0.0 | 0.904 | 38.0 | LOS D | 31.1 | 217.9 | 0.78 | 0.84 | 0.93 | 37.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.11: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Upgraded Intersection Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 37 | 61 | 94 |
| Green Time (sec) | 30 | 20 | 26 | 7 |
| Phase Time (sec) | 34 | 27 | 30 | 14 |
| Phase Split | $32 \%$ | $26 \%$ | $29 \%$ | $13 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B1.12: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 90 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE <br> [ Veh. Dist] veh <br> m |  | Prop. Que | Effective Stop Rate | Aver. Aver. <br> No. Speed <br> Cycles <br> km/h |  |
| South: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 31 | 0.0 | 31 | 0.0 | 0.295 | 29.2 | LOS C | 2.1 | 14.6 | 0.94 | 0.73 | 0.94 | 41.8 |
| 2 T1 | 40 | 0.0 | 40 | 0.0 | * 0.295 | 23.6 | LOS C | 2.1 | 14.6 | 0.94 | 0.73 | 0.94 | 42.2 |
| $3 \quad \mathrm{R} 2$ | 24 | 0.0 | 24 | 0.0 | 0.144 | 49.1 | LOS D | 1.0 | 7.2 | 0.96 | 0.70 | 0.96 | 33.1 |
| Approach | 95 | 0.0 | 95 | 0.0 | 0.295 | 31.9 | LOS C | 2.1 | 14.6 | 0.95 | 0.72 | 0.95 | 39.3 |
| East: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 10 | 0.0 | 10 | 0.0 | 0.007 | 6.6 | LOSA | 0.0 | 0.3 | 0.21 | 0.58 | 0.21 | 53.5 |
| 5 T1 | 750 | 0.0 | 750 | 0.0 | 0.288 | 9.2 | LOSA | 7.8 | 54.8 | 0.52 | 0.45 | 0.52 | 52.2 |
| 6 R2 | 577 | 0.0 | 577 | 0.0 | * 0.896 | 57.5 | LOS E | 14.9 | 104.2 | 1.00 | 1.03 | 1.41 | 30.8 |
| Approach | 1337 | 0.0 | 1337 | 0.0 | 0.896 | 30.0 | LOS C | 14.9 | 104.2 | 0.72 | 0.70 | 0.90 | 40.2 |
| North: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 954 | 0.0 | 954 | 0.0 | 0.461 | 12.6 | LOS B | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.7 |
| 8 T1 | 40 | 0.0 | 40 | 0.0 | 0.075 | 28.1 | LOS C | 1.3 | 9.4 | 0.80 | 0.60 | 0.80 | 41.3 |
| 9 R2 | 414 | 0.0 | 414 | 0.0 | *0.819 | 53.0 | LOS D | 9.9 | 69.2 | 1.00 | 0.93 | 1.26 | 31.9 |
| Approach | 1408 | 0.0 | 1408 | 0.0 | 0.819 | 25.0 | LOS C | 9.9 | 69.2 | 0.32 | 0.65 | 0.39 | 44.9 |
| West: Heidelberg Rd (R550/K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 862 | 0.0 | 862 | 0.0 | 0.551 | 9.0 | LOS A | 13.5 | 94.4 | 0.45 | 0.69 | 0.45 | 51.5 |
| 11 T1 | 1363 | 0.0 | 1363 | 0.0 | * 0.837 | 30.4 | LOS C | 30.0 | 210.2 | 0.94 | 0.92 | 1.05 | 40.2 |
| 12 R 2 | 47 | 0.0 | 47 | 0.0 | 0.135 | 24.4 | LOS C | 1.3 | 9.4 | 0.67 | 0.72 | 0.67 | 42.1 |
| Approach | 2272 | 0.0 | 2272 | 0.0 | 0.837 | 22.2 | LOS C | 30.0 | 210.2 | 0.75 | 0.83 | 0.81 | 43.9 |
| All <br> Vehicles | 5112 | 0.0 | 5112 | 0.0 | 0.896 | 25.2 | LOS C | 30.0 | 210.2 | 0.63 | 0.74 | 0.72 | 43.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B1.12: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 2))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase A
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 0 | 21 | 61 | 79 |
| Green Time (sec) | 14 | 36 | 11 | 7 |
| Phase Time (sec) | 18 | 43 | 15 | 14 |
| Phase Split | $20 \%$ | $48 \%$ | $17 \%$ | $16 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B2: SITE LAYOUT <br> 目 Existing Intersection Geometry

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## ANNEXURE B2.1: MOVEMENT SUMMARY

## 目 Site: [Scenario 1 AM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT <br> MES <br> HV ] <br> \% | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 47 | 0.0 | 49 | 0.0 | 0.079 | 19.6 | LOS B | 2.1 | 15.0 | 0.53 | 0.63 | 0.53 | 45.2 |
| 2 T1 | 18 | 0.0 | 19 | 0.0 | 0.079 | 14.0 | LOS B | 2.1 | 15.0 | 0.53 | 0.63 | 0.53 | 46.2 |
| 3 R 2 | 12 | 0.0 | 13 | 0.0 | 0.079 | 19.6 | LOS B | 2.1 | 15.0 | 0.53 | 0.63 | 0.53 | 45.3 |
| Approach | 77 | 0.0 | 81 | 0.0 | 0.079 | 18.3 | LOS B | 2.1 | 15.0 | 0.53 | 0.63 | 0.53 | 45.4 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 26 | 0.0 | 27 | 0.0 | 0.036 | 29.3 | LOS C | 0.9 | 6.5 | 0.67 | 0.69 | 0.67 | 39.8 |
| 5 T1 | 714 | 0.0 | 752 | 0.0 | * 0.967 | 67.2 | LOS E | 53.8 | 376.8 | 1.00 | 1.21 | 1.39 | 28.5 |
| 6 R2 | 32 | 0.0 | 34 | 0.0 | 0.097 | 38.7 | LOS D | 1.4 | 9.6 | 0.79 | 0.72 | 0.79 | 36.0 |
| Approach | 772 | 0.0 | 813 | 0.0 | 0.967 | 64.8 | LOS E | 53.8 | 376.8 | 0.98 | 1.17 | 1.34 | 29.0 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 16 | 0.0 | 17 | 0.0 | 0.016 | 19.0 | LOS B | 0.4 | 3.0 | 0.50 | 0.65 | 0.50 | 44.8 |
| 8 T1 | 27 | 0.0 | 28 | 0.0 | * 0.953 | 59.3 | LOS E | 53.0 | 371.2 | 1.00 | 1.07 | 1.35 | 29.1 |
| 9 R 2 | 675 | 0.0 | 711 | 0.0 | 0.953 | 64.9 | LOS E | 53.0 | 371.2 | 1.00 | 1.07 | 1.35 | 28.8 |
| Approach | 718 | 0.0 | 756 | 0.0 | 0.953 | 63.6 | LOS E | 53.0 | 371.2 | 0.99 | 1.06 | 1.33 | 29.0 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 142 | 0.0 | 149 | 0.0 | 0.103 | 6.2 | LOS A | 0.6 | 4.4 | 0.16 | 0.59 | 0.16 | 53.7 |
| 11 T1 | 288 | 0.0 | 303 | 0.0 | 0.384 | 27.6 | LOS C | 11.9 | 83.5 | 0.79 | 0.67 | 0.79 | 41.3 |
| 12 R 2 | 21 | 0.0 | 22 | 0.0 | 0.271 | 66.0 | LOS E | 1.2 | 8.7 | 1.00 | 0.68 | 1.00 | 28.2 |
| Approach | 451 | 0.0 | 475 | 0.0 | 0.384 | 22.7 | LOS C | 11.9 | 83.5 | 0.60 | 0.65 | 0.60 | 43.5 |
| All <br> Vehicles | 2018 | 0.0 | 2124 | 0.0 | 0.967 | 53.2 | LOS D | 53.8 | 376.8 | 0.88 | 0.99 | 1.14 | 31.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.1: PHASING SUMMARY

## 目 Site: [Scenario 1 AM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 64 | 0 |
| Green Time (sec) | 40 | 57 |
| Phase Time (sec) | 47 | 63 |
| Phase Split | $43 \%$ | $57 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## ANNEXURE B2.2: MOVEMENT SUMMARY

## 目 Site: [Scenario 1 PM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT <br> MES <br> HV ] <br> \% | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> QU <br> [ Veh. <br> veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 12 | 0.0 | 13 | 0.0 | 0.155 | 26.7 | LOS C | 1.5 | 10.8 | 0.85 | 0.70 | 0.85 | 42.1 |
| 2 T1 | 26 | 0.0 | 27 | 0.0 | 0.155 | 21.1 | LOS C | 1.5 | 10.8 | 0.85 | 0.70 | 0.85 | 42.9 |
| 3 R2 | 22 | 0.0 | 23 | 0.0 | 0.155 | 26.7 | LOS C | 1.5 | 10.8 | 0.85 | 0.70 | 0.85 | 42.2 |
| Approach | 60 | 0.0 | 63 | 0.0 | 0.155 | 24.3 | LOS C | 1.5 | 10.8 | 0.85 | 0.70 | 0.85 | 42.5 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 13 | 0.0 | 14 | 0.0 | 0.012 | 11.5 | LOS B | 0.2 | 1.2 | 0.45 | 0.63 | 0.45 | 49.3 |
| 5 T1 | 371 | 0.0 | 391 | 0.0 | 0.317 | 7.4 | LOS A | 6.0 | 42.2 | 0.56 | 0.49 | 0.56 | 53.5 |
| 6 R2 | 10 | 0.0 | 11 | 0.0 | 0.027 | 17.5 | LOS B | 0.2 | 1.3 | 0.63 | 0.66 | 0.63 | 45.5 |
| Approach | 394 | 0.0 | 415 | 0.0 | 0.317 | 7.8 | LOS A | 6.0 | 42.2 | 0.56 | 0.50 | 0.56 | 53.1 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 13 | 0.0 | 14 | 0.0 | 0.031 | 25.7 | LOS C | 0.3 | 2.2 | 0.81 | 0.67 | 0.81 | 41.4 |
| 8 T1 | 17 | 0.0 | 18 | 0.0 | * 0.491 | 23.2 | LOS C | 5.0 | 34.9 | 0.92 | 0.79 | 0.92 | 41.0 |
| 9 R2 | 159 | 0.0 | 167 | 0.0 | 0.491 | 28.8 | LOS C | 5.0 | 34.9 | 0.92 | 0.79 | 0.92 | 40.3 |
| Approach | 189 | 0.0 | 199 | 0.0 | 0.491 | 28.1 | LOS C | 5.0 | 34.9 | 0.92 | 0.79 | 0.92 | 40.5 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 390 | 0.0 | 411 | 0.0 | 0.291 | 6.6 | LOS A | 1.9 | 13.4 | 0.30 | 0.64 | 0.30 | 53.2 |
| 11 T1 | 607 | 0.0 | 639 | 0.0 | * 0.519 | 8.6 | LOS A | 11.5 | 80.5 | 0.66 | 0.59 | 0.66 | 52.6 |
| 12 R 2 | 22 | 0.0 | 23 | 0.0 | 0.040 | 14.3 | LOS B | 0.4 | 2.5 | 0.55 | 0.68 | 0.55 | 47.1 |
| Approach | 1019 | 0.0 | 1073 | 0.0 | 0.519 | 8.0 | LOS A | 11.5 | 80.5 | 0.52 | 0.61 | 0.52 | 52.7 |
| All <br> Vehicles | 1662 | 0.0 | 1749 | 0.0 | 0.519 | 10.8 | LOS B | 11.5 | 80.5 | 0.59 | 0.61 | 0.59 | 50.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.2: PHASING SUMMARY

## 目 Site: [Scenario 1 PM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 20 | 0 |
| Green Time (sec) | 34 | 13 |
| Phase Time (sec) | 41 | 19 |
| Phase Split | $68 \%$ | $32 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## ANNEXURE B2.3: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 53 | 0.0 | 53 | 0.0 | 0.099 | 23.1 | LOS C | 2.6 | 18.0 | 0.59 | 0.66 | 0.59 | 43.3 |
| 2 T1 | 20 | 0.0 | 20 | 0.0 | 0.099 | 17.5 | LOS B | 2.6 | 18.0 | 0.59 | 0.66 | 0.59 | 44.2 |
| 3 R2 | 14 | 0.0 | 14 | 0.0 | 0.099 | 23.1 | LOS C | 2.6 | 18.0 | 0.59 | 0.66 | 0.59 | 43.4 |
| Approach | 87 | 0.0 | 87 | 0.0 | 0.099 | 21.8 | LOS C | 2.6 | 18.0 | 0.59 | 0.66 | 0.59 | 43.5 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 29 | 0.0 | 29 | 0.0 | 0.034 | 26.0 | LOS C | 0.9 | 6.4 | 0.62 | 0.68 | 0.62 | 41.2 |
| 5 T1 | 1670 | 0.0 | 1670 | 0.0 | * 1.897 | 850.7 | LOS F | 427.4 | 2991.7 | 1.00 | 4.10 | 4.97 | 3.9 |
| 6 R2 | 109 | 0.0 | 109 | 0.0 | 0.667 | 57.0 | LOS E | 6.0 | 41.9 | 0.99 | 0.85 | 1.09 | 30.5 |
| Approach | 1808 | 0.0 | 1808 | 0.0 | 1.897 | 789.7 | LOS F | 427.4 | 2991.7 | 0.99 | 3.85 | 4.66 | 4.2 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 179 | 0.0 | 179 | 0.0 | 0.183 | 23.2 | LOS C | 5.4 | 38.1 | 0.61 | 0.73 | 0.61 | 42.6 |
| 8 T1 | 31 | 0.0 | 31 | 0.0 | 1.895 | 853.9 | LOS F | 321.8 | 2252.7 | 1.00 | 2.66 | 4.98 | 3.9 |
| 9 R2 | 1216 | 0.0 | 1216 | 0.0 | *1.895 | 859.5 | LOS F | 321.8 | 2252.7 | 1.00 | 2.66 | 4.98 | 3.9 |
| Approach | 1426 | 0.0 | 1426 | 0.0 | 1.895 | 754.4 | LOS F | 321.8 | 2252.7 | 0.95 | 2.42 | 4.43 | 4.4 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 335 | 0.0 | 335 | 0.0 | 0.239 | 7.4 | LOS A | 3.1 | 22.0 | 0.27 | 0.63 | 0.27 | 52.8 |
| 11 T1 | 667 | 0.0 | 667 | 0.0 | 0.764 | 29.6 | LOS C | 30.3 | 212.1 | 0.92 | 0.82 | 0.92 | 40.4 |
| 12 R2 | 24 | 0.0 | 24 | 0.0 | 0.293 | 66.1 | LOS E | 1.4 | 9.5 | 1.00 | 0.69 | 1.00 | 28.2 |
| Approach | 1026 | 0.0 | 1026 | 0.0 | 0.764 | 23.2 | LOS C | 30.3 | 212.1 | 0.71 | 0.76 | 0.71 | 43.3 |
| All Vehicles | 4347 | 0.0 | 4347 | 0.0 | 1.897 | 581.8 | LOS F | 427.4 | 2991.7 | 0.90 | 2.59 | 3.57 | 5.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.3: PHASING SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 59 | 0 |
| Green Time (sec) | 45 | 52 |
| Phase Time (sec) | 52 | 58 |
| Phase Split | $47 \%$ | $53 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B2.4: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 80 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT <br> MES <br> HV ] <br> \% | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { EUE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 0.0 | 14 | 0.0 | 0.193 | 34.9 | LOS C | 2.3 | 15.8 | 0.87 | 0.71 | 0.87 | 38.4 |
| 2 T1 | 29 | 0.0 | 29 | 0.0 | 0.193 | 29.4 | LOS C | 2.3 | 15.8 | 0.87 | 0.71 | 0.87 | 39.1 |
| 3 R 2 | 25 | 0.0 | 25 | 0.0 | 0.193 | 34.9 | LOS C | 2.3 | 15.8 | 0.87 | 0.71 | 0.87 | 38.5 |
| Approach | 68 | 0.0 | 68 | 0.0 | 0.193 | 32.6 | LOS C | 2.3 | 15.8 | 0.87 | 0.71 | 0.87 | 38.7 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 15 | 0.0 | 15 | 0.0 | 0.011 | 11.1 | LOS B | 0.2 | 1.5 | 0.38 | 0.63 | 0.38 | 49.6 |
| 5 T1 | 834 | 0.0 | 834 | 0.0 | 0.655 | 9.1 | LOS A | 19.0 | 132.7 | 0.64 | 0.58 | 0.64 | 52.2 |
| 6 R2 | 144 | 0.0 | 144 | 0.0 | 1.280 | 297.8 | LOS F | 19.3 | 135.1 | 1.00 | 1.74 | 3.89 | 9.9 |
| Approach | 993 | 0.0 | 993 | 0.0 | 1.280 | 51.0 | LOS D | 19.3 | 135.1 | 0.69 | 0.75 | 1.10 | 32.1 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 79 | 0.0 | 79 | 0.0 | 0.191 | 34.7 | LOS C | 2.6 | 18.3 | 0.87 | 0.75 | 0.87 | 37.6 |
| 8 T1 | 19 | 0.0 | 19 | 0.0 | * 1.237 | 259.6 | LOS F | 49.2 | 344.5 | 1.00 | 1.98 | 3.55 | 11.0 |
| 9 R 2 | 368 | 0.0 | 368 | 0.0 | 1.237 | 265.2 | LOS F | 49.2 | 344.5 | 1.00 | 1.98 | 3.55 | 11.0 |
| Approach | 466 | 0.0 | 466 | 0.0 | 1.237 | 225.9 | LOS F | 49.2 | 344.5 | 0.98 | 1.77 | 3.09 | 12.4 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 852 | 0.0 | 852 | 0.0 | 0.526 | 7.2 | LOS A | 6.2 | 43.4 | 0.39 | 0.69 | 0.39 | 52.9 |
| 11 T1 | 1520 | 0.0 | 1520 | 0.0 | * 1.136 | 164.1 | LOS F | 159.1 | 1113.6 | 1.00 | 2.23 | 2.62 | 16.1 |
| 12 R 2 | 25 | 0.0 | 25 | 0.0 | 0.083 | 21.3 | LOS C | 0.6 | 4.3 | 0.63 | 0.70 | 0.63 | 43.2 |
| Approach | 2397 | 0.0 | 2397 | 0.0 | 1.136 | 106.9 | LOS F | 159.1 | 1113.6 | 0.78 | 1.66 | 1.80 | 21.6 |
| All <br> Vehicles | 3924 | 0.0 | 3924 | 0.0 | 1.280 | 105.6 | LOS F | 159.1 | 1113.6 | 0.78 | 1.43 | 1.76 | 21.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.4: PHASING SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Existing Intersection <br> Geometry)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=80$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 23 | 0 |
| Green Time (sec) | 51 | 16 |
| Phase Time (sec) | 58 | 22 |
| Phase Split | $73 \%$ | $28 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## ANNEXURE B2: SITE LAYOUT <br> Upgraded Intersection Geometry (PHASE 1)

