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**GEOTECHNICAL INVESTIGATION FOR TOWNSHIP ESTABLISHMENT  
ACORN CITY URBAN MIXED-USE DEVELOPMENT.**

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**DAVEL &  
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**CONSULTING ENGINEERING GEOLOGISTS**

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**REPORT DVH-20-28 REV.2**

**GEOTECHNICAL INVESTIGATION FOR TOWNSHIP REZONING,  
ACORN CITY URBAN MIXED-USE DEVELOPMENT**

**GEOTECHNICAL REPORT**

**February 2022**

Prepared for:  
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Fourways  
2055

Prepared by:  
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## EXECUTIVE SUMMARY

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The following key points are considered pertinent to the current report.

- The site is underlain by medium to coarse grained quartz-feldspar-biotite gneiss of the Swazian Erathem.
- Two geotechnical soils zones, Zone S and Zone C2 have been identified across the area of investigation.
- No perched water table or zones of seepage were intersected in any of the test pits excavated across the site at the time of the fieldwork.
- Conventional and / or deeper than normal strip / spread foundations could be employed for the structures across Zone S.
- Special foundation procedures such as reinforced concrete raft foundations or suitably designed piled foundations would be required for the structures across Zone C2.
- The area of investigation (Zone S and Zone C2) classifies as soft excavation material to depths in excess of 3,0m.
- The upper in situ soils (hillwash, pebble marker and reworked / residual granite) are considered suitable for use as poor quality general fill only.




**DZANA INVESTMENTS (PTY) LTD**

**GEOTECHNICAL INVESTIGATION FOR TOWNSHIP REZONING**  
**ACORN CITY URBAN MIXED-USE DEVELOPMENT**

**GEOTECHNICAL REPORT**

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<b>DVH CONSULTING QUALITY VERIFICATION</b>		
	<b>PREPARED BY</b>	<b>REVIEWED BY</b>
<b>ORIGINAL</b>	Mr J Davel	Mr J van Huyssteen
<b>DATE</b>	February 2022	February 2022
<b>SIGNATURE</b>		

# 1 INTRODUCTION

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## 1.1 General

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DVH Consulting was appointed by Dzana Investments (Pty) Ltd in May 2020 to undertake a geotechnical investigation for the township rezoning for the proposed Acorn City Urban Mixed-Use Development, Acornhoek. This after DVH Consulting had on 1 March 2020 provided Mr J Oosthuizen of L&S Consulting Engineers with a cost proposal (Q050-2020) for the geotechnical investigation.

The Acorn City Urban Mixed-use development will comprise retail, commercial and residential components as well as the associated internal road infrastructure. Exact earthworks details are unknown at this stage.

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## 1.2 Terms of Reference

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The terms of reference for the investigation are as follow:

- i) to establish in broad terms the nature and relevant engineering properties of the upper soil and rock strata underlying the site.
- ii) to comment on suitable excavation procedures for the installation of services.
- iii) to provided preliminary recommendations related to the suitability of the on-site soils for used as construction materials for bulk fill terraces and as layerworks for access roads and parking areas.
- iv) to present general foundation recommendations for the proposed development.
- v) to comment on any other geotechnical aspects as these may affect the development.

## 2 SITE LOCALITY AND DESCRIPTION

The area of investigation covers approximately 52 hectares and is situated on a large portion of open land immediately east of the R40 road, approximately 3km south of the existing Acornhoek Mall. The topography of the site is variable with the eastern portions of the site sloping generally towards the south east while the western portions of the site contain two shallow valleys which act as areas of preferential drainage and slope towards the west. The site is covered by veld grass and areas of thick bush. The site locality is presented in Figure 1 below.



**Figure 1. Site Locality, Acorn City Urban Mixed-use Development.**

## 3 METHOD OF INVESTIGATION

### 3.1 Fieldwork

The fieldwork operation was carried out on 1 and 2 June 2020 utilising a JCB 3CX tractor-loader-backhoe (backactor). The backactor excavated thirty-two test pits (TP1, TP3 to TP8, TP10, TP12 to TP27 and TP29 to TP36) across the area of investigation where access to the machine was possible. Test pits TP2, TP9, TP11 and TP28 were not excavated owing to thick bush preventing access to the test pit positions. The test pits were excavated to refusal of the backactor or until the excavation limit of the machine was obtained at 3,0m. A qualified engineering geologist profiled all the test pit excavations in situ and where necessary took

disturbed and undisturbed soil samples. The soil samples were submitted to Civilab (SANAS Accredited) for the required laboratory testing. The positions of the test pits are shown on the site plan enclosed in Appendix A. The recorded test pit soil profiles are presented in Appendix B. The test pit coordinates are included in Appendix B.

### 3.2 Laboratory Testing

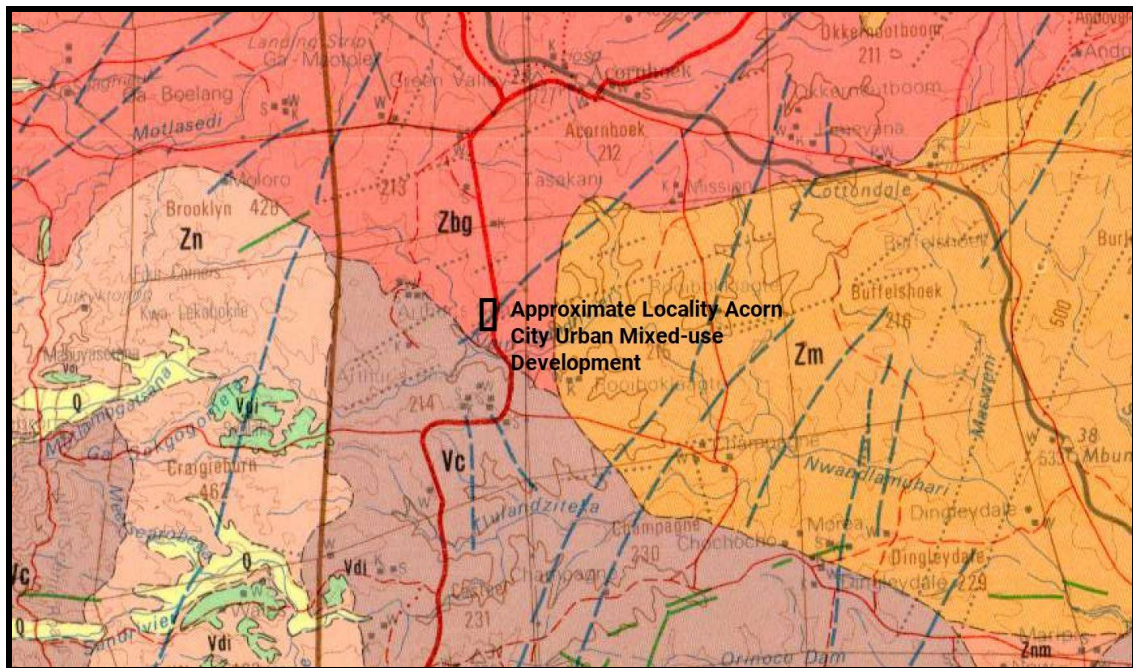
The following laboratory testing has been carried out on the soil samples recovered during the fieldwork operation. The laboratory test results have been used to confirm the suitability of the on-site soils for use as construction materials and to identify any problematic soil parameters related to the in-situ soils.

<b>Test Description</b>	<b>Test Methods</b>
Atterberg limits and particle size distribution	SANS 3001 GR1, SANS 3001 GR3, SANS 3001 GR10
Moisture/Density and California Bearing Ratio (CBR) tests to evaluate compaction and strength characteristics	SANS 3001 GR30, SANS 3001 GR40
pH of Soil	TMH1 A20
Conductivity of Saturated Soil Paste	TMH1 A21T
Collapse Potential Consolidometer	BS 1377 Part 5

The laboratory test results are summarised in Table 1, Section 7. The full set of laboratory test results is presented in Appendix C.



## 4 REGIONAL & SITE-SPECIFIC GEOLOGY



Key:

Zbg – Grey to pale brown, medium to coarse grained quartz-feldspar-biotite gneiss

**Figure 2. Regional Geology Acorn City Urban Mixed-use Development.**

According to the available geological maps (1:250 000, 2430 Pilgrims Rest) the area of investigation is underlain by **medium to coarse grained quartz-feldspar-biotite gneiss** of the Swazian Eratthem. This was confirmed during the fieldwork operation. Owing to weathering of the gneiss bedrock residual gneiss soils occur across the area of investigation. The upper soil layer comprises a layer of transported hillwash.

Based on the recorded soil profiles, and considering the foundation recommendations presented in Section 6, the site has been subdivided into two geotechnical soil zones.

Geotechnical Soil Zone	General Soil Profile Description
Zone S	Transported Hillwash overlying localised Transported Pebble Marker overlying Reworked Residual Gneiss overlying competent Residual Gneiss.
Zone C2	Transported Hillwash overlying localised Transported Pebble Marker overlying thick potentially collapsible Reworked Residual Gneiss overlying Residual Gneiss.

These geotechnical soil zones are based on the classification systems as provided by the NHBC Home Builders Manual (2015) and SANS 10400-H Foundations (2012).



The approximate areal extent of each soil zone is shown on the site plan enclosed in Appendix A. The recorded soil profile within each soil zone is described in the following subsections.

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#### 4.1 Zone S

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Zone S covers the northernmost and western portions of the site, test pits TP1, TP20, TP21, TP22 and TP24 to TP36 refer.

The upper soil horizon within Zone S comprises 0,2m to 0,8m of medium dense intact silty sand of **transported hillwash** origin. The hillwash is locally underlain by medium dense intact silty sand with scattered to abundant quartz gravel. This gravel layer represents the **transported pebble marker** and occurs to depths varying between 0,3m and 0,9m. No pebble marker was noted in test pits TP21, TP25, TP29, TP30 and TP32.

The hillwash and pebble marker are underlain by medium dense / medium dense to dense and locally loose weakly ferruginised silty sand varying to micaceous slightly silty clayey sand representing **reworked residual gneiss**. The reworked residual gneiss extends to depths varying between 0,7m and 2,2m (average depth 1,1m). The reworked residual gneiss is underlain by medium dense / medium dense to dense jointed silty sand / micaceous silty sand **residual gneiss**. The excavation limit of the machine was obtained at 3,0m within the residual gneiss in all of the test pits excavated across Zone S.

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#### 4.2 Zone C2

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Zone C2 occurs across the eastern and central-northern portions of the site. Test pits TP3 to TP19, TP22 and TP23 refer.

The upper soil layer across Zone C2 comprises medium dense and locally firm intact silty sand / slightly silty clayey sand of **transported hillwash** origin. The hillwash extends to depths of the order of 0,3m to 1,7m (average depth 0,8m) across Zone C2. The hillwash is locally underlain by a medium dense **transported pebble marker**. The pebble marker extends to depths varying between 0,4m and 1,9m in test pits TP3, TP4, TP12 to TP16, TP18, TP19 and TP23. No pebble marker was noted in the remaining test pits across Zone C2.

The hillwash and pebble marker horizons within Zone C2 are underlain by loose to medium dense / medium dense intact micaceous slightly silty clayey sand / micaceous silty sand **reworked residual gneiss**. The reworked residual gneiss generally extends to depths varying between 1,6m and 2,3m but locally extends to depths in excess of 3,0m, the excavation limit of the machine, in test pits TP3, TP17, TP19 and TP22. The reworked residual gneiss is underlain by loose / loose to medium dense jointed micaceous slightly clayey silty sand / silty sand **residual**

**gneiss** to depths in excess of 3,0m, the excavation limit of the backactor, in those test pits where it occurs across Zone C2.

An exception to the general soil profile within Zone C2 was noted in test pit TP8 where refusal of the backactor was obtained at 1,3m depth upon an apparent gneiss corestone / boulder.

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### 4.3 Groundwater

No perched water table or zones of seepage were noted in any of the test pits excavated across the site (Zone S and Zone C2) at the time of the fieldwork.

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## 5 FOUNDATION RECOMMENDATIONS

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### 5.1 Zone S

Owing to the poor consistency and in-situ soil structure of the hillwash and pebble marker horizons, we are of the opinion that these soil strata would potentially be highly compressible and / or collapsible. These soil layers are thus unsuitable for use as founding horizons for conventional foundations.

Dependant on final earthworks levels **conventional and/ or deeper than normal strip / spread foundations** could be utilised should the foundations be placed upon the underlying medium dense or better reworked residual gneiss. These founding horizons occur at depths varying between 0,2m and 0,9m (average depth 0,5m) below present ground level across Zone S. An allowable bearing pressure of 200kPa could be applied to the above founding horizons.

An allowable bearing pressure of 300kPa could be utilised for the medium dense or better residual gneiss soils occurring across Zone S. This founding horizon occurs at depths varying between 0,4m to 2,2m (average depth 1,2m) below present ground level. Dependant on final earthworks levels **conventional and/ or deeper than normal strip / spread foundations** could be utilised as suitable foundation types.

Settlement analyses have been carried out using the method proposed by Mayne and Poulos, 1999. A Youngs Modulus of 25MPa / 30MPa was assumed for the medium dense reworked / residual gneiss respectively. The settlement analyses indicate that total settlements of the order of 5mm to 10mm could occur for conventional strip / spread foundations under the foundation loads provided above. Differential settlements should be taken as 50% of the total settlements.

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## 5.2 Zone C2

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Owing to the poor consistency and in-situ soil structure of the hillwash and pebble marker as well as the thick underlying reworked residual gneiss across Zone C2, we are of the opinion that these soil strata would be potentially highly compressible and / or collapsible. This was confirmed via collapse potential tests carried out on undisturbed samples of the hillwash and reworked residual gneiss. A collapse potential of 2,81% was recorded in the hillwash while collapse potential of between 11,75% and 13,41% were recorded in the reworked residual gneiss under and applied load of 200kPa. According to Schwartz, 1985, these collapse potentials can be classified as moderate to sever trouble.

Furthermore, the underlying residual gneiss across Zone C2 has a poor in situ consistency, loose / loose to medium dense, and is thus regarded as being potentially highly compressible under foundation loading. These soil layers are thus unsuitable for use founding horizons for conventional foundations.

Considering the test pit soil profiles as recorded across Zone C2 it is apparent that special foundation procedures would need to be adopted for the structures within Zone C2.

One of the following foundation solutions could be employed.

- i) The structures could be placed upon suitably designed **reinforced concrete raft foundations**. The rafts could be placed at shallow depth within the upper in situ soils. A Modulus of Subgrade Reaction (k) value of 40kPa/mm could be applied to the in-situ soils to facilitate the design of the raft foundations.
- ii) The structures could be founded upon suitably designed **piled foundations**. Further geotechnical works in the form of dynamic probe super heavy (DPSH) testing or the in-situ profiling of large diameter augered trial holes would be required to determine suitable pile types and pile founding depths.

## 6 EXCAVATION PROCEDURES

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The site has been evaluated in terms of excavation procedures as defined in the SANS documents (SANS 1200D, DA and DB). Based on the criteria in the SANS documents the area of investigation (Zone S and Zone C2) classifies as **soft excavation** material to depths in excess of 3,0m.

## 7 MATERIALS USAGE

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Laboratory testing has been carried out on the soil samples obtained during the fieldwork in order to evaluate the suitability of the on-site soils for use as construction material in bulk fill operations and as layerworks for access roads and parking areas.

Based on analyses of the laboratory test results as well as a visual assessment from the fieldwork, the following recommendations are considered appropriate to the in-situ soils encountered across the site with regards to the above.

- The upper 150mm of in situ soils across the vegetated portions of the site contains abundant organic matter and is thus unsuitable for use as construction material. This material should be removed to spoil prior to construction commencing. It is envisaged that in the vicinity of large trees, that at least the upper 0,5m of in situ soils, would have to be removed owing to the presence of abundant tree roots. This depth would have to be verified upon commencement of site clearing.
- The in-situ soils across the area of investigation (hillwash, pebble marker and reworked / residual gneiss) are considered suitable for use poor quality bulk fill material only. Owing to the high plasticity indexes of the in-situ soils as well as the high liner shrinkage results, it is envisaged that shrinkage cracks would be observed in the bulk fill platforms should the in-situ soils be utilised as bulk fill material. A cover layer of good quality bulk fill would therefore be required to form the upper portions of the bulk fill platforms.

Based on the above it is anticipated that it would be necessary to import material onto site for use in the construction of bulk fill platforms and as layerworks for surface beds, access roads and parking areas. This material should be of minimum G7 quality.

Table 1. Summary of Laboratory Test Results

Test Pit	Depth (m)	Soil Horizon	Grading Modulus	Atterberg Limits			Max. Dry Density (kg/m <sup>3</sup> )	Optimum Moisture Content (%)	Swell (%)	California Bearing Ratio (CBR) (%)			Materials Classification	
				Liquid Limit (LL)	Plasticity Index (PI)	Linear Shrinkage (%)				90	93	95	TRH-14	COLTO
TP4	0,1 – 1,5	Hillwash / Reworked Residual Gneiss	1,5	46	22	10	1745	17,3	0,6	9	12	14	G9	NONE
TP7	0,1 – 1,5	Hillwash / Reworked Residual Gneiss	1,4	47	23	10,5	1697	18,1	0,9	5	6	7	G10	NONE
TP30	1,1 – 3,0	Residual Gneiss	2,5	46	23	8,5	2000	9,4	0,3	26	33	37	G8	NONE
TP16	0,1 – 1,5	Hillwash / Reworked Residual Gneiss	1,5	49	24	10,5	1728	17,4	1,2	7	8	9	G9	NONE
TP32	0,1 – 1,0	Hillwash / Residual Gneiss	1,9	38	18	8	1941	10,4	0,1	22	24	26	G8	NONE
TP5	1,1 – 1,5	Reworked Residual Gneiss	1,25	45	21	9,5	NA	NA	NA	NA	NA	NA	NA	NA
TP8	0,1 – 1,3	Hillwash	0,85	45	22	10	NA	NA	NA	NA	NA	NA	NA	NA
TP12	0,4 – 2,1	Reworked Residual Gneiss	0,86	54	28	11,5	NA	NA	NA	NA	NA	NA	NA	NA
TP13	0,1 – 0,9	Hillwash	0,85	47	23	10,5	NA	NA	NA	NA	NA	NA	NA	NA
TP15	0,4 – 2,1	Reworked Residual Gneiss	0,84	47	23	10	NA	NA	NA	NA	NA	NA	NA	NA
TP18	2,3 – 3,0	Residual Gneiss	1,05	43	20	8	NA	NA	NA	NA	NA	NA	NA	NA
TP19	0,5 – 1,6	Hillwash	0,95	50	23	10	NA	NA	NA	NA	NA	NA	NA	NA
TP21	0,9 – 3,0	Residual Gneiss	1,06	45	23	10	NA	NA	NA	NA	NA	NA	NA	NA
TP22	0,1 – 0,9	Hillwash	0,94	45	21	10	NA	NA	NA	NA	NA	NA	NA	NA
TP23	0,5 – 1,6	Reworked Residual Gneiss	0,96	54	27	12	NA	NA	NA	NA	NA	NA	NA	NA
TP26	0,9 – 2,2	Reworked Residual Gneiss	0,84	50	21	9,5	NA	NA	NA	NA	NA	NA	NA	NA
TP27	0,8 – 3,0	Residual Gneiss	1,06	46	19	9	NA	NA	NA	NA	NA	NA	NA	NA
TP31	0,7 – 3,0	Residual Gneiss	1,27	42	24	9,5	NA	NA	NA	NA	NA	NA	NA	NA
TP35	0,7 – 3,0	Residual Gneiss	1,58	40	18	7	NA	NA	NA	NA	NA	NA	NA	NA

## 7.1 Soil Chemistry

**Table 2. Relationship Between Soils Resistivity and Corrosivity of Soils to buried Metals.**

Soil Resistivity (ohm.cm)	Corrosivity	Conductivity (mSm <sup>-1</sup> )
0 – 2000	Very Corrosive	>50
2000 – 5000	Corrosive	50 – 20
5000 – 10000	Mildly Corrosive	20 – 10
Over 10000	Generally Not	<10

**Table 3. Results of Soil Chemistry Tests**

Test Pit	Depth (m)	Soil Horizon	pH	Soil Resistivity (ohm.cm)	Conductivity (mSm <sup>-1</sup> )
TP8	0,1 – 1,3	Hillwash	6,2	25000	4
TP12	0,4 – 2,1	Reworked Residual Gneiss	5,7	33333	3
TP13	0,1 – 0,9	Hillwash	5,6	33333	3
TP15	0,4 – 2,1	Reworked Residual Gneiss	5,9	33333	3
TP18	2,3 – 3,0	Residual Gneiss	6,1	25000	4
TP21	0,9 – 3,0	Residual Gneiss	6,2	20000	5
TP22	0,1 - 0,9	Hillwash	5,7	33333	3
TP23	0,5 – 1,6	Reworked Residual Gneiss	5,9	39370	1
TP26	0,9 – 2,2	Reworked Residual Gneiss	6,1	20000	5
TP27	0,8 – 3,0	Residual Gneiss	6,3	20000	5
TP31	0,7 – 3,0	Residual Gneiss	6,4	25000	4
TP35	0,7 – 3,0	Residual Gneiss	6,6	25000	4

Based on Table 2 and Table 3 we can see that the in-situ soils across the area of investigation are considered to non-corrosive to buried concrete and steel. As such no protective measures would be required for the foundations and buried services associated with the future development of the site.

## 8 GENERAL

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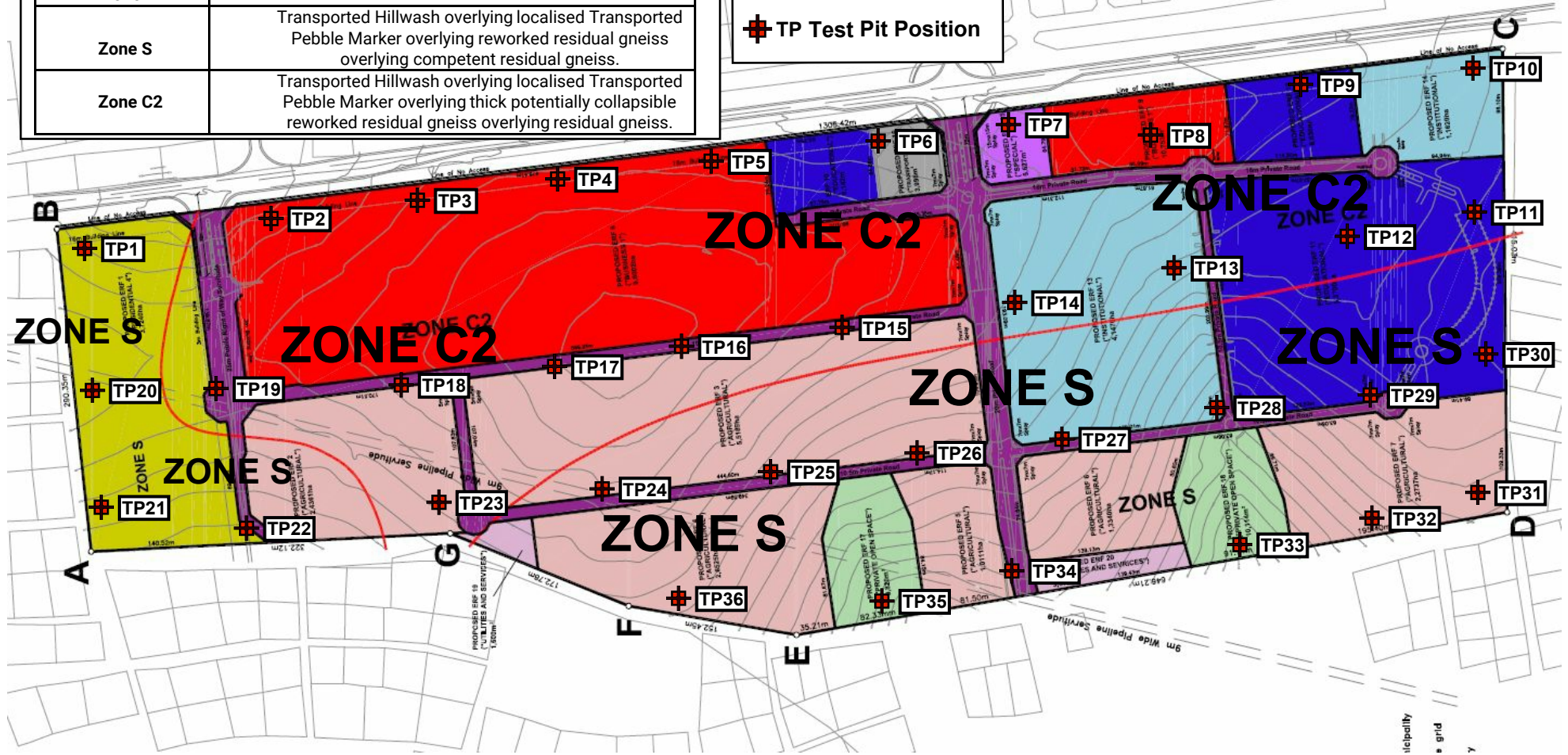
The following comments are considered relevant to the current investigation.

- The current investigation and report are of a general nature, as such they should not be utilised for design purposes. A further detailed design-level geotechnical investigation would need to be undertaken in order to accurately define the geotechnical zonal boundaries and to determine the depths to the recommended founding layers for individual stands. In addition, further laboratory testing would need to be carried out on the in-situ soils across the site in order to determine their suitability for use as construction materials.
- A separate letter report (Report DVH-21-108 Evaluation Of Founding Conditions & Excavatibility for Proposed Fuel Station, Acorn City) has been compiled specifically for the propose fuel station development at Acorn City. This is presented in Appendix D of the current report and should be read in conjunction with the current report.



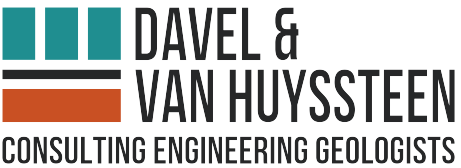
Geotechnical Soil Zone	General Soil Profile Description
Zone S	Transported Hillwash overlying localised Transported Pebble Marker overlying reworked residual gneiss overlying competent residual gneiss.
Zone C2	Transported Hillwash overlying localised Transported Pebble Marker overlying thick potentially collapsible reworked residual gneiss overlying residual gneiss.

**KEY:**  
 TP Test Pit Position



**PROJECT: DVH-20-28  
 ACORN CITY URBAN MIXED USE  
 DEVELOPMENT  
 JUNE 2020**

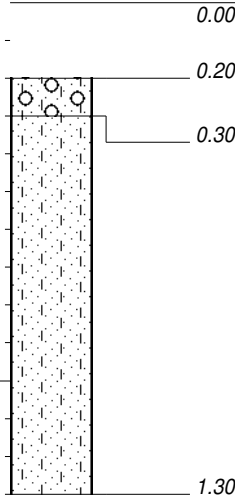
**SITE PLAN INDICATING  
 LOCATIONS OF TEST PIT EXCAVATIONS**



**DAVEL &  
 VAN HUYSSTEEN**  
 CONSULTING ENGINEERING GEOLOGISTS



Scale  
1:20



Moist dark brown medium dense intact silty sand. Hillwash.