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
4 N


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## ANNEXURE B2.5: MOVEMENT SUMMARY

## 目ite: [Scenario 2 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | ND VS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 53 | 0.0 | 53 | 0.0 | 0.547 | 62.6 | LOS E | 4.0 | 28.3 | 1.00 | 0.76 | 1.01 | 29.6 |
| 2 T1 | 20 | 0.0 | 20 | 0.0 | * 0.547 | 57.1 | LOS E | 4.0 | 28.3 | 1.00 | 0.76 | 1.01 | 30.0 |
| 3 R 2 | 14 | 0.0 | 14 | 0.0 | 0.102 | 59.9 | LOS E | 0.7 | 5.1 | 0.97 | 0.68 | 0.97 | 30.1 |
| Approach | 87 | 0.0 | 87 | 0.0 | 0.547 | 60.9 | LOS E | 4.0 | 28.3 | 1.00 | 0.75 | 1.01 | 29.8 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 29 | 0.0 | 29 | 0.0 | 0.031 | 23.5 | LOS C | 0.9 | 6.0 | 0.59 | 0.67 | 0.59 | 42.4 |
| 5 T1 | 1670 | 0.0 | 1670 | 0.0 | * 0.919 | 44.4 | LOS D | 53.7 | 375.8 | 0.96 | 1.03 | 1.16 | 34.7 |
| 6 R2 | 109 | 0.0 | 109 | 0.0 | 0.338 | 34.3 | LOS C | 4.4 | 30.8 | 0.78 | 0.77 | 0.78 | 37.9 |
| Approach | 1808 | 0.0 | 1808 | 0.0 | 0.919 | 43.4 | LOS D | 53.7 | 375.8 | 0.95 | 1.01 | 1.13 | 35.0 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 179 | 0.0 | 179 | 0.0 | 0.181 | 8.2 | LOS A | 2.3 | 16.4 | 0.33 | 0.60 | 0.33 | 53.0 |
| 8 T1 | 31 | 0.0 | 31 | 0.0 | 0.181 | 2.5 | LOS A | 2.3 | 16.4 | 0.33 | 0.60 | 0.33 | 53.6 |
| 9 R2 | 1216 | 0.0 | 1216 | 0.0 | * 0.903 | 56.4 | LOS E | 37.2 | 260.4 | 1.00 | 0.99 | 1.22 | 30.9 |
| Approach | 1426 | 0.0 | 1426 | 0.0 | 0.903 | 49.2 | LOS D | 37.2 | 260.4 | 0.90 | 0.93 | 1.09 | 33.0 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 335 | 0.0 | 335 | 0.0 | 0.249 | 7.3 | LOS A | 3.2 | 22.7 | 0.24 | 0.62 | 0.24 | 52.9 |
| 11 T1 | 667 | 0.0 | 667 | 0.0 | 0.337 | 21.1 | LOS C | 11.5 | 80.5 | 0.70 | 0.60 | 0.70 | 44.6 |
| 12 R 2 | 24 | 0.0 | 24 | 0.0 | 0.272 | 61.7 | LOS E | 1.3 | 9.2 | 0.98 | 0.72 | 0.98 | 29.4 |
| Approach | 1026 | 0.0 | 1026 | 0.0 | 0.337 | 17.5 | LOS B | 11.5 | 80.5 | 0.56 | 0.61 | 0.56 | 46.4 |
| All Vehicles | 4347 | 0.0 | 4347 | 0.0 | 0.919 |  | LOS D | 53.7 | 375.8 | 0.84 | 0.88 | 0.98 | 36.3 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.5: PHASING SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase C
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 11 | 67 | 0 |
| Green Time (sec) | 49 | 36 | 7 |
| Phase Time (sec) | 56 | 40 | 14 |
| Phase Split | $51 \%$ | $36 \%$ | $13 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B2.6: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay $\qquad$ | Level of Service | $\begin{gathered} 95 \% \text { B } \\ \text { QU } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 14 | 0.0 | 14 | 0.0 | 0.172 | 32.6 | LOS C | 1.2 | 8.4 | 0.93 | 0.70 | 0.93 | 40.0 |
| 2 T1 | 29 | 0.0 | 29 | 0.0 | * 0.172 | 27.1 | LOS C | 1.2 | 8.4 | 0.93 | 0.70 | 0.93 | 40.8 |
| 3 R 2 | 25 | 0.0 | 25 | 0.0 | 0.099 | 32.2 | LOS C | 0.7 | 4.8 | 0.92 | 0.70 | 0.92 | 38.9 |
| Approach | 68 | 0.0 | 68 | 0.0 | 0.172 | 30.1 | LOS C | 1.2 | 8.4 | 0.93 | 0.70 | 0.93 | 39.9 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 15 | 0.0 | 15 | 0.0 | 0.016 | 14.7 | LOS B | 0.2 | 1.6 | 0.56 | 0.65 | 0.56 | 47.3 |
| 5 T1 | 834 | 0.0 | 834 | 0.0 | 0.402 | 11.4 | LOS B | 8.1 | 56.4 | 0.70 | 0.60 | 0.70 | 50.6 |
| 6 R2 | 144 | 0.0 | 144 | 0.0 | * 0.819 | 40.1 | LOS D | 5.1 | 35.9 | 1.00 | 1.01 | 1.51 | 35.8 |
| Approach | 993 | 0.0 | 993 | 0.0 | 0.819 | 15.6 | LOS B | 8.1 | 56.4 | 0.74 | 0.66 | 0.82 | 47.7 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 79 | 0.0 | 79 | 0.0 | 0.127 | 11.9 | LOS B | 1.4 | 9.6 | 0.57 | 0.65 | 0.57 | 50.3 |
| 8 T1 | 19 | 0.0 | 19 | 0.0 | 0.127 | 6.3 | LOS A | 1.4 | 9.6 | 0.57 | 0.65 | 0.57 | 50.9 |
| 9 R2 | 368 | 0.0 | 368 | 0.0 | * 0.762 | 37.3 | LOS D | 5.9 | 41.2 | 1.00 | 0.91 | 1.26 | 36.9 |
| Approach | 466 | 0.0 | 466 | 0.0 | 0.762 | 31.7 | LOS C | 5.9 | 41.2 | 0.91 | 0.85 | 1.11 | 39.1 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 852 | 0.0 | 852 | 0.0 | 0.670 | 10.1 | LOS B | 12.3 | 85.9 | 0.65 | 0.76 | 0.65 | 50.7 |
| 11 T1 | 1520 | 0.0 | 1520 | 0.0 | 0.733 | 14.6 | LOS B | 18.6 | 130.0 | 0.87 | 0.79 | 0.89 | 48.4 |
| 12 R 2 | 25 | 0.0 | 25 | 0.0 | 0.076 | 20.1 | LOS C | 0.5 | 3.6 | 0.69 | 0.70 | 0.69 | 44.2 |
| Approach | 2397 | 0.0 | 2397 | 0.0 | 0.733 | 13.1 | LOS B | 18.6 | 130.0 | 0.79 | 0.78 | 0.80 | 49.2 |
| All <br> Vehicles | 3924 | 0.0 | 3924 | 0.0 | 0.819 | 16.2 | LOS B | 18.6 | 130.0 | 0.79 | 0.76 | 0.85 | 47.2 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.6: PHASING SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase C
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 11 | 46 | 0 |
| Green Time (sec) | 28 | 7 | 7 |
| Phase Time (sec) | 35 | 11 | 14 |
| Phase Split | $58 \%$ | $18 \%$ | $23 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

| Output Phase Sequence |  |  |  |
| :---: | :---: | :---: | :---: |
| Phase A | Phase B | Phase C | REF |
| Kingfish St ل1 | Kingfish St dl | Kingfish St لإ |  |
|  |  |  |  |
|  |  |  |  |

REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

## ANNEXURE B2.7: MOVEMENT SUMMARY

## 目ite: [Scenario 3 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 57 | 0.0 | 57 | 0.0 | 0.565 | 60.0 | LOS E | 4.2 | 29.2 | 1.00 | 0.77 | 1.03 | 30.2 |
| 2 T1 | 22 | 0.0 | 22 | 0.0 | * 0.565 | 54.4 | LOS D | 4.2 | 29.2 | 1.00 | 0.77 | 1.03 | 30.7 |
| 3 R 2 | 15 | 0.0 | 15 | 0.0 | 0.103 | 57.1 | LOS E | 0.8 | 5.3 | 0.97 | 0.68 | 0.97 | 30.8 |
| Approach | 94 | 0.0 | 94 | 0.0 | 0.565 | 58.2 | LOS E | 4.2 | 29.2 | 0.99 | 0.76 | 1.02 | 30.4 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 32 | 0.0 | 32 | 0.0 | 0.038 | 25.1 | LOS C | 1.0 | 6.7 | 0.62 | 0.68 | 0.62 | 41.7 |
| 5 T1 | 1733 | 0.0 | 1733 | 0.0 | * 1.002 | 82.0 | LOS F | 70.4 | 492.9 | 1.00 | 1.34 | 1.54 | 25.6 |
| 6 R2 | 147 | 0.0 | 147 | 0.0 | 0.402 | 29.8 | LOS C | 5.0 | 35.1 | 0.87 | 0.77 | 0.87 | 39.8 |
| Approach | 1912 | 0.0 | 1912 | 0.0 | 1.002 | 77.0 | LOS E | 70.4 | 492.9 | 0.98 | 1.28 | 1.47 | 26.5 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 251 | 0.0 | 251 | 0.0 | 0.211 | 8.2 | LOS A | 3.5 | 24.5 | 0.31 | 0.60 | 0.31 | 52.7 |
| 8 T1 | 33 | 0.0 | 33 | 0.0 | 0.211 | 2.5 | LOS A | 3.5 | 24.5 | 0.31 | 0.60 | 0.31 | 53.4 |
| 9 R2 | 1422 | 0.0 | 1422 | 0.0 | *1.006 | 93.2 | LOS F | 58.4 | 408.9 | 1.00 | 1.17 | 1.60 | 23.6 |
| Approach | 1706 | 0.0 | 1706 | 0.0 | 1.006 | 78.9 | LOS E | 58.4 | 408.9 | 0.89 | 1.07 | 1.39 | 26.0 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{ll} 10 & L \\ 11 & T \\ 12 & \mathrm{~F} \end{array}$ | 401 | 0.0 | 401 | 0.0 | 0.273 | 6.4 | LOS A | 2.3 | 16.3 | 0.20 | 0.61 | 0.20 | 53.6 |
|  | 692 | 0.0 | 692 | 0.0 | 0.564 | 35.1 | LOS D | 15.2 | 106.6 | 0.91 | 0.78 | 0.91 | 38.1 |
|  | 26 | 0.0 | 26 | 0.0 | 0.303 | 63.4 | LOS E | 1.4 | 9.8 | 1.00 | 0.69 | 1.00 | 29.0 |
| Approach | 1119 | 0.0 | 1119 | 0.0 | 0.564 | 25.5 | LOS C | 15.2 | 106.6 | 0.66 | 0.72 | 0.66 | 42.2 |
| All <br> Vehicles | 4831 | 0.0 | 4831 | 0.0 | 1.006 |  | LOS E | 70.4 | 492.9 | 0.87 | 1.07 | 1.25 | 28.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.7: PHASING SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase C
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 28 | 61 | 0 | 11 |
| Green Time (sec) | 29 | 37 | 7 | 10 |
| Phase Time (sec) | 36 | 41 | 14 | 14 |
| Phase Split | $34 \%$ | $39 \%$ | $13 \%$ | $13 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B2.8: MOVEMENT SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 90 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \hline \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% B QU [ Veh. veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver Speed <br> km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 15 | 0.0 | 15 | 0.0 | 0.283 | 49.9 | LOS D | 2.1 | 14.4 | 0.98 | 0.72 | 0.98 | 33.7 |
| 2 T1 | 32 | 0.0 | 32 | 0.0 | * 0.283 | 44.4 | LOS D | 2.1 | 14.4 | 0.98 | 0.72 | 0.98 | 34.2 |
| 3 R 2 | 27 | 0.0 | 27 | 0.0 | 0.159 | 49.2 | LOS D | 1.2 | 8.1 | 0.97 | 0.71 | 0.97 | 32.9 |
| Approach | 74 | 0.0 | 74 | 0.0 | 0.283 | 47.3 | LOS D | 2.1 | 14.4 | 0.97 | 0.72 | 0.97 | 33.6 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 16 | 0.0 | 16 | 0.0 | 0.013 | 13.5 | LOS B | 0.3 | 2.0 | 0.43 | 0.64 | 0.43 | 48.0 |
| 5 T1 | 867 | 0.0 | 867 | 0.0 | 0.331 | 10.0 | LOS B | 9.6 | 67.0 | 0.55 | 0.48 | 0.55 | 51.5 |
| 6 R2 | 200 | 0.0 | 200 | 0.0 | * 0.727 | 28.0 | LOS C | 5.2 | 36.7 | 1.00 | 0.87 | 1.13 | 40.6 |
| Approach | 1083 | 0.0 | 1083 | 0.0 | 0.727 | 13.4 | LOS B | 9.6 | 67.0 | 0.63 | 0.55 | 0.65 | 49.0 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 107 | 0.0 | 107 | 0.0 | 0.148 | 15.3 | LOS B | 2.8 | 19.8 | 0.55 | 0.66 | 0.55 | 48.0 |
| 8 T1 | 21 | 0.0 | 21 | 0.0 | 0.148 | 9.7 | LOS A | 2.8 | 19.8 | 0.55 | 0.66 | 0.55 | 48.5 |
| 9 R2 | 440 | 0.0 | 440 | 0.0 | * 0.798 | 51.3 | LOS D | 10.3 | 72.2 | 1.00 | 0.91 | 1.21 | 32.3 |
| Approach | 568 | 0.0 | 568 | 0.0 | 0.798 | 43.0 | LOS D | 10.3 | 72.2 | 0.90 | 0.86 | 1.06 | 34.9 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1019 | 0.0 | 1019 | 0.0 | 0.715 | 9.6 | LOS A | 16.1 | 112.9 | 0.62 | 0.78 | 0.62 | 51.3 |
| 11 T1 | 1573 | 0.0 | 1573 | 0.0 | * 0.846 | 26.7 | LOS C | 35.5 | 248.4 | 0.90 | 0.89 | 0.99 | 41.8 |
| 12 R 2 | 27 | 0.0 | 27 | 0.0 | 0.077 | 20.1 | LOS C | 0.7 | 4.7 | 0.58 | 0.69 | 0.58 | 44.2 |
| Approach | 2619 | 0.0 | 2619 | 0.0 | 0.846 | 19.9 | LOS B | 35.5 | 248.4 | 0.78 | 0.84 | 0.84 | 45.1 |
| All Vehicles | 4344 | 0.0 | 4344 | 0.0 | 0.846 |  | LOS C | 35.5 | 248.4 | 0.76 | 0.77 | 0.83 | 44.0 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.8: PHASING SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase C
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 25 | 71 | 0 | 11 |
| Green Time (sec) | 42 | 12 | 7 | 7 |
| Phase Time (sec) | 49 | 16 | 14 | 11 |
| Phase Split | $54 \%$ | $18 \%$ | $16 \%$ | $12 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B2.9: MOVEMENT SUMMARY

## 目ite: [Scenario 4 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 57 | 0.0 | 57 | 0.0 | 0.592 | 63.0 | LOS E | 4.4 | 30.8 | 1.00 | 0.78 | 1.05 | 29.5 |
| 2 T1 | 22 | 0.0 | 22 | 0.0 | * 0.592 | 57.5 | LOS E | 4.4 | 30.8 | 1.00 | 0.78 | 1.05 | 29.9 |
| 3 R 2 | 15 | 0.0 | 15 | 0.0 | 0.108 | 59.9 | LOS E | 0.8 | 5.5 | 0.97 | 0.68 | 0.97 | 30.1 |
| Approach | 94 | 0.0 | 94 | 0.0 | 0.592 | 61.2 | LOS E | 4.4 | 30.8 | 1.00 | 0.76 | 1.03 | 29.7 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 32 | 0.0 | 32 | 0.0 | 0.034 | 23.0 | LOS C | 0.9 | 6.5 | 0.58 | 0.68 | 0.58 | 42.7 |
| 5 T1 | 2134 | 0.0 | 2134 | 0.0 | *1.109 | 156.4 | LOS F | 122.2 | 855.4 | 1.00 | 1.77 | 2.07 | 16.6 |
| 6 R2 | 147 | 0.0 | 147 | 0.0 | 0.398 | 28.0 | LOS C | 4.8 | 33.8 | 0.85 | 0.77 | 0.85 | 40.6 |
| Approach | 2313 | 0.0 | 2313 | 0.0 | 1.109 | 146.4 | LOS F | 122.2 | 855.4 | 0.98 | 1.69 | 1.97 | 17.4 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 251 | 0.0 | 251 | 0.0 | 0.224 | 9.0 | LOS A | 4.3 | 30.3 | 0.35 | 0.62 | 0.35 | 52.1 |
| 8 T1 | 33 | 0.0 | 33 | 0.0 | 0.224 | 3.4 | LOS A | 4.3 | 30.3 | 0.35 | 0.62 | 0.35 | 52.7 |
| 9 R2 | 1422 | 0.0 | 1422 | 0.0 | *1.105 | 165.2 | LOS F | 79.3 | 555.4 | 1.00 | 1.40 | 2.12 | 15.9 |
| Approach | 1706 | 0.0 | 1706 | 0.0 | 1.105 | 139.1 | LOS F | 79.3 | 555.4 | 0.89 | 1.27 | 1.82 | 18.0 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{ll} 10 & L \\ 11 & T \\ 12 & \mathrm{~F} \end{array}$ | 401 | 0.0 | 401 | 0.0 | 0.273 | 6.4 | LOS A | 2.3 | 16.3 | 0.20 | 0.61 | 0.20 | 53.6 |
|  | 832 | 0.0 | 832 | 0.0 | 0.588 | 33.7 | LOS C | 18.7 | 130.7 | 0.90 | 0.78 | 0.90 | 38.6 |
|  | 26 | 0.0 | 26 | 0.0 | 0.318 | 66.3 | LOS E | 1.5 | 10.3 | 1.00 | 0.69 | 1.00 | 28.4 |
| Approach | 1259 | 0.0 | 1259 | 0.0 | 0.588 | 25.7 | LOS C | 18.7 | 130.7 | 0.68 | 0.72 | 0.68 | 42.1 |
| All Vehicles |  |  | 5372 | 0.0 | 1.109 | 114.3 | LOS F | 122.2855 .4 |  | 0.88 | 1.31 | 1.61 | 20.6 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.9: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase C
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 29 | 68 | 0 | 11 |
| Green Time (sec) | 35 | 35 | 7 | 11 |
| Phase Time (sec) | 42 | 39 | 14 | 15 |
| Phase Split | $38 \%$ | $35 \%$ | $13 \%$ | $14 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B2.10: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh <br> veh | CK OF UE Dist $]$ m | Prop. Que | Effective Stop Rate | Aver. No Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 15 | 0.0 | 15 | 0.0 | 0.377 | 67.2 | LOS E | 2.8 | 19.5 | 1.00 | 0.74 | 1.00 | 29.1 |
| 2 T1 | 32 | 0.0 | 32 | 0.0 | * 0.377 | 61.7 | LOS E | 2.8 | 19.5 | 1.00 | 0.74 | 1.00 | 29.5 |
| 3 R2 | 27 | 0.0 | 27 | 0.0 | 0.212 | 66.2 | LOS E | 1.6 | 11.0 | 0.99 | 0.71 | 0.99 | 28.6 |
| Approach | 74 | 0.0 | 74 | 0.0 | 0.377 | 64.5 | LOS E | 2.8 | 19.5 | 0.99 | 0.73 | 0.99 | 29.1 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 16 | 0.0 | 16 | 0.0 | 0.011 | 11.8 | LOS B | 0.3 | 2.0 | 0.33 | 0.63 | 0.33 | 49.1 |
| 5 T1 | 1026 | 0.0 | 1026 | 0.0 | 0.338 | 8.2 | LOSA | 12.0 | 84.3 | 0.44 | 0.40 | 0.44 | 52.9 |
| 6 R2 | 200 | 0.0 | 200 | 0.0 | *1.003 | 85.7 | LOS F | 13.6 | 95.0 | 1.00 | 1.13 | 1.80 | 20.5 |
| Approach | 1242 | 0.0 | 1242 | 0.0 | 1.003 | 20.7 | LOS C | 13.6 | 95.0 | 0.53 | 0.52 | 0.66 | 42.1 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 107 | 0.0 | 107 | 0.0 | 0.196 | 29.7 | LOS C | 5.3 | 37.3 | 0.73 | 0.73 | 0.73 | 40.4 |
| 8 T1 | 21 | 0.0 | 21 | 0.0 | 0.196 | 24.1 | LOS C | 5.3 | 37.3 | 0.73 | 0.73 | 0.73 | 40.8 |
| 9 R2 | 440 | 0.0 | 440 | 0.0 | * 0.982 | 96.1 | LOS F | 17.1 | 119.7 | 1.00 | 1.11 | 1.65 | 23.2 |
| Approach | 568 | 0.0 | 568 | 0.0 | 0.982 | 80.9 | LOS F | 17.1 | 119.7 | 0.94 | 1.02 | 1.44 | 25.7 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1019 | 0.0 | 1019 | 0.0 | 0.677 | 9.6 | LOS A | 17.1 | 119.7 | 0.54 | 0.75 | 0.54 | 51.3 |
| 11 T1 | 1942 | 0.0 | 1942 | 0.0 | * 0.974 | 57.6 | LOS E | 87.6 | 613.0 | 0.86 | 1.05 | 1.18 | 30.9 |
| 12 R 2 | 27 | 0.0 | 27 | 0.0 | 0.081 | 17.0 | LOS B | 0.7 | 4.8 | 0.45 | 0.67 | 0.45 | 46.0 |
| Approach | 2988 | 0.0 | 2988 | 0.0 | 0.974 | 40.9 | LOS D | 87.6 | 613.0 | 0.74 | 0.94 | 0.95 | 35.9 |
| All <br> Vehicles | 4872 | 0.0 | 4872 | 0.0 | 1.003 | 40.8 | LOS D | 87.6 | 613.0 | 0.72 | 0.84 | 0.93 | 35.4 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.10: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 1))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=120$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase C
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 25 | 100 | 0 | 11 |
| Green Time (sec) | 71 | 13 | 7 | 7 |
| Phase Time (sec) | 78 | 17 | 14 | 11 |
| Phase Split | $65 \%$ | $14 \%$ | $12 \%$ | $9 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B2: SITE LAYOUT <br> Upgraded Intersection Geometry (PHASE 2)

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
$q^{\prime N}$


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## ANNEXURE B2.11: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT <br> MES <br> HV ] <br> \% | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 57 | 0.0 | 57 | 0.0 | 0.592 | 63.0 | LOS E | 4.4 | 30.8 | 1.00 | 0.78 | 1.05 | 29.5 |
| 2 T1 | 22 | 0.0 | 22 | 0.0 | * 0.592 | 57.5 | LOS E | 4.4 | 30.8 | 1.00 | 0.78 | 1.05 | 29.9 |
| 3 R2 | 15 | 0.0 | 15 | 0.0 | 0.109 | 59.9 | LOS E | 0.8 | 5.5 | 0.97 | 0.68 | 0.97 | 30.2 |
| Approach | 94 | 0.0 | 94 | 0.0 | 0.592 | 61.3 | LOS E | 4.4 | 30.8 | 1.00 | 0.76 | 1.03 | 29.7 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 32 | 0.0 | 32 | 0.0 | 0.041 | 28.0 | LOS C | 1.1 | 7.4 | 0.65 | 0.69 | 0.65 | 40.3 |
| 5 T1 | 2134 | 0.0 | 2134 | 0.0 | * 0.907 | 46.5 | LOS D | 44.9 | 314.3 | 0.98 | 1.03 | 1.18 | 34.1 |
| 6 R2 | 147 | 0.0 | 147 | 0.0 | 0.593 | 43.1 | LOS D | 7.0 | 49.3 | 0.91 | 0.82 | 0.91 | 34.9 |
| Approach | 2313 | 0.0 | 2313 | 0.0 | 0.907 | 46.0 | LOS D | 44.9 | 314.3 | 0.97 | 1.01 | 1.15 | 34.2 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 251 | 0.0 | 251 | 0.0 | 0.224 | 8.7 | LOS A | 3.6 | 25.3 | 0.31 | 0.61 | 0.31 | 52.9 |
| 8 T1 | 33 | 0.0 | 33 | 0.0 | 0.224 | 2.4 | LOS A | 3.6 | 25.3 | 0.31 | 0.61 | 0.31 | 53.5 |
| 9 R2 | 1422 | 0.0 | 1422 | 0.0 | * 0.906 | 52.4 | LOS D | 44.2 | 309.2 | 0.99 | 0.99 | 1.19 | 32.2 |
| Approach | 1706 | 0.0 | 1706 | 0.0 | 0.906 | 45.0 | LOS D | 44.2 | 309.2 | 0.88 | 0.93 | 1.04 | 34.4 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 401 | 0.0 | 401 | 0.0 | 0.319 | 9.1 | LOS A | 5.9 | 41.0 | 0.36 | 0.67 | 0.36 | 51.5 |
| 11 T1 | 832 | 0.0 | 832 | 0.0 | 0.348 | 25.8 | LOS C | 11.2 | 78.1 | 0.75 | 0.64 | 0.75 | 42.3 |
| 12 R 2 | 26 | 0.0 | 26 | 0.0 | 0.308 | 63.1 | LOS E | 1.4 | 10.1 | 0.99 | 0.72 | 0.99 | 29.2 |
| Approach | 1259 | 0.0 | 1259 | 0.0 | 0.348 | 21.3 | LOS C | 11.2 | 78.1 | 0.63 | 0.65 | 0.63 | 44.4 |
| All <br> Vehicles | 5372 | 0.0 | 5372 | 0.0 | 0.907 | 40.2 | LOS D | 44.9 | 314.3 | 0.86 | 0.90 | 0.99 | 36.1 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.11: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase C
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 11 | 60 | 0 |
| Green Time (sec) | 42 | 43 | 7 |
| Phase Time (sec) | 49 | 47 | 14 |
| Phase Split | $45 \%$ | $43 \%$ | $13 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B2.12: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=80$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { JT } \\ & \text { WES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver Speed <br> km/h |
| South: Garthview St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 15 | 0.0 | 15 | 0.0 | 0.251 | 44.2 | LOS D | 1.8 | 12.6 | 0.97 | 0.72 | 0.97 | 35.6 |
| 2 T1 | 32 | 0.0 | 32 | 0.0 | * 0.251 | 38.6 | LOS D | 1.8 | 12.6 | 0.97 | 0.72 | 0.97 | 36.2 |
| 3 R2 | 27 | 0.0 | 27 | 0.0 | 0.142 | 43.6 | LOS D | 1.0 | 7.1 | 0.95 | 0.70 | 0.95 | 34.9 |
| Approach | 74 | 0.0 | 74 | 0.0 | 0.251 | 41.5 | LOS D | 1.8 | 12.6 | 0.96 | 0.71 | 0.96 | 35.6 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 16 | 0.0 | 16 | 0.0 | 0.014 | 14.1 | LOS B | 0.3 | 1.9 | 0.47 | 0.64 | 0.47 | 47.6 |
| 5 T1 | 1026 | 0.0 | 1026 | 0.0 | 0.280 | 10.2 | LOS B | 7.0 | 49.1 | 0.57 | 0.49 | 0.57 | 51.4 |
| 6 R2 | 200 | 0.0 | 200 | 0.0 | *0.652 | 23.0 | LOS C | 4.3 | 30.3 | 0.96 | 0.83 | 1.01 | 43.1 |
| Approach | 1242 | 0.0 | 1242 | 0.0 | 0.652 | 12.3 | LOS B | 7.0 | 49.1 | 0.63 | 0.54 | 0.64 | 49.8 |
| North: Kingfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 107 | 0.0 | 107 | 0.0 | 0.140 | 15.6 | LOS B | 2.1 | 15.0 | 0.49 | 0.64 | 0.49 | 50.2 |
| 8 T1 | 21 | 0.0 | 21 | 0.0 | 0.140 | 6.3 | LOSA | 2.1 | 15.0 | 0.49 | 0.64 | 0.49 | 50.8 |
| 9 R2 | 440 | 0.0 | 440 | 0.0 | * 0.773 | 45.6 | LOS D | 9.1 | 63.7 | 1.00 | 0.91 | 1.19 | 34.2 |
| Approach | 568 | 0.0 | 568 | 0.0 | 0.773 | 38.5 | LOS D | 9.1 | 63.7 | 0.89 | 0.85 | 1.03 | 36.9 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 1019 | 0.0 | 1019 | 0.0 | 0.725 | 8.4 | LOS A | 12.3 | 86.3 | 0.57 | 0.76 | 0.57 | 52.1 |
| 11 T1 | 1942 | 0.0 | 1942 | 0.0 | * 0.752 | 22.6 | LOS C | 23.3 | 163.2 | 0.89 | 0.80 | 0.91 | 44.4 |
| 12 R 2 | 27 | 0.0 | 27 | 0.0 | 0.091 | 21.5 | LOS C | 0.7 | 4.7 | 0.64 | 0.69 | 0.64 | 43.7 |
| Approach | 2988 | 0.0 | 2988 | 0.0 | 0.752 | 17.7 | LOS B | 23.3 | 163.2 | 0.78 | 0.79 | 0.79 | 46.7 |
| All <br> Vehicles | 4872 | 0.0 | 4872 | 0.0 | 0.773 | 19.1 | LOS B | 23.3 | 163.2 | 0.76 | 0.73 | 0.78 | 45.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B2.12: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Upgraded Intersection <br> Geometry (PHASE 2))]

## New Site

Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 80 seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase C
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 25 | 62 | 0 | 11 |
| Green Time (sec) | 33 | 11 | 7 | 7 |
| Phase Time (sec) | 40 | 15 | 14 | 11 |
| Phase Split | $50 \%$ | $19 \%$ | $18 \%$ | $14 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3: SITE LAYOUT

Existing Intersection Geometry
Site Category: -
Stop (All-Way)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings


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## ANNEXURE B3.1: MOVEMENT SUMMARY

(10) Site: [Scenario 1 AM (Site

Folder: Existing Intersection Geometry)]
Site Category: -
Stop (All-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn |  | $\begin{gathered} \text { JT } \\ \text { MES } \\ \text { HV ] } \\ \% \end{gathered}$ |  | $\begin{aligned} & \text { WD } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ <br> sec | Level of Service |  | CK OF Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 34 | 0.0 | 36 | 0.0 | 0.032 | 7.1 | LOS A | 0.1 | 0.8 | 0.44 | 0.62 | 0.44 | 52.7 |
| 22 T1 | 18 | 0.0 | 19 | 0.0 | 0.021 | 9.6 | LOS A | 0.1 | 0.5 | 0.36 | 0.86 | 0.36 | 51.2 |
| 23 R2 | 1 | 0.0 | 1 | 0.0 | 0.002 | 12.3 | LOS B | 0.0 | 0.0 | 0.52 | 0.83 | 0.52 | 49.7 |
| Approach | 53 | 0.0 | 56 | 0.0 | 0.032 | 8.1 | LOS A | 0.1 | 0.8 | 0.41 | 0.71 | 0.41 | 52.2 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 5.6 | LOS A | 0.0 | 0.0 | 0.06 | 0.52 | 0.06 | 54.1 |
| 5 T1 | 264 | 0.0 | 278 | 0.0 | 0.275 | 9.3 | LOSA | 1.2 | 8.4 | 0.34 | 0.89 | 0.34 | 51.4 |
| 6 R2 | 188 | 0.0 | 198 | 0.0 | 0.331 | 12.9 | LOS B | 1.5 | 10.2 | 0.56 | 1.04 | 0.67 | 49.4 |
| Approach | 453 | 0.0 | 477 | 0.0 | 0.331 | 10.8 | LOS B | 1.5 | 10.2 | 0.43 | 0.95 | 0.48 | 50.5 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 309 | 0.0 | 325 | 0.0 | 0.222 | 6.1 | LOS A | 1.0 | 7.2 | 0.27 | 0.55 | 0.27 | 53.3 |
| 28 T1 | 13 | 0.0 | 14 | 0.0 | 0.013 | 8.9 | LOS A | 0.0 | 0.3 | 0.26 | 0.86 | 0.26 | 51.5 |
| 9 R2 | 163 | 0.0 | 172 | 0.0 | 0.278 | 12.1 | LOS B | 1.1 | 7.8 | 0.53 | 1.01 | 0.58 | 49.8 |
| Approach | 485 | 0.0 | 511 | 0.0 | 0.278 | 8.2 | LOS A | 1.1 | 7.8 | 0.36 | 0.71 | 0.37 | 52.0 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 47 | 0.0 | 49 | 0.0 | 0.036 | 6.2 | LOS A | 0.1 | 1.0 | 0.29 | 0.54 | 0.29 | 53.2 |
| 11 T1 | 133 | 0.0 | 140 | 0.0 | 0.121 | 8.4 | LOS A | 0.5 | 3.3 | 0.12 | 0.92 | 0.12 | 51.7 |
| 32 R2 | 2 | 0.0 | 2 | 0.0 | 0.003 | 10.1 | LOS B | 0.0 | 0.1 | 0.39 | 0.83 | 0.39 | 51.0 |
| Approach | 182 | 0.0 | 192 | 0.0 | 0.121 | 7.9 | LOS A | 0.5 | 3.3 | 0.17 | 0.82 | 0.17 | 52.1 |
| All <br> Vehicles | 1173 | 0.0 | 1235 | 0.0 | 0.331 | 9.1 | NA | 1.5 | 10.2 | 0.36 | 0.82 | 0.38 | 51.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Minor Road Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## ANNEXURE B3.2: MOVEMENT SUMMARY