As above but contains abundant quartz gravel. Pebble Marker.

Moist blotched orange red brown medium dense to dense ferruginised silty sand. Reworked residual gneiss with zones of residual gneiss.

Moist orange brown speckled off white flecked gold medium dense jointed micaceous slightly clayey silty sand. Residual gneiss.

3.00

NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
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DRILLED BY :  
PROFILED BY : J Davel

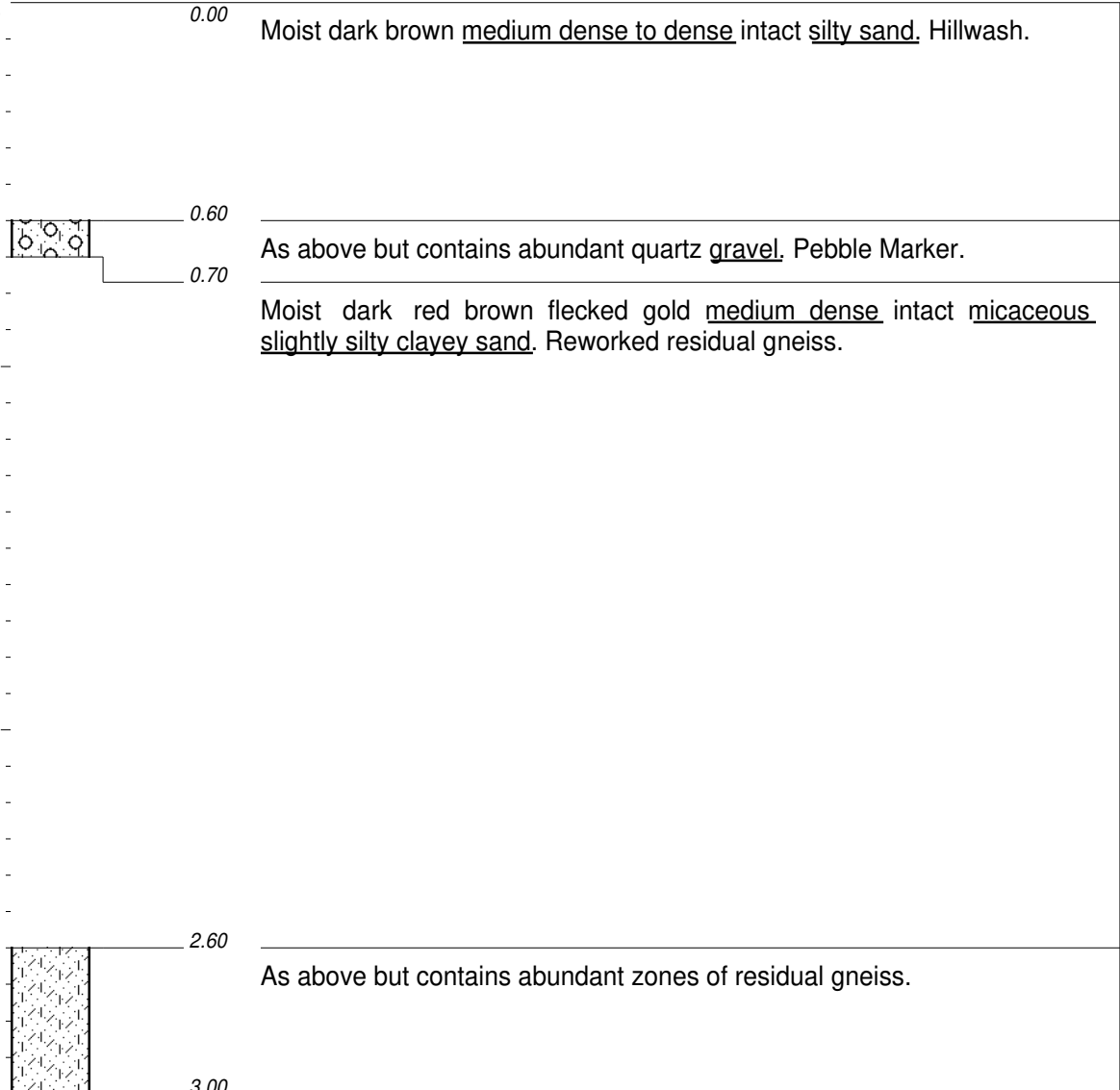
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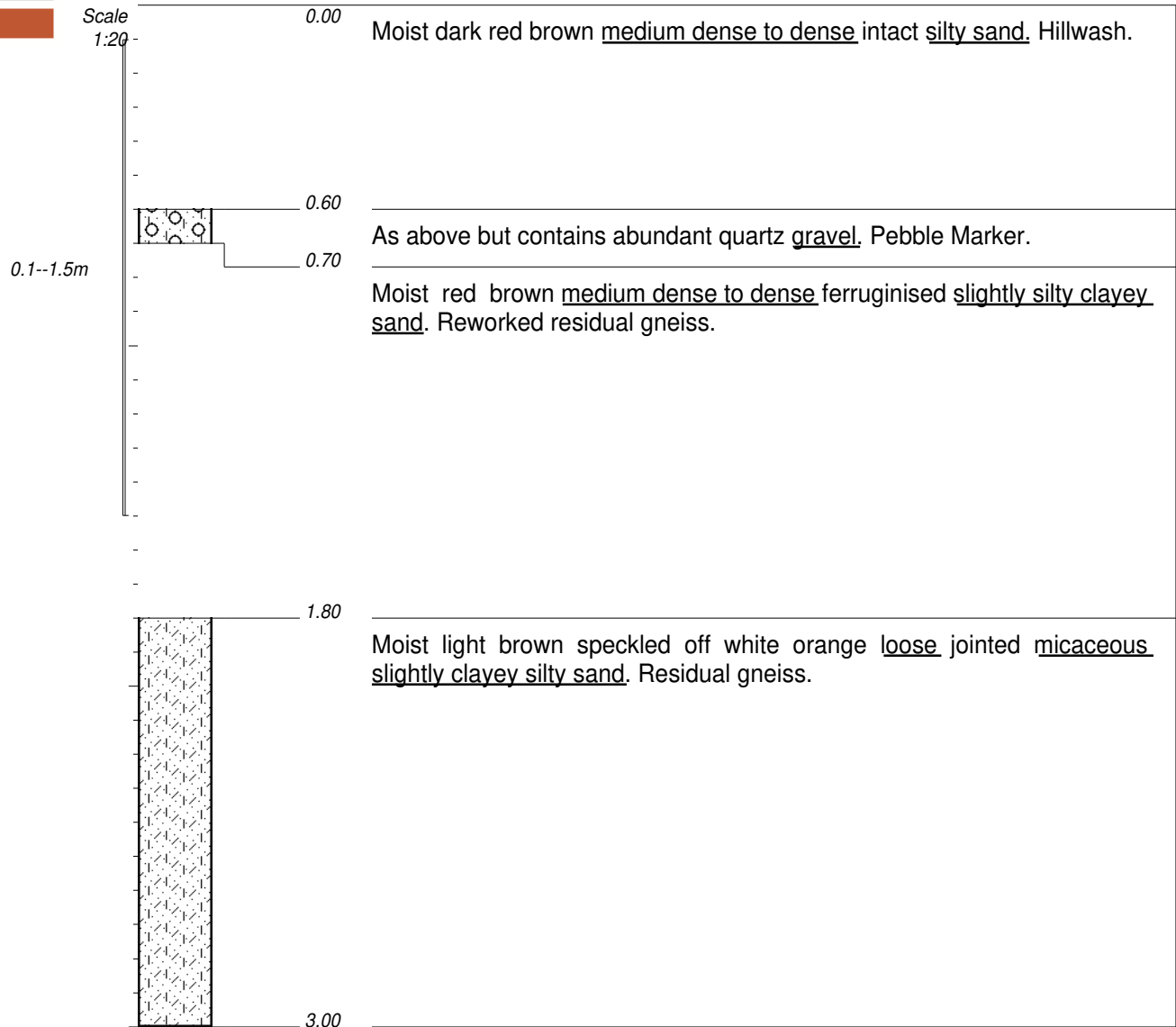
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

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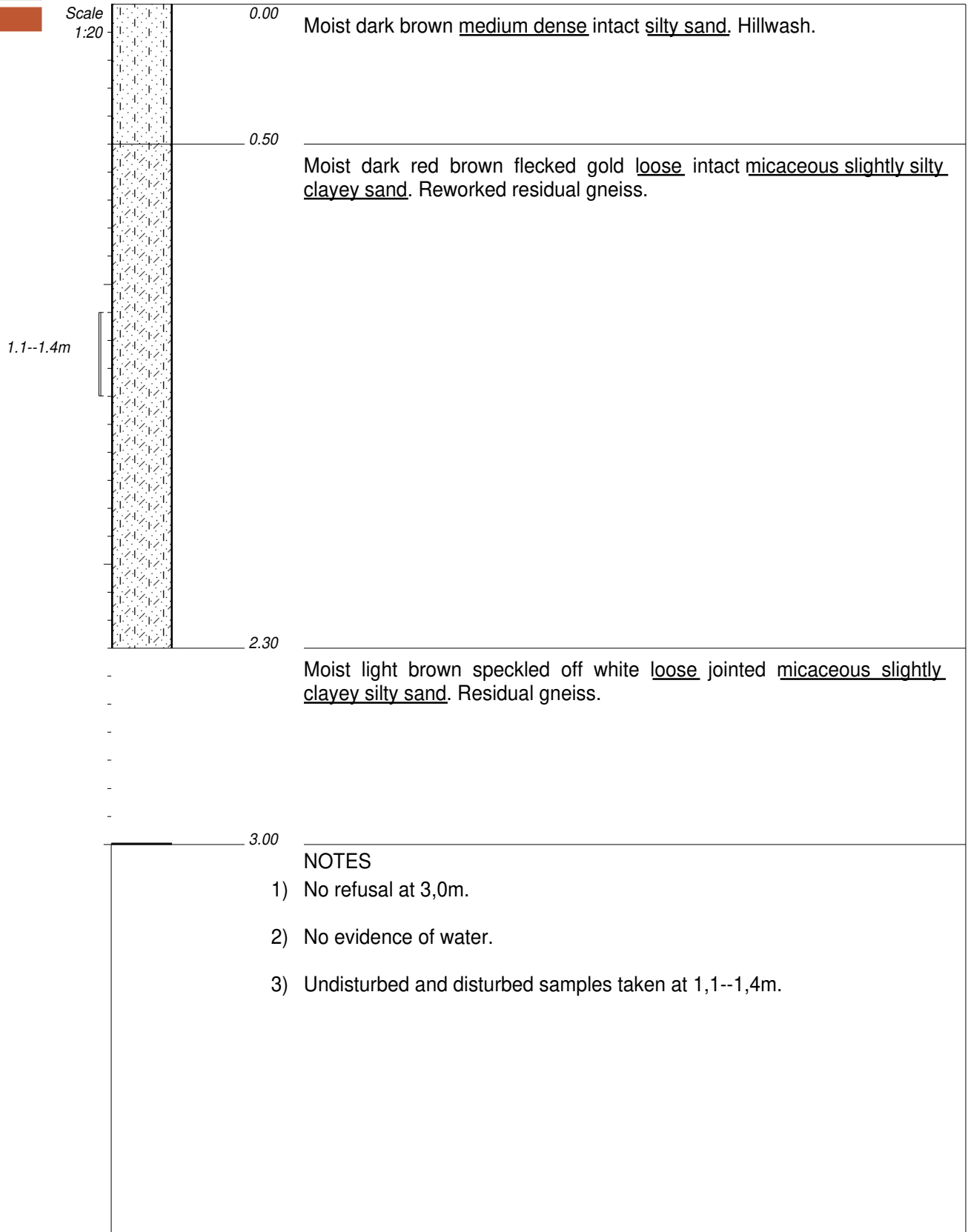
- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,1--1,5m.

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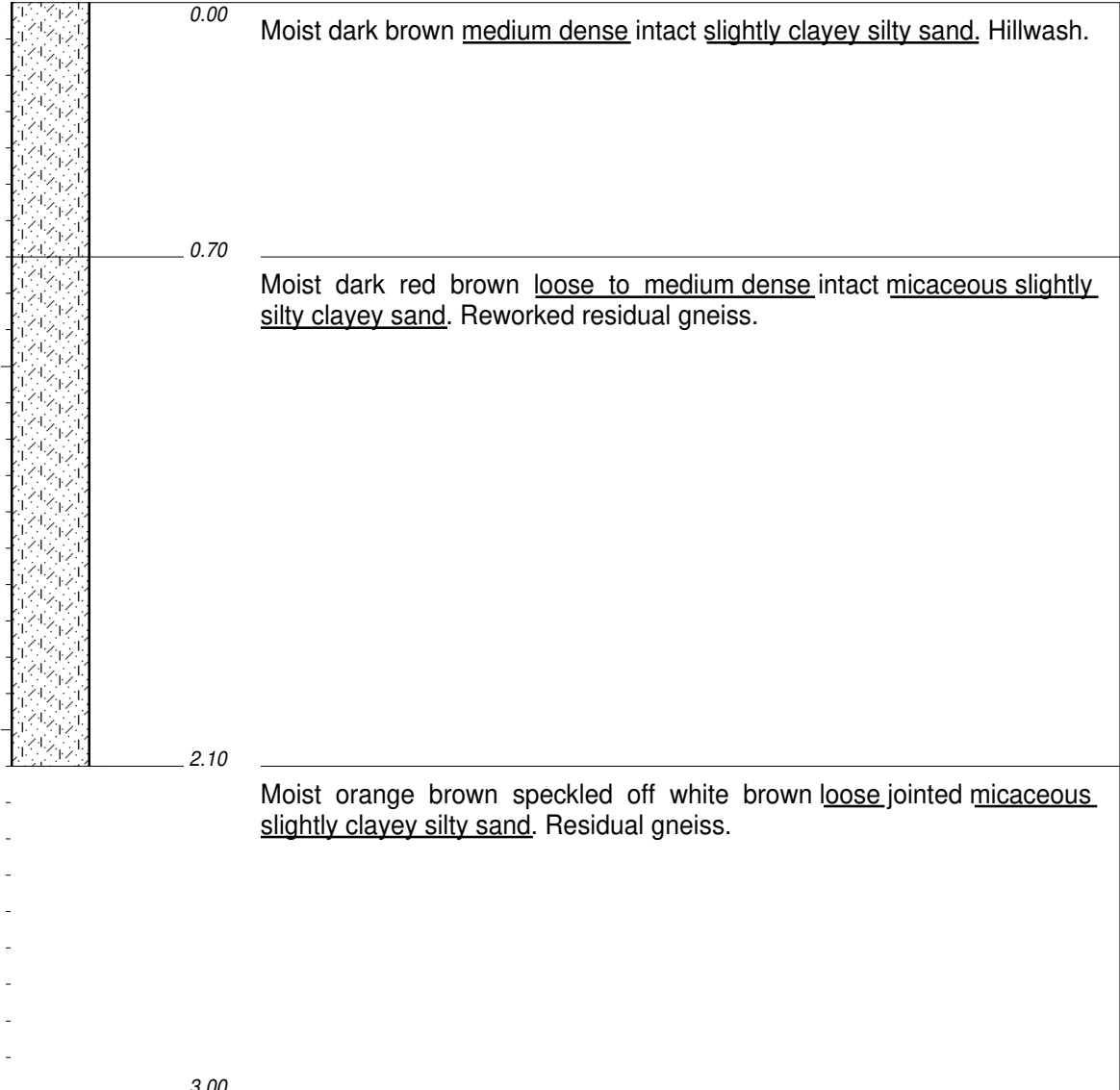
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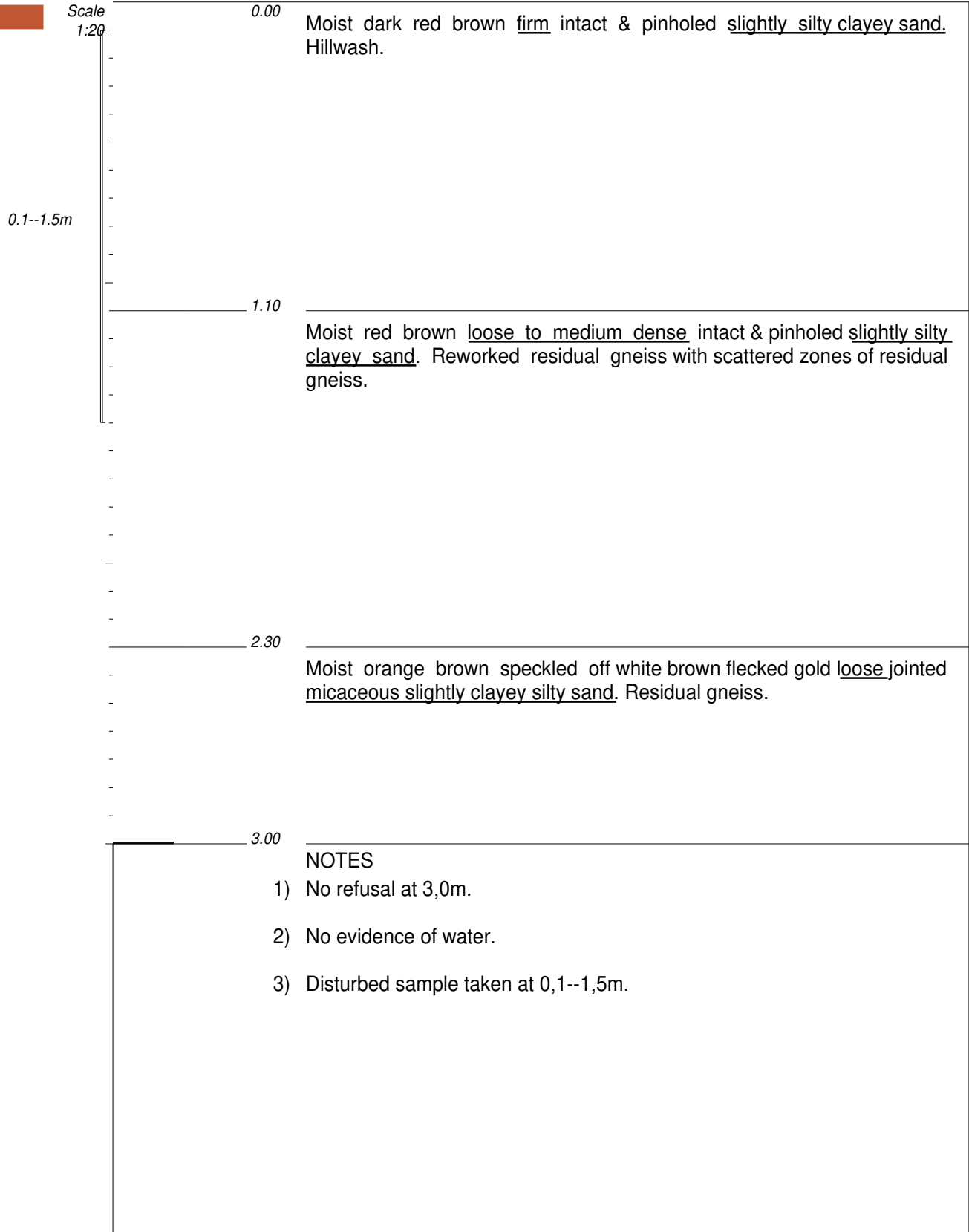


- NOTES
- 1) No refusal at 3,0m.
  - 2) No evidence of water.

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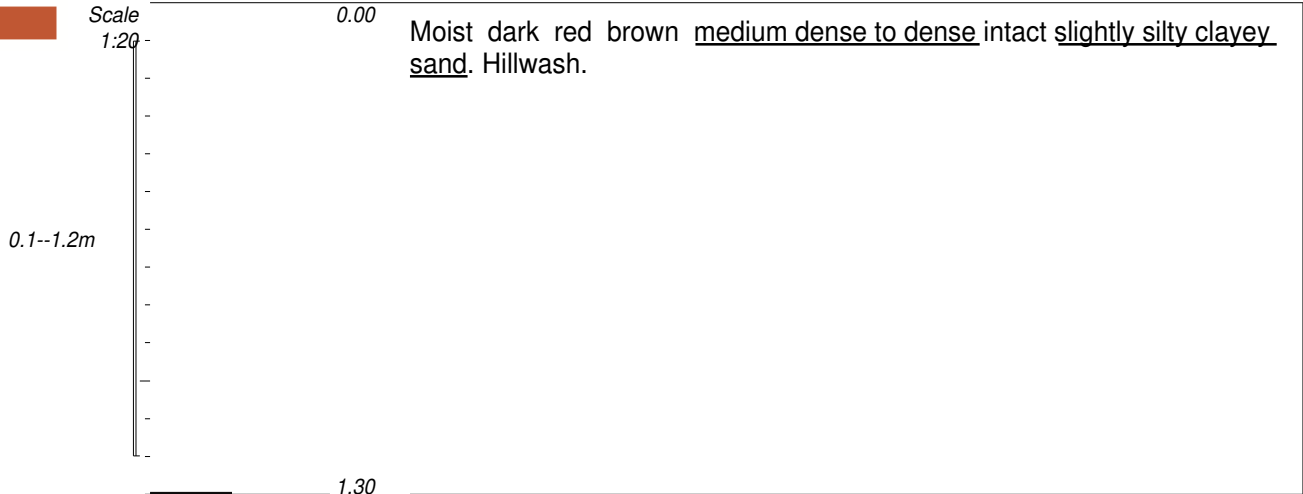


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1.30

NOTES

- 1) Refusal at 1,3m on apparent large granite corestone?
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,1--1,2m.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

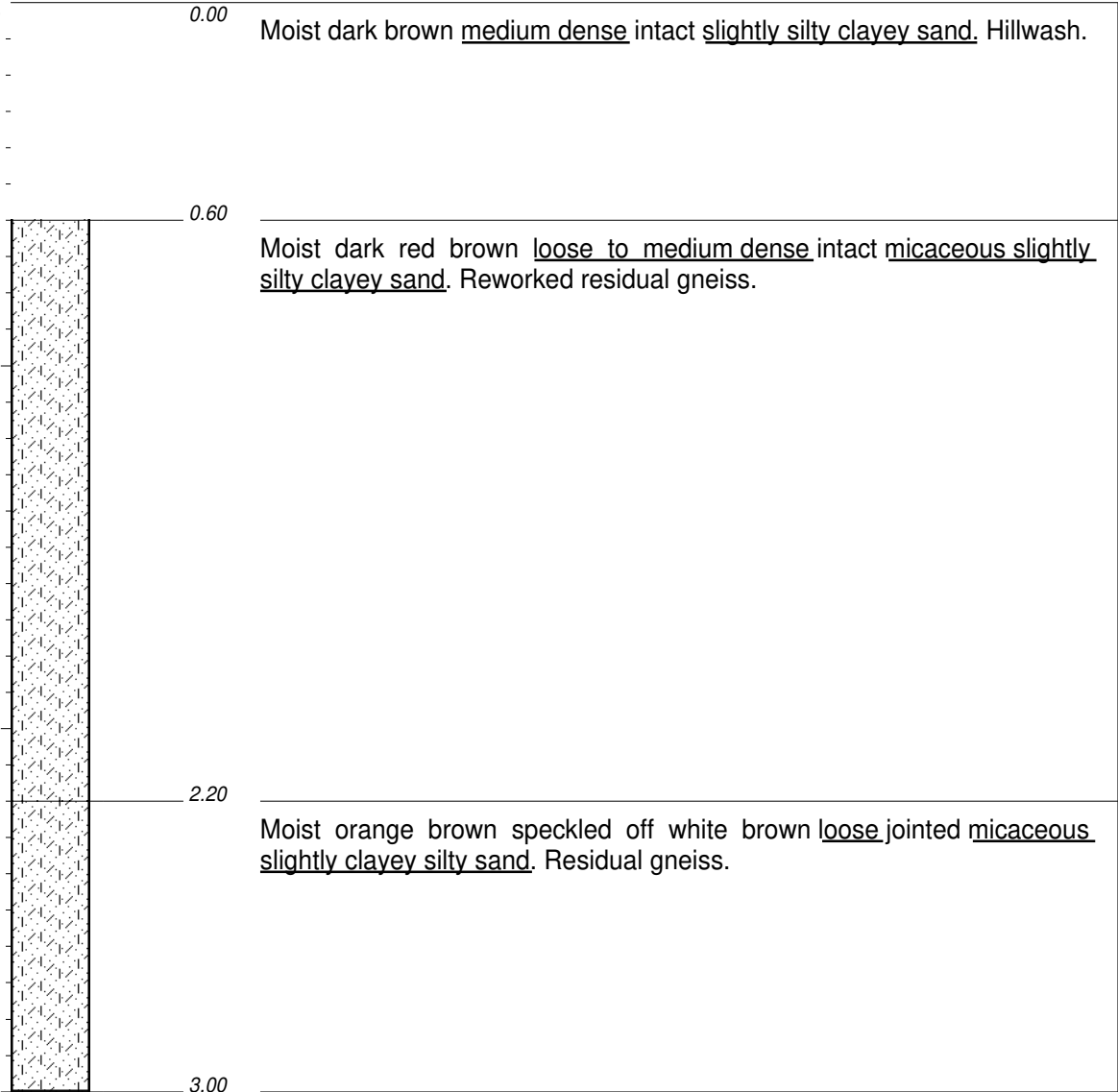
INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :

TYPE SET BY : JvH  
 SETUP FILE : STANDARD.SET



Scale  
1:20



NOTES

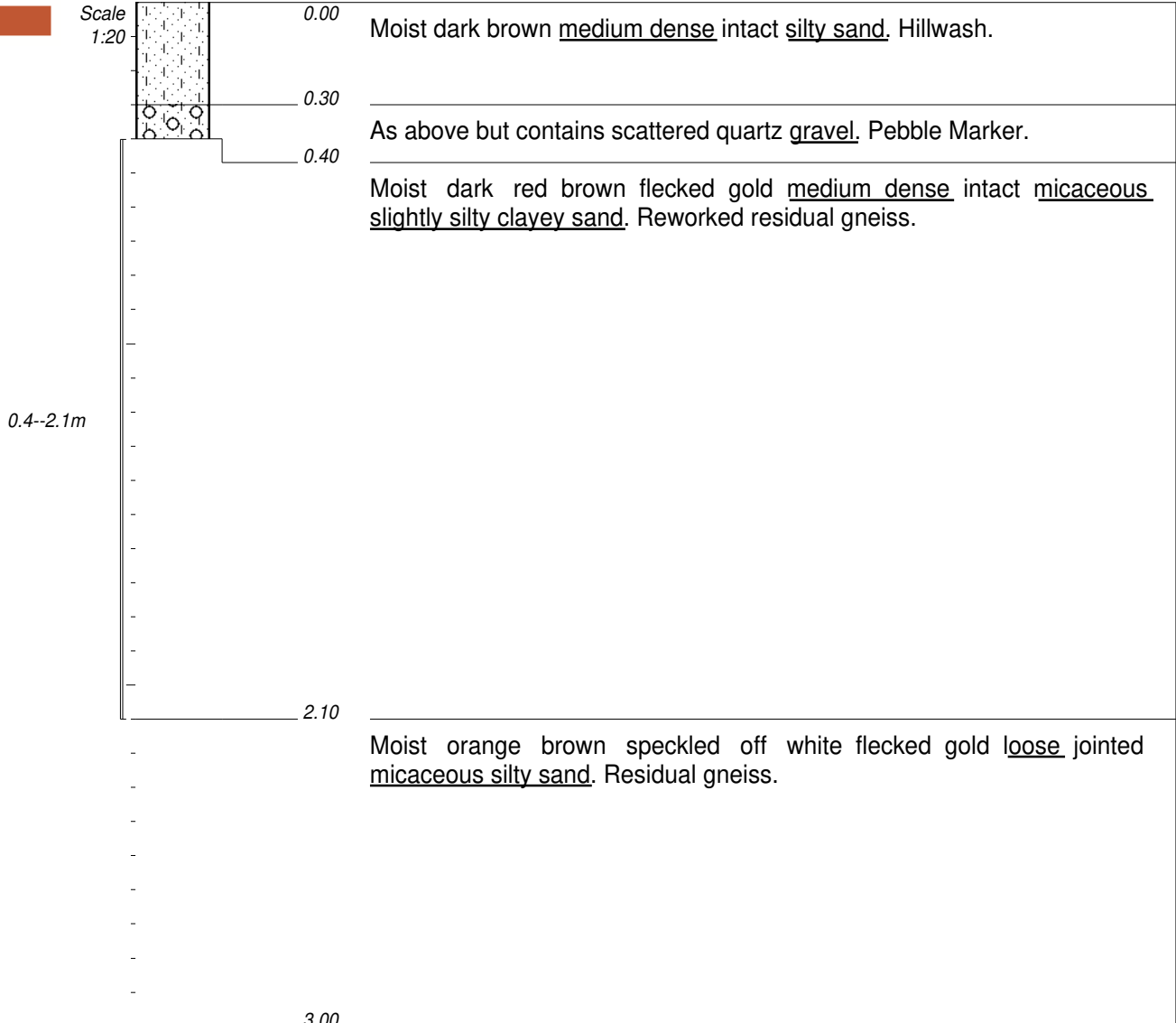
- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :

TYPE SET BY : JvH  
SETUP FILE : STANDARD.SET

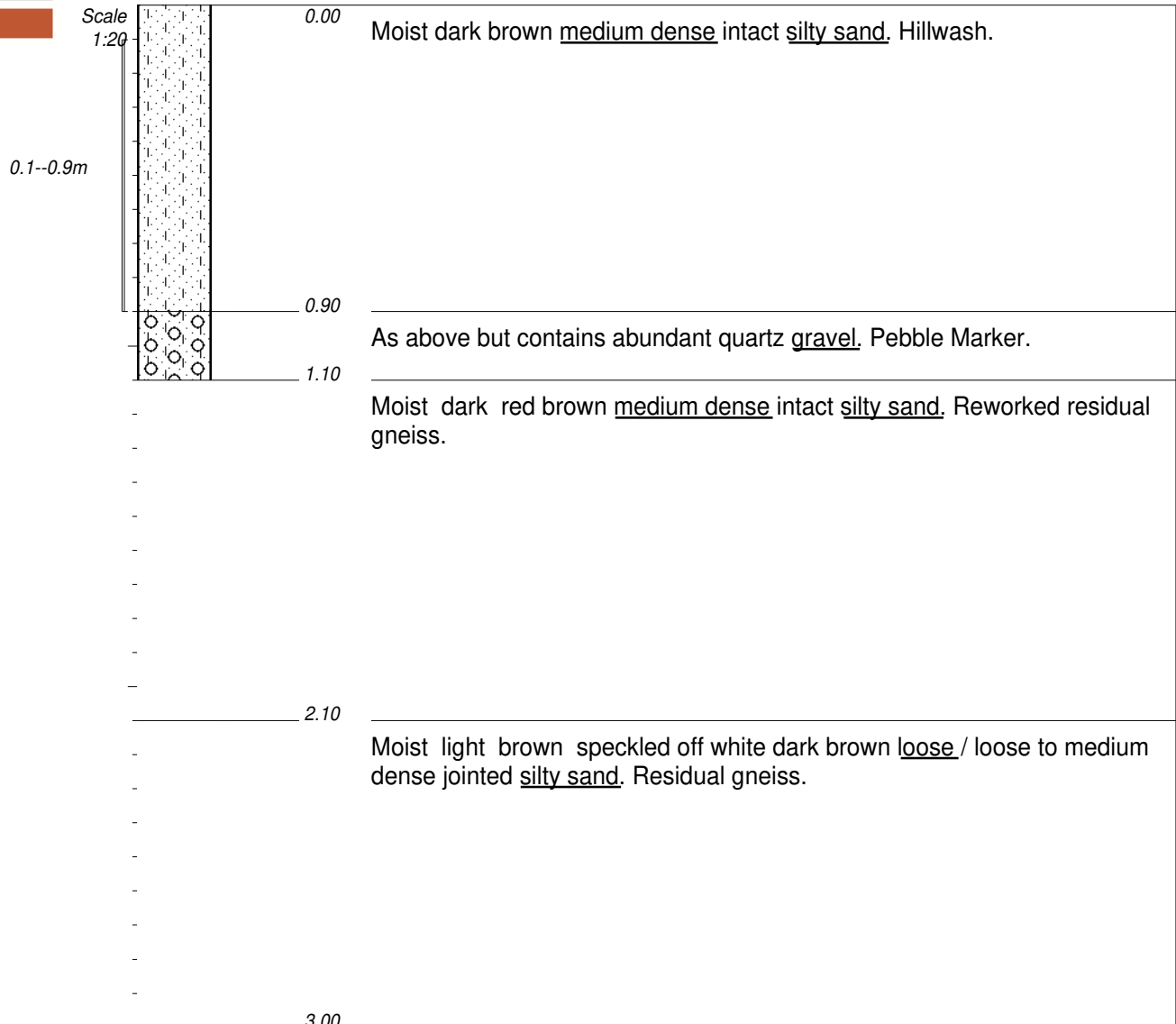


- NOTES
- 1) No refusal at 3,0m.
  - 2) No evidence of water.
  - 3) Disturbed sample taken at 0,4--2,1m.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel  
TYPE SET BY : JvH  
SETUP FILE : STANDARD.SET

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :  
HOLE No: TP12



NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,1--0,9m.

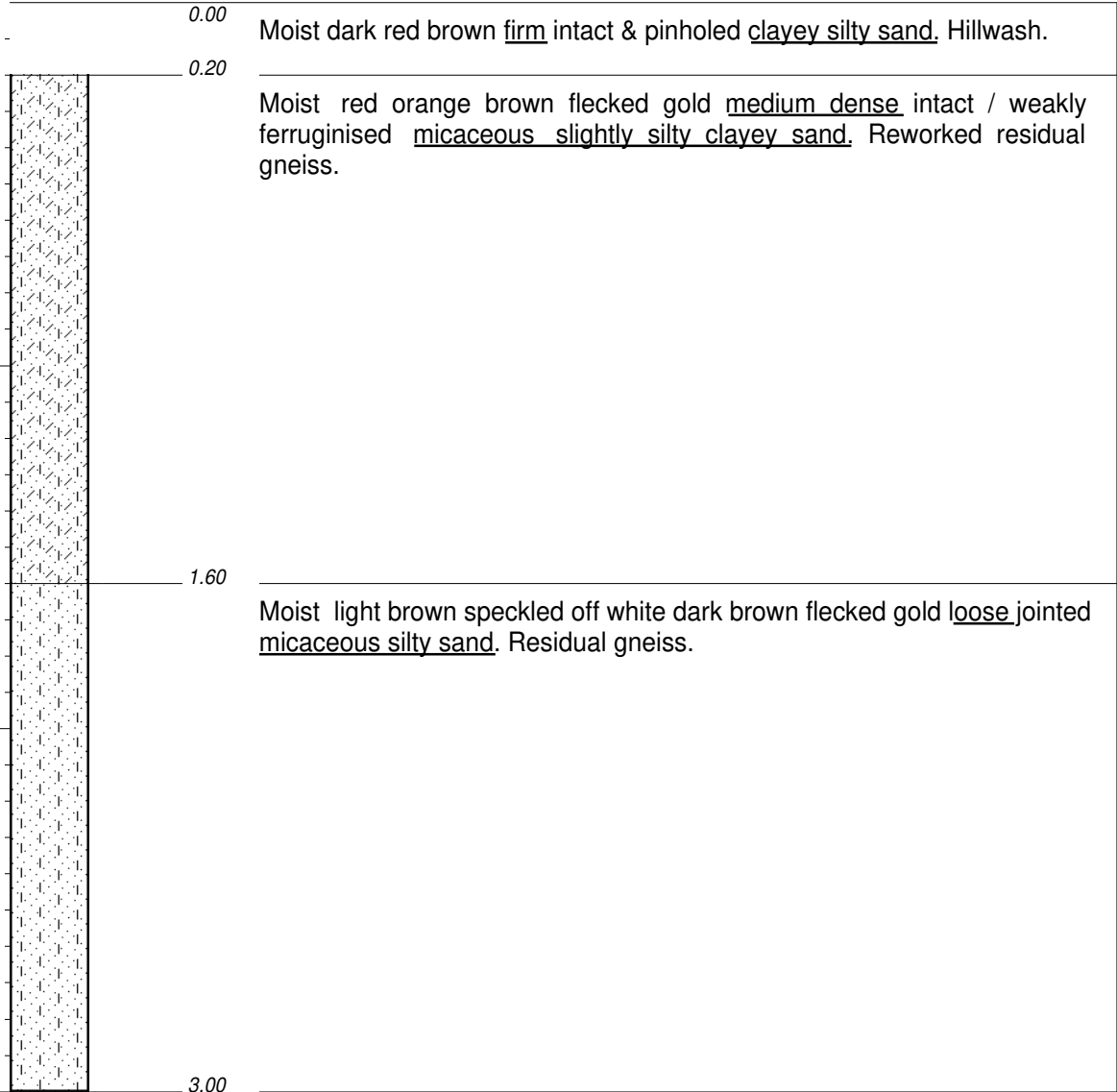
CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :



Scale  
1:20



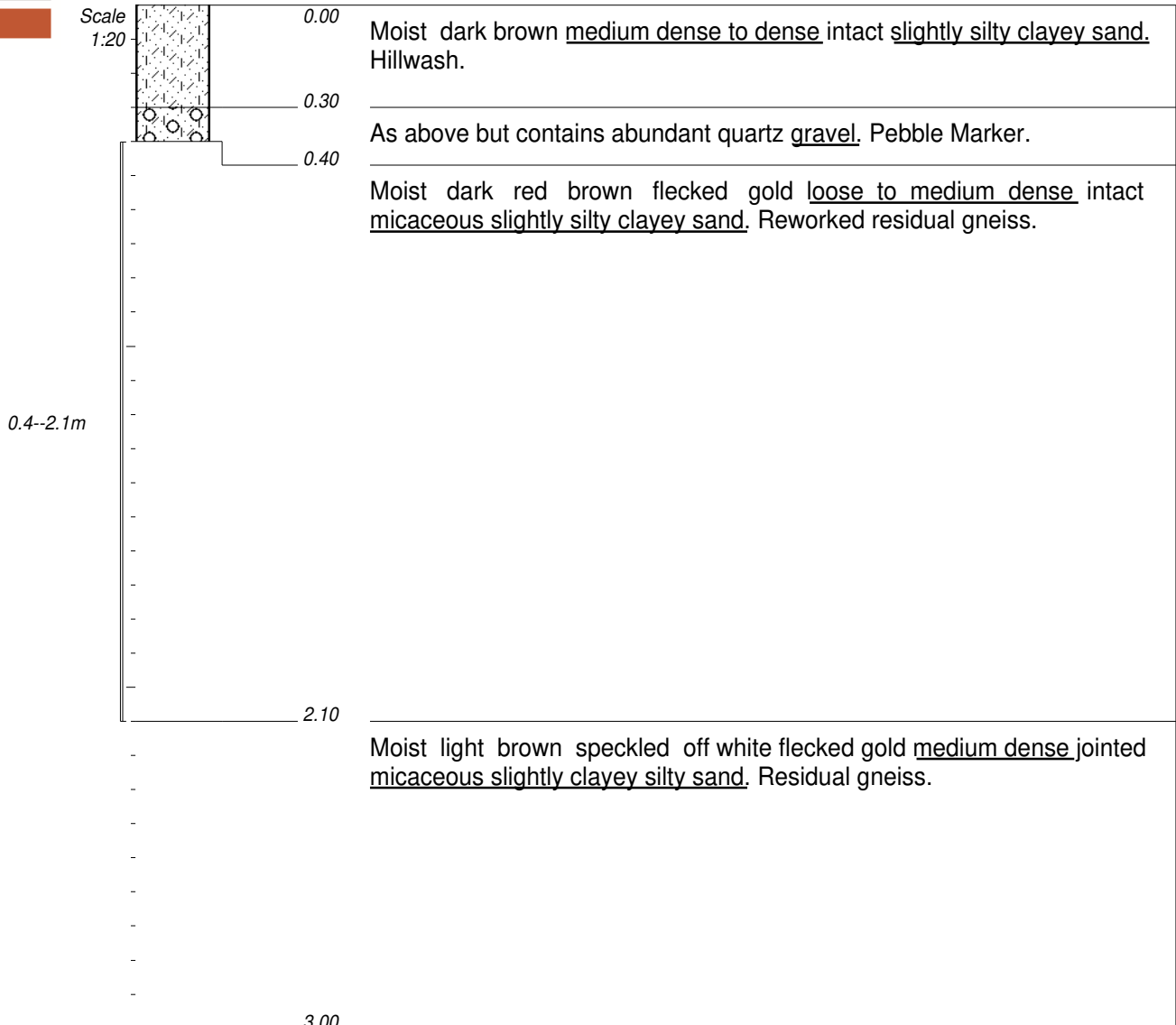
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



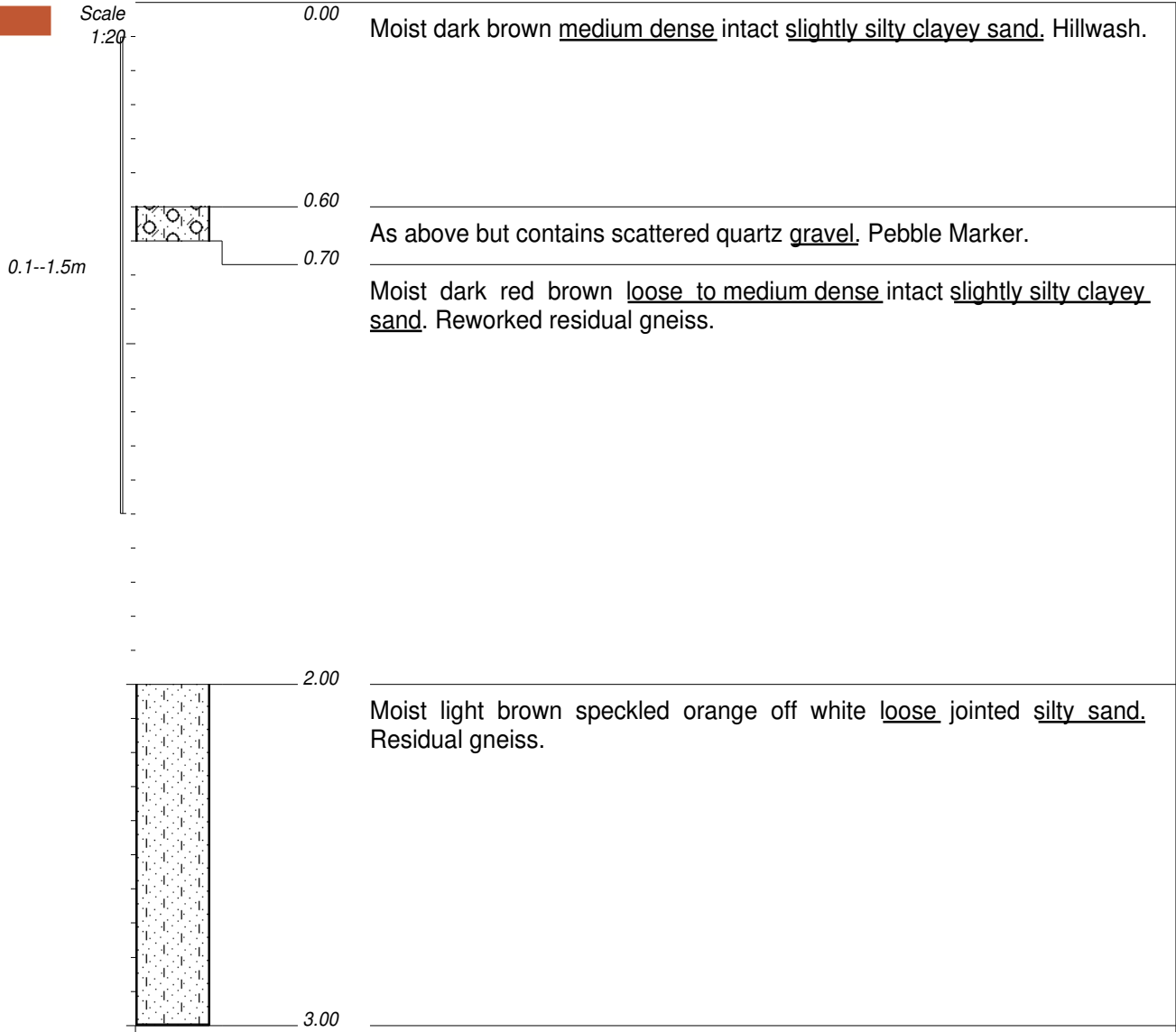
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,4--2,1m.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,1--1,5m.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel  
 TYPE SET BY : JvH  
 SETUP FILE : STANDARD.SET

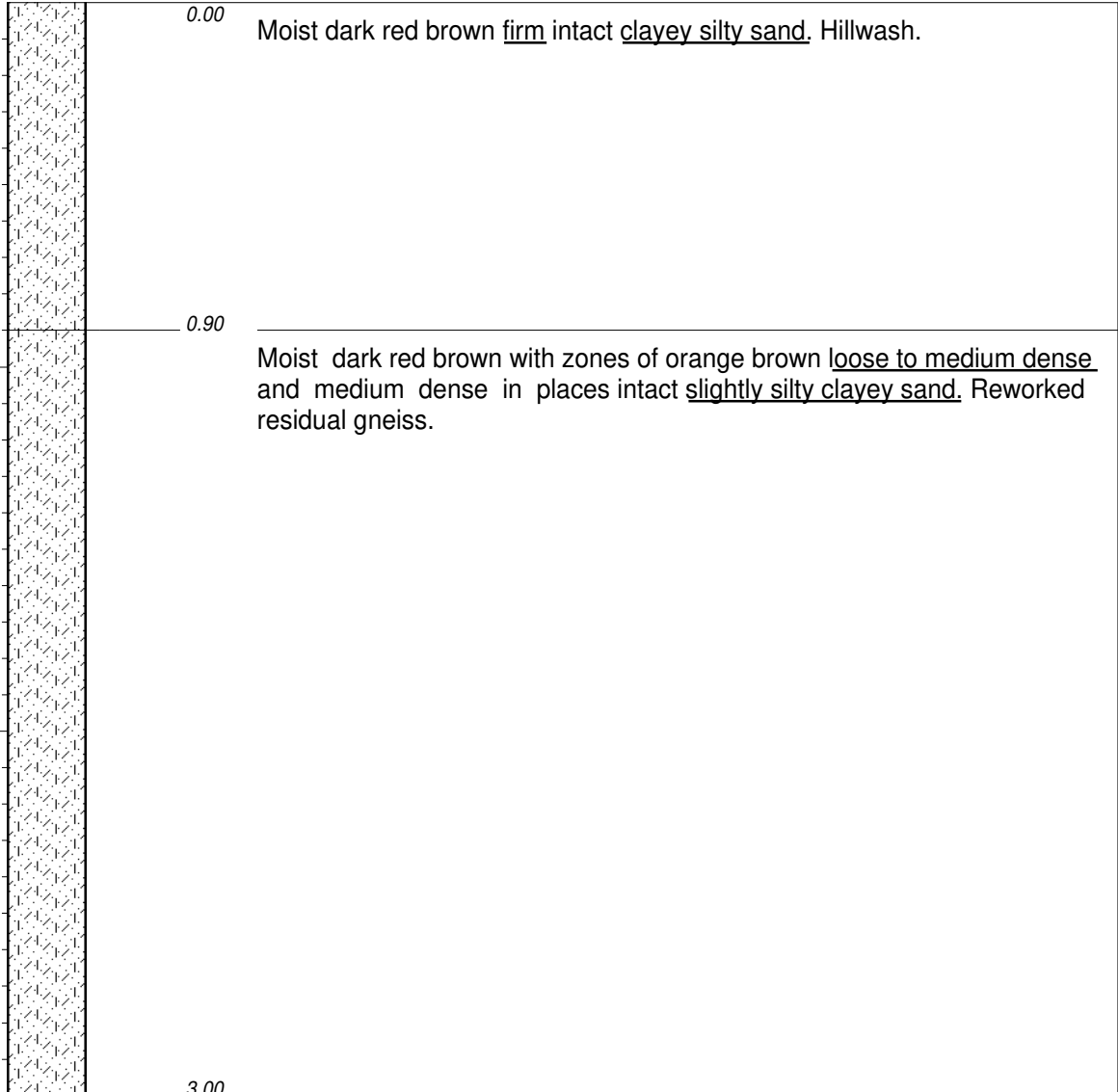
INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :





Scale  
1:20



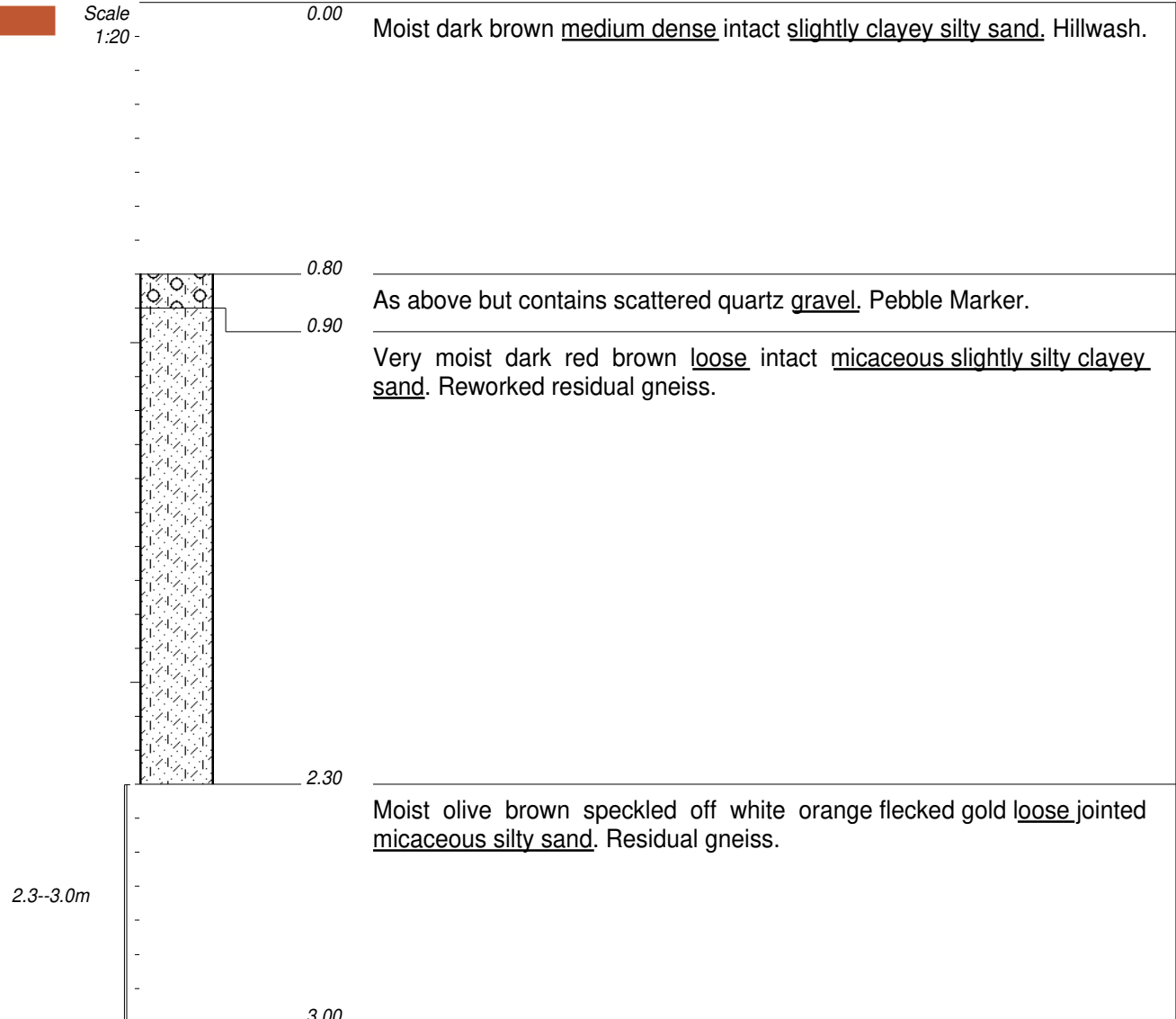
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :



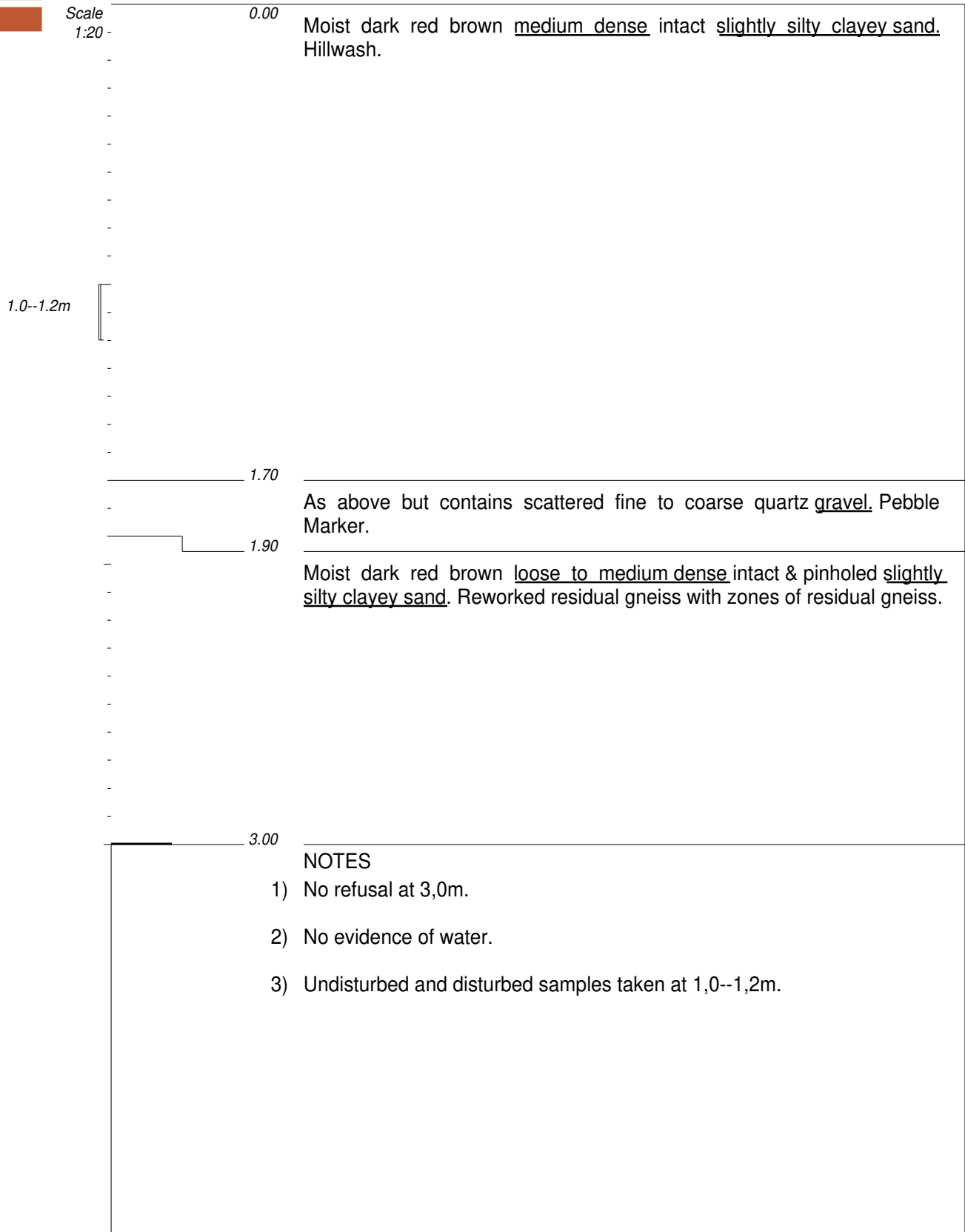
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 2,3--3,0m.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



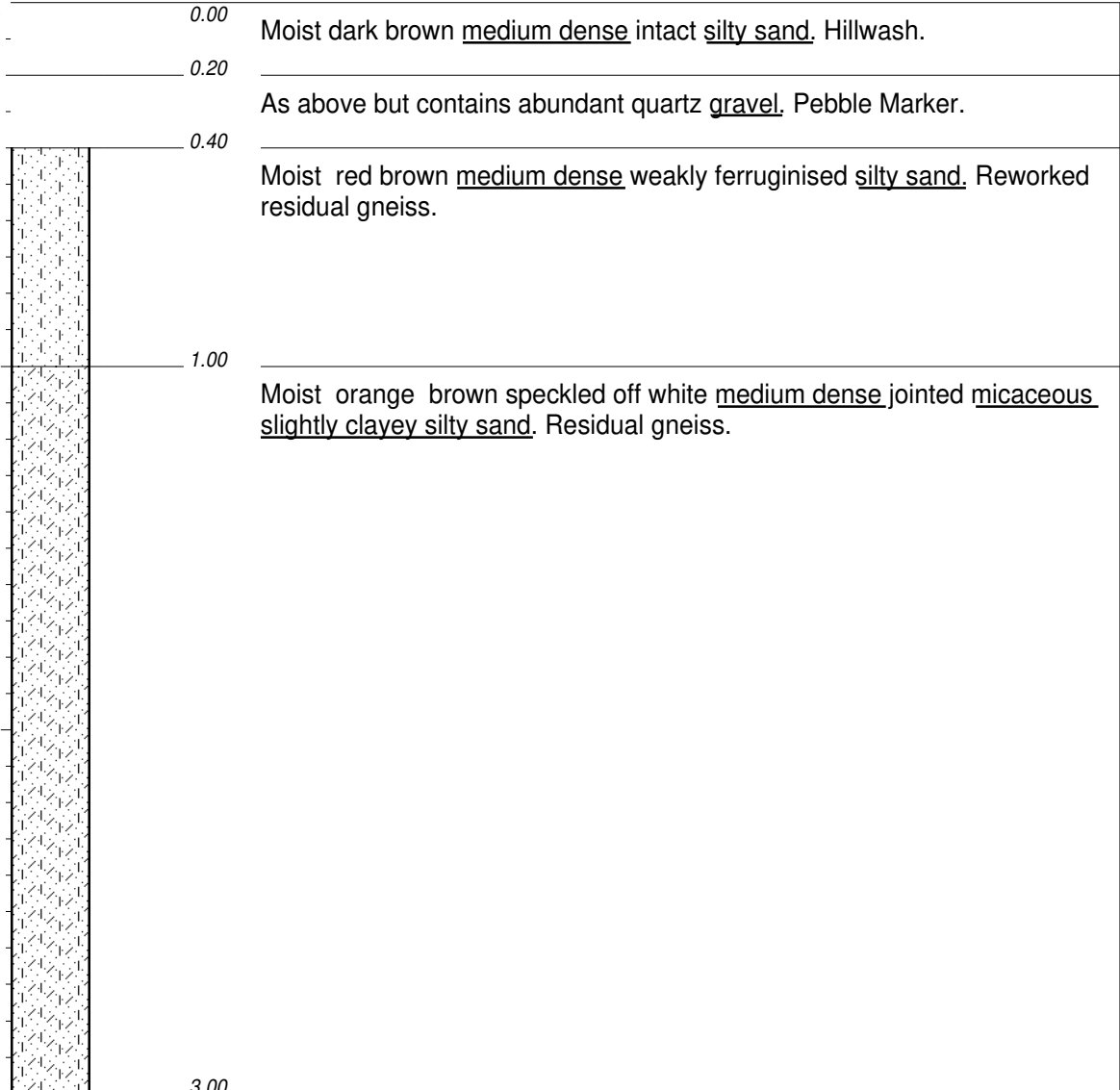
CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel  
 TYPE SET BY : JvH  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :



Scale  
1:20



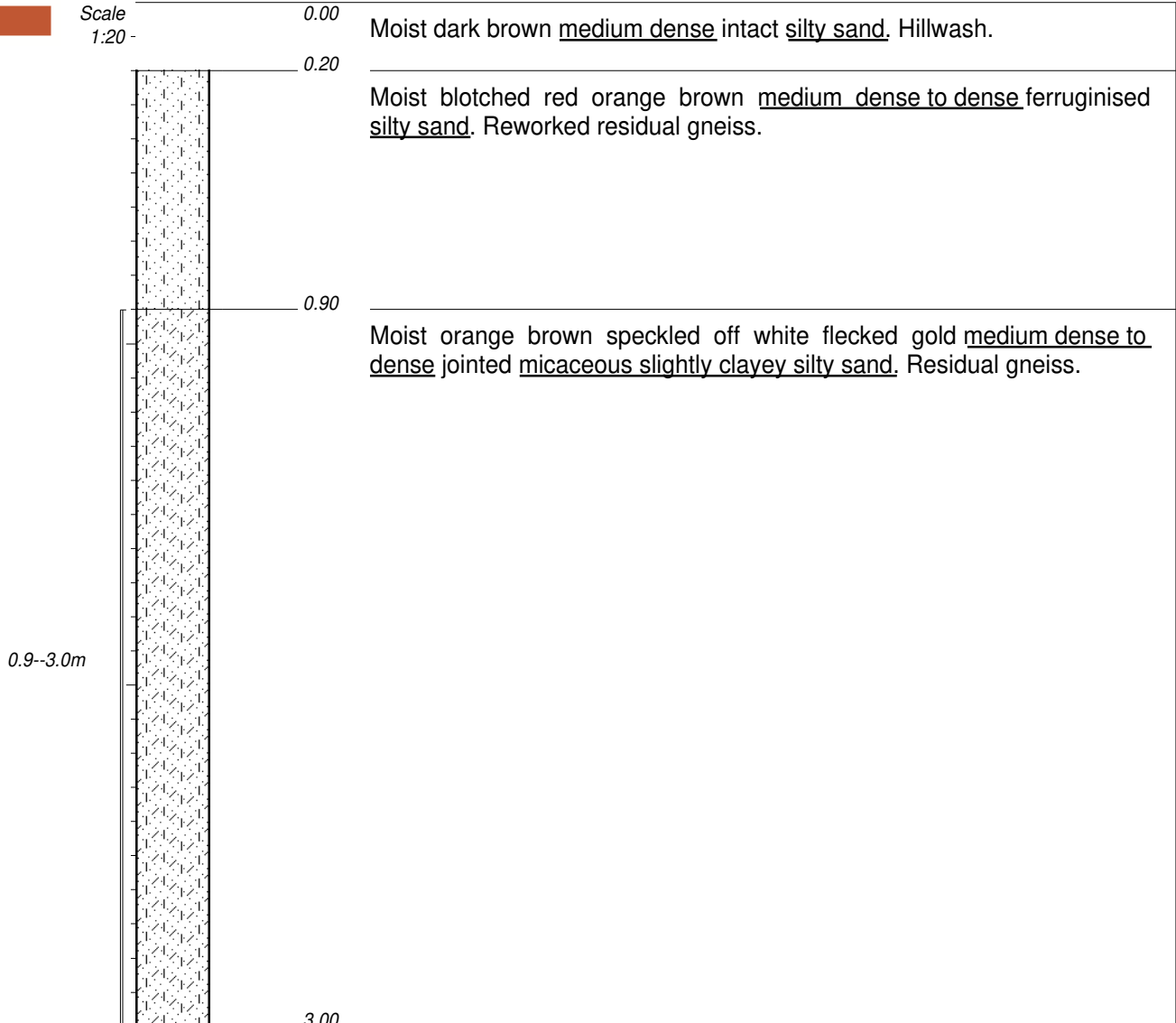
NOTES

- 1) N refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



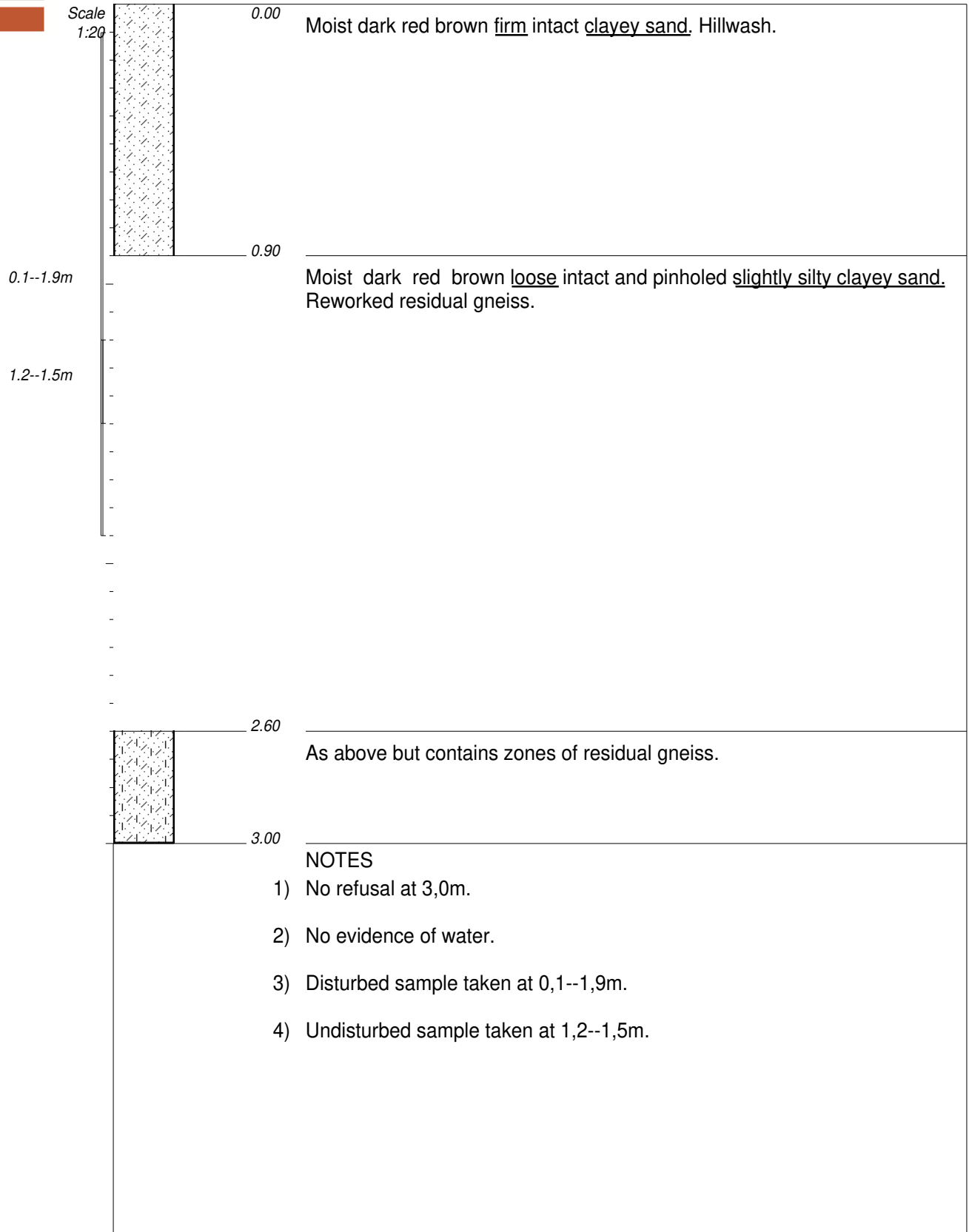
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,9--3,0m.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

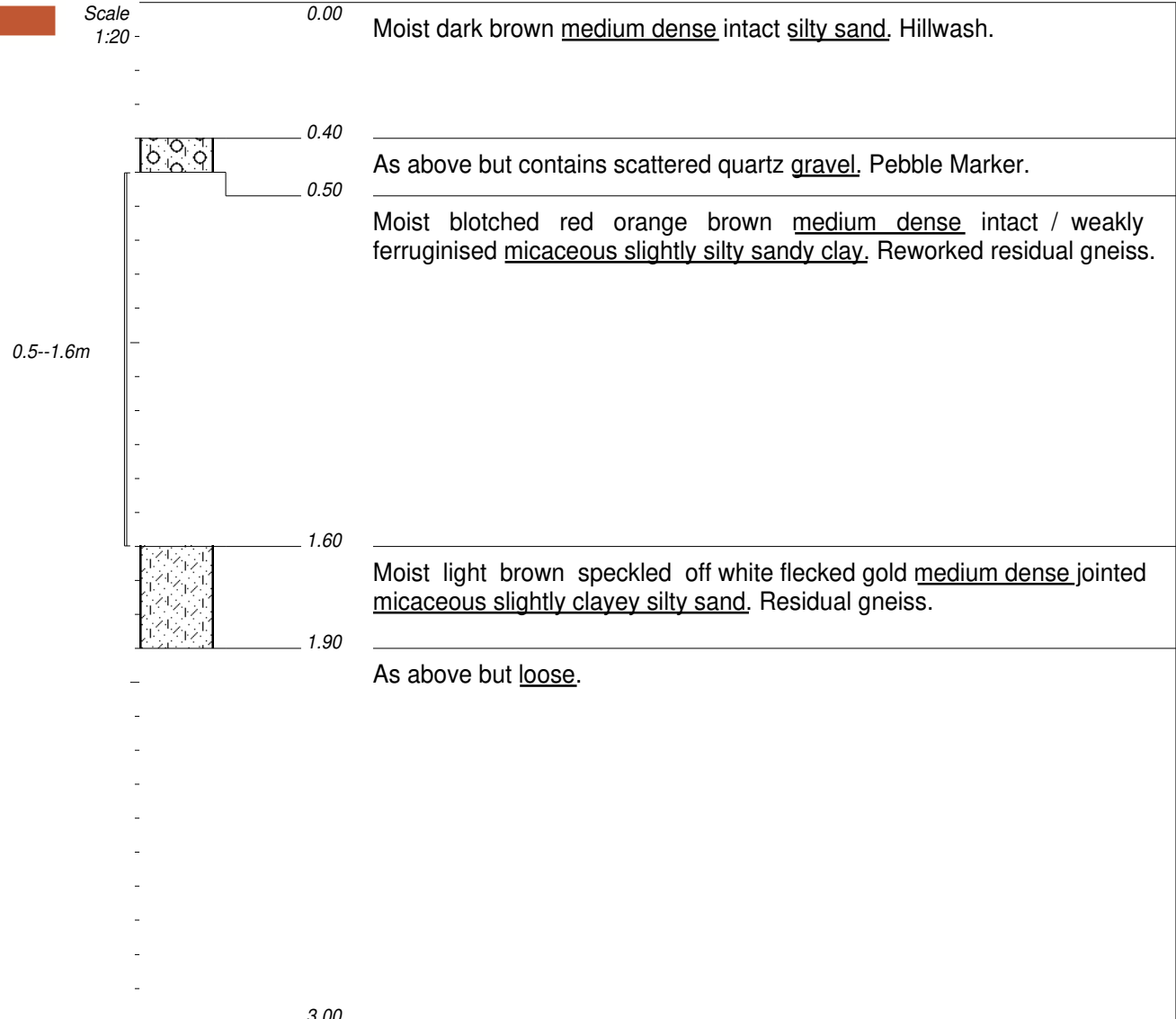
ELEVATION :  
 X-COORD :  
 Y-COORD :



CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,5--1,6m.

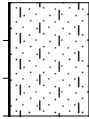
CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



Scale  
1:20



0.00

Moist dark brown medium dense intact silty sand. Hillwash.

0.30

As above but contains abundant fine to coarse quartz gravel. Pebble Marker.

0.50

Moist dark brown mottled and blotched orange brown medium dense intact / weakly ferruginised slightly silty clayey sand. Reworked residual gneiss with scattered zones of residual gneiss.

1.00

Moist orange brown speckled off white flecked gold medium dense jointed micaceous slightly clayey silty sand. Residual gneiss.

2.50

NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

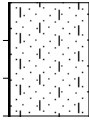
INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :





Scale  
1:20



0.00

Moist dark brown medium dense intact silty sand. Hillwash.

0.30

Moist blotched dark brown orange medium dense intact / weakly ferruginised slightly silty clayey sand. Reworked residual gneiss.

0.90

Moist orange brown speckled off white flecked gold medium dense jointed micaceous silty sand. Residual gneiss.

3.00

NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

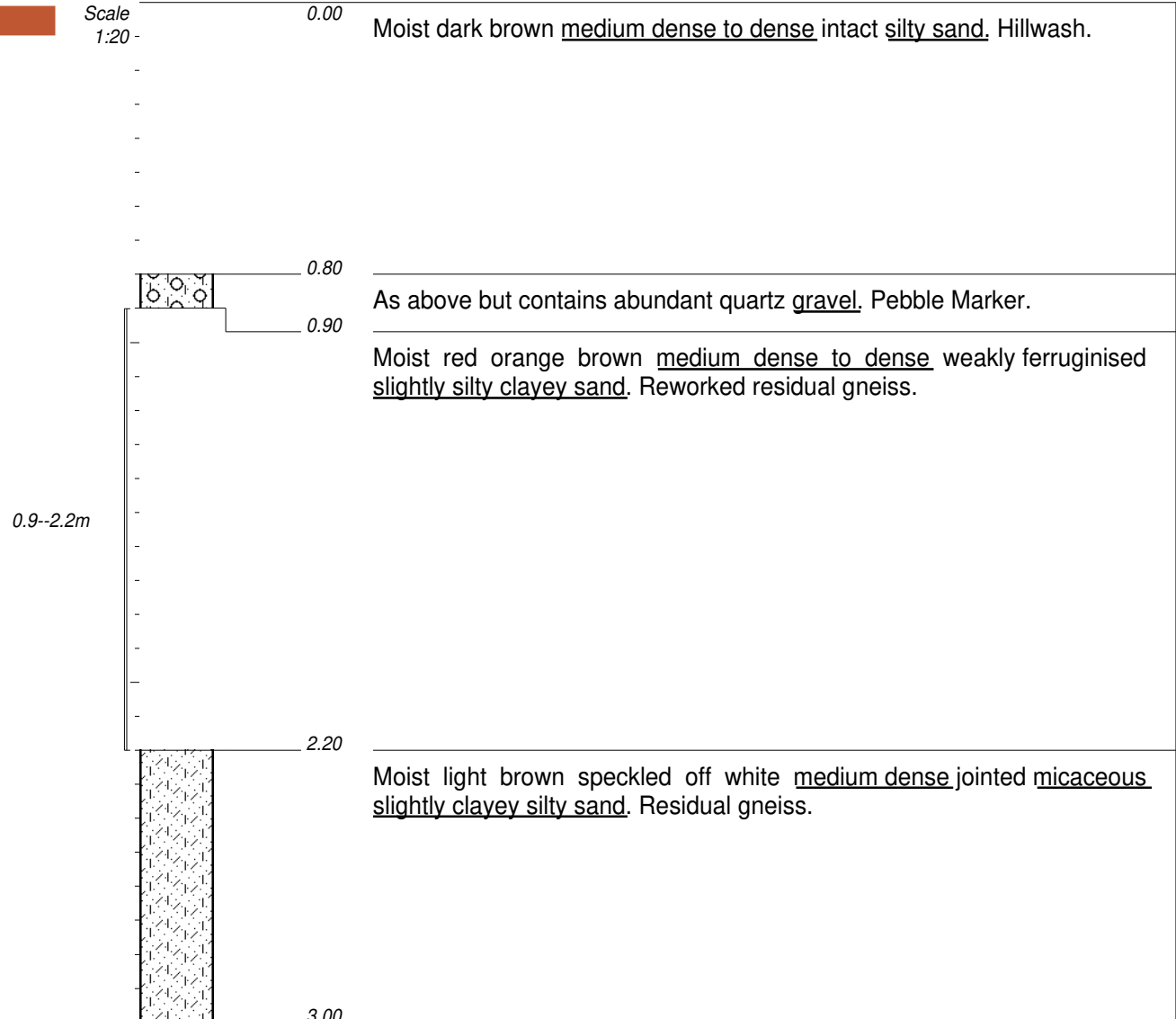
CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

TYPE SET BY : JvH  
SETUP FILE : STANDARD.SET

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020

DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



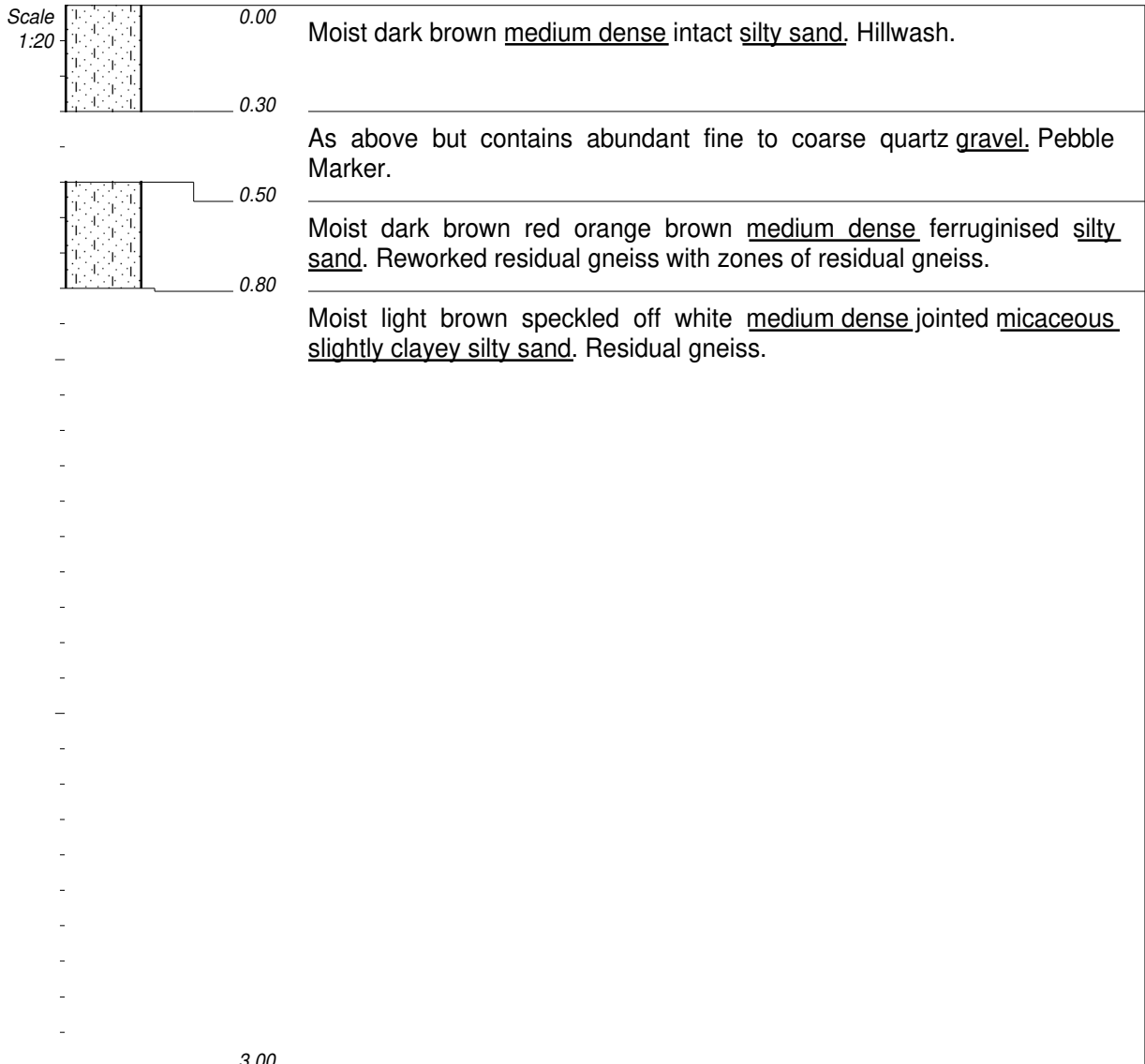
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,9--2,2m.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :



NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

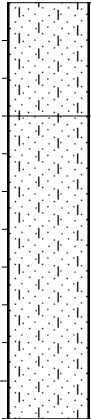
CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



Scale  
1:20



0.00

Moist dark brown medium dense intact silty sand. Hillwash.