(9i) Site: [Scenario 1 AM (Site
Folder: Existing Intersection Geometry)]
Site Category: -
Stop (All-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { IN } \\ & \text { VOLI } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{gathered} \text { DEM } \\ \text { FLO } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \\ & \text { Cycles } \end{aligned}$ | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 1 | 0.0 | 1 | 0.0 | 0.001 | 6.4 | LOSA | 0.0 | 0.0 | 0.33 | 0.50 | 0.33 | 53.1 |
| 22 T1 | 22 | 0.0 | 23 | 0.0 | 0.022 | 8.9 | LOSA | 0.1 | 0.6 | 0.25 | 0.87 | 0.25 | 51.6 |
| 23 R2 | 1 | 0.0 | 1 | 0.0 | 0.002 | 13.9 | LOS B | 0.0 | 0.1 | 0.61 | 0.83 | 0.61 | 48.8 |
| Approach | 24 | 0.0 | 25 | 0.0 | 0.022 | 9.0 | LOS A | 0.1 | 0.6 | 0.27 | 0.85 | 0.27 | 51.5 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 5 | 0.0 | 5 | 0.0 | 0.003 | 5.8 | LOSA | 0.0 | 0.1 | 0.13 | 0.51 | 0.13 | 53.8 |
| 5 T1 | 144 | 0.0 | 152 | 0.0 | 0.152 | 9.2 | LOSA | 0.6 | 4.1 | 0.32 | 0.89 | 0.32 | 51.4 |
| 6 R2 | 301 | 0.0 | 317 | 0.0 | 0.602 | 17.3 | LOS C | 3.9 | 27.0 | 0.72 | 1.17 | 1.26 | 46.8 |
| Approach | 450 | 0.0 | 474 | 0.0 | 0.602 | 14.6 | LOS B | 3.9 | 27.0 | 0.59 | 1.07 | 0.95 | 48.2 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 288 | 0.0 | 303 | 0.0 | 0.231 | 6.6 | LOS A | 1.0 | 7.3 | 0.38 | 0.60 | 0.38 | 52.9 |
| 28 T1 | 37 | 0.0 | 39 | 0.0 | 0.048 | 10.2 | LOS B | 0.2 | 1.2 | 0.42 | 0.89 | 0.42 | 50.9 |
| 9 R2 | 119 | 0.0 | 125 | 0.0 | 0.230 | 12.9 | LOS B | 0.8 | 5.9 | 0.56 | 1.01 | 0.58 | 49.3 |
| Approach | 444 | 0.0 | 467 | 0.0 | 0.231 | 8.6 | LOS A | 1.0 | 7.3 | 0.43 | 0.74 | 0.44 | 51.7 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 221 | 0.0 | 233 | 0.0 | 0.189 | 6.9 | LOSA | 0.8 | 5.6 | 0.42 | 0.63 | 0.42 | 52.8 |
| 11 T1 | 253 | 0.0 | 266 | 0.0 | 0.227 | 8.3 | LOSA | 1.0 | 6.9 | 0.10 | 0.93 | 0.10 | 51.7 |
| 32 R 2 | 19 | 0.0 | 20 | 0.0 | 0.024 | 9.4 | LOSA | 0.1 | 0.6 | 0.31 | 0.87 | 0.31 | 51.4 |
| Approach | 493 | 0.0 | 519 | 0.0 | 0.227 | 7.7 | LOS A | 1.0 | 6.9 | 0.25 | 0.79 | 0.25 | 52.2 |
| All Vehicles | 1411 | 0.0 | 1485 | 0.0 | 0.602 | 10.2 | NA | 3.9 | 27.0 | 0.42 | 0.87 | 0.53 | 50.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Minor Road Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## ANNEXURE B3: SITE LAYOUT

8
Signalized Intersection (Existing Geometry)
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings


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## ANNEXURE B3.3: MOVEMENT SUMMARY

## 目ite: [Scenario 2 AM (Site Folder: <br> Signalized Intersection (Existing Geometry))]

Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=65$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Aver. Delay sec | Level of Service |  | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 211 | 0.0 | 211 | 0.0 | 0.227 | 13.2 | LOS B | 3.3 | 23.1 | 0.59 | 0.71 | 0.59 | 48.7 |
| 22 T1 | 38 | 0.0 | 38 | 0.0 | * 0.162 | 29.8 | LOS C | 1.1 | 8.0 | 0.94 | 0.68 | 0.94 | 40.3 |
| 23 R2 | 433 | 0.0 | 433 | 0.0 | * 0.824 | 32.5 | LOS C | 13.6 | 95.1 | 1.00 | 0.98 | 1.22 | 38.5 |
| Approach | 682 | 0.0 | 682 | 0.0 | 0.824 | 26.4 | LOS C | 13.6 | 95.1 | 0.87 | 0.88 | 1.01 | 41.3 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 276 | 0.0 | 276 | 0.0 | 0.197 | 6.8 | LOSA | 1.6 | 11.1 | 0.29 | 0.63 | 0.29 | 53.2 |
| 5 T1 | 684 | 0.0 | 684 | 0.0 | 0.824 | 19.4 | LOS B | 19.6 | 137.5 | 0.82 | 0.84 | 0.97 | 45.5 |
| 6 R2 | 548 | 0.0 | 548 | 0.0 | *1.394 | 382.5 | LOS F | 77.6 | 543.4 | 1.00 | 2.49 | 5.19 | 7.9 |
| Approach | 1508 | 0.0 | 1508 | 0.0 | 1.394 | 149.1 | LOS F | 77.6 | 543.4 | 0.79 | 1.40 | 2.38 | 16.8 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $7 \quad$ L2 | 922 | 0.0 | 922 | 0.0 | 1.218 | 229.2 | LOS F | 96.4 | 674.8 | 1.00 | 2.16 | 3.80 | 12.0 |
| 28 T1 | 38 | 0.0 | 38 | 0.0 | 0.162 | 29.8 | LOS C | 1.1 | 8.0 | 0.94 | 0.68 | 0.94 | 40.3 |
| 9 R2 | 266 | 0.0 | 266 | 0.0 | 0.506 | 25.2 | LOS C | 6.9 | 48.4 | 0.91 | 0.80 | 0.91 | 41.7 |
| Approach | 1226 | 0.0 | 1226 | 0.0 | 1.218 | 178.8 | LOS F | 96.4 | 674.8 | 0.98 | 1.82 | 3.09 | 14.6 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 120 | 0.0 | 120 | 0.0 | 0.088 | 7.6 | LOS A | 0.8 | 5.8 | 0.34 | 0.63 | 0.34 | 52.7 |
| 11 T1 | 727 | 0.0 | 727 | 0.0 | *1.210 | 227.0 | LOS F | 81.6 | 571.0 | 1.00 | 2.62 | 3.76 | 12.5 |
| 32 R 2 | 97 | 0.0 | 97 | 0.0 | 0.367 | 28.8 | LOS C | 2.7 | 19.0 | 0.87 | 0.77 | 0.87 | 40.1 |
| Approach | 944 | 0.0 | 944 | 0.0 | 1.210 | 178.7 | LOS F | 81.6 | 571.0 | 0.90 | 2.18 | 3.03 | 15.1 |
| All Vehicles | 4360 | 0.0 | 4360 | 0.0 | 1.394 | 144.7 | LOS F | 96.4 | 674.8 | 0.88 | 1.61 | 2.51 | 17.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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## ANNEXURE B3.3: PHASING SUMMARY

## 首 Site: [Scenario 2 AM (Site Folder:

Signalized Intersection (Existing Geometry))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=65$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 42 | 0 | 17 | 28 |
| Green Time (sec) | 19 | 10 | 7 | 8 |
| Phase Time (sec) | 26 | 14 | 13 | 12 |
| Phase Split | $40 \%$ | $22 \%$ | $20 \%$ | $18 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3.4: MOVEMENT SUMMARY

## 慁ite: [Scenario 2 PM (Site Folder: <br> Signalized Intersection (Existing Geometry))]

Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=85$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | ND VS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> QU <br> [ Veh. veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 120 | 0.0 | 120 | 0.0 | 0.129 | 14.4 | LOS B | 2.3 | 16.0 | 0.51 | 0.67 | 0.51 | 48.0 |
| 22 T1 | 43 | 0.0 | 43 | 0.0 | 0.240 | 41.3 | LOS D | 1.8 | 12.3 | 0.97 | 0.71 | 0.97 | 35.8 |
| 23 R2 | 331 | 0.0 | 331 | 0.0 | * 0.864 | 46.6 | LOS D | 14.3 | 100.0 | 1.00 | 1.01 | 1.30 | 33.6 |
| Approach | 494 | 0.0 | 494 | 0.0 | 0.864 | 38.3 | LOS D | 14.3 | 100.0 | 0.88 | 0.90 | 1.08 | 36.4 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 475 | 0.0 | 475 | 0.0 | 0.323 | 6.6 | LOS A | 3.0 | 21.1 | 0.25 | 0.62 | 0.25 | 53.4 |
| 5 T1 | 672 | 0.0 | 672 | 0.0 | * 1.154 | 188.6 | LOS F | 72.7 | 509.2 | 1.00 | 2.11 | 2.77 | 14.4 |
| 6 R2 | 874 | 0.0 | 874 | 0.0 | *1.500 | 485.6 | LOS F | 150.4 | 1053.1 | 1.00 | 2.35 | 4.72 | 6.4 |
| Approach | 2021 | 0.0 | 2021 | 0.0 | 1.500 | 274.3 | LOS F | 150.4 | 1053.1 | 0.82 | 1.86 | 3.02 | 10.6 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 660 | 0.0 | 660 | 0.0 | 0.762 | 23.5 | LOS C | 16.3 | 113.8 | 0.85 | 0.94 | 0.87 | 43.0 |
| 28 T1 | 56 | 0.0 | 56 | 0.0 | * 0.313 | 41.7 | LOS D | 2.3 | 16.1 | 0.98 | 0.73 | 0.98 | 35.6 |
| 9 R2 | 206 | 0.0 | 206 | 0.0 | 0.525 | 36.1 | LOS D | 7.5 | 52.6 | 0.95 | 0.80 | 0.95 | 37.1 |
| Approach | 922 | 0.0 | 922 | 0.0 | 0.762 | 27.4 | LOS C | 16.3 | 113.8 | 0.88 | 0.90 | 0.90 | 41.0 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 338 | 0.0 | 338 | 0.0 | 0.293 | 12.2 | LOS B | 5.8 | 40.6 | 0.52 | 0.70 | 0.52 | 49.4 |
| 11 T1 | 655 | 0.0 | 655 | 0.0 | 1.112 | 154.8 | LOS F | 63.3 | 443.3 | 1.00 | 1.92 | 2.48 | 16.7 |
| 32 R 2 | 205 | 0.0 | 205 | 0.0 | 0.308 | 18.5 | LOS B | 3.8 | 26.7 | 0.80 | 0.76 | 0.80 | 45.2 |
| Approach | 1198 | 0.0 | 1198 | 0.0 | 1.112 | 91.2 | LOS F | 63.3 | 443.3 | 0.83 | 1.38 | 1.64 | 23.7 |
| All <br> Vehicles | 4635 | 0.0 | 4635 | 0.0 | 1.500 | 152.7 | LOS F | 150.4 | 1053.1 | 0.84 | 1.44 | 2.04 | 16.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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## ANNEXURE B3.4: PHASING SUMMARY

## 首ite: [Scenario 2 PM (Site Folder:

Signalized Intersection (Existing Geometry))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=85$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 57 | 0 | 17 | 28 |
| Green Time (sec) | 24 | 10 | 7 | 23 |
| Phase Time (sec) | 31 | 14 | 13 | 27 |
| Phase Split | $36 \%$ | $16 \%$ | $15 \%$ | $32 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3: SITE LAYOUT <br> 8 <br> Upgraded Intersection Geometry (PHASE 1))]

Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## ANNEXURE B3.5: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=80$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & \text { 95\% B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \\ & \text { Cycles } \end{aligned}$ | Aver. Speed <br> km/h |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 211 | 0.0 | 211 | 0.0 | 0.236 | 14.7 | LOS B | 4.0 | 28.2 | 0.58 | 0.71 | 0.58 | 47.8 |
| 22 T1 | 38 | 0.0 | 38 | 0.0 | * 0.200 | 39.1 | LOS D | 1.4 | 10.1 | 0.96 | 0.70 | 0.96 | 37.0 |
| 23 R2 | 433 | 0.0 | 433 | 0.0 | * 0.661 | 27.6 | LOS C | 13.7 | 95.9 | 0.92 | 0.83 | 0.92 | 40.8 |
| Approach | 682 | 0.0 | 682 | 0.0 | 0.661 | 24.3 | LOS C | 13.7 | 95.9 | 0.82 | 0.79 | 0.82 | 42.5 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 276 | 0.0 | 276 | 0.0 | 0.195 | 7.1 | LOS A | 2.0 | 14.3 | 0.28 | 0.63 | 0.28 | 53.0 |
| 5 T1 | 684 | 0.0 | 684 | 0.0 | 0.700 | 19.0 | LOS B | 21.4 | 150.0 | 0.86 | 0.77 | 0.86 | 45.8 |
| 6 R2 | 548 | 0.0 | 548 | 0.0 | * 0.864 | 43.9 | LOS D | 15.8 | 110.5 | 0.98 | 0.92 | 1.17 | 34.7 |
| Approach | 1508 | 0.0 | 1508 | 0.0 | 0.864 | 25.9 | LOS C | 21.4 | 150.0 | 0.80 | 0.80 | 0.87 | 42.0 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 922 | 0.0 | 922 | 0.0 | 0.446 | 8.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.7 |
| 28 T1 | 38 | 0.0 | 38 | 0.0 | 0.200 | 38.3 | LOS D | 1.4 | 10.1 | 0.96 | 0.70 | 0.96 | 37.0 |
| 9 R2 | 266 | 0.0 | 266 | 0.0 | 0.406 | 25.5 | LOS C | 7.6 | 53.2 | 0.83 | 0.79 | 0.83 | 41.9 |
| Approach | 1226 | 0.0 | 1226 | 0.0 | 0.446 | 12.7 | LOS B | 7.6 | 53.2 | 0.21 | 0.59 | 0.21 | 50.6 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 120 | 0.0 | 120 | 0.0 | 0.082 | 8.9 | LOSA | 1.2 | 8.1 | 0.31 | 0.62 | 0.31 | 52.3 |
| 11 T1 | 727 | 0.0 | 727 | 0.0 | * 0.837 | 39.2 | LOS D | 15.4 | 108.0 | 1.00 | 0.99 | 1.23 | 36.6 |
| 32 R 2 | 97 | 0.0 | 97 | 0.0 | 0.445 | 37.7 | LOS D | 3.5 | 24.7 | 0.92 | 0.79 | 0.92 | 36.5 |
| Approach | 944 | 0.0 | 944 | 0.0 | 0.837 | 35.2 | LOS D | 15.4 | 108.0 | 0.90 | 0.92 | 1.08 | 38.0 |
| All <br> Vehicles | 4360 | 0.0 | 4360 | 0.0 | 0.864 | 23.9 | LOS C | 21.4 | 150.0 | 0.66 | 0.76 | 0.72 | 43.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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## ANNEXURE B3.5: PHASING SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=80$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 4
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 60 | 0 | 26 | 37 |
| Green Time (sec) | 16 | 19 | 7 | 16 |
| Phase Time (sec) | 23 | 23 | 14 | 20 |
| Phase Split | $29 \%$ | $29 \%$ | $18 \%$ | $25 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3.6: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 70 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|} \hline \text { Mov Turn } \\ \text { ID } \end{array}$ | $\begin{aligned} & \text { IN } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & \text { 95\% Bf } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 120 | 0.0 | 120 | 0.0 | 0.118 | 11.8 | LOS B | 1.7 | 11.9 | 0.50 | 0.68 | 0.50 | 49.7 |
| 22 T1 | 43 | 0.0 | 43 | 0.0 | 0.198 | 35.5 | LOS D | 1.4 | 9.9 | 0.95 | 0.70 | 0.95 | 39.2 |
| 23 R2 | 331 | 0.0 | 331 | 0.0 | * 0.860 | 40.8 | LOS D | 11.9 | 83.0 | 1.00 | 1.06 | 1.35 | 35.6 |
| Approach | 494 | 0.0 | 494 | 0.0 | 0.860 | 33.3 | LOS C | 11.9 | 83.0 | 0.87 | 0.93 | 1.11 | 38.6 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 475 | 0.0 | 475 | 0.0 | 0.364 | 9.2 | LOSA | 5.5 | 38.7 | 0.46 | 0.70 | 0.46 | 51.5 |
| $5 \quad \mathrm{~T} 1$ | 672 | 0.0 | 672 | 0.0 | 0.570 | 11.4 | LOS B | 15.2 | 106.1 | 0.71 | 0.64 | 0.71 | 50.6 |
| 6 R2 | 874 | 0.0 | 874 | 0.0 | * 0.918 | 41.0 | LOS D | 25.0 | 175.2 | 0.96 | 0.98 | 1.24 | 35.9 |
| Approach | 2021 | 0.0 | 2021 | 0.0 | 0.918 | 23.7 | LOS C | 25.0 | 175.2 | 0.76 | 0.80 | 0.88 | 43.2 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 660 | 0.0 | 660 | 0.0 | 0.319 | 6.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.8 |
| 28 T1 | 56 | 0.0 | 56 | 0.0 | * 0.258 | 33.0 | LOS C | 1.9 | 13.0 | 0.96 | 0.71 | 0.96 | 39.1 |
| 9 R2 | 206 | 0.0 | 206 | 0.0 | 0.523 | 30.7 | LOS C | 6.2 | 43.7 | 0.95 | 0.79 | 0.95 | 39.5 |
| Approach | 922 | 0.0 | 922 | 0.0 | 0.523 | 13.8 | LOS B | 6.2 | 43.7 | 0.27 | 0.60 | 0.27 | 49.4 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 338 | 0.0 | 338 | 0.0 | 0.279 | 13.7 | LOS B | 4.8 | 33.9 | 0.50 | 0.69 | 0.50 | 50.2 |
| 11 T1 | 655 | 0.0 | 655 | 0.0 | 0.812 | 34.3 | LOS C | 12.1 | 84.5 | 1.00 | 0.96 | 1.23 | 38.5 |
| 32 R 2 | 205 | 0.0 | 205 | 0.0 | * 0.911 | 53.8 | LOS D | 9.3 | 65.4 | 1.00 | 1.13 | 1.69 | 31.5 |
| Approach | 1198 | 0.0 | 1198 | 0.0 | 0.911 | 31.8 | LOS C | 12.1 | 84.5 | 0.86 | 0.91 | 1.10 | 39.6 |
| All Vehicles | 4635 | 0.0 | 4635 | 0.0 | 0.918 | 24.8 | LOS C | 25.0 | 175.2 | 0.70 | 0.80 | 0.84 | 42.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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Project: I:\PROJECTSIP0573_Sky City Townships\5 - Traffic Design \& Technical\5.3 SIDRAIK91 - Cosmopolitan Dr.sip9