0.30

Moist dark red brown blotched orange brown medium dense to dense ferruginised micaceous silty sand. Reworked residual gneiss with zones of residual gneiss.

1.10

Moist orange brown speckled off white brown flecked gold medium dense to dense jointed micaceous silty sand. Residual gneiss.

3.00

NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

TYPE SET BY : JvH  
SETUP FILE : STANDARD.SET

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020

DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



Scale  
1:20

0.00

Moist red brown medium dense intact silty sand. Hillwash.

0.20

Moist red brown medium dense intact silty sand. Reworked residual gneiss.

1.10

Moist orange brown speckled off white medium dense jointed micaceous silty sand. Residual gneiss.

1.1--3.0m

3.00

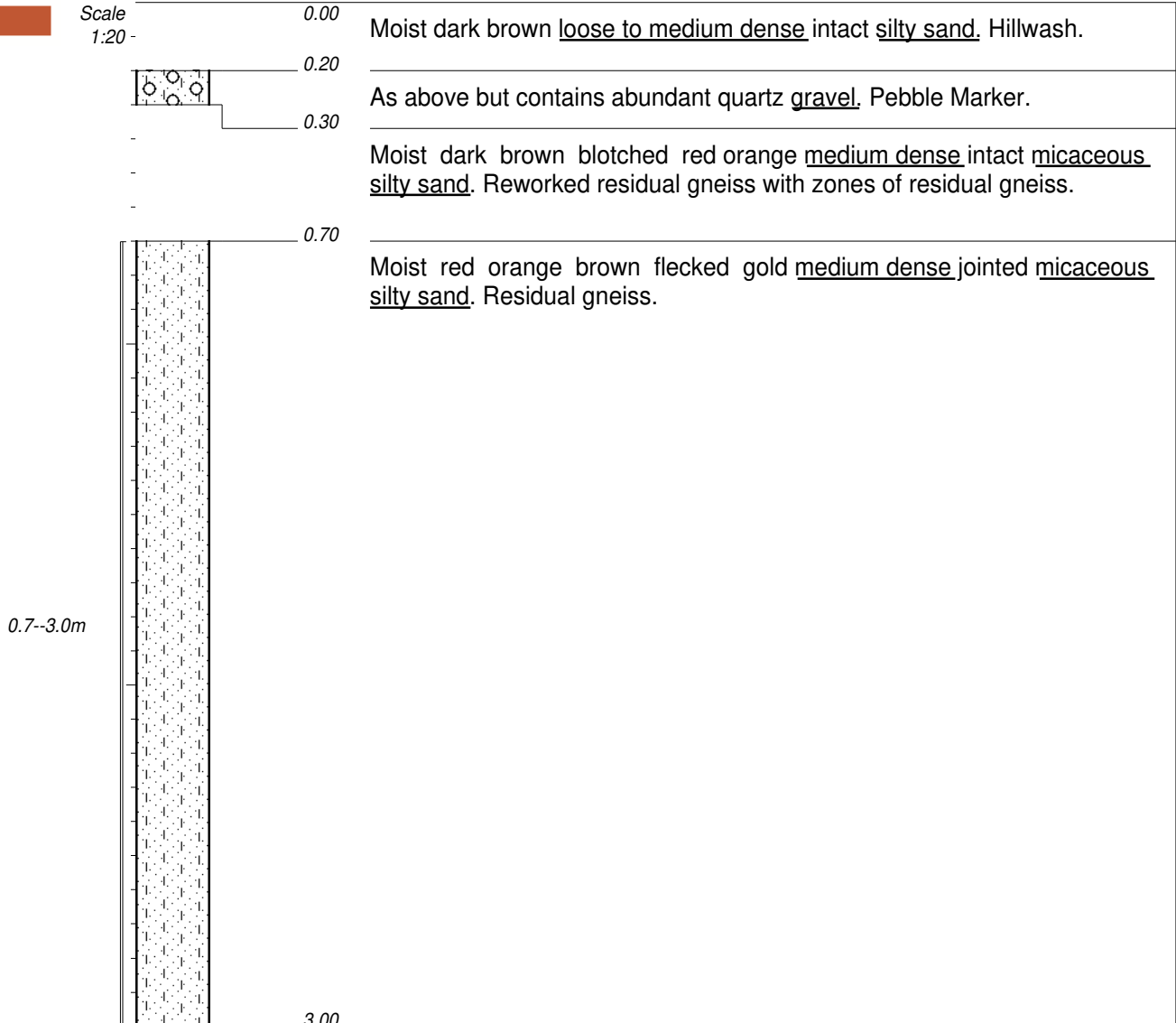
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 1,1--3,0m.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



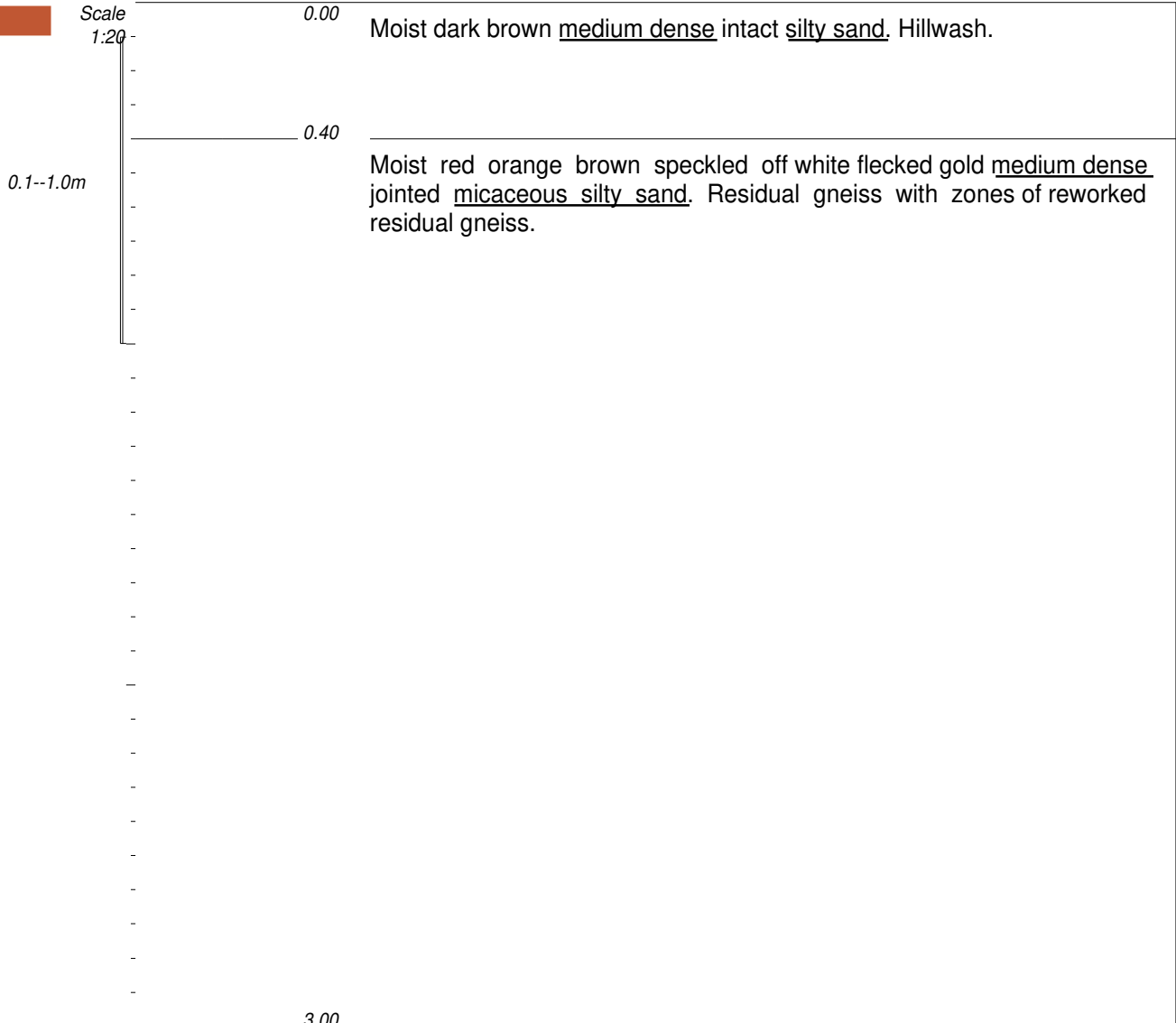
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,7--3,0m.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :



NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,1--1,0m.

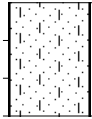
CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :



Scale  
1:20



0.00

Moist dark brown medium dense intact silty sand. Hillwash.

0.30

As above but contains scattered fine to coarse quartz gravel. Pebble Marker.

0.50

Moist red orange brown medium dense intact silty sand. Reworked residual gneiss.

1.20

Moist orange brown speckled off white dark brown medium dense jointed micaceous silty sand. Residual gneiss.

3.00

NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

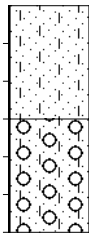
INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :





Scale  
1:20



0.00

Moist dark brown medium dense intact silty sand. Hillwash.

0.30

As above but contains abundant fine to coarse quartz gravel. Pebble Marker.

0.60

Moist dark brown loose to medium dense intact silty sand. Reworked residual gneiss.

1.10

Moist orange brown speckled off white flecked gold medium dense jointed micaceous silty sand. Residual gneiss.

3.00

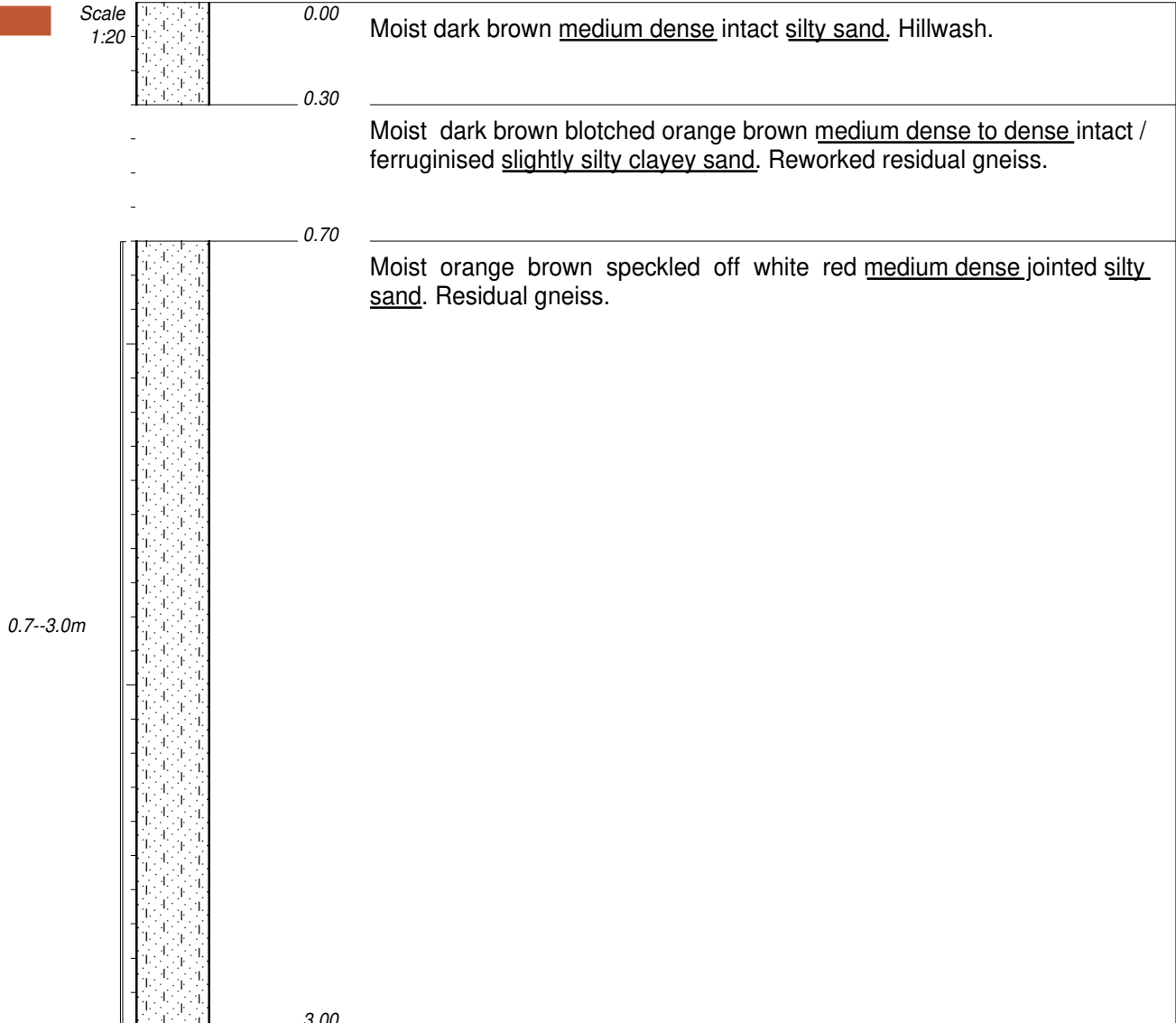
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
MACHINE : JCB 3CX  
DRILLED BY :  
PROFILED BY : J Davel

INCLINATION :  
DIAM :  
DATE :  
DATE : 01/06/2020  
DATE : 01/07/2020 12:03  
TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
X-COORD :  
Y-COORD :



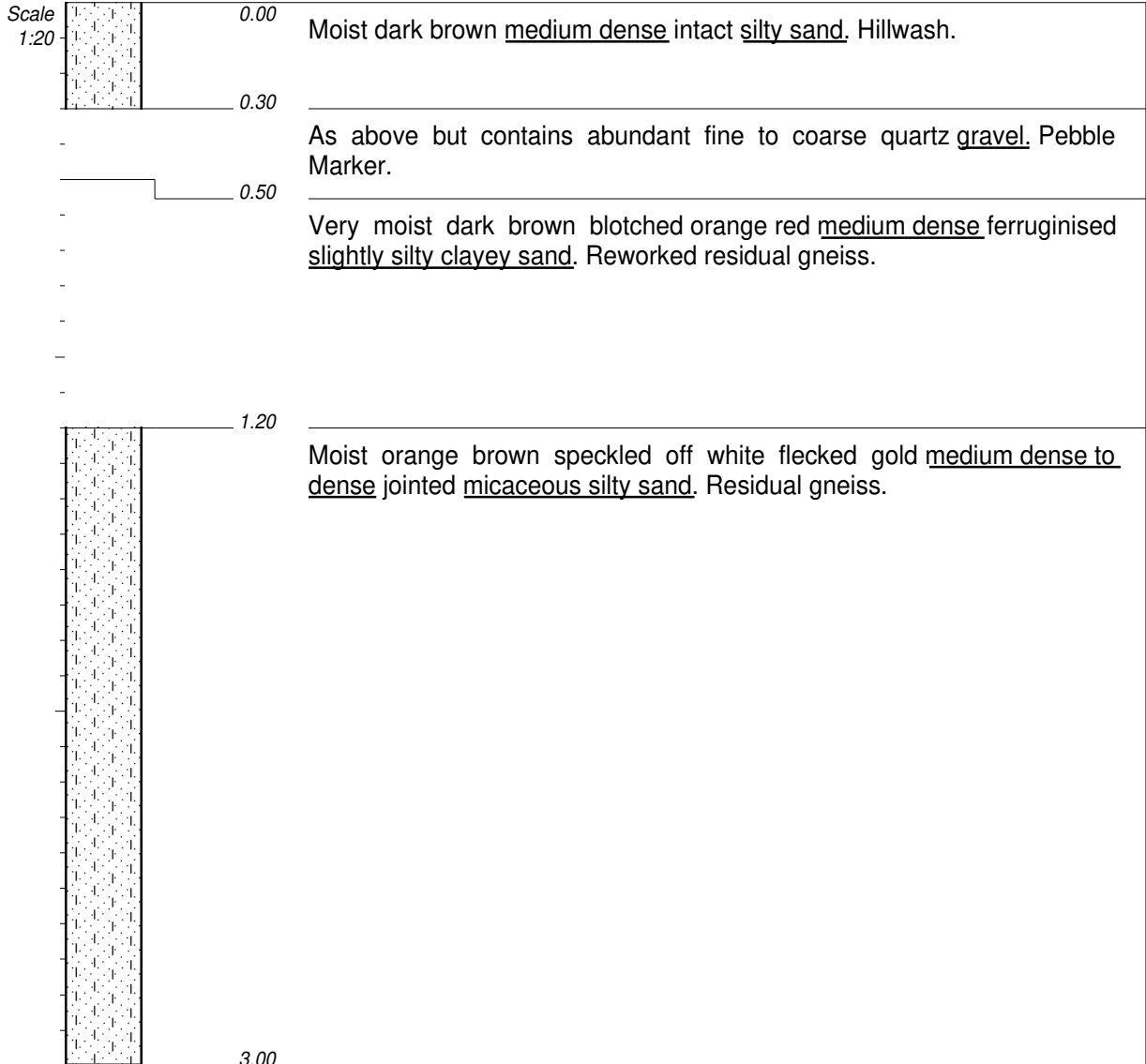
NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.
- 3) Disturbed sample taken at 0,7--3,0m.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel  
 TYPE SET BY : JvH  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :



NOTES

- 1) No refusal at 3,0m.
- 2) No evidence of water.

CONTRACTOR :  
 MACHINE : JCB 3CX  
 DRILLED BY :  
 PROFILED BY : J Davel

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 01/06/2020  
 DATE : 01/07/2020 12:03  
 TEXT : ..iles\2028TPAcornCity.txt

ELEVATION :  
 X-COORD :  
 Y-COORD :

TYPE SET BY : JvH  
 SETUP FILE : STANDARD.SET

**DVH-20-28 Acorn City Mixed Use Development – Test Pit Coordinates (WGS84 Lo. 31)**

<b>Test Pit Number</b>	<b>Y Coordinate</b>	<b>X Coordinate</b>
TP01	Y-004148	X2725287
TP02	Y-004167	X2725428
TP03	Y-004186	X2725571
TP04	Y-004206	X2725718
TP05	Y-004220	X2725855
TP06	Y-004238	X2725989
TP07	Y-004255	X2726127
TP08	Y-004228	X2726267
TP09	Y-004289	X2726411
TP10	Y-004293	X2726531
TP11	Y-004167	X2726535
TP12	Y-004146	X2726390
TP13	Y-004125	X2726249
TP14	Y-004104	X2726101
TP15	Y-004081	X2725958
TP16	Y-004065	X2725817
TP17	Y-004049	X2725673
TP18	Y-004033	X2725533
TP19	Y-004018	X2725398
TP20	Y-004010	X2725299
TP21	Y-003923	X2725297
TP22	Y-003880	X2725456
TP23	Y-003895	X2725593
TP24	Y-003919	X2725733
TP25	Y-003940	X2725866
TP26	Y-003961	X2726002
TP27	Y-003981	X2726144
TP28	Y-003997	X2726282
TP29	Y-004011	X2726406
TP30	Y-004024	X2726539
TP31	Y-003903	X2726546
TP32	Y-003884	X2726408
TP33	Y-003859	X2726264
TP34	Y-003839	X2726104
TP35	Y-003822	X2725950
TP36	Y-003837	X2725784

<b>Client</b> :	DAVEL & VAN HUYSTEEN CONSULTING (PTY)	<b>Client Reference</b> :	
<b>Address</b> :	9 LANGWA STREET	<b>Order No.</b> :	Justin
	STRIJDOPARK		
	RANDBURG		
<b>Attention</b> :		<b>Date Received</b> :	03/06/2020
<b>Facsimile</b> :		<b>Date Tested</b> :	03/06/2020 - 26/06/2020
<b>E-mail</b> :	justin.davel@dvhgeotech.co.za; justin.vanhuy:	<b>Date Reported</b> :	26/06/2020
<b>Project</b> :	Acorn City	<b>Report Status</b> :	Final
<b>Project No.</b> :	2020-B-553	<b>Page</b> :	1 of 28

Herewith please find the test report(s) pertaining to the above project. All tests were conducted in accordance with prescribed test method(s). Information herein consists of the following:

Test(s) conducted / Item(s) measured	Qty.	Test Method(s)	Authorized By**	Page(s)
Moisture Density Relationship	5.000	SANS 3001 GR30	S Pullen/B Mvubu	21-25
pH of Soil *	12.000	TMH1 A20	B Mvubu	2-13
Conductivity of saturated soil paste *	12.000	TMH1 A21T	B Mvubu	2-13
Atterberg Limits <0.425mm	19.000	SANS 3001 GR10	S Pullen/J Marques/ B Mvubu	14-20, 26-28
Sieve Analysis 0.075mm	19.000	SANS 3001 GR1	S Pullen/J Marques/ B Mvubu	14-20, 26-28
California Bearing Ratio (CBR)	5.000	SANS 3001 GR40	B Mvubu	26-28
Oedometer: Collapse Potential	3.000	BS 1377 Part5	C Pertesen	3Files; 9Pages

Any test results contained in this report and marked with \* in the table above are "not SANAS accredited" and are not included in the schedule of accreditation for this laboratory.

Any information contained in this test report pertain only to the areas and/or samples tested. Documents may only be reproduced or published in their full context.

While every care is taken to ensure that all tests are carried out in accordance with recognised standards, neither Civilab (Proprietary) Limited nor its employess shall be liable in any way whatsoever for any error made in the execution or reporting of tests or any erroneous conclusions drawn therefrom or for any consequences thereof.

All interpretations, Interpolations, Opinions and/or Classifications contained in this report falls outside our scope of accreditation.

The following parameters, where applicable, were excluded from the classification procedure: Chemical modifications, Additional fines, Fractured Faces, Soluble Salts, pH, Conductivity, Coarse Sand Ratio, Durability (COLTO: G4-G9).

The following parameters, where applicable, were assumed: Rock types were assumed to be of an Arenaceous nature with Siliceous cementing material.

Unless otherwise requested or stated, all samples will be discarded after a period of 3 months.

This report is completely confidential between the parties (Civilab and Civilab's client) and shall not be disclosed to anybody else, unless agreed upon in writing or made publicly available by the client or required to make available by law.

Deviations in Test Methods:

Technical Signatory:	
Signature:	

\*\*All results are authorized electronically by approved managers and/or technical signatories.

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## AGGREGATE TEST REPORT

Laboratory Number	4		
Field Number	TP8		
Client Reference			
Depth (m)	0.1-1.3		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

% Passing		mm		Fines Modulus			
		mm		Clay Content	SANS 3001 GR3	%	37
		mm		Organic Impurities		Ref.	
		mm		Flakiness Index	Total		
		mm					%
		mm		Average Least Dimension	Manual		mm
		mm			Machine		
		mm			Computation		
		mm		Aggregate Crushing Value	Dry		%
		mm			Wet		
		mm			Eth. Glycol		
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN
		mm			Wet		
		mm			Eth. Glycol		
		mm		Bulk Density	Wet/Dry Ratio		%
		mm			Loose		kg/m <sup>3</sup>
		mm		Compacted			
		mm		Water Absorption		%	
Sand Equivalent, Se							
pH			6.2				
Relative Density of Soils				Bulk Particle Density		kg/m <sup>3</sup>	
Durability Mill Index				Aggregate			
Moisture Content		%		Apparent Particle Density		kg/m <sup>3</sup>	
Compactibility Factor							
Conductivity		S.m <sup>-1</sup>	0.004				
Total Water Soluble	Salts	%		Adjusted Relative			
	Sulphates	%					
Soluble	Salts	%		LA Abrasion	1000 Revs	%	
	Sulphates	%			500 Revs		
Soundness	Fine	%		Riedel & Weber			
	Coarse			Akali Silica Reaction		%	
	Fractions	No.		Drying Shrinkage		%	
Methylene Blue Absorption				Wetting Expansion		%	
Soluble Deleterious Impurities		%		Fractured Faces		%	
Chloride Content		%		Coarse Sand Ratio		%	
Low Density Material		%		Shape: Voids		%	
Presence of Sugar				Shell Content		%	
Mill Abrasion				Durability	Ballast		
Tretton Value				Eth. Glycol Durability on	Concrete		
Vialit Adhesion @	5°C	%			Crushed		
	25°C	%		_ Stone	Seal		



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## AGGREGATE TEST REPORT

Laboratory Number	7		
Field Number	TP13		
Client Reference			
Depth (m)	0.1-0.9		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	47	
				Clay Content					
		mm		Organic Impurities			Ref.		
		mm		Flakiness Index	Total		%		
		mm							
		mm		Average Least Dimension	Manual		mm		
		mm			Machine				
		mm			Computation				
		mm		Aggregate Crushing Value	Dry		%		
		mm			Wet				
		mm			Eth. Glycol				
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN		
		mm			Wet				
		mm			Eth. Glycol				
		mm		Bulk Density	Loose		kg/m <sup>3</sup>		
		mm			Compacted				
		mm		Water Absorption			%		
		mm							
Sand Equivalent, Se pH			5.6	Bulk Particle Density	Aggregate		kg/m <sup>3</sup>		
Relative Density of Soils									
Durability Mill Index				Apparent Particle Density			kg/m <sup>3</sup>		
Moisture Content		%							
Compactibility Factor									
Conductivity		S.m <sup>-1</sup>	0.003	LA Abrasion	1000 Revs		%		
Total Water Soluble	Salts Sulphates	%						500 Revs	
Soluble	Salts Sulphates	%							
Soundness	Fine	%		Riedel & Weber					
	Coarse Fractions	No.		Akali Silica Reaction			%		
Methylene Blue Absorption				Drying Shrinkage			%		
Soluble Deleterious Impurities		%		Wetting Expansion			%		
Chloride Content		%		Fractured Faces			%		
Low Density Material		%		Coarse Sand Ratio			%		
Presence of Sugar				Shape: Voids			%		
Mill Abrasion				Shell Content			%		
Treton Value				Durability	Ballast				
Vialit Adhesion @	5°C	%		Eth. Glycol	Concrete				
	25°C	%		Durability on	Crushed				
				_ Stone	Seal				



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## AGGREGATE TEST REPORT

Laboratory Number	8		
Field Number	TP15		
Client Reference			
Depth (m)	0.4-2.1		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	35	
				mm	Clay Content				
		mm		Organic Impurities			Ref.		
		mm		Flakiness Index	Total		%		
		mm							
		mm		Average Least Dimension	Manual		mm		
		mm			Machine				
		mm			Computation				
		mm		Aggregate Crushing Value	Dry		%		
		mm			Wet				
		mm			Eth. Glycol				
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN		
		mm			Wet				
		mm			Eth. Glycol				
		mm		Bulk Density	Loose		kg/m <sup>3</sup>		
		mm			Compacted				
		mm		Water Absorption			%		
		mm							
Sand Equivalent, Se pH			5.9	Bulk Particle Density	Aggregate		kg/m <sup>3</sup>		
Relative Density of Soils									
Durability Mill Index				Apparent Particle Density			kg/m <sup>3</sup>		
Moisture Content		%							
Compactibility Factor									
Conductivity		S.m <sup>-1</sup>	0.003	LA Abrasion	1000 Revs		%		
Total Water Soluble	Salts Sulphates	%						500 Revs	
Soluble	Salts Sulphates	%							
Soundness	Fine	%		Riedel & Weber					
	Coarse Fractions	No.		Akali Silica Reaction			%		
Methylene Blue Absorption				Drying Shrinkage			%		
Soluble Deleterious Impurities		%		Wetting Expansion			%		
Chloride Content		%		Fractured Faces			%		
Low Density Material		%		Coarse Sand Ratio			%		
Presence of Sugar				Shape: Voids			%		
Mill Abrasion				Shell Content			%		
Treton Value				Durability	Ballast				
Vialit Adhesion @	5°C	%		Eth. Glycol	Concrete				
	25°C	%		Durability on	Crushed				
				_ Stone	Seal				

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## AGGREGATE TEST REPORT

Laboratory Number	10		
Field Number	TP18		
Client Reference			
Depth (m)	2.3-3.0		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	5	
				mm	Clay Content				
		mm		Organic Impurities			Ref.		
		mm		Flakiness Index	Total		%		
		mm							
		mm		Average Least Dimension	Manual		mm		
		mm			Machine				
		mm			Computation				
		mm		Aggregate Crushing Value	Dry		%		
		mm			Wet				
		mm			Eth. Glycol				
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN		
		mm			Wet				
		mm			Eth. Glycol				
		mm		Bulk Density	Loose		kg/m <sup>3</sup>		
		mm			Compacted				
		mm		Water Absorption			%		
		mm							
Sand Equivalent, Se pH			6.1	Bulk Particle Density	Aggregate		kg/m <sup>3</sup>		
Relative Density of Soils									
Durability Mill Index				Apparent Particle Density			kg/m <sup>3</sup>		
Moisture Content		%							
Compactibility Factor									
Conductivity		S.m <sup>-1</sup>	0.004	LA Abrasion	1000 Revs		%		
Total Water Soluble	Salts Sulphates	%						500 Revs	
Soluble	Salts Sulphates	%							
Soundness	Fine	%		Riedel & Weber					
	Coarse Fractions	No.		Akali Silica Reaction			%		
Methylene Blue Absorption				Drying Shrinkage			%		
Soluble Deleterious Impurities		%		Wetting Expansion			%		
Chloride Content		%		Fractured Faces			%		
Low Density Material		%		Coarse Sand Ratio			%		
Presence of Sugar				Shape: Voids			%		
Mill Abrasion				Shell Content			%		
Treton Value				Durability	Ballast				
Vialit Adhesion @	5°C	%		Eth. Glycol	Concrete				
	25°C	%		Durability on	Crushed				
				_ Stone	Seal				

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## AGGREGATE TEST REPORT

Laboratory Number	12		
Field Number	TP21		
Client Reference			
Depth (m)	0.9-3.0		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	20	
				Clay Content					
		mm		Organic Impurities			Ref.		
		mm		Flakiness Index	Total		%		
		mm							
		mm		Average Least Dimension	Manual		mm		
		mm			Machine				
		mm			Computation				
		mm		Aggregate Crushing Value	Dry		%		
		mm			Wet				
		mm			Eth. Glycol				
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN		
		mm			Wet				
		mm			Eth. Glycol				
		mm		Bulk Density	Loose		kg/m <sup>3</sup>		
		mm			Compacted				
		mm		Water Absorption			%		
		mm							
Sand Equivalent, Se pH			6.2	Bulk Particle Density	Aggregate		kg/m <sup>3</sup>		
Relative Density of Soils									
Durability Mill Index				Apparent Particle Density			kg/m <sup>3</sup>		
Moisture Content		%							
Compactibility Factor									
Conductivity		S.m <sup>-1</sup>	0.005	LA Abrasion	1000 Revs		%		
Total Water Soluble	Salts Sulphates	%						500 Revs	
Soluble	Salts Sulphates	%							
Soundness	Fine	%		Riedel & Weber					
	Coarse Fractions	No.		Akali Silica Reaction			%		
Methylene Blue Absorption				Drying Shrinkage			%		
Soluble Deleterious Impurities		%		Wetting Expansion			%		
Chloride Content		%		Fractured Faces			%		
Low Density Material		%		Coarse Sand Ratio			%		
Presence of Sugar				Shape: Voids			%		
Mill Abrasion				Shell Content			%		
Treton Value				Durability	Ballast				
Vialit Adhesion @	5°C	%		Eth. Glycol	Concrete				
	25°C	%		Durability on	Crushed				
				_ Stone	Seal				

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## AGGREGATE TEST REPORT

Laboratory Number		13	
Field Number		TP22	
Client Reference			
Depth (m)		0.1-0.9	
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

Test Name	Units	Value	Remarks	Finess Modulus		SANS 3001 GR3	%	42	
				mm	mm				
% Passing		mm		Clay Content			Ref.		
		mm		Organic Impurities	Total		%		
		mm			Flakiness Index			%	
		mm		Average Least Dimension	Manual		mm		
		mm			Machine				
		mm			Computation				
		mm		Aggregate Crushing Value	Dry		%		
		mm			Wet				
		mm			Eth. Glycol				
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN		
		mm			Wet				
		mm			Eth. Glycol				
		mm		Bulk Density	Loose		kg/m <sup>3</sup>		
		mm			Compacted				
		mm		Water Absorption			%		
		mm							
Sand Equivalent, Se pH		5.7		Bulk Particle Density	Aggregate	kg/m <sup>3</sup>			
Relative Density of Soils					Apparent Particle Density		kg/m <sup>3</sup>		
Durability Mill Index				Adjusted Relative					
Moisture Content	%					1000 Revs			
Compactibility Factor				500 Revs		%			
Conductivity	S.m <sup>-1</sup>	0.003		Riedel & Weber					
Total Water Soluble	Salts Sulphates	%			Akali Silica Reaction		%		
Soluble	Salts Sulphates	%		Drying Shrinkage		%			
				Wetting Expansion		%			
Soundness	Fine	%		Fractured Faces		%			
	Coarse	No.		Coarse Sand Ratio		%			
	Fractions			Shape: Voids		%			
Methylene Blue Absorption				Shell Content		%			
Soluble Deleterious Impurities		%		Durability	Ballast				
Chloride Content		%		Eth. Glycol	Concrete				
Low Density Material		%		Durability on	Crushed				
Presence of Sugar				_ Stone	Seal				
Mill Abrasion									
Treton Value									
Vialit Adhesion @	5°C	%							
	25°C	%							

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## AGGREGATE TEST REPORT

Laboratory Number	15		
Field Number	TP23		
Client Reference			
Depth (m)	0.5-1.6		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	42
				Clay Content				
% Passing		mm		Organic Impurities			Ref.	
		mm		Flakiness Index	Total		%	
		mm						
		mm		Average Least Dimension	Manual		mm	
		mm			Machine			
		mm			Computation			
		mm		Aggregate Crushing Value	Dry		%	
		mm			Wet			
		mm			Eth. Glycol			
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN	
		mm			Wet			
		mm			Eth. Glycol			
		mm		Bulk Density	Loose		kg/m <sup>3</sup>	
		mm			Compacted			
		mm		Water Absorption			%	
		mm						
	Sand Equivalent, Se pH			5.9	Bulk Particle Density	Aggregate	kg/m <sup>3</sup>	
Relative Density of Soils								
Durability Mill Index				Apparent Particle Density		kg/m <sup>3</sup>		
Moisture Content		%						
Compactibility Factor								
Conductivity		S.m <sup>-1</sup>	0.001	Adjusted Relative				
Total Water Soluble	Salts Sulphates	%						
Soluble	Salts	%		LA Abrasion	1000 Revs	%		
	Sulphates	%			500 Revs			
Soundness	Fine	%		Riedel & Weber				
	Coarse			Akali Silica Reaction		%		
	Fractions	No.		Drying Shrinkage		%		
Methylene Blue Absorption				Wetting Expansion		%		
Soluble Deleterious Impurities		%		Fractured Faces		%		
Chloride Content		%		Coarse Sand Ratio		%		
Low Density Material		%		Shape: Voids		%		
Presence of Sugar				Shell Content		%		
Mill Abrasion				Durability	Ballast			
Treton Value				Eth. Glycol	Concrete			
Vialit Adhesion @	5°C	%		Durability on	Crushed			
	25°C	%			_ Stone	Seal		

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## AGGREGATE TEST REPORT

Laboratory Number	16		
Field Number	TP26		
Client Reference			
Depth (m)	0.9-2.2		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	39
				Clay Content				
% Passing		mm		Organic Impurities			Ref.	
		mm		Flakiness Index	Total		%	
		mm						
		mm		Average Least Dimension	Manual		mm	
		mm			Machine			
		mm			Computation			
		mm		Aggregate Crushing Value	Dry		%	
		mm			Wet			
		mm			Eth. Glycol			
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN	
		mm			Wet			
		mm			Eth. Glycol			
		mm		Bulk Density	Loose		kg/m <sup>3</sup>	
		mm			Compacted			
		mm		Water Absorption			%	
		mm						
	Sand Equivalent, Se pH			6.1	Bulk Particle Density	Aggregate	kg/m <sup>3</sup>	
Relative Density of Soils								
Durability Mill Index				Apparent Particle Density		kg/m <sup>3</sup>		
Moisture Content		%						
Compactibility Factor								
Conductivity		S.m <sup>-1</sup>	0.005	Adjusted Relative				
Total Water Soluble	Salts Sulphates	%						
Soluble	Salts	%		LA Abrasion	1000 Revs 500 Revs	%		
	Sulphates	%						
Soundness	Fine	%		Riedel & Weber				
	Coarse	No.		Akali Silica Reaction		%		
	Fractions			Drying Shrinkage		%		
Methylene Blue Absorption				Wetting Expansion		%		
Soluble Deleterious Impurities		%		Fractured Faces		%		
Chloride Content		%		Coarse Sand Ratio		%		
Low Density Material		%		Shape: Voids		%		
Presence of Sugar				Shell Content		%		
Mill Abrasion				Durability	Ballast			
Treton Value				Eth. Glycol	Concrete			
Vialit Adhesion @	5°C	%		Durability on _ Stone	Crushed			
	25°C	%			Seal			



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## AGGREGATE TEST REPORT

Laboratory Number	17		
Field Number	TP27		
Client Reference			
Depth (m)	0.8-3.0		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	17	
				mm	Clay Content				
		mm		Organic Impurities			Ref.		
		mm		Flakiness Index	Total		%		
		mm							
		mm		Average Least Dimension	Manual		mm		
		mm			Machine				
		mm			Computation				
		mm		Aggregate Crushing Value	Dry		%		
		mm			Wet				
		mm			Eth. Glycol				
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN		
		mm			Wet				
		mm			Eth. Glycol				
		mm		Bulk Density	Loose		kg/m <sup>3</sup>		
		mm			Compacted				
		mm		Water Absorption			%		
		mm							
Sand Equivalent, Se pH			6.3	Bulk Particle Density	Aggregate		kg/m <sup>3</sup>		
Relative Density of Soils									
Durability Mill Index				Apparent Particle Density			kg/m <sup>3</sup>		
Moisture Content		%							
Compactibility Factor									
Conductivity		S.m <sup>-1</sup>	0.005	LA Abrasion	1000 Revs		%		
Total Water Soluble	Salts Sulphates	%						500 Revs	
Soluble	Salts Sulphates	%							
Soundness	Fine	%		Riedel & Weber					
	Coarse Fractions	No.		Akali Silica Reaction			%		
Methylene Blue Absorption				Drying Shrinkage			%		
Soluble Deleterious Impurities		%		Wetting Expansion			%		
Chloride Content		%		Fractured Faces			%		
Low Density Material		%		Coarse Sand Ratio			%		
Presence of Sugar				Shape: Voids			%		
Mill Abrasion				Shell Content			%		
Treton Value				Durability	Ballast				
Vialit Adhesion @	5°C	%		Eth. Glycol	Concrete				
	25°C	%		Durability on	Crushed				
				_ Stone	Seal				

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## AGGREGATE TEST REPORT

Laboratory Number	18		
Field Number	TP31		
Client Reference			
Depth (m)	0.7-3.0		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

		mm		Finess Modulus		SANS 3001 GR3	%	15	
				mm	Clay Content				
		mm		Organic Impurities			Ref.		
		mm		Flakiness Index	Total		%		
		mm							
		mm		Average Least Dimension	Manual		mm		
		mm			Machine				
		mm			Computation				
		mm		Aggregate Crushing Value	Dry		%		
		mm			Wet				
		mm			Eth. Glycol				
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN		
		mm			Wet				
		mm			Eth. Glycol				
		mm		Bulk Density	Loose		kg/m <sup>3</sup>		
		mm			Compacted				
		mm		Water Absorption			%		
		mm							
Sand Equivalent, Se pH			6.4	Bulk Particle Density	Aggregate		kg/m <sup>3</sup>		
Relative Density of Soils									
Durability Mill Index				Apparent Particle Density			kg/m <sup>3</sup>		
Moisture Content		%							
Compactibility Factor									
Conductivity		S.m <sup>-1</sup>	0.004	LA Abrasion	1000 Revs		%		
Total Water Soluble	Salts Sulphates	%						500 Revs	
Soluble	Salts Sulphates	%							
Soundness	Fine	%		Riedel & Weber					
	Coarse			Akali Silica Reaction			%		
	Fractions	No.		Drying Shrinkage			%		
Methylene Blue Absorption				Wetting Expansion			%		
Soluble Deleterious Impurities		%		Fractured Faces			%		
Chloride Content		%		Coarse Sand Ratio			%		
Low Density Material		%		Shape: Voids			%		
Presence of Sugar				Shell Content			%		
Mill Abrasion				Durability	Ballast				
Treton Value				Eth. Glycol	Concrete				
Vialit Adhesion @	5°C	%		Durability on	Crushed				
	25°C	%			_ Stone	Seal			



Client	:	DAVEL & VAN HUYSSTEEN CONSULTING (PTY)	Date Received:	03/06/2020
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## AGGREGATE TEST REPORT

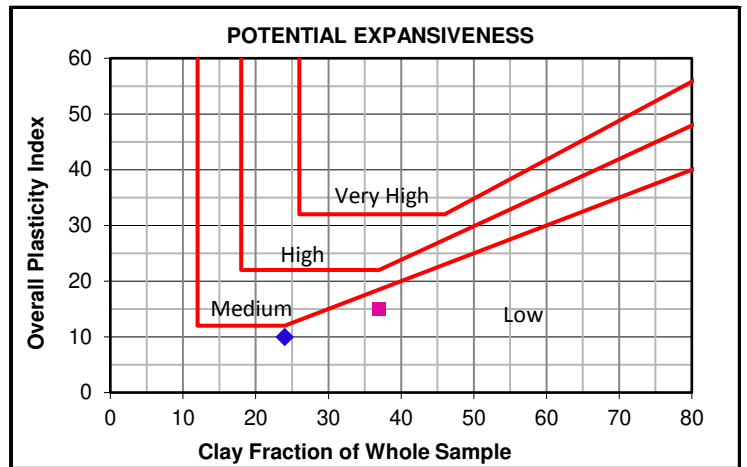
Laboratory Number	20		
Field Number	TP35		
Client Reference			
Depth (m)	0.7-3.0		
Position			
Coordinates	X		
	Y		
Description			
Additional Information			
Calcrete/Crushed			
Stabilizing Agent			

	% Passing	mm		Finess Modulus			
		mm		Clay Content	SANS 3001 GR3	%	6
		mm		Organic Impurities		Ref.	
		mm		Flakiness Index	Total		%
		mm					
		mm		Average Least Dimension	Manual		mm
		mm			Machine		
		mm			Computation		
		mm		Aggregate Crushing Value	Dry		%
		mm			Wet		
		mm			Eth. Glycol		
		mm		10% Fines Aggregate Crushing Test (FACT)	Dry		kN
		mm			Wet		
		mm			Eth. Glycol		
		mm		Bulk Density	Loose		kg/m <sup>3</sup>
		mm			Compacted		
		mm		Water Absorption			%
		mm					
Sand Equivalent, Se pH			6.6				
Relative Density of Soils				Bulk Particle Density	Aggregate	kg/m <sup>3</sup>	
Durability Mill Index				Apparent Particle Density		kg/m <sup>3</sup>	
Moisture Content	%						
Compactibility Factor				Adjusted Relative		kg/m <sup>3</sup>	
Conductivity	S.m <sup>-1</sup>	0.004					
Total Water Soluble	Salts Sulphates	%		LA Abrasion	1000 Revs	%	
Soluble	Salts Sulphates	%			500 Revs		
Soundness	Fine	%		Riedel & Weber			
	Coarse Fractions	No.		Akali Silica Reaction		%	
Methylene Blue Absorption				Drying Shrinkage		%	
Soluble Deleterious Impurities		%		Wetting Expansion		%	
Chloride Content		%		Fractured Faces		%	
Low Density Material		%		Coarse Sand Ratio		%	
Presence of Sugar				Shape: Voids		%	
Mill Abrasion				Shell Content		%	
Treton Value				Durability	Ballast		
Vialit Adhesion @	5°C	%		Eth. Glycol	Concrete		
	25°C	%		Durability on	Crushed		
				_ Stone	Seal		

Client :	DAVEL & VAN HUYSSSTEEN CONSULTING (PTY)	Date Received:	03/06/2020
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## FOUNDATION INDICATOR

Laboratory Number	2 <span style="color:blue">◆</span>	4 <span style="color:magenta">■</span>
Field Number	TP5	TP8
Client Reference		
Depth (m)	1.1-1.5	0.1-1.3
Position		
Coordinates	X Y	
Description		
Additional Information		
Calcrete / Crushed Stabilizing Agent		

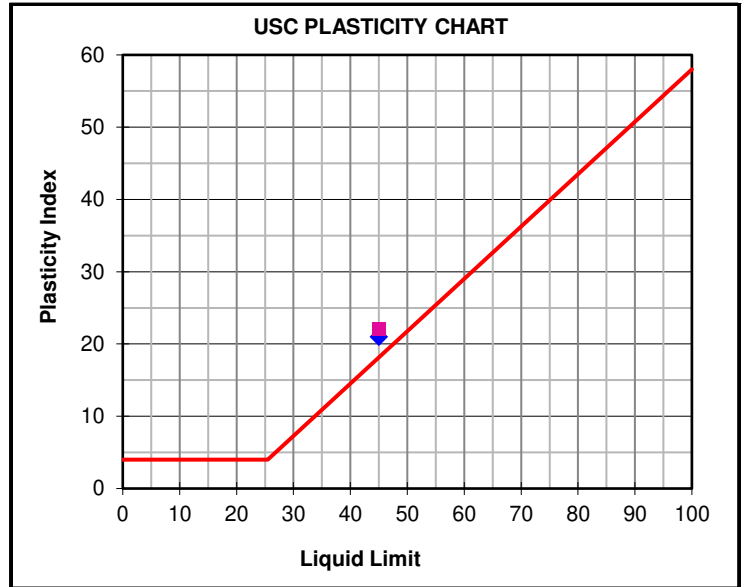


### Moisture Content & Relative Density

Moisture Content (%)		
Relative Density (S.G.)		

### Sieve Analysis (Wet Prep) SANS 3001 GR1

Percentage Passing	100 mm	75 mm	63 mm	50 mm	37.5 mm	28 mm	20 mm	14 mm	5 mm	2 mm	1 mm	0.425 mm	0.250 mm	0.150 mm	0.075 mm
	100	100	100	100	100	100	100	100	100	85	98	49	45	42	41
Grading Modulus	1.25	0.85													



### Hydrometer Analysis SANS 3001 GR3

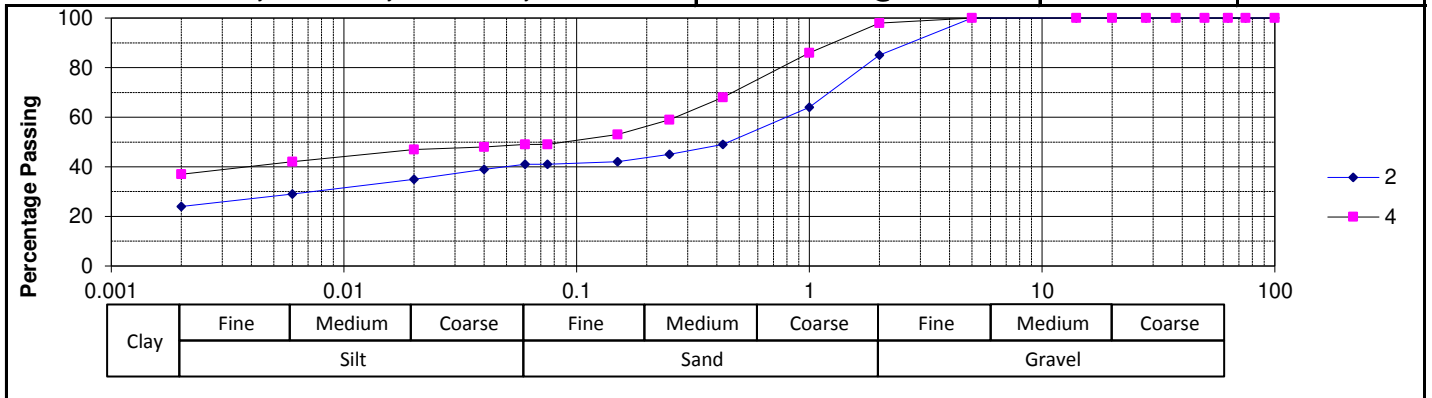
Percentage Passing	0.060 mm	0.040 mm	0.020 mm	0.006 mm	0.002 mm
	41	39	35	29	24
Gravel	%	15	2		
Sand	%	44	49		
Silt	%	17	12		
Clay	%	24	37		

Laboratory Number	2 <span style="color:blue">◆</span>	4 <span style="color:magenta">■</span>
Atterberg Limits -425µ	SANS 3001 GR10	
Liquid Limit	%	45
Plasticity Index	%	21
Linear Shrinkage	%	9.5
Overall PI	%	10

### Classifications

HRB (AASHTO)	A-7-6(4)	A-7-6(7)
Unified (ASTM D2487)	SC	SC
Weston Swell @ 1 kPa		

Note: An assumed S.G. may be used in Hydrometer Analysis calculations



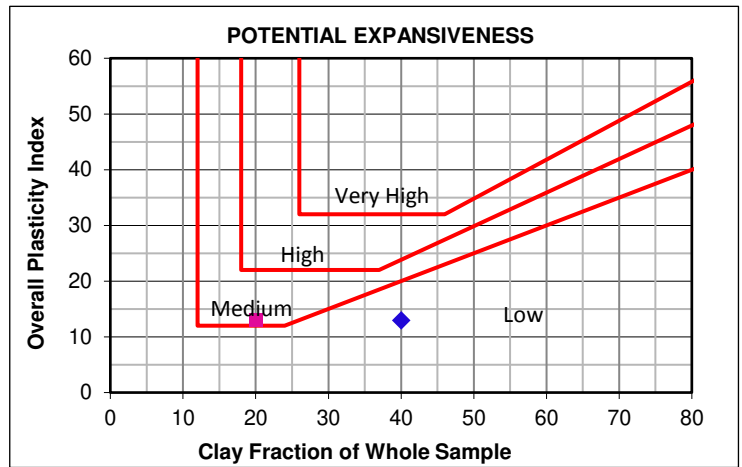




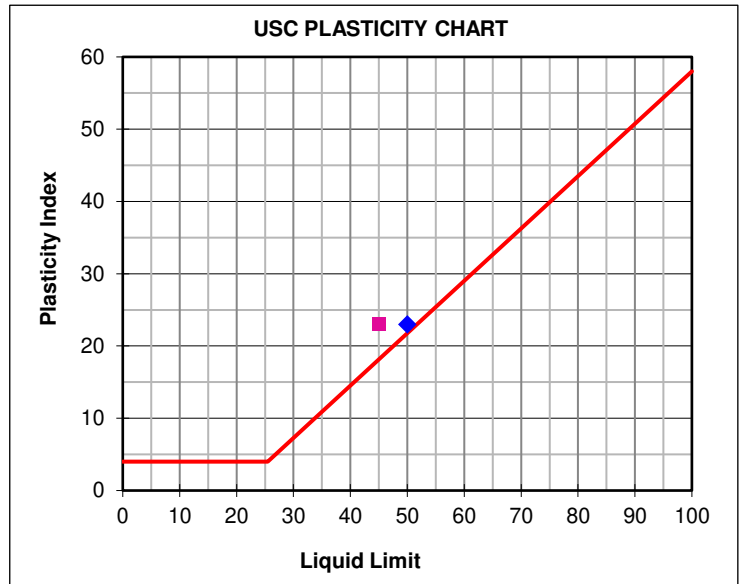
Client :	DAVEL & VAN HUYSSSTEEN CONSULTING (PTY)	Date Received:	03/06/2020
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## FOUNDATION INDICATOR

Laboratory Number	11 <span style="color:blue">◆</span>	12 <span style="color:magenta">■</span>
Field Number	TP19	TP21
Client Reference		
Depth (m)	0.5-1.6	0.9-3.0
Position		
Coordinates	X Y	
Description		
Additional Information		
Calcrete / Crushed Stabilizing Agent		



<b>Moisture Content &amp; Relative Density</b>		
Moisture Content (%)		
Relative Density (S.G.)		