## ANNEXURE B3.6: PHASING SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 70 seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 4
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 53 | 0 | 14 | 25 |
| Green Time (sec) | 13 | 7 | 7 | 21 |
| Phase Time (sec) | 20 | 11 | 14 | 25 |
| Phase Split | $29 \%$ | $16 \%$ | $20 \%$ | $36 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3.7: MOVEMENT SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & \text { 95\% B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \\ & \text { Cycles } \end{aligned}$ | Aver. Speed <br> km/h |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 214 | 0.0 | 214 | 0.0 | 0.238 | 15.6 | LOS B | 4.6 | 31.9 | 0.57 | 0.71 | 0.57 | 47.2 |
| 22 T1 | 40 | 0.0 | 40 | 0.0 | *0.237 | 45.2 | LOS D | 1.7 | 12.1 | 0.97 | 0.71 | 0.97 | 35.0 |
| 23 R2 | 433 | 0.0 | 433 | 0.0 | * 0.701 | 31.9 | LOS C | 15.9 | 111.2 | 0.94 | 0.84 | 0.95 | 38.9 |
| Approach | 687 | 0.0 | 687 | 0.0 | 0.701 | 27.6 | LOS C | 15.9 | 111.2 | 0.83 | 0.80 | 0.83 | 40.9 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 276 | 0.0 | 276 | 0.0 | 0.192 | 7.2 | LOS A | 2.2 | 15.3 | 0.26 | 0.63 | 0.26 | 53.0 |
| 5 T1 | 707 | 0.0 | 707 | 0.0 | 0.686 | 18.6 | LOS B | 23.4 | 163.6 | 0.82 | 0.73 | 0.82 | 46.0 |
| 6 R2 | 661 | 0.0 | 661 | 0.0 | * 0.852 | 44.5 | LOS D | 20.6 | 144.0 | 0.97 | 0.90 | 1.10 | 34.6 |
| Approach | 1644 | 0.0 | 1644 | 0.0 | 0.852 | 27.1 | LOS C | 23.4 | 163.6 | 0.78 | 0.78 | 0.84 | 41.4 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1151 | 0.0 | 1151 | 0.0 | 0.556 | 9.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.6 |
| 28 T1 | 39 | 0.0 | 39 | 0.0 | 0.231 | 44.0 | LOS D | 1.7 | 11.8 | 0.97 | 0.71 | 0.97 | 35.0 |
| 9 R2 | 281 | 0.0 | 281 | 0.0 | 0.451 | 29.5 | LOS C | 9.4 | 65.5 | 0.86 | 0.80 | 0.86 | 40.1 |
| Approach | 1471 | 0.0 | 1471 | 0.0 | 0.556 | 14.5 | LOS B | 9.4 | 65.5 | 0.19 | 0.58 | 0.19 | 50.4 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 124 | 0.0 | 124 | 0.0 | 0.089 | 10.3 | LOS B | 1.5 | 10.7 | 0.34 | 0.63 | 0.34 | 51.5 |
| 11 T1 | 739 | 0.0 | 739 | 0.0 | * 0.858 | 45.0 | LOS D | 18.0 | 126.2 | 1.00 | 1.01 | 1.25 | 34.6 |
| 32 R2 | 97 | 0.0 | 97 | 0.0 | 0.471 | 41.8 | LOS D | 4.0 | 27.9 | 0.93 | 0.79 | 0.93 | 35.1 |
| Approach | 960 | 0.0 | 960 | 0.0 | 0.858 | 40.2 | LOS D | 18.0 | 126.2 | 0.91 | 0.94 | 1.10 | 36.2 |
| All <br> Vehicles | 4762 | 0.0 | 4762 | 0.0 | 0.858 | 25.9 | LOS C | 23.4 | 163.6 | 0.63 | 0.75 | 0.69 | 42.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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## ANNEXURE B3.7: PHASING SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 4
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 68 | 0 | 28 | 39 |
| Green Time (sec) | 18 | 21 | 7 | 22 |
| Phase Time (sec) | 25 | 25 | 14 | 26 |
| Phase Split | $28 \%$ | $28 \%$ | $16 \%$ | $29 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than 100\%.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3.8: MOVEMENT SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|} \hline \text { Mov Turn } \\ \text { ID } \end{array}$ | $\begin{aligned} & \text { IN } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & \text { 95\% Bf } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 120 | 0.0 | 120 | 0.0 | 0.128 | 15.8 | LOS B | 2.8 | 19.3 | 0.49 | 0.67 | 0.49 | 47.1 |
| 22 T1 | 45 | 0.0 | 45 | 0.0 | 0.311 | 56.3 | LOS E | 2.3 | 16.2 | 0.99 | 0.73 | 0.99 | 32.3 |
| 23 R2 | 331 | 0.0 | 331 | 0.0 | * 0.872 | 55.1 | LOS E | 17.7 | 124.2 | 1.00 | 0.98 | 1.27 | 31.3 |
| Approach | 496 | 0.0 | 496 | 0.0 | 0.872 | 45.7 | LOS D | 17.7 | 124.2 | 0.88 | 0.88 | 1.05 | 34.2 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 475 | 0.0 | 475 | 0.0 | 0.323 | 6.7 | LOS A | 3.7 | 25.7 | 0.24 | 0.63 | 0.24 | 53.3 |
| $5 \quad \mathrm{~T} 1$ | 684 | 0.0 | 684 | 0.0 | * 1.149 | 192.6 | LOS F | 80.3 | 562.2 | 1.00 | 1.97 | 2.42 | 14.2 |
| 6 R2 | 1063 | 0.0 | 1063 | 0.0 | * 1.158 | 144.6 | LOS F | 80.3 | 561.8 | 0.97 | 1.29 | 1.89 | 17.6 |
| Approach | 2222 | 0.0 | 2222 | 0.0 | 1.158 | 129.9 | LOS F | 80.3 | 562.2 | 0.82 | 1.36 | 1.70 | 18.9 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 763 | 0.0 | 763 | 0.0 | 0.369 | 7.2 | LOSA | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.8 |
| 28 T1 | 59 | 0.0 | 59 | 0.0 | * 0.407 | 53.4 | LOS D | 3.1 | 21.4 | 1.00 | 0.74 | 1.00 | 32.2 |
| 9 R2 | 216 | 0.0 | 216 | 0.0 | 0.555 | 43.7 | LOS D | 9.7 | 68.1 | 0.96 | 0.81 | 0.96 | 34.7 |
| Approach | 1038 | 0.0 | 1038 | 0.0 | 0.555 | 17.4 | LOS B | 9.7 | 68.1 | 0.26 | 0.60 | 0.26 | 47.3 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 357 | 0.0 | 357 | 0.0 | 0.290 | 18.9 | LOS B | 8.5 | 59.7 | 0.52 | 0.70 | 0.52 | 47.3 |
| 11 T1 | 677 | 0.0 | 677 | 0.0 | 0.564 | 35.2 | LOS D | 14.9 | 104.4 | 0.91 | 0.78 | 0.91 | 38.1 |
| 32 R 2 | 207 | 0.0 | 207 | 0.0 | 0.281 | 19.7 | LOS B | 4.4 | 30.5 | 0.76 | 0.75 | 0.76 | 44.5 |
| Approach | 1241 | 0.0 | 1241 | 0.0 | 0.564 | 27.9 | LOS C | 14.9 | 104.4 | 0.77 | 0.75 | 0.77 | 41.4 |
| All Vehicles | 4997 | 0.0 | 4997 | 0.0 | 1.158 | 72.9 | LOS E | 80.3 | 562.2 | 0.70 | 1.00 | 1.11 | 27.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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## ANNEXURE B3.8: PHASING SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder:

Upgraded Intersection Geometry (PHASE 1))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 3
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 72 | 0 | 21 | 32 |
| Green Time (sec) | 29 | 14 | 7 | 33 |
| Phase Time (sec) | 36 | 18 | 14 | 37 |
| Phase Split | $34 \%$ | $17 \%$ | $13 \%$ | $35 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3: SITE LAYOUT <br> 8 <br> Upgraded Intersection Geometry (PHASE 2))]

Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## ANNEXURE B3.9: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: <br> Upgraded Intersection Geometry (PHASE 2))]

Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{gathered} \text { JT } \\ \text { VES } \\ \text { HV ] } \\ \% \end{gathered}$ | $\begin{aligned} & \text { DEN } \\ & \text { FL( } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{gathered} \text { ND } \\ \text { NS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { EUE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 214 | 0.0 | 214 | 0.0 | 0.216 | 12.4 | LOS B | 4.2 | 29.5 | 0.43 | 0.67 | 0.43 | 49.3 |
| 22 T1 | 40 | 0.0 | 40 | 0.0 | * 0.289 | 56.4 | LOS E | 2.2 | 15.1 | 0.99 | 0.72 | 0.99 | 31.6 |
| 23 R2 | 487 | 0.0 | 487 | 0.0 | * 0.786 | 40.5 | LOS D | 23.2 | 162.4 | 0.97 | 0.88 | 1.02 | 35.9 |
| Approach | 741 | 0.0 | 741 | 0.0 | 0.786 | 33.2 | LOS C | 23.2 | 162.4 | 0.81 | 0.81 | 0.85 | 38.7 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 297 | 0.0 | 297 | 0.0 | 0.196 | 6.2 | LOS A | 1.4 | 9.9 | 0.16 | 0.60 | 0.16 | 53.7 |
| 5 T1 | 895 | 0.0 | 895 | 0.0 | 0.671 | 36.3 | LOS D | 21.0 | 147.2 | 0.94 | 0.81 | 0.94 | 37.7 |
| 6 R2 | 661 | 0.0 | 661 | 0.0 | * 0.953 | 68.6 | LOS E | 24.6 | 172.4 | 1.00 | 1.00 | 1.33 | 28.2 |
| Approach | 1853 | 0.0 | 1853 | 0.0 | 0.953 | 43.0 | LOS D | 24.6 | 172.4 | 0.84 | 0.84 | 0.95 | 35.1 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1151 | 0.0 | 1151 | 0.0 | 0.556 | 22.8 | LOS C | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.6 |
| 28 T1 | 39 | 0.0 | 39 | 0.0 | 0.282 | 55.5 | LOS E | 2.1 | 14.7 | 0.99 | 0.72 | 0.99 | 31.6 |
| 9 R2 | 281 | 0.0 | 281 | 0.0 | 0.441 | 34.4 | LOS C | 11.3 | 79.2 | 0.85 | 0.80 | 0.85 | 38.0 |
| Approach | 1471 | 0.0 | 1471 | 0.0 | 0.556 | 25.9 | LOS C | 11.3 | 79.2 | 0.19 | 0.58 | 0.19 | 49.6 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 124 | 0.0 | 124 | 0.0 | 0.081 | 9.7 | LOS A | 1.6 | 11.2 | 0.29 | 0.62 | 0.29 | 51.8 |
| 11 T1 | 1187 | 0.0 | 1187 | 0.0 | * 0.964 | 69.6 | LOS E | 42.1 | 295.0 | 1.00 | 1.22 | 1.43 | 28.1 |
| 32 R 2 | 97 | 0.0 | 97 | 0.0 | 0.190 | 23.2 | LOS C | 2.7 | 18.6 | 0.77 | 0.74 | 0.77 | 42.9 |
| Approach | 1408 | 0.0 | 1408 | 0.0 | 0.964 | 61.1 | LOS E | 42.1 | 295.0 | 0.92 | 1.13 | 1.28 | 30.0 |
| All <br> Vehicles | 5473 | 0.0 | 5473 | 0.0 | 0.964 | 41.7 | LOS D | 42.1 | 295.0 | 0.68 | 0.84 | 0.82 | 36.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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Project: I:\PROJECTSIP0573_Sky City Townships\5 - Traffic Design \& Technical\5.3 SIDRAIK91 - Cosmopolitan Dr.sip9

## ANNEXURE B3.9: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder:

Upgraded Intersection Geometry (PHASE 2))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 110 seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 3
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 73 | 0 | 35 | 46 |
| Green Time (sec) | 33 | 28 | 7 | 20 |
| Phase Time (sec) | 40 | 32 | 14 | 24 |
| Phase Split | $36 \%$ | $29 \%$ | $13 \%$ | $22 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B3.10: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: <br> Upgraded Intersection Geometry (PHASE 2))]

Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|l\|} \hline \text { Mov Turn } \\ \text { ID } \end{array}$ | $\begin{aligned} & \text { IN } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{aligned} & \text { 95\% Bf } \\ & \text { QUE } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 120 | 0.0 | 120 | 0.0 | 0.121 | 14.3 | LOS B | 2.5 | 17.6 | 0.46 | 0.66 | 0.46 | 48.1 |
| 22 T1 | 45 | 0.0 | 45 | 0.0 | 0.311 | 57.0 | LOS E | 2.3 | 16.2 | 0.99 | 0.73 | 0.99 | 32.4 |
| 23 R2 | 352 | 0.0 | 352 | 0.0 | * 0.778 | 44.9 | LOS D | 16.9 | 118.2 | 1.00 | 0.89 | 1.09 | 34.4 |
| Approach | 517 | 0.0 | 517 | 0.0 | 0.778 | 38.9 | LOS D | 16.9 | 118.2 | 0.87 | 0.82 | 0.93 | 36.6 |
| NorthEast: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 522 | 0.0 | 522 | 0.0 | 0.352 | 6.7 | LOSA | 4.2 | 29.5 | 0.24 | 0.62 | 0.24 | 53.3 |
| $5 \quad \mathrm{~T} 1$ | 1069 | 0.0 | 1069 | 0.0 | * 0.971 | 72.2 | LOS E | 40.2 | 281.5 | 1.00 | 1.24 | 1.50 | 27.5 |
| 6 R2 | 1063 | 0.0 | 1063 | 0.0 | * 0.975 | 67.0 | LOS E | 41.2 | 288.6 | 1.00 | 1.02 | 1.32 | 28.9 |
| Approach | 2654 | 0.0 | 2654 | 0.0 | 0.975 | 57.2 | LOS E | 41.2 | 288.6 | 0.85 | 1.03 | 1.18 | 31.1 |
| NorthWest: Cosmopolitan Dr |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 763 | 0.0 | 763 | 0.0 | 0.369 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.53 | 0.00 | 54.8 |
| 28 T1 | 59 | 0.0 | 59 | 0.0 | * 0.407 | 53.4 | LOS D | 3.1 | 21.4 | 1.00 | 0.74 | 1.00 | 32.2 |
| 9 R2 | 216 | 0.0 | 216 | 0.0 | 0.462 | 39.6 | LOS D | 9.1 | 63.9 | 0.92 | 0.80 | 0.92 | 36.1 |
| Approach | 1038 | 0.0 | 1038 | 0.0 | 0.462 | 17.1 | LOS B | 9.1 | 63.9 | 0.25 | 0.60 | 0.25 | 47.8 |
| SouthWest: K91 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 357 | 0.0 | 357 | 0.0 | 0.275 | 17.8 | LOS B | 7.7 | 54.0 | 0.48 | 0.69 | 0.48 | 48.5 |
| 11 T1 | 854 | 0.0 | 854 | 0.0 | 0.760 | 39.3 | LOS D | 21.9 | 153.1 | 0.97 | 0.87 | 1.02 | 36.6 |
| 32 R 2 | 207 | 0.0 | 207 | 0.0 | 0.309 | 21.5 | LOS C | 4.8 | 33.8 | 0.80 | 0.75 | 0.80 | 43.7 |
| Approach | 1418 | 0.0 | 1418 | 0.0 | 0.760 | 31.3 | LOS C | 21.9 | 153.1 | 0.82 | 0.81 | 0.85 | 40.0 |
| All Vehicles | 5627 | 0.0 | 5627 | 0.0 | 0.975 | 41.6 | LOS D | 41.2 | 288.6 | 0.73 | 0.88 | 0.90 | 35.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)


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## ANNEXURE B3.10: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder:

Upgraded Intersection Geometry (PHASE 2))]
Future 2026 Base Peak Hour Traffic Volumes + Palm Ridge Ext. 10, 12 \& 13 Trips + Watervalspruit Ext. 54 Trips + Watervalspruit Service Plan Stage 2 Remaining Trips + Estimated Total Development Trips
Site Category: -
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 3
Reference Phase: Phase B
Input Phase Sequence: A, B, C, D
Output Phase Sequence: A, B, C, D

## Phase Timing Summary

| Phase | A | B | C | D |
| :--- | :---: | :---: | :---: | :---: |
| Phase Change Time (sec) | 73 | 0 | 25 | 36 |
| Green Time (sec) | 28 | 18 | 7 | 30 |
| Phase Time (sec) | 35 | 22 | 14 | 34 |
| Phase Split | $33 \%$ | $21 \%$ | $13 \%$ | $32 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.

## Output Phase Sequence

Phase A

REF: Reference Phase
VAR: Variable Phase

## ANNEXURE B4: SITE LAYOUT

目
Proposed Intersection Geometry (PHASE 1)
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
1 N


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## ANNEXURE B4.1: MOVEMENT SUMMARY

## 慁ite: [Scenario 2 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 342 | 0.0 | 342 | 0.0 | 0.774 | 25.6 | Los C | 9.5 | 66.7 | 1.00 | 0.98 | 1.21 | 41.9 |
| 2 T1 | 54 | 0.0 | 54 | 0.0 | 0.186 | 26.0 | LOS C | 1.5 | 10.3 | 0.92 | 0.69 | 0.92 | 42.1 |
| 3 R 2 | 72 | 0.0 | 72 | 0.0 | 0.276 | 32.2 | LOS C | 2.0 | 14.0 | 0.94 | 0.75 | 0.94 | 38.7 |
| Approach | 468 | 0.0 | 468 | 0.0 | 0.774 | 26.7 | LOS C | 9.5 | 66.7 | 0.98 | 0.91 | 1.13 | 41.4 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 35 | 0.0 | 35 | 0.0 | 0.029 | 8.4 | LOSA | 0.3 | 1.9 | 0.41 | 0.63 | 0.41 | 52.1 |
| 5 T1 | 1114 | 0.0 | 1114 | 0.0 | 0.791 | 9.6 | LOSA | 24.9 | 174.3 | 0.78 | 0.74 | 0.81 | 51.9 |
| 6 R2 | 119 | 0.0 | 119 | 0.0 | 0.300 | 16.8 | LOS B | 2.3 | 15.9 | 0.66 | 0.74 | 0.66 | 46.2 |
| Approach | 1268 | 0.0 | 1268 | 0.0 | 0.791 | 10.2 | LOS B | 24.9 | 174.3 | 0.76 | 0.74 | 0.79 | 51.3 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 152 | 0.0 | 152 | 0.0 | 0.230 | 9.5 | LOS A | 1.6 | 11.0 | 0.51 | 0.69 | 0.51 | 51.3 |
| 8 T1 | 26 | 0.0 | 26 | 0.0 | 0.090 | 25.5 | LOS C | 0.7 | 4.9 | 0.91 | 0.65 | 0.91 | 42.3 |
| 9 R2 | 94 | 0.0 | 94 | 0.0 | * 0.390 | 33.7 | LOS C | 2.7 | 19.0 | 0.97 | 0.76 | 0.97 | 38.1 |
| Approach | 272 | 0.0 | 272 | 0.0 | 0.390 | 19.4 | LOS B | 2.7 | 19.0 | 0.71 | 0.71 | 0.71 | 45.0 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{ll} 10 & L \\ 11 & T \\ 12 & \mathrm{~F} \end{array}$ | 31 | 0.0 | 31 | 0.0 | 0.026 | 7.3 | LOS A | 0.2 | 1.2 | 0.33 | 0.61 | 0.33 | 52.9 |
|  | 747 | 0.0 | 747 | 0.0 | 0.529 | 6.0 | LOS A | 11.6 | 81.5 | 0.57 | 0.52 | 0.57 | 54.6 |
|  | 143 | 0.0 | 143 | 0.0 | * 0.686 | 30.7 | LOS C | 4.4 | 30.7 | 0.94 | 0.90 | 1.15 | 39.3 |
| Approach | 921 | 0.0 | 921 | 0.0 | 0.686 | 9.9 | LOS A | 11.6 | 81.5 | 0.62 | 0.58 | 0.66 | 51.4 |
| All <br> Vehicles |  |  | 2929 | 0.0 | 0.791 | 13.6 | LOS B | 24.9 | 174.3 | 0.75 | 0.71 | 0.79 | 48.8 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.1: PHASING SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 15 | 0 |
| Green Time (sec) | 39 | 8 |
| Phase Time (sec) | 46 | 14 |
| Phase Split | $77 \%$ | $23 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

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## ANNEXURE B4.2: MOVEMENT SUMMARY

## 慁ite: [Scenario 2 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=95$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { IT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. <br> veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 134 | 0.0 | 134 | 0.0 | 0.176 | 8.8 | LOS A | 1.6 | 11.2 | 0.36 | 0.65 | 0.36 | 51.8 |
| 2 T1 | 21 | 0.0 | 21 | 0.0 | 0.131 | 46.2 | LOS D | 0.9 | 6.6 | 0.97 | 0.68 | 0.97 | 34.2 |
| 3 R 2 | 28 | 0.0 | 28 | 0.0 | 0.217 | 53.8 | LOS D | 1.3 | 9.1 | 0.98 | 0.71 | 0.98 | 31.5 |
| Approach | 183 | 0.0 | 183 | 0.0 | 0.217 | 20.0 | LOS B | 1.6 | 11.2 | 0.53 | 0.67 | 0.53 | 44.8 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 58 | 0.0 | 58 | 0.0 | 0.052 | 8.1 | LOS A | 0.5 | 3.5 | 0.33 | 0.62 | 0.33 | 52.3 |
| 5 T1 | 750 | 0.0 | 750 | 0.0 | 0.512 | 8.2 | LOSA | 17.0 | 119.2 | 0.54 | 0.49 | 0.54 | 52.9 |
| 6 R2 | 150 | 0.0 | 150 | 0.0 | 0.480 | 20.8 | LOS C | 4.3 | 30.1 | 0.84 | 0.80 | 0.84 | 43.9 |
| Approach | 958 | 0.0 | 958 | 0.0 | 0.512 | 10.2 | LOS B | 17.0 | 119.2 | 0.57 | 0.55 | 0.57 | 51.2 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 123 | 0.0 | 123 | 0.0 | 0.228 | 17.2 | LOS B | 3.1 | 21.8 | 0.63 | 0.73 | 0.63 | 46.4 |
| 8 T1 | 44 | 0.0 | 44 | 0.0 | * 0.275 | 47.1 | LOS D | 2.0 | 14.2 | 0.98 | 0.72 | 0.98 | 33.9 |
| 9 R2 | 37 | 0.0 | 37 | 0.0 | 0.254 | 52.8 | LOS D | 1.7 | 12.0 | 0.98 | 0.72 | 0.98 | 31.8 |
| Approach | 204 | 0.0 | 204 | 0.0 | 0.275 | 30.1 | LOS C | 3.1 | 21.8 | 0.77 | 0.73 | 0.77 | 39.9 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 88 | 0.0 | 88 | 0.0 | 0.067 | 8.2 | LOS A | 0.8 | 5.9 | 0.33 | 0.63 | 0.33 | 52.3 |
| 11 T1 | 1141 | 0.0 | 1141 | 0.0 | * 0.820 | 11.3 | LOS B | 35.8 | 250.7 | 0.75 | 0.70 | 0.75 | 50.6 |
| 12 R 2 | 295 | 0.0 | 295 | 0.0 | * 0.563 | 12.3 | LOS B | 5.0 | 34.9 | 0.64 | 0.76 | 0.64 | 48.9 |
| Approach | 1524 | 0.0 | 1524 | 0.0 | 0.820 | 11.3 | LOS B | 35.8 | 250.7 | 0.70 | 0.70 | 0.70 | 50.4 |
| All Vehicles | 2869 | 0.0 | 2869 | 0.0 | 0.820 |  | LOS B | 35.8 | 250.7 | 0.65 | 0.65 | 0.65 | 49.3 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.2: PHASING SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=95$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 27 | 0 | 14 |
| Green Time (sec) | 64 | 7 | 7 |
| Phase Time (sec) | 71 | 13 | 11 |
| Phase Split | $75 \%$ | $14 \%$ | $12 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

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## ANNEXURE B4.3: MOVEMENT SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn $\qquad$ v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 342 | 0.0 | 342 | 0.0 | 0.821 | 30.8 | LOS C | 10.2 | 71.2 | 1.00 | 1.04 | 1.31 | 39.6 |
| 2 T1 | 54 | 0.0 | 54 | 0.0 | 0.186 | 26.0 | LOS C | 1.5 | 10.3 | 0.92 | 0.69 | 0.92 | 42.1 |
| 3 R2 | 72 | 0.0 | 72 | 0.0 | 0.276 | 32.2 | LOS C | 2.0 | 14.0 | 0.94 | 0.75 | 0.94 | 38.7 |
| Approach | 468 | 0.0 | 468 | 0.0 | 0.821 | 30.5 | LOS C | 10.2 | 71.2 | 0.98 | 0.95 | 1.21 | 39.7 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 35 | 0.0 | 35 | 0.0 | 0.028 | 8.4 | LOS A | 0.3 | 1.9 | 0.41 | 0.63 | 0.41 | 52.1 |
| 5 T1 | 1178 | 0.0 | 1178 | 0.0 | 0.842 | 13.2 | LOS B | 31.0 | 216.9 | 0.83 | 0.85 | 0.93 | 49.3 |
| 6 R2 | 119 | 0.0 | 119 | 0.0 | 0.353 | 18.5 | LOS B | 2.5 | 17.3 | 0.71 | 0.76 | 0.71 | 45.2 |
| Approach | 1332 | 0.0 | 1332 | 0.0 | 0.842 | 13.6 | LOS B | 31.0 | 216.9 | 0.81 | 0.83 | 0.90 | 49.0 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 152 | 0.0 | 152 | 0.0 | 0.255 | 10.4 | LOS B | 1.8 | 12.6 | 0.56 | 0.71 | 0.56 | 50.7 |
| 8 T1 | 26 | 0.0 | 26 | 0.0 | 0.090 | 25.5 | LOS C | 0.7 | 4.9 | 0.91 | 0.65 | 0.91 | 42.3 |
| 9 R2 | 94 | 0.0 | 94 | 0.0 | * 0.390 | 33.7 | LOS C | 2.7 | 19.0 | 0.97 | 0.76 | 0.97 | 38.1 |
| Approach | 272 | 0.0 | 272 | 0.0 | 0.390 | 19.9 | LOS B | 2.7 | 19.0 | 0.73 | 0.72 | 0.73 | 44.7 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 31 | 0.0 | 31 | 0.0 | 0.026 | 7.5 | LOS A | 0.2 | 1.3 | 0.35 | 0.62 | 0.35 | 52.8 |
| 11 T1 | 841 | 0.0 | 841 | 0.0 | 0.596 | 6.4 | LOS A | 14.0 | 98.3 | 0.62 | 0.56 | 0.62 | 54.3 |
| 12 R 2 | 143 | 0.0 | 143 | 0.0 | * 0.759 | 35.3 | LOS D | 4.8 | 33.5 | 0.98 | 0.96 | 1.33 | 37.4 |
| Approach | 1015 | 0.0 | 1015 | 0.0 | 0.759 | 10.5 | LOS B | 14.0 | 98.3 | 0.66 | 0.62 | 0.71 | 51.0 |
| All Vehicles | 3087 | 0.0 | 3087 | 0.0 | 0.842 |  | LOS B | 31.0 | 216.9 | 0.78 | 0.77 | 0.87 | 47.5 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.3: PHASING SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder: Proposed Intersection Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 15 | 0 |
| Green Time (sec) | 39 | 8 |
| Phase Time (sec) | 46 | 14 |
| Phase Split | $77 \%$ | $23 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B4.4: MOVEMENT SUMMARY

## 慁ite: [Scenario 3 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { IT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. <br> veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 134 | 0.0 | 134 | 0.0 | 0.190 | 9.5 | LOS A | 2.0 | 13.8 | 0.37 | 0.66 | 0.37 | 51.3 |
| 2 T1 | 21 | 0.0 | 21 | 0.0 | 0.152 | 54.7 | LOS D | 1.1 | 7.8 | 0.98 | 0.68 | 0.98 | 31.7 |
| 3 R 2 | 28 | 0.0 | 28 | 0.0 | 0.261 | 63.5 | LOS E | 1.5 | 10.8 | 1.00 | 0.71 | 1.00 | 29.1 |
| Approach | 183 | 0.0 | 183 | 0.0 | 0.261 | 22.9 | LOS C | 2.0 | 13.8 | 0.53 | 0.67 | 0.53 | 43.2 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 58 | 0.0 | 58 | 0.0 | 0.054 | 9.5 | LOS A | 0.7 | 5.1 | 0.37 | 0.63 | 0.37 | 51.4 |
| 5 T1 | 830 | 0.0 | 830 | 0.0 | 0.546 | 8.4 | LOSA | 21.2 | 148.2 | 0.53 | 0.48 | 0.53 | 52.7 |
| 6 R2 | 150 | 0.0 | 150 | 0.0 | 0.487 | 24.5 | LOS C | 5.6 | 39.0 | 0.88 | 0.82 | 0.88 | 42.1 |
| Approach | 1038 | 0.0 | 1038 | 0.0 | 0.546 | 10.8 | LOS B | 21.2 | 148.2 | 0.57 | 0.54 | 0.57 | 50.8 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 123 | 0.0 | 123 | 0.0 | 0.245 | 20.2 | LOS C | 3.9 | 27.2 | 0.66 | 0.75 | 0.66 | 44.7 |
| 8 T1 | 44 | 0.0 | 44 | 0.0 | * 0.318 | 55.7 | LOS E | 2.4 | 16.6 | 0.99 | 0.73 | 0.99 | 31.4 |
| 9 R2 | 37 | 0.0 | 37 | 0.0 | 0.299 | 62.4 | LOS E | 2.0 | 14.1 | 0.99 | 0.72 | 0.99 | 29.3 |
| Approach | 204 | 0.0 | 204 | 0.0 | 0.318 | 35.5 | LOS D | 3.9 | 27.2 | 0.79 | 0.74 | 0.79 | 37.7 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 88 | 0.0 | 88 | 0.0 | 0.070 | 10.0 | LOS A | 1.2 | 8.6 | 0.37 | 0.64 | 0.37 | 51.0 |
| 11 T1 | 1205 | 0.0 | 1205 | 0.0 | * 0.838 | 11.7 | LOS B | 42.7 | 299.0 | 0.74 | 0.69 | 0.74 | 50.3 |
| 12 R 2 | 295 | 0.0 | 295 | 0.0 | * 0.594 | 13.5 | LOS B | 6.7 | 47.1 | 0.66 | 0.77 | 0.66 | 48.2 |
| Approach | 1588 | 0.0 | 1588 | 0.0 | 0.838 | 12.0 | LOS B | 42.7 | 299.0 | 0.70 | 0.70 | 0.70 | 50.0 |
| All <br> Vehicles | 3013 | 0.0 | 3013 | 0.0 | 0.838 |  | LOS B | 42.7 | 299.0 | 0.65 | 0.65 | 0.65 | 48.7 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.4: PHASING SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 29 | 0 | 14 |
| Green Time (sec) | 77 | 7 | 9 |
| Phase Time (sec) | 84 | 13 | 13 |
| Phase Split | $76 \%$ | $12 \%$ | $12 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

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## ANNEXURE B4.5: MOVEMENT SUMMARY

## 目ite: [Scenario 4 AM (Site Folder: Proposed Intersection

Geometry (PHASE 1))]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { IT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh. <br> veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 493 | 0.0 | 493 | 0.0 | 1.244 | 254.0 | LOS F | 65.4 | 457.9 | 1.00 | 1.53 | 2.88 | 10.3 |
| 2 T1 | 108 | 0.0 | 108 | 0.0 | 0.684 | 57.3 | LOS E | 6.0 | 42.3 | 1.00 | 0.82 | 1.11 | 30.9 |
| 3 R 2 | 82 | 0.0 | 82 | 0.0 | 0.688 | 65.2 | LOS E | 4.7 | 32.8 | 1.00 | 0.81 | 1.14 | 28.7 |
| Approach | 683 | 0.0 | 683 | 0.0 | 1.244 | 200.3 | LOS F | 65.4 | 457.9 | 1.00 | 1.33 | 2.39 | 12.6 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 38 | 0.0 | 38 | 0.0 | 0.023 | 7.0 | LOSA | 0.3 | 2.0 | 0.21 | 0.59 | 0.21 | 53.2 |
| 5 T1 | 1876 | 0.0 | 1876 | 0.0 | * 1.236 | 254.7 | LOS F | 277.4 | 1941.6 | 1.00 | 2.32 | 2.71 | 11.5 |
| 6 R2 | 119 | 0.0 | 119 | 0.0 | 0.383 | 17.8 | LOS B | 3.2 | 22.1 | 0.70 | 0.76 | 0.70 | 45.6 |
| Approach | 2033 | 0.0 | 2033 | 0.0 | 1.236 | 236.2 | LOS F | 277.4 | 1941.6 | 0.97 | 2.20 | 2.55 | 12.2 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 152 | 0.0 | 152 | 0.0 | 0.307 | 16.4 | LOS B | 4.1 | 28.9 | 0.62 | 0.74 | 0.62 | 46.9 |
| 8 T1 | 47 | 0.0 | 47 | 0.0 | 0.297 | 54.3 | LOS D | 2.5 | 17.5 | 0.98 | 0.73 | 0.98 | 31.7 |
| 9 R2 | 94 | 0.0 | 94 | 0.0 | *1.213 | 254.6 | LOS F | 12.5 | 87.4 | 1.00 | 1.37 | 2.90 | 11.2 |
| Approach | 293 | 0.0 | 293 | 0.0 | 1.213 | 98.9 | LOS F | 12.5 | 87.4 | 0.80 | 0.94 | 1.41 | 22.3 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 31 | 0.0 | 31 | 0.0 | 0.024 | 7.9 | LOS A | 0.3 | 1.8 | 0.29 | 0.61 | 0.29 | 52.6 |
| 11 T1 | 1109 | 0.0 | 1109 | 0.0 | 0.732 | 10.0 | LOS B | 34.7 | 242.6 | 0.65 | 0.60 | 0.65 | 51.5 |
| 12 R 2 | 203 | 0.0 | 203 | 0.0 | * 0.951 | 71.5 | LOS E | 11.1 | 77.8 | 1.00 | 1.13 | 1.58 | 27.3 |
| Approach | 1343 | 0.0 | 1343 | 0.0 | 0.951 | 19.3 | LOS B | 34.7 | 242.6 | 0.69 | 0.68 | 0.78 | 45.5 |
| All <br> Vehicles | 4352 | 0.0 | 4352 | 0.0 | 1.244 | 154.4 | LOS F | 277.4 | 1941.6 | 0.88 | 1.51 | 1.90 | 16.5 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.5: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 28 | 0 | 15 |
| Green Time (sec) | 78 | 8 | 7 |
| Phase Time (sec) | 85 | 14 | 11 |
| Phase Split | $77 \%$ | $13 \%$ | $10 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

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## ANNEXURE B4.6: MOVEMENT SUMMARY

## 目ite: [Scenario 4 PM (Site Folder: Proposed Intersection

Geometry (PHASE 1))]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh <br> [ Veh. <br> veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 194 | 0.0 | 194 | 0.0 | 0.359 | 17.9 | LOS B | 6.1 | 42.5 | 0.67 | 0.77 | 0.67 | 46.0 |
| 2 T1 | 42 | 0.0 | 42 | 0.0 | 0.304 | 55.6 | LOS E | 2.3 | 15.8 | 0.99 | 0.72 | 0.99 | 31.4 |
| 3 R 2 | 32 | 0.0 | 32 | 0.0 | 0.425 | 67.1 | LOS E | 1.8 | 12.8 | 1.00 | 0.70 | 1.00 | 28.2 |
| Approach | 268 | 0.0 | 268 | 0.0 | 0.425 | 29.7 | LOS C | 6.1 | 42.5 | 0.76 | 0.75 | 0.76 | 40.1 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 67 | 0.0 | 67 | 0.0 | 0.080 | 18.7 | LOS B | 1.6 | 11.0 | 0.66 | 0.69 | 0.66 | 45.5 |
| 5 T1 | 1106 | 0.0 | 1106 | 0.0 | 0.759 | 10.6 | LOS B | 35.6 | 248.9 | 0.67 | 0.62 | 0.67 | 51.1 |
| 6 R2 | 150 | 0.0 | 150 | 0.0 | 0.597 | 47.1 | LOS D | 6.5 | 45.8 | 0.99 | 0.84 | 0.99 | 33.4 |
| Approach | 1323 | 0.0 | 1323 | 0.0 | 0.759 | 15.2 | LOS B | 35.6 | 248.9 | 0.70 | 0.65 | 0.70 | 47.9 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 123 | 0.0 | 123 | 0.0 | 0.285 | 40.8 | LOS D | 5.3 | 37.4 | 0.85 | 0.76 | 0.85 | 35.8 |
| 8 T1 | 91 | 0.0 | 91 | 0.0 | * 0.658 | 58.1 | LOS E | 5.1 | 35.8 | 1.00 | 0.81 | 1.10 | 30.7 |
| 9 R2 | 37 | 0.0 | 37 | 0.0 | 0.340 | 63.8 | LOS E | 2.0 | 14.3 | 1.00 | 0.72 | 1.00 | 29.0 |
| Approach | 251 | 0.0 | 251 | 0.0 | 0.658 | 50.4 | LOS D | 5.3 | 37.4 | 0.93 | 0.77 | 0.96 | 32.7 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{ll} 10 & L \\ 11 & T \\ 12 & \mathrm{~F} \end{array}$ | 88 | 0.0 | 88 | 0.0 | 0.052 | 6.6 | LOS A | 0.6 | 3.9 | 0.19 | 0.60 | 0.19 | 53.5 |
|  | 1826 | 0.0 | 1826 | 0.0 | * 1.243 | 261.7 | LOS F | 273.4 | 1913.8 | 1.00 | 2.35 | 2.75 | 11.2 |
|  | 428 | 0.0 | 428 | 0.0 | *1.243 | 278.6 | LOS F | 61.0 | 426.7 | 1.00 | 1.73 | 2.94 | 10.1 |
| Approach | 2342 | 0.0 | 2342 | 0.0 | 1.243 | 255.2 | LOS F | 273.4 | 1913.8 | 0.97 | 2.17 | 2.69 | 11.3 |
| All Vehicles |  |  | 4184 | 0.0 | 1.243 | 152.6 | LOS F | $273.4 \quad 1913.8$ |  | 0.87 | 1.51 | 1.83 | 16.8 |

Site Level of Service (LOS) Method: Delay \& v/C (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.6: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 29 | 0 | 14 |
| Green Time (sec) | 77 | 7 | 9 |
| Phase Time (sec) | 84 | 13 | 13 |
| Phase Split | $76 \%$ | $12 \%$ | $12 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs
Other Movement Class (MC) Stopped

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## ANNEXURE B4: SITE LAYOUT

8
Proposed Intersection Geometry (PHASE 2)
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
"


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## ANNEXURE B4.7: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 75 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | UT <br> MES <br> HV ] <br> \% | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L 2 | 493 | 0.0 | 493 | 0.0 | 0.805 | 33.1 | LOS C | 15.0 | 104.7 | 0.97 | 1.06 | 1.12 | 38.6 |
| 2 T1 | 108 | 0.0 | 108 | 0.0 | * 0.533 | 37.1 | LOS D | 4.0 | 28.1 | 1.00 | 0.77 | 1.00 | 37.4 |
| 3 R 2 | 82 | 0.0 | 82 | 0.0 | 0.483 | 43.7 | LOS D | 3.1 | 21.5 | 1.00 | 0.76 | 1.00 | 34.7 |
| Approach | 683 | 0.0 | 683 | 0.0 | 0.805 | 35.0 | LOS C | 15.0 | 104.7 | 0.98 | 0.98 | 1.09 | 37.9 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 38 | 0.0 | 38 | 0.0 | 0.031 | 8.7 | LOS A | 0.3 | 2.4 | 0.40 | 0.63 | 0.40 | 51.9 |
| $5 \quad$ T1 | 1876 | 0.0 | 1876 | 0.0 | * 0.801 | 15.5 | LOS B | 29.0 | 203.1 | 0.84 | 0.79 | 0.88 | 47.9 |
| 6 R2 | 119 | 0.0 | 119 | 0.0 | 0.244 | 11.2 | LOS B | 1.4 | 9.6 | 0.57 | 0.70 | 0.57 | 49.8 |
| Approach | 2033 | 0.0 | 2033 | 0.0 | 0.801 | 15.1 | LOS B | 29.0 | 203.1 | 0.81 | 0.79 | 0.85 | 48.0 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 152 | 0.0 | 152 | 0.0 | 0.200 | 8.4 | LOS A | 1.5 | 10.4 | 0.41 | 0.67 | 0.41 | 52.1 |
| 8 T1 | 47 | 0.0 | 47 | 0.0 | 0.232 | 35.7 | LOS D | 1.7 | 11.7 | 0.96 | 0.71 | 0.96 | 38.0 |
| 9 R 2 | 94 | 0.0 | 94 | 0.0 | 0.733 | 47.9 | LOS D | 3.8 | 26.5 | 1.00 | 0.84 | 1.25 | 33.3 |
| Approach | 293 | 0.0 | 293 | 0.0 | 0.733 | 25.5 | LOS C | 3.8 | 26.5 | 0.69 | 0.73 | 0.77 | 42.0 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 31 | 0.0 | 31 | 0.0 | 0.024 | 6.9 | LOS A | 0.2 | 1.2 | 0.25 | 0.60 | 0.25 | 53.2 |
| 11 T1 | 1109 | 0.0 | 1109 | 0.0 | 0.456 | 10.4 | LOS B | 11.9 | 83.4 | 0.63 | 0.56 | 0.63 | 51.2 |
| 12 R 2 | 203 | 0.0 | 203 | 0.0 | * 0.573 | 20.1 | LOS C | 5.0 | 34.7 | 0.96 | 0.83 | 0.96 | 44.5 |
| Approach | 1343 | 0.0 | 1343 | 0.0 | 0.573 | 11.8 | LOS B | 11.9 | 83.4 | 0.67 | 0.60 | 0.67 | 50.1 |
| All <br> Vehicles | 4352 | 0.0 | 4352 | 0.0 | 0.805 | 17.9 | LOS B | 29.0 | 203.1 | 0.79 | 0.76 | 0.83 | 46.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.7: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=75$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 29 | 0 | 14 |
| Green Time (sec) | 42 | 7 | 8 |
| Phase Time (sec) | 49 | 14 | 12 |
| Phase Split | $65 \%$ | $19 \%$ | $16 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$| Opposed Slip/Bypass-Lane |
| :--- |
|  |

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## ANNEXURE B4.8: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=100$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | TT MES <br> HV ] <br> \% |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh <br> veh | CK OF UE Dist $]$ m | Prop. Que | Effective Stop Rate | Aver. No Cycles | Aver. Speed km/h |
| South: Silverdory St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 194 | 0.0 | 194 | 0.0 | 0.257 | 8.1 | LOS A | 2.3 | 16.0 | 0.34 | 0.66 | 0.34 | 52.4 |
| 2 T1 | 42 | 0.0 | 42 | 0.0 | 0.276 | 49.9 | LOS D | 2.0 | 14.3 | 0.98 | 0.72 | 0.98 | 33.1 |
| 3 R2 | 32 | 0.0 | 32 | 0.0 | 0.359 | 60.8 | LOS E | 1.7 | 11.6 | 1.00 | 0.70 | 1.00 | 29.8 |
| Approach | 268 | 0.0 | 268 | 0.0 | 0.359 | 20.9 | LOS C | 2.3 | 16.0 | 0.52 | 0.67 | 0.52 | 44.3 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 67 | 0.0 | 67 | 0.0 | 0.116 | 23.8 | LOS C | 1.9 | 13.0 | 0.76 | 0.71 | 0.76 | 42.8 |
| 5 T1 | 1106 | 0.0 | 1106 | 0.0 | 0.411 | 10.2 | LOS B | 13.5 | 94.6 | 0.55 | 0.49 | 0.55 | 51.4 |
| 6 R2 | 150 | 0.0 | 150 | 0.0 | 0.395 | 21.4 | LOS C | 5.0 | 34.8 | 0.88 | 0.82 | 0.88 | 43.8 |
| Approach | 1323 | 0.0 | 1323 | 0.0 | 0.411 | 12.2 | LOS B | 13.5 | 94.6 | 0.60 | 0.54 | 0.60 | 49.9 |
| North: Salamanderfish St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 123 | 0.0 | 123 | 0.0 | 0.209 | 17.0 | LOS B | 3.4 | 24.0 | 0.64 | 0.74 | 0.64 | 46.4 |
| 8 T1 | 91 | 0.0 | 91 | 0.0 | * 0.598 | 51.8 | LOS D | 4.6 | 32.2 | 1.00 | 0.79 | 1.05 | 32.6 |
| 9 R2 | 37 | 0.0 | 37 | 0.0 | 0.302 | 57.1 | LOS E | 1.8 | 12.9 | 0.99 | 0.72 | 0.99 | 30.8 |
| Approach | 251 | 0.0 | 251 | 0.0 | 0.598 | 35.5 | LOS D | 4.6 | 32.2 | 0.82 | 0.76 | 0.84 | 37.8 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 88 | 0.0 | 88 | 0.0 | 0.074 | 10.5 | LOS B | 1.2 | 8.7 | 0.42 | 0.65 | 0.42 | 50.6 |
| 11 T1 | 1826 | 0.0 | 1826 | 0.0 | * 0.792 | 13.6 | LOS B | 34.3 | 240.0 | 0.72 | 0.66 | 0.72 | 49.1 |
| 12 R 2 | 428 | 0.0 | 428 | 0.0 | * 0.790 | 22.5 | LOS C | 17.0 | 118.8 | 1.00 | 0.96 | 1.10 | 43.2 |
| Approach | 2342 | 0.0 | 2342 | 0.0 | 0.792 | 15.1 | LOS B | 34.3 | 240.0 | 0.76 | 0.72 | 0.78 | 47.9 |
| All <br> Vehicles | 4184 | 0.0 | 4184 | 0.0 | 0.792 | 15.8 | LOS B | 34.3 | 240.0 | 0.70 | 0.66 | 0.71 | 47.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B4.8: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=100$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 34 | 0 | 14 |
| Green Time (sec) | 62 | 7 | 13 |
| Phase Time (sec) | 69 | 14 | 17 |
| Phase Split | $69 \%$ | $14 \%$ | $17 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement
Other Movement Class (MC) Running
Mixed Running \& Stopped MCs

Other Movement Class (MC) Stopped $\quad$| Opposed Slip/Bypass-Lane |
| :--- |
|  |

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## ANNEXURE B5: SITE LAYOUT

## 目 Site: [Scenario 2 AM (Site Folder: Proposed Intersection

Geometry (PHASE 1))]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.
§ $\mathrm{N} \quad$ Heidelberg Rd (R...K154)


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## ANNEXURE B5.1: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 100 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | UT MES HV ] \% | $\begin{array}{\|} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. <br> Delay <br> sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. <br> Speed <br> km/h |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 316 | 0.0 | 316 | 0.0 | 0.580 | 12.2 | LOS B | 7.9 | 55.0 | 0.62 | 0.76 | 0.62 | 49.4 |
| 3 R2 | 55 | 0.0 | 55 | 0.0 | * 0.302 | 53.4 | LOS D | 2.6 | 18.4 | 0.97 | 0.74 | 0.97 | 31.4 |
| Approach | 371 | 0.0 | 371 | 0.0 | 0.580 | 18.3 | LOS B | 7.9 | 55.0 | 0.67 | 0.76 | 0.67 | 45.6 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 23 | 0.0 | 23 | 0.0 | 0.015 | 8.1 | LOS A | 0.2 | 1.7 | 0.23 | 0.61 | 0.23 | 51.7 |
| 5 T1 | 952 | 0.0 | 952 | 0.0 | * 0.575 | 4.6 | LOS A | 18.2 | 127.1 | 0.43 | 0.40 | 0.43 | 55.8 |
| Approach | 975 | 0.0 | 975 | 0.0 | 0.575 | 4.7 | LOS A | 18.2 | 127.1 | 0.43 | 0.41 | 0.43 | 55.7 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 852 | 0.0 | 852 | 0.0 | 0.515 | 4.3 | LOS A | 15.0 | 104.7 | 0.40 | 0.37 | 0.40 | 56.1 |
| 12 R 2 | 119 | 0.0 | 119 | 0.0 | 0.378 | 16.6 | LOS B | 3.1 | 21.4 | 0.54 | 0.73 | 0.54 | 46.0 |
| Approach | 971 | 0.0 | 971 | 0.0 | 0.515 | 5.8 | LOS A | 15.0 | 104.7 | 0.42 | 0.41 | 0.42 | 54.6 |
| All <br> Vehicles | 2317 | 0.0 | 2317 | 0.0 | 0.580 | 7.3 | LOS A | 18.2 | 127.1 | 0.46 | 0.47 | 0.46 | 53.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.1: PHASING SUMMARY

## 目 Site: [Scenario 2 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=100$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 16 | 0 |
| Green Time (sec) | 78 | 9 |
| Phase Time (sec) | 85 | 15 |
| Phase Split | $85 \%$ | $15 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

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## ANNEXURE B5.2: MOVEMENT SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 85 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | INPUTVOLUMES$[$ TotalHV ] ]veh/h |  | $\begin{gathered} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. <br> Satn <br> v/c | Aver. Level of Delay Servicesec |  | 95\% BACK OF QUEUE <br> [ Veh. Dist] <br> veh m |  | Prop. Que | Effective Stop Rate | Aver. Aver. <br> No. Speed Cycles <br> km/h |  |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 126 | 0.0 | 126 | 0.0 | 0.158 | 10.1 | LOS B | 1.8 | 12.3 | 0.43 | 0.67 | 0.43 | 50.9 |
| 3 R2 | 22 | 0.0 | 22 | 0.0 | * 0.132 | 46.3 | LOS D | 0.9 | 6.2 | 0.96 | 0.70 | 0.96 | 33.5 |
| Approach | 148 | 0.0 | 148 | 0.0 | 0.158 | 15.5 | LOS B | 1.8 | 12.3 | 0.51 | 0.68 | 0.51 | 47.2 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 47 | 0.0 | 47 | 0.0 | 0.037 | 11.6 | LOS B | 0.7 | 5.0 | 0.39 | 0.65 | 0.39 | 49.2 |
| 5 T1 | 832 | 0.0 | 832 | 0.0 | * 0.617 | 9.9 | LOS A | 20.5 | 143.3 | 0.65 | 0.59 | 0.65 | 51.6 |
| Approach | 879 | 0.0 | 879 | 0.0 | 0.617 | 10.0 | LOS A | 20.5 | 143.3 | 0.64 | 0.60 | 0.64 | 51.5 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1010 | 0.0 | 1010 | 0.0 | 0.622 | 4.8 | LOS A | 18.5 | 129.7 | 0.49 | 0.45 | 0.49 | 55.6 |
| 12 R2 | 282 | 0.0 | 282 | 0.0 | * 0.625 | 14.7 | LOS B | 5.7 | 39.7 | 0.78 | 0.80 | 0.78 | 47.1 |
| Approach | 1292 | 0.0 | 1292 | 0.0 | 0.625 | 6.9 | LOS A | 18.5 | 129.7 | 0.55 | 0.53 | 0.55 | 53.5 |
| All <br> Vehicles | 2319 | 0.0 | 2319 | 0.0 | 0.625 | 8.6 | LOS A | 20.5 | 143.3 | 0.58 | 0.56 | 0.58 | 52.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.2: PHASING SUMMARY

## 目 Site: [Scenario 2 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=85$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 27 | 0 | 14 |
| Green Time (sec) | 54 | 7 | 7 |
| Phase Time (sec) | 61 | 13 | 11 |
| Phase Split | $72 \%$ | $15 \%$ | $13 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B5.3: MOVEMENT SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 80 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 316 | 0.0 | 316 | 0.0 | 0.643 | 14.7 | LOS B | 8.3 | 58.1 | 0.79 | 0.82 | 0.79 | 47.8 |
| 3 R 2 | 55 | 0.0 | 55 | 0.0 | * 0.311 | 44.6 | LOS D | 2.1 | 14.9 | 0.97 | 0.74 | 0.97 | 34.0 |
| Approach | 371 | 0.0 | 371 | 0.0 | 0.643 | 19.2 | LOS B | 8.3 | 58.1 | 0.82 | 0.81 | 0.82 | 45.1 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 23 | 0.0 | 23 | 0.0 | 0.015 | 8.2 | LOS A | 0.2 | 1.5 | 0.26 | 0.62 | 0.26 | 51.6 |
| 5 T1 | 1016 | 0.0 | 1016 | 0.0 | * 0.638 | 5.1 | LOS A | 18.8 | 131.5 | 0.52 | 0.48 | 0.52 | 55.4 |
| Approach | 1039 | 0.0 | 1039 | 0.0 | 0.638 | 5.2 | LOS A | 18.8 | 131.5 | 0.52 | 0.48 | 0.52 | 55.3 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 946 | 0.0 | 946 | 0.0 | 0.594 | 4.8 | LOS A | 16.4 | 115.1 | 0.49 | 0.45 | 0.49 | 55.6 |
| 12 R 2 | 119 | 0.0 | 119 | 0.0 | 0.430 | 18.8 | LOS B | 3.0 | 21.1 | 0.65 | 0.76 | 0.65 | 44.8 |
| Approach | 1065 | 0.0 | 1065 | 0.0 | 0.594 | 6.4 | LOS A | 16.4 | 115.1 | 0.51 | 0.49 | 0.51 | 54.2 |
| All <br> Vehicles | 2475 | 0.0 | 2475 | 0.0 | 0.643 | 7.8 | LOS A | 18.8 | 131.5 | 0.56 | 0.53 | 0.56 | 53.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.3: PHASING SUMMARY

## 目 Site: [Scenario 3 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=80$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B
Output Phase Sequence: A, B

Phase Timing Summary

| Phase | A | B |
| :--- | :---: | :---: |
| Phase Change Time (sec) | 14 | 0 |
| Green Time (sec) | 60 | 7 |
| Phase Time (sec) | 67 | 13 |
| Phase Split | $84 \%$ | $16 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B5.4: MOVEMENT SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | JT MES HV ] \% |  | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> [ Veh. veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 126 | 0.0 | 126 | 0.0 | 0.166 | 11.9 | LOS B | 2.4 | 17.0 | 0.44 | 0.68 | 0.44 | 49.7 |
| 3 R 2 | 22 | 0.0 | 22 | 0.0 | * 0.171 | 60.5 | LOS E | 1.2 | 8.2 | 0.98 | 0.70 | 0.98 | 29.6 |
| Approach | 148 | 0.0 | 148 | 0.0 | 0.171 | 19.1 | LOS B | 2.4 | 17.0 | 0.52 | 0.68 | 0.52 | 45.2 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 47 | 0.0 | 47 | 0.0 | 0.035 | 12.2 | LOS B | 0.8 | 5.9 | 0.36 | 0.65 | 0.36 | 48.9 |
| 5 T1 | 912 | 0.0 | 912 | 0.0 | * 0.656 | 11.5 | LOS B | 28.3 | 198.3 | 0.64 | 0.59 | 0.64 | 50.4 |
| Approach | 959 | 0.0 | 959 | 0.0 | 0.656 | 11.6 | LOS B | 28.3 | 198.3 | 0.63 | 0.59 | 0.63 | 50.4 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1074 | 0.0 | 1074 | 0.0 | 0.619 | 3.9 | LOS A | 20.7 | 145.1 | 0.40 | 0.38 | 0.40 | 56.4 |
| 12 R 2 | 282 | 0.0 | 282 | 0.0 | * 0.587 | 17.6 | LOS B | 8.8 | 61.6 | 0.81 | 0.82 | 0.81 | 45.4 |
| Approach | 1356 | 0.0 | 1356 | 0.0 | 0.619 | 6.7 | LOS A | 20.7 | 145.1 | 0.49 | 0.47 | 0.49 | 53.7 |
| All <br> Vehicles | 2463 | 0.0 | 2463 | 0.0 | 0.656 | 9.3 | LOS A | 28.3 | 198.3 | 0.54 | 0.53 | 0.54 | 51.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.4: PHASING SUMMARY

## 目 Site: [Scenario 3 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=110$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 33 | 0 | 14 |
| Green Time (sec) | 73 | 7 | 13 |
| Phase Time (sec) | 80 | 13 | 17 |
| Phase Split | $73 \%$ | $12 \%$ | $15 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B5.5: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection

Geometry (PHASE 1))]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 90 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1014 | 0.0 | 1014 | 0.0 | 1.210 | 224.9 | LOS F | 113.5 | 794.6 | 1.00 | 1.72 | 2.99 | 11.9 |
| 3 R 2 | 216 | 0.0 | 216 | 0.0 | * 0.641 | 44.6 | LOS D | 9.2 | 64.3 | 0.98 | 0.83 | 1.01 | 34.0 |
| Approach | 1230 | 0.0 | 1230 | 0.0 | 1.210 | 193.2 | LOS F | 113.5 | 794.6 | 1.00 | 1.57 | 2.64 | 13.4 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 93 | 0.0 | 93 | 0.0 | 0.088 | 16.9 | LOS B | 2.0 | 14.1 | 0.53 | 0.69 | 0.53 | 46.0 |
| 5 T1 | 1019 | 0.0 | 1019 | 0.0 | * 0.961 | 50.5 | LOS D | 60.5 | 423.5 | 1.00 | 1.21 | 1.37 | 32.8 |
| Approach | 1112 | 0.0 | 1112 | 0.0 | 0.961 | 47.7 | LOS D | 60.5 | 423.5 | 0.96 | 1.17 | 1.30 | 33.6 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 955 | 0.0 | 955 | 0.0 | 0.810 | 9.8 | LOS A | 24.7 | 172.6 | 0.61 | 0.58 | 0.63 | 51.6 |
| 12 R 2 | 387 | 0.0 | 387 | 0.0 | * 1.070 | 114.8 | LOS F | 26.9 | 188.5 | 1.00 | 1.31 | 2.24 | 18.1 |
| Approach | 1342 | 0.0 | 1342 | 0.0 | 1.070 | 40.1 | LOS D | 26.9 | 188.5 | 0.73 | 0.79 | 1.10 | 33.7 |
| All <br> Vehicles | 3684 | 0.0 | 3684 | 0.0 | 1.210 | 93.5 | LOS F | 113.5 | 794.6 | 0.89 | 1.16 | 1.67 | 22.3 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.5: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=90$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 39 | 0 | 22 |
| Green Time (sec) | 47 | 15 | 11 |
| Phase Time (sec) | 54 | 21 | 15 |
| Phase Split | $60 \%$ | $23 \%$ | $17 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B5.6: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Proposed Intersection

Geometry (PHASE 1))]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 105 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | T <br> MES <br> HV ] <br> \% |  | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 402 | 0.0 | 402 | 0.0 | 0.422 | 25.6 | LOS C | 11.7 | 81.6 | 0.70 | 0.86 | 0.70 | 42.0 |
| 3 R 2 | 85 | 0.0 | 85 | 0.0 | * 0.631 | 60.8 | LOS E | 4.6 | 31.9 | 1.00 | 0.80 | 1.08 | 29.6 |
| Approach | 487 | 0.0 | 487 | 0.0 | 0.631 | 31.7 | LOS C | 11.7 | 81.6 | 0.75 | 0.85 | 0.77 | 39.1 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 183 | 0.0 | 183 | 0.0 | 0.194 | 22.9 | LOS C | 5.4 | 37.9 | 0.62 | 0.74 | 0.62 | 42.7 |
| $5 \quad$ T1 | 921 | 0.0 | 921 | 0.0 | * 1.029 | 97.1 | LOS F | 80.3 | 562.4 | 1.00 | 1.45 | 1.68 | 23.0 |
| Approach | 1104 | 0.0 | 1104 | 0.0 | 1.029 | 84.8 | LOS F | 80.3 | 562.4 | 0.94 | 1.33 | 1.50 | 24.9 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1078 | 0.0 | 1078 | 0.0 | 0.628 | 4.1 | LOS A | 20.9 | 146.4 | 0.42 | 0.39 | 0.42 | 56.2 |
| 12 R 2 | 903 | 0.0 | 903 | 0.0 | * 1.287 | 295.0 | LOS F | 117.8 | 824.4 | 1.00 | 1.66 | 3.12 | 9.4 |
| Approach | 1981 | 0.0 | 1981 | 0.0 | 1.287 | 136.7 | LOS F | 117.8 | 824.4 | 0.69 | 0.97 | 1.65 | 17.2 |
| All <br> Vehicles | 3572 | 0.0 | 3572 | 0.0 | 1.287 | 106.3 | LOS F | 117.8 | 824.4 | 0.77 | 1.07 | 1.48 | 20.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.6: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 1))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=105$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 1
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 52 | 0 | 14 |
| Green Time (sec) | 49 | 7 | 32 |
| Phase Time (sec) | 56 | 13 | 36 |
| Phase Split | $53 \%$ | $12 \%$ | $34 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B5: SITE LAYOUT

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection

Geometry (PHASE 2))]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## ANNEXURE B5.7: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | T <br> MES <br> HV ] <br> \% |  | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> [ Veh. veh | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 1014 | 0.0 | 1014 | 0.0 | 0.869 | 24.9 | LOS C | 26.9 | 188.2 | 0.92 | 1.04 | 1.11 | 42.3 |
| 3 R 2 | 216 | 0.0 | 216 | 0.0 | * 0.713 | 34.6 | LOS C | 6.6 | 46.3 | 1.00 | 0.88 | 1.15 | 37.8 |
| Approach | 1230 | 0.0 | 1230 | 0.0 | 0.869 | 26.6 | LOS C | 26.9 | 188.2 | 0.93 | 1.02 | 1.11 | 41.4 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 93 | 0.0 | 93 | 0.0 | 0.138 | 21.2 | LOS C | 1.9 | 13.5 | 0.73 | 0.73 | 0.73 | 43.9 |
| $5 \quad$ T1 | 1019 | 0.0 | 1019 | 0.0 | 0.720 | 20.3 | LOS C | 13.8 | 96.9 | 0.94 | 0.85 | 0.99 | 45.0 |
| Approach | 1112 | 0.0 | 1112 | 0.0 | 0.720 | 20.4 | LOS C | 13.8 | 96.9 | 0.92 | 0.84 | 0.97 | 44.9 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 955 | 0.0 | 955 | 0.0 | * 0.711 | 7.9 | LOS A | 18.7 | 130.7 | 0.72 | 0.66 | 0.72 | 53.1 |
| 12 R 2 | 387 | 0.0 | 387 | 0.0 | 0.496 | 27.6 | LOS C | 6.1 | 43.0 | 0.90 | 0.79 | 0.90 | 40.7 |
| Approach | 1342 | 0.0 | 1342 | 0.0 | 0.711 | 13.6 | LOS B | 18.7 | 130.7 | 0.77 | 0.70 | 0.77 | 48.8 |
| All <br> Vehicles | 3684 | 0.0 | 3684 | 0.0 | 0.869 | 20.0 | LOS B | 26.9 | 188.2 | 0.87 | 0.85 | 0.95 | 44.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.7: PHASING SUMMARY

## 目 Site: [Scenario 4 AM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=60$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 36 | 0 | 16 |
| Green Time (sec) | 20 | 9 | 14 |
| Phase Time (sec) | 27 | 15 | 18 |
| Phase Split | $45 \%$ | $25 \%$ | $30 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

## ANNEXURE B5.8: MOVEMENT SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 70 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{array}{r} \text { DEN } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed $\mathrm{km} / \mathrm{h}$ |
| South: Yellow Jack St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 402 | 0.0 | 402 | 0.0 | 0.318 | 9.5 | LOS A | 5.1 | 35.7 | 0.49 | 0.70 | 0.49 | 51.3 |
| 3 R2 | 85 | 0.0 | 85 | 0.0 | * 0.421 | 39.5 | LOS D | 2.9 | 20.3 | 0.98 | 0.76 | 0.98 | 36.0 |
| Approach | 487 | 0.0 | 487 | 0.0 | 0.421 | 14.7 | LOS B | 5.1 | 35.7 | 0.57 | 0.71 | 0.57 | 47.7 |
| East: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 183 | 0.0 | 183 | 0.0 | 0.302 | 28.2 | LOS C | 4.9 | 34.2 | 0.81 | 0.77 | 0.81 | 41.2 |
| 5 T1 | 921 | 0.0 | 921 | 0.0 | * 0.723 | 25.0 | LOS C | 14.8 | 103.3 | 0.95 | 0.86 | 1.00 | 42.5 |
| Approach | 1104 | 0.0 | 1104 | 0.0 | 0.723 | 25.6 | LOS C | 14.8 | 103.3 | 0.93 | 0.84 | 0.97 | 42.3 |
| West: Heidelberg Rd (R550 / K154) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 T1 | 1078 | 0.0 | 1078 | 0.0 | 0.711 | 6.2 | LOS A | 21.2 | 148.6 | 0.63 | 0.58 | 0.63 | 54.5 |
| 12 R 2 | 903 | 0.0 | 903 | 0.0 | * 0.755 | 28.0 | LOS C | 17.5 | 122.3 | 0.90 | 0.86 | 0.94 | 40.7 |
| Approach | 1981 | 0.0 | 1981 | 0.0 | 0.755 | 16.2 | LOS B | 21.2 | 148.6 | 0.75 | 0.71 | 0.77 | 47.2 |
| All <br> Vehicles | 3572 | 0.0 | 3572 | 0.0 | 0.755 | 18.9 | LOS B | 21.2 | 148.6 | 0.78 | 0.75 | 0.81 | 45.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

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## ANNEXURE B5.8: PHASING SUMMARY

## 目 Site: [Scenario 4 PM (Site Folder: Proposed Intersection <br> Geometry (PHASE 2))]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=70$ seconds (Site Optimum Cycle Time - Minimum Delay)

Timings based on settings in the Site Phasing \& Timing dialog
Phase Times determined by the program
Phase Sequence: Option 2
Reference Phase: Phase B
Input Phase Sequence: A, B, C
Output Phase Sequence: A, B, C

Phase Timing Summary

| Phase | A | B | C |
| :--- | :---: | :---: | :---: |
| Phase Change Time (sec) | 45 | 0 | 14 |
| Green Time (sec) | 21 | 7 | 25 |
| Phase Time (sec) | 28 | 13 | 29 |
| Phase Split | $40 \%$ | $19 \%$ | $41 \%$ |

See the Timing Analysis report for more detailed information including input values of Yellow Time and All-Red Time, and information on any adjustments to Intergreen Time, Phase Time and Green Time values in cases of Pedestrian Actuation, Minor Phase Actuation and Phase Frequency values (user-specified or implied) less than $100 \%$.


REF: Reference Phase
VAR: Variable Phase
Normal Movement
Slip/Bypass-Lane Movement
Stopped Movement

Other Movement Class (MC) Running | Permitted/Opposed |
| :--- |
| Mixed Running \& Stopped MCs |