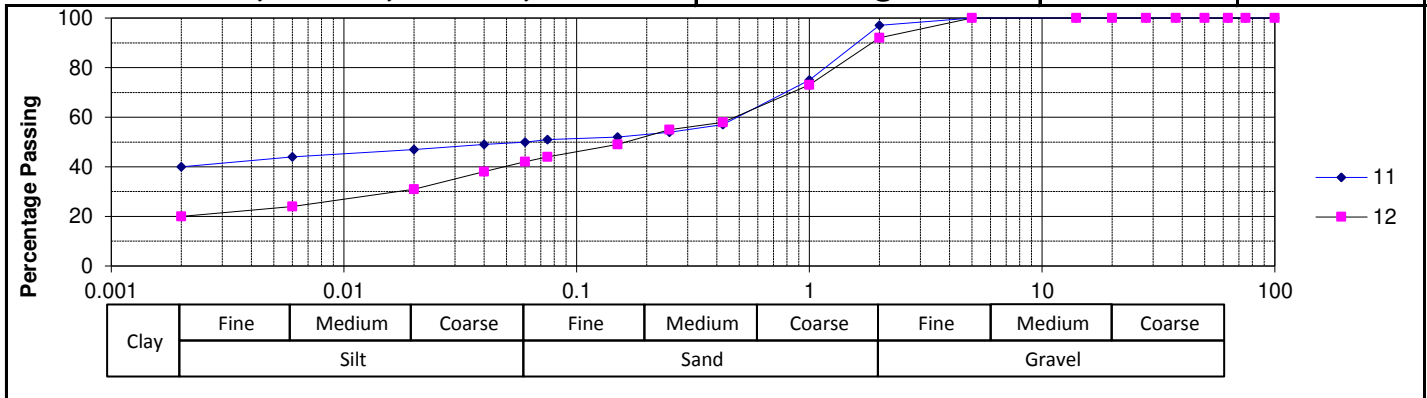
<b>Sieve Analysis (Wet Prep) SANS 3001 GR1</b>			
Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	100	100
	28 mm	100	100
	20 mm	100	100
	14 mm	100	100
	5 mm	100	100
	2 mm	97	92
	1 mm	75	73
	0.425 mm	57	58
	0.250 mm	54	55
0.150 mm	52	49	
0.075 mm	51	44	
Grading Modulus	0.95	1.06	

Laboratory Number	11 <span style="color:blue">◆</span>	12 <span style="color:magenta">■</span>
<b>Atterberg Limits -425µ SANS 3001 GR10</b>		
Liquid Limit	% 50	45
Plasticity Index	% 23	23
Linear Shrinkage	% 10.0	10.0
Overall PI	% 13	13

<b>Hydrometer Analysis SANS 3001 GR3</b>			
Percentage Passing	0.060 mm	50	42
	0.040 mm	49	38
	0.020 mm	47	31
	0.006 mm	44	24
	0.002 mm	40	20
Gravel	% 3	8	
Sand	% 47	50	
Silt	% 10	22	
Clay	% 40	20	

<b>Classifications</b>		
HRB (AASHTO)	A-7-6(9)	A-7-6(6)
Unified (ASTM D2487)	CH	SC
Weston Swell @ 1 kPa		

Note: An assumed S.G. may be used in Hydrometer Analysis calculations

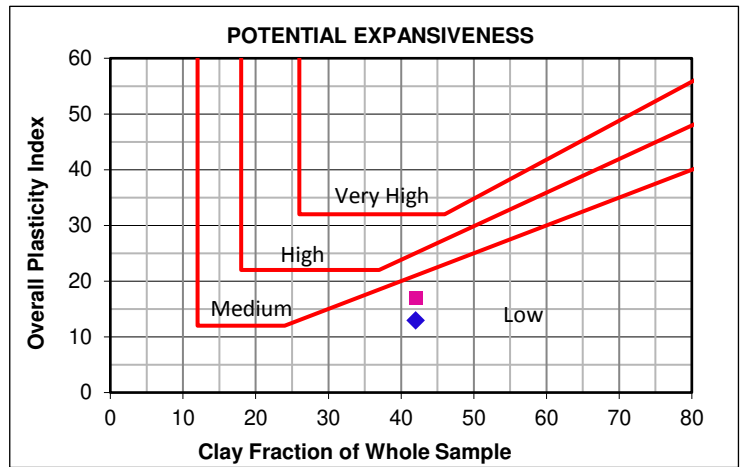




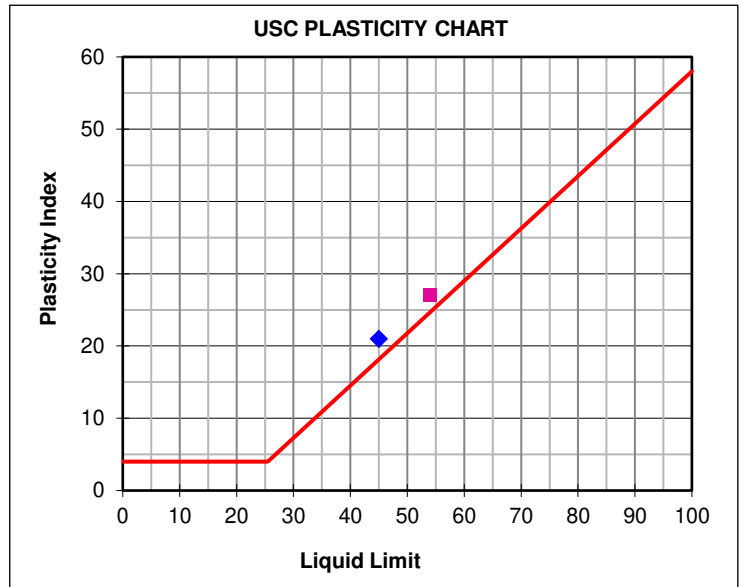
Client :	DAVEL & VAN HUYSSSTEEN CONSULTING (PTY)	Date Received:	03/06/2020
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## FOUNDATION INDICATOR

Laboratory Number	13 <span style="color:blue">◆</span>	15 <span style="color:magenta">■</span>
Field Number	TP22	TP23
Client Reference		
Depth (m)	0.1-0.9	0.5-1.6
Position		
Coordinates	X Y	
Description		
Additional Information		
Calcrete / Crushed Stabilizing Agent		



<b>Moisture Content &amp; Relative Density</b>		
Moisture Content (%)		
Relative Density (S.G.)		



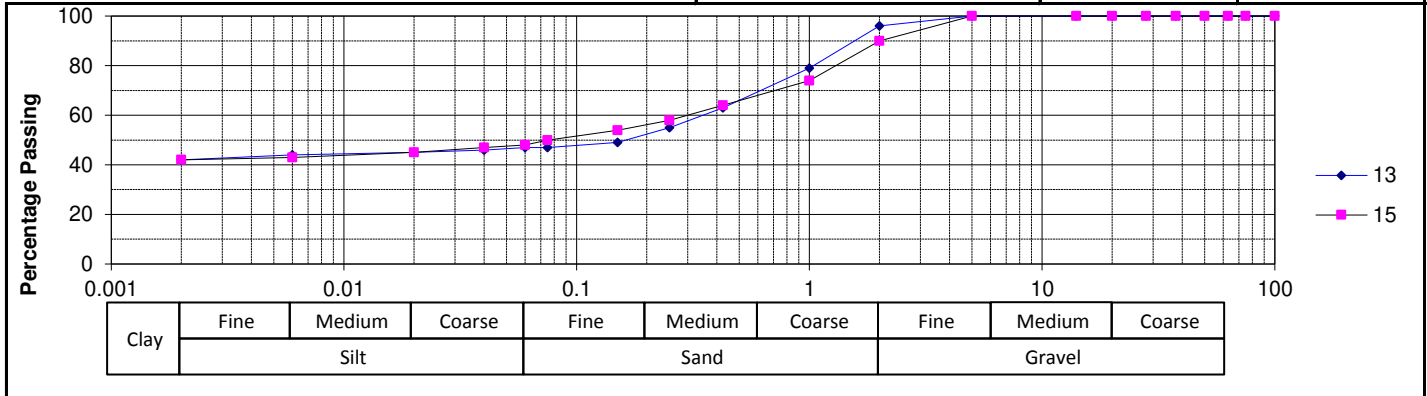
<b>Sieve Analysis (Wet Prep) SANS 3001 GR1</b>			
Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	100	100
	28 mm	100	100
	20 mm	100	100
	14 mm	100	100
	5 mm	100	100
	2 mm	96	90
	1 mm	79	74
	0.425 mm	63	64
	0.250 mm	55	58
0.150 mm	49	54	
0.075 mm	47	50	
Grading Modulus	0.94	0.96	

Laboratory Number	13 <span style="color:blue">◆</span>	15 <span style="color:magenta">■</span>
<b>Atterberg Limits -425µ SANS 3001 GR10</b>		
Liquid Limit	% 45	54
Plasticity Index	% 21	27
Linear Shrinkage	% 10.0	12.0
Overall PI	% 13	17

<b>Hydrometer Analysis SANS 3001 GR3</b>			
Percentage Passing	0.060 mm	47	48
	0.040 mm	46	47
	0.020 mm	45	45
	0.006 mm	44	43
	0.002 mm	42	42
Gravel	% 4	10	
Sand	% 49	35	
Silt	% 5	13	
Clay	% 42	42	

<b>Classifications</b>		
HRB (AASHTO)	A-7-6(6)	A-7-6(10)
Unified (ASTM D2487)	SC	CH
Weston Swell @ 1 kPa		

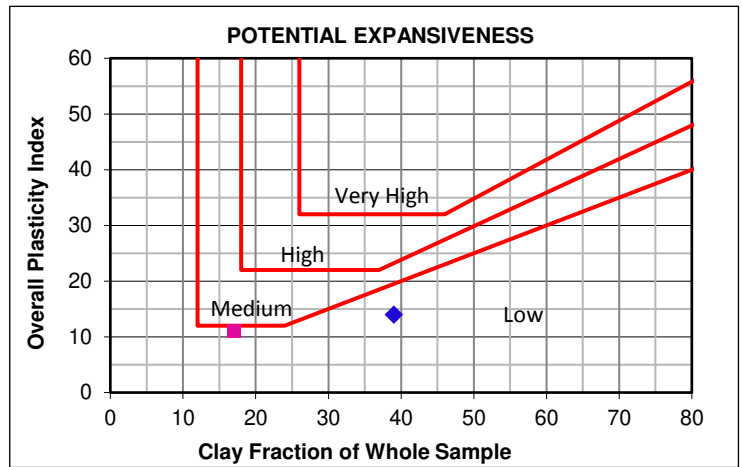
Note: An assumed S.G. may be used in Hydrometer Analysis calculations



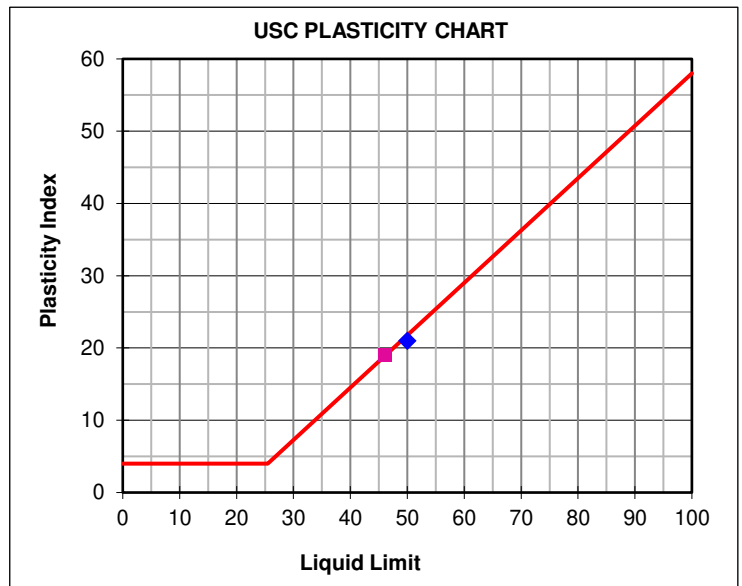
Client :	DAVEL & VAN HUYSSSTEEN CONSULTING (PTY)	Date Received:	03/06/2020
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## FOUNDATION INDICATOR

Laboratory Number	16 <span style="color:blue">◆</span>	17 <span style="color:magenta">■</span>
Field Number	TP26	TP27
Client Reference		
Depth (m)	0.9-2.2	0.8-3.0
Position		
Coordinates	X Y	
Description		
Additional Information		
Calcrete / Crushed Stabilizing Agent		



<b>Moisture Content &amp; Relative Density</b>		
Moisture Content (%)		
Relative Density (S.G.)		

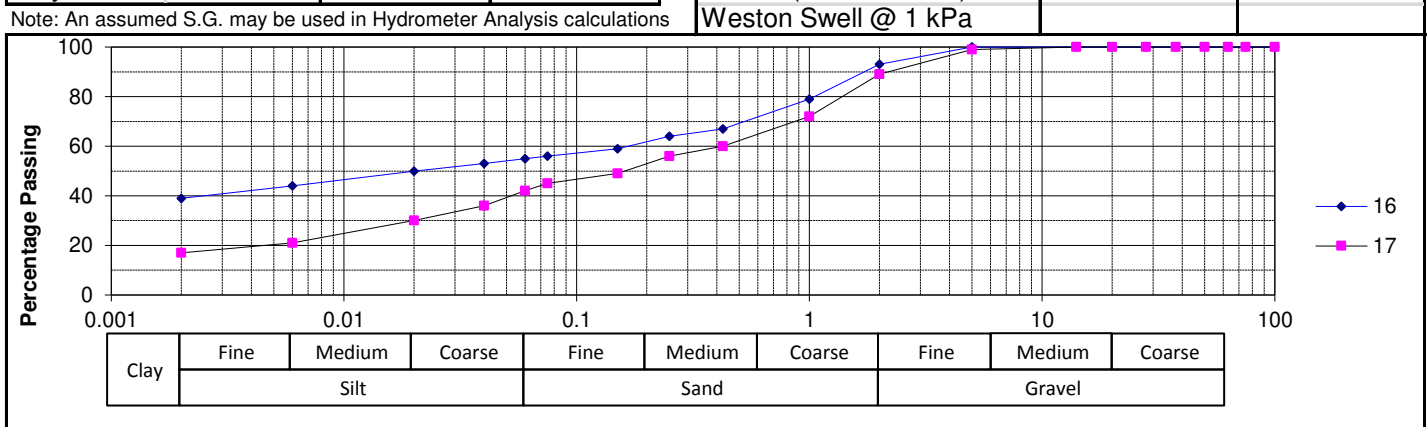


<b>Sieve Analysis (Wet Prep) SANS 3001 GR1</b>			
Percentage Passing	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
	50 mm	100	100
	37.5 mm	100	100
	28 mm	100	100
	20 mm	100	100
	14 mm	100	100
	5 mm	100	99
	2 mm	93	89
	1 mm	79	72
	0.425 mm	67	60
	0.250 mm	64	56
	0.150 mm	59	49
0.075 mm	56	45	
Grading Modulus	0.84	1.06	

<b>Hydrometer Analysis SANS 3001 GR3</b>			
Percentage Passing	0.060 mm	55	42
	0.040 mm	53	36
	0.020 mm	50	30
	0.006 mm	44	21
	0.002 mm	39	17
Gravel	%	7	11
Sand	%	38	47
Silt	%	16	25
Clay	%	39	17

Laboratory Number	16 <span style="color:blue">◆</span>	17 <span style="color:magenta">■</span>	
<b>Atterberg Limits -425µ SANS 3001 GR10</b>			
Liquid Limit	%	50	46
Plasticity Index	%	21	19
Linear Shrinkage	%	9.5	9.0
Overall PI	%	14	11

<b>Classifications</b>		
HRB (AASHTO)	A-7-6(10)	A-7-6(5)
Unified (ASTM D2487)	MH	SC
Weston Swell @ 1 kPa		

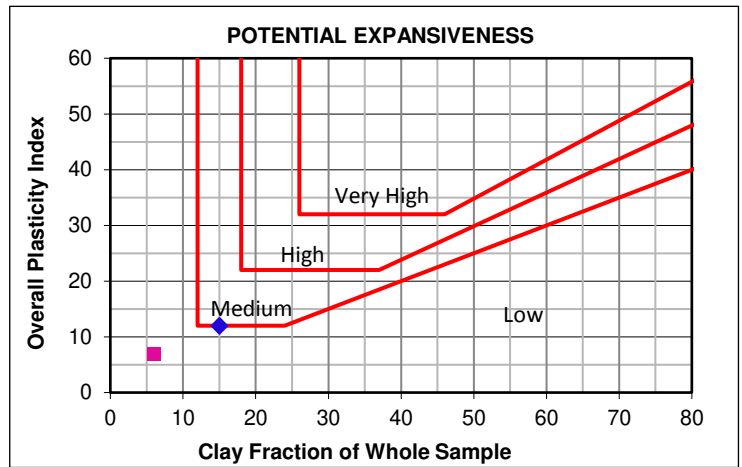


Note: An assumed S.G. may be used in Hydrometer Analysis calculations

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## FOUNDATION INDICATOR

Laboratory Number	18 ◆	20 ■
Field Number	TP31	TP35
Client Reference		
Depth (m)	0.7-3.0	0.7-3.0
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed Stabilizing Agent		

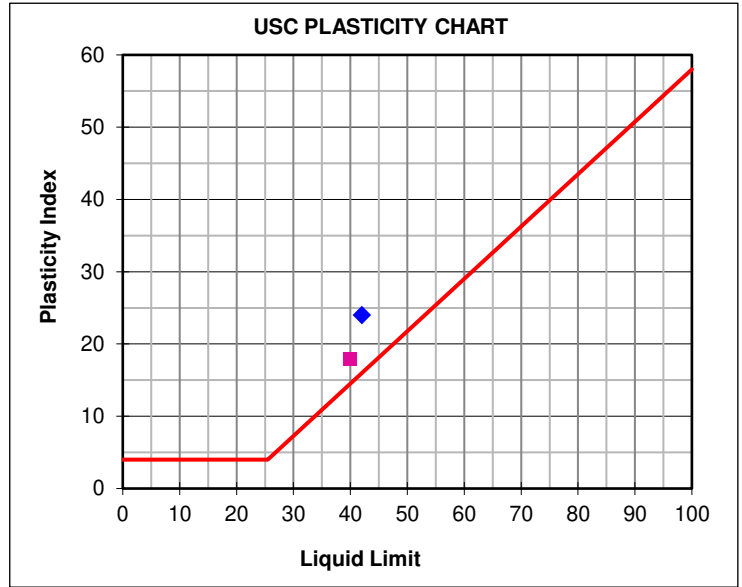


### Moisture Content & Relative Density

Moisture Content (%)		
Relative Density (S.G.)		

### Sieve Analysis (Wet Prep) SANS 3001 GR1

Percentage Passing	100 mm	75 mm	63 mm	50 mm	37.5 mm	28 mm	20 mm	14 mm	5 mm	2 mm	1 mm	0.425 mm	0.250 mm	0.150 mm	0.075 mm	Grading Modulus	
	100	100	100	100	100	100	100	100	99	96	80	56	39	33	28	23	1.27
																	1.58



### Hydrometer Analysis SANS 3001 GR3

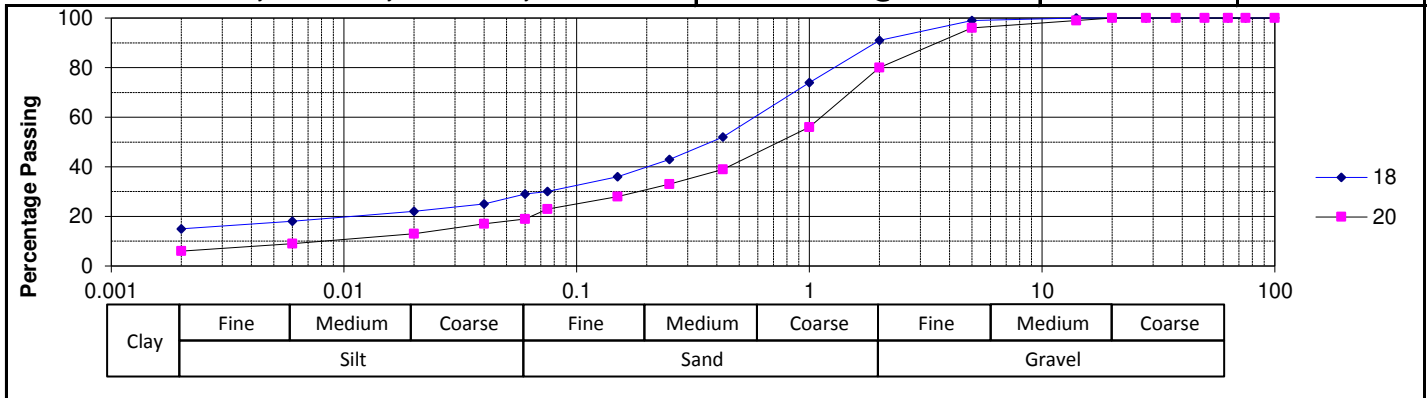
Percentage Passing	0.060 mm	0.040 mm	0.020 mm	0.006 mm	0.002 mm	Gravel	Sand	Silt	Clay
	29	25	22	18	15	9	62	14	15
	19	17	13	9	6	20	61	13	6

Laboratory Number	18 ◆	20 ■
Atterberg Limits -425µ	SANS 3001 GR10	
Liquid Limit	% 42	40
Plasticity Index	% 24	18
Linear Shrinkage	% 9.5	7.0
Overall PI	% 12	7

### Classifications

HRB (AASHTO)	A-2-7(2)	A-2-6(1)
Unified (ASTM D2487)	SC	SC
Weston Swell @ 1 kPa		

Note: An assumed S.G. may be used in Hydrometer Analysis calculations





Client : DAVEL & VAN HUYSSTEEN CONSULTING (PTY)  
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## MOISTURE DENSITY RELATIONSHIP

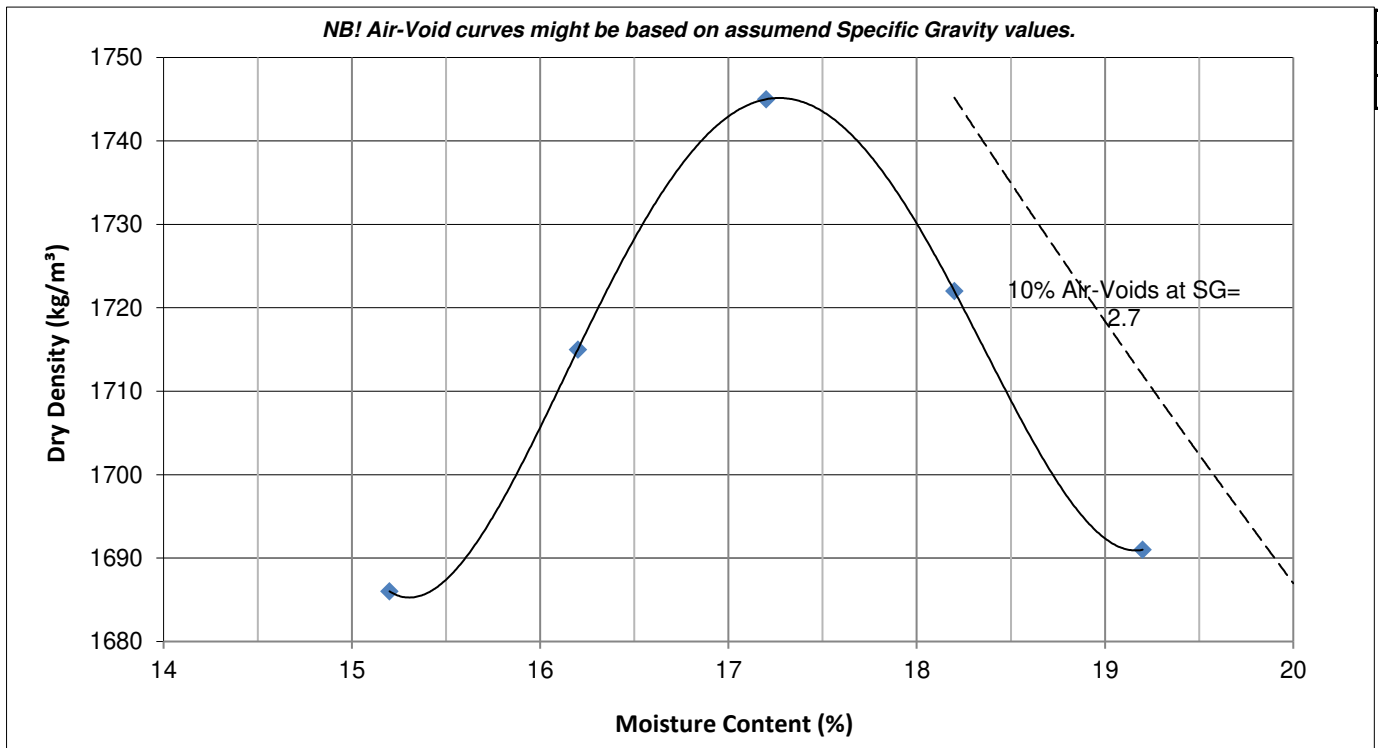
Laboratory Number	1	
Field Number	TP4	
Client Reference		
Depth (m)	0.1-1.5	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

**Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30**

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m <sup>3</sup>	1686	1715	1745	1722	1691	
Moisture Content	%	15.2	16.2	17.2	18.2	19.2	

Max. Dry Density	kg/m <sup>3</sup>	1745
Optimum Moisture	%	17.3



Client : DAVEL & VAN HUYSSTEEN CONSULTING (PTY)  
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## MOISTURE DENSITY RELATIONSHIP

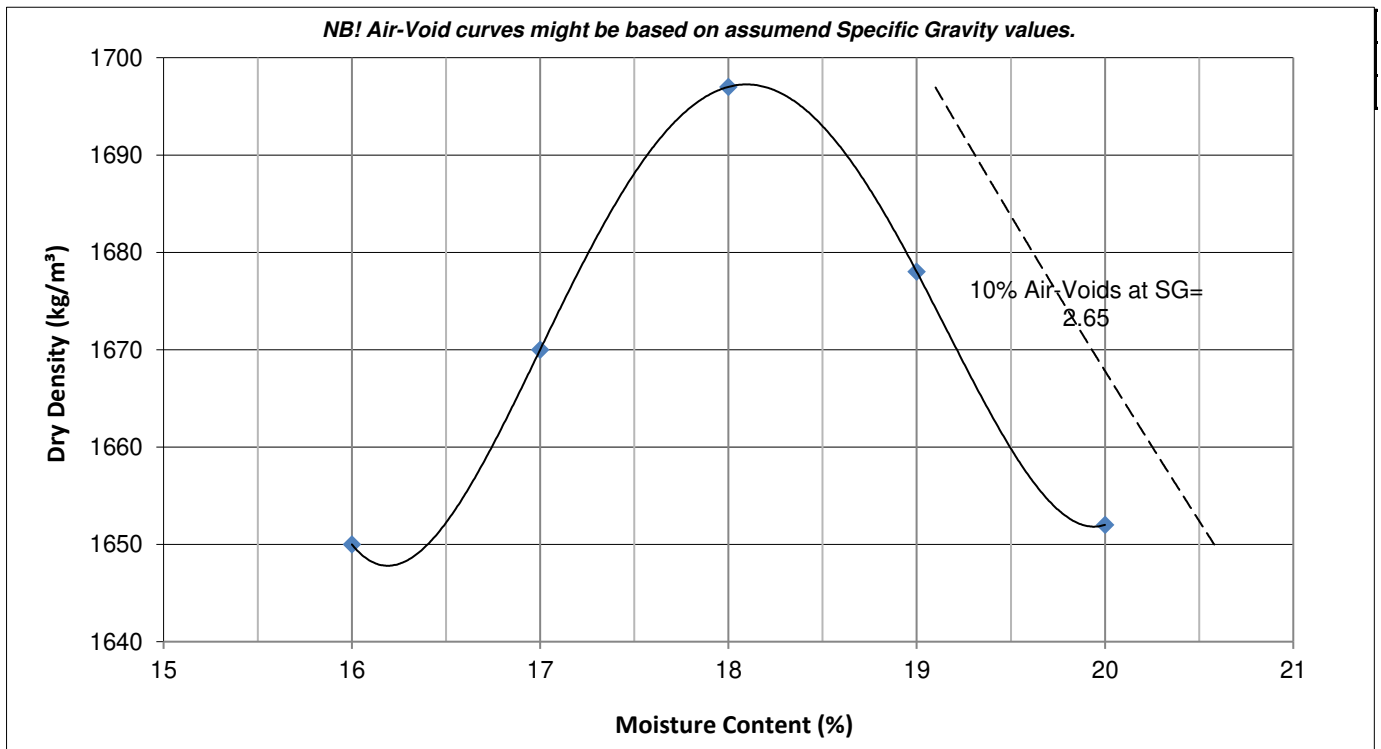
Laboratory Number	3	
Field Number	TP7	
Client Reference		
Depth (m)	0.1-2.5	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

**Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30**

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m <sup>3</sup>	1650	1670	1697	1678	1652	
Moisture Content	%	16	17	18	19	20	

Max. Dry Density	kg/m <sup>3</sup>	1697
Optimum Moisture	%	18.1



Client : DAVEL & VAN HUYSTEEN CONSULTING (PTY)  
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## MOISTURE DENSITY RELATIONSHIP

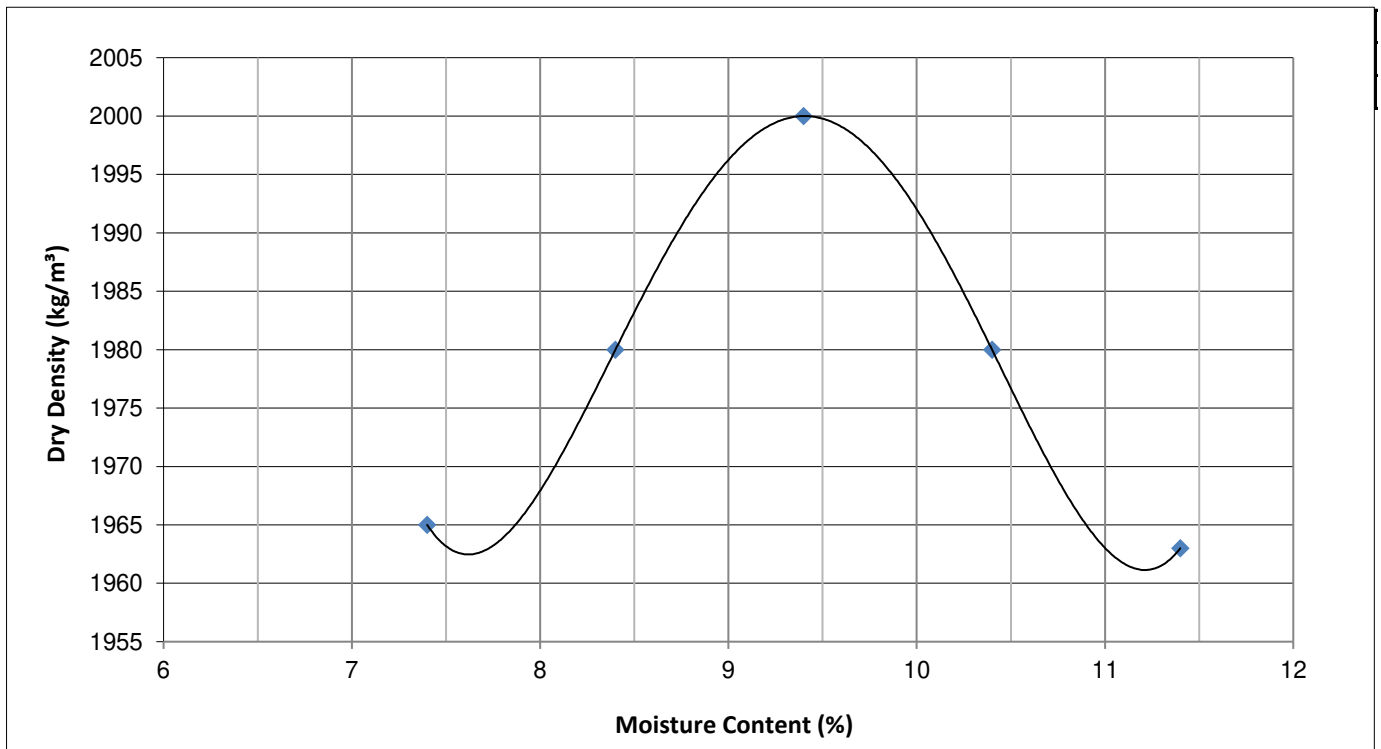
Laboratory Number	5	
Field Number	TP11	
Client Reference		
Depth (m)	1.1-3.0	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

**Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30**

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m <sup>3</sup>	1965	1980	2000	1980	1963	
Moisture Content	%	7.4	8.4	9.4	10.4	11.4	

Max. Dry Density	kg/m <sup>3</sup>	2000
Optimum Moisture	%	9.4



Client : DAVEL & VAN HUYSTEEN CONSULTING (PTY)  
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## MOISTURE DENSITY RELATIONSHIP

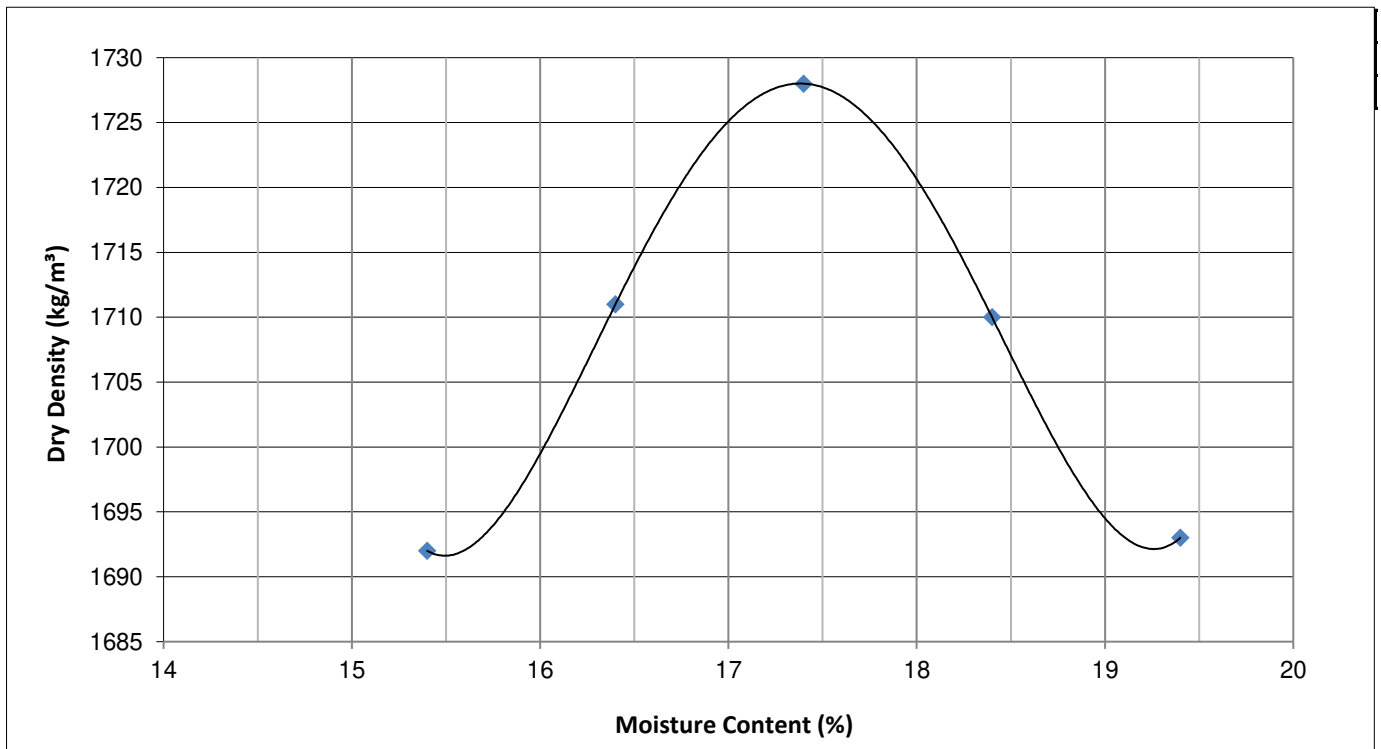
Laboratory Number	9	
Field Number	TP16	
Client Reference		
Depth (m)	0.1-1.5	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

**Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30**

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m <sup>3</sup>	1692	1711	1728	1710	1693	
Moisture Content	%	15.4	16.4	17.4	18.4	19.4	

Max. Dry Density	kg/m <sup>3</sup>	1728
Optimum Moisture	%	17.4



Client : DAVEL & VAN HUYSTEEN CONSULTING (PTY)  
 Project : Acorn City  
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## MOISTURE DENSITY RELATIONSHIP

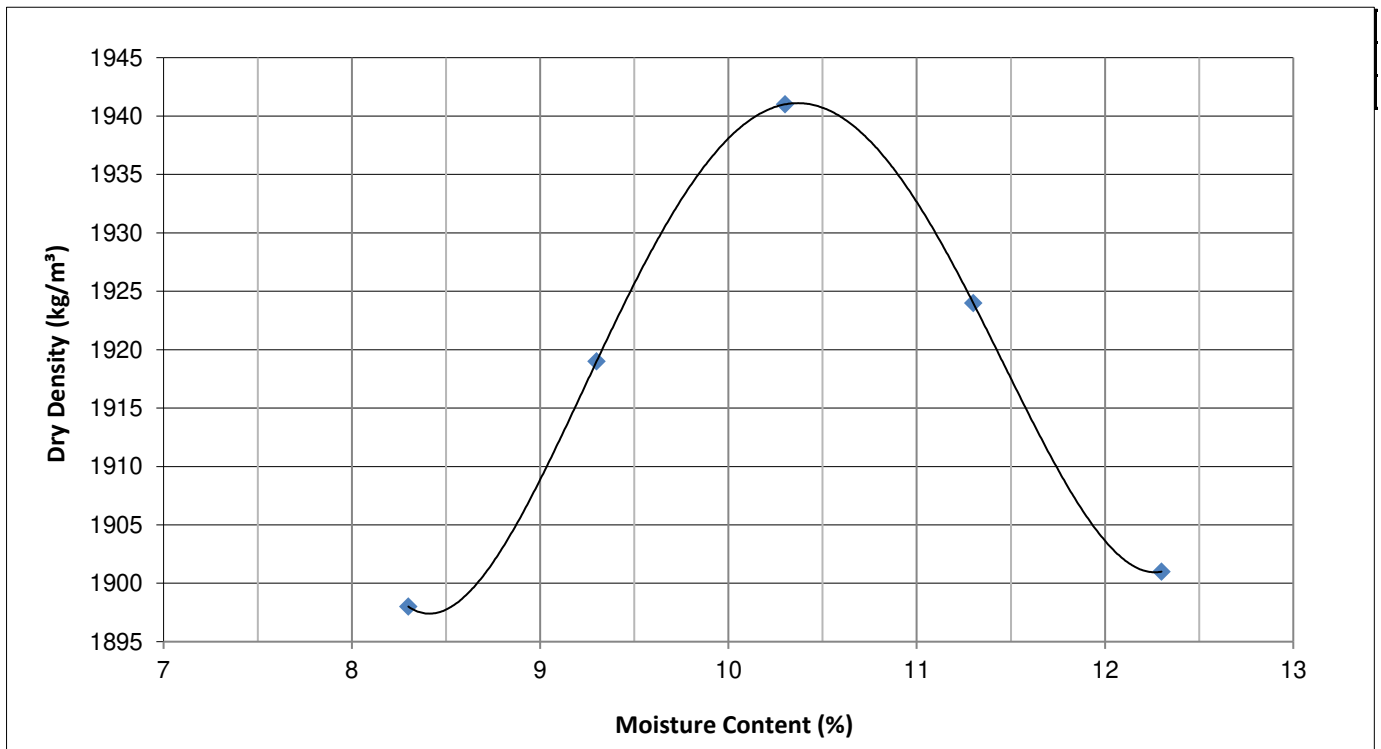
Laboratory Number	19	
Field Number	TP32	
Client Reference		
Depth (m)	0.1-1.0	
Position		
Coordinates	X	
	Y	
Description		
Additional Information		
Calcrete / Crushed		
Stabilizing Agent		

**Maximum Dry Density & Optimum Moisture Content - SANS 3001 GR30**

Compactive Effort:	Modified AASHTO
--------------------	-----------------

Dry Density	kg/m <sup>3</sup>	1898	1919	1941	1924	1901	
Moisture Content	%	8.3	9.3	10.3	11.3	12.3	

Max. Dry Density	kg/m <sup>3</sup>	1941
Optimum Moisture	%	10.4



Client : DAVEL & VAN HUYSSTEEN CONSULTING (PTY)  
 Project : Acorn City  
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## CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

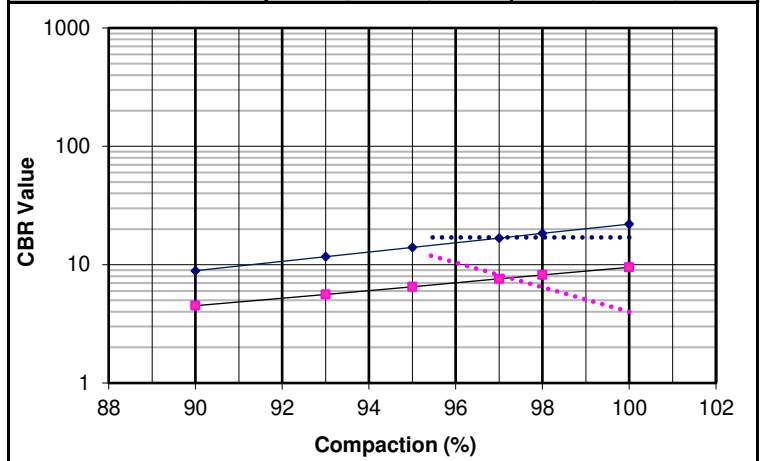
Laboratory No.	1	3
Field Number	TP4	TP7
Client Reference		
Depth (m)	0.1-1.5	0.1-2.5
Position		
Coordinates	X	
	Y	
Description		
Additional information		
Calcrete/Crushed		
Stabilizing Agent		

Laboratory No.	1	3
Maximum Dry Density & Optimum Moisture Content		SANS 3001 GR30
MDD	kg/m <sup>3</sup>	1745
OMC	%	17.3
		1697
		18.1

California Bearing Ratio		SANS 3001 GR40				
Compaction Data						
Moisture	%	17.2			18.2	
Dry Density	kg/m <sup>3</sup>	1764	1683	1596	1703	1625
Compaction	%	100.0	95.4	90.5	100.0	95.4

Penetration Data						
CBR at	2.50 mm	17	17	9	7	9
	5.00 mm	15	13	7	8	8
	7.50 mm	14	11	6	8	7
Swell	%	0.6	1.2	1.5	0.9	1.3
Final Moisture (%)		21.3	21.7	23.6	23.7	24.4

Sieve Analysis (Wet preparation)		SANS 3001 GR1
Percentage Passing	100 mm	100
	75 mm	100
	63 mm	100
	50 mm	100
	37.5 mm	100
	28 mm	100
	20 mm	100
	14 mm	99
	5 mm	98
	2 mm	86
	1 mm	59
	0.425 mm	34
	0.250 mm	31
	0.150 mm	28
0.075 mm	26	
Grading Modulus	1.5	

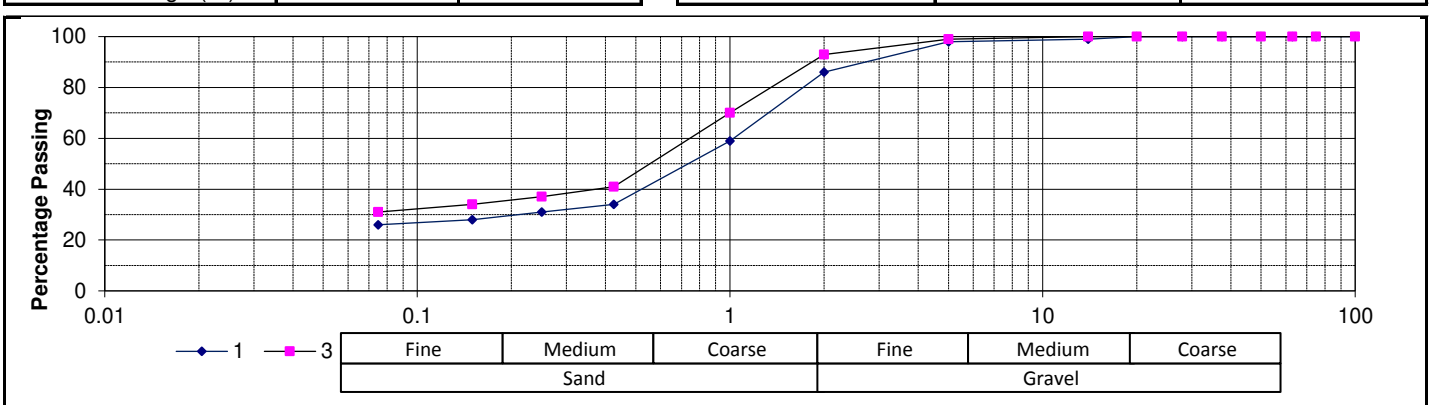


Interpolated CBR Data			
@ 100%	Mod. AASHTO	22	10
@ 98%		18	8
@ 97%		17	8
@ 95%		14	7
@ 93%		12	6
@ 90%		9	5
@ SANS3001 Midpoint		18	8

Soil Mortar Analysis	
Coarse Sand	60
Coarse Fine Sand	4
Medium Fine Sand	3
Fine Fine Sand	3
Silt and Clay	30

Atterberg Limits		SANS 3001 GR10
Liquid Limit (%)	46	
Plasticity Index (%)	22	
Linear Shrinkage (%)	10.0	

HRB (AASHTO)	A-2-7(1)
COLTO	
TRH14	G9



Classifications	
HRB (AASHTO)	A-2-7(1)
COLTO	
TRH14	G9

Client : DAVEL & VAN HUYSSTEEN CONSULTING (PTY)  
 Project : Acorn City  
 Project No. : 2020-B-553

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## CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

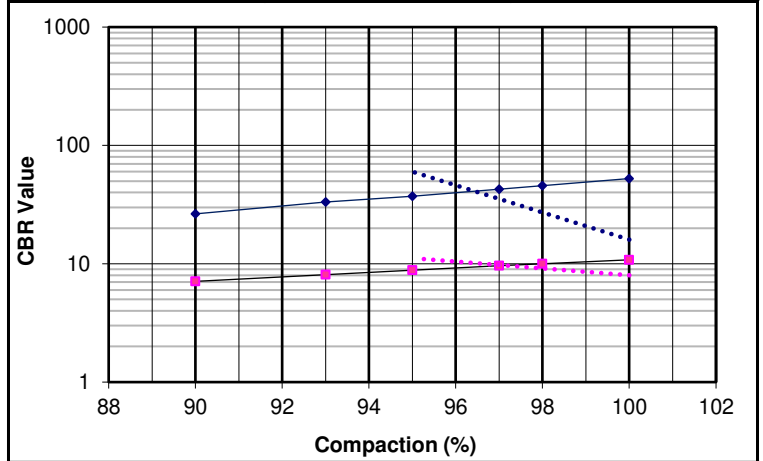
Laboratory No.	5	9
Field Number	TP11	TP16
Client Reference		
Depth (m)	1.1-3.0	0.1-1.5
Position		
Coordinates	X Y	
Description		
Additional information		
Calcrete/Crushed		
Stabilizing Agent		

Laboratory No.	5	9
Maximum Dry Density & Optimum Moisture Content		SANS 3001 GR30
MDD	kg/m <sup>3</sup>	2000
OMC	%	9.4
		1728
		17.4

California Bearing Ratio		SANS 3001 GR40
Compaction Data		
Moisture	%	9.4
Dry Density	kg/m <sup>3</sup>	2027
Compaction	%	100.0
		1925
		1824
		1724
		1642
		1556
		100.0
		95.0
		90.0
		100.0
		95.2
		90.3

Penetration Data		
CBR at	2.50 mm	55
	5.00 mm	67
	7.50 mm	69
		35
		41
		42
		26
		28
		28
		8
		11
		7
		18
		9
		6
		16
		7
		5
Swell	%	0.3
		0.2
		0.5
		1.2
		1.5
		0.9
Final Moisture (%)		11.8
		14
		18.7
		21.5
		23.1
		25.9

Sieve Analysis (Wet preparation)		SANS 3001 GR1
Percentage Passing	100 mm	100
	75 mm	100
	63 mm	100
	50 mm	100
	37.5 mm	100
	28 mm	100
	20 mm	100
	14 mm	93
	5 mm	60
	2 mm	34
	1 mm	20
	0.425 mm	11
	0.250 mm	10
	0.150 mm	9
	0.075 mm	8
Grading Modulus		2.5
		1.5

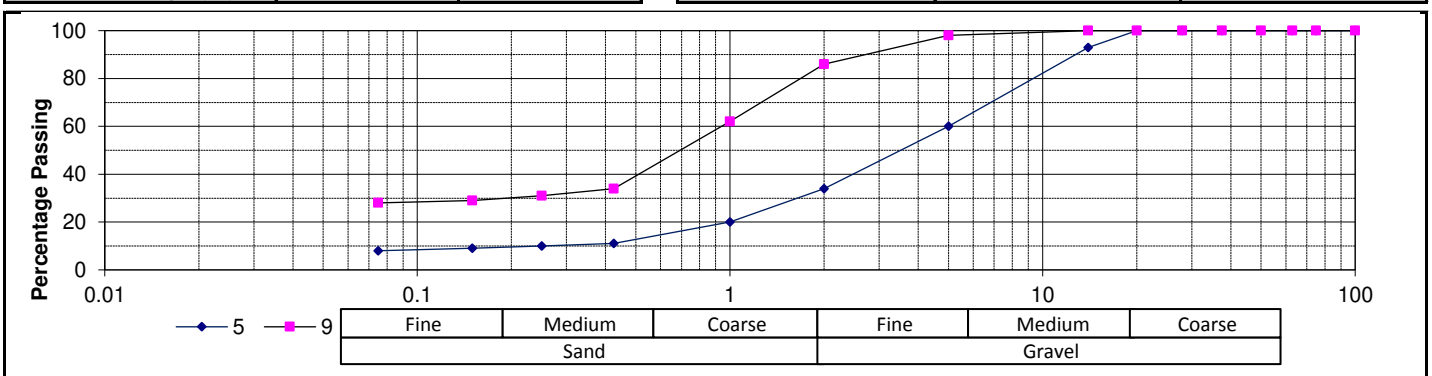


Interpolated CBR Data			
CBR	@ 100%	53	11
	@ 98%	46	10
	@ 97%	43	10
	@ 95%	37	9
	@ 93%	33	8
	@ 90%	26	7
	@ SANS3001 Midpoint	31	10

Soil Mortar Analysis		
Coarse Sand	68	60
Coarse Fine Sand	2	4
Medium Fine Sand	3	2
Fine Fine Sand	3	1
Silt and Clay	24	33

Classifications		
HRB (AASHTO)	A-2-7(0)	A-2-7(2)
COLTO		
TRH14	G8	G9

Atterberg Limits		SANS 3001 GR10
Liquid Limit (%)	46	49
Plasticity Index (%)	23	24
Linear Shrinkage (%)	8.5	10.5





Client : DAVEL & VAN HUYSSTEEN CONSULTING (PTY)  
 Project : Acorn City  
 Project No. : 2020-B-553

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## CALIFORNIA BEARING RATIO (CBR) & ROAD INDICATOR REPORT

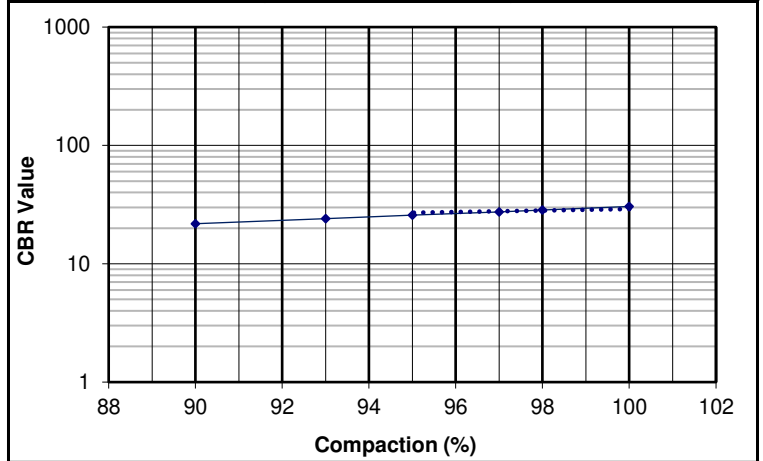
Laboratory No.	19	◆	■
Field Number	TP32		
Client Reference			
Depth (m)	0.1-1.0		
Position			
Coordinates	X		
	Y		
Description			
Additional information			
Calcrete/Crushed			
Stabilizing Agent			

Laboratory No.	19	◆	■
Maximum Dry Density & Optimum Moisture Content		SANS 3001 GR30	
MDD	kg/m <sup>3</sup>	1941	
OMC	%	10.4	

California Bearing Ratio		SANS 3001 GR40		
Compaction Data				
Moisture	%	10.5		
Dry Density	kg/m <sup>3</sup>	1965	1866	1759
Compaction	%	100.0	95.0	89.5

Penetration Data				
CBR at	2.50 mm	29	27	21
	5.00 mm	34	28	21
	7.50 mm	34	27	21
Swell	%	0.1	0.2	0.5
Final Moisture (%)		13.3	14.4	19.8

Sieve Analysis (Wet preparation)		SANS 3001 GR1
Percentage Passing	100 mm	100
	75 mm	100
	63 mm	100
	50 mm	100
	37.5 mm	100
	28 mm	100
	20 mm	100
	14 mm	99
	5 mm	88
	2 mm	69
	1 mm	45
	0.425 mm	22
	0.250 mm	20
	0.150 mm	17
0.075 mm	15	
Grading Modulus	1.9	

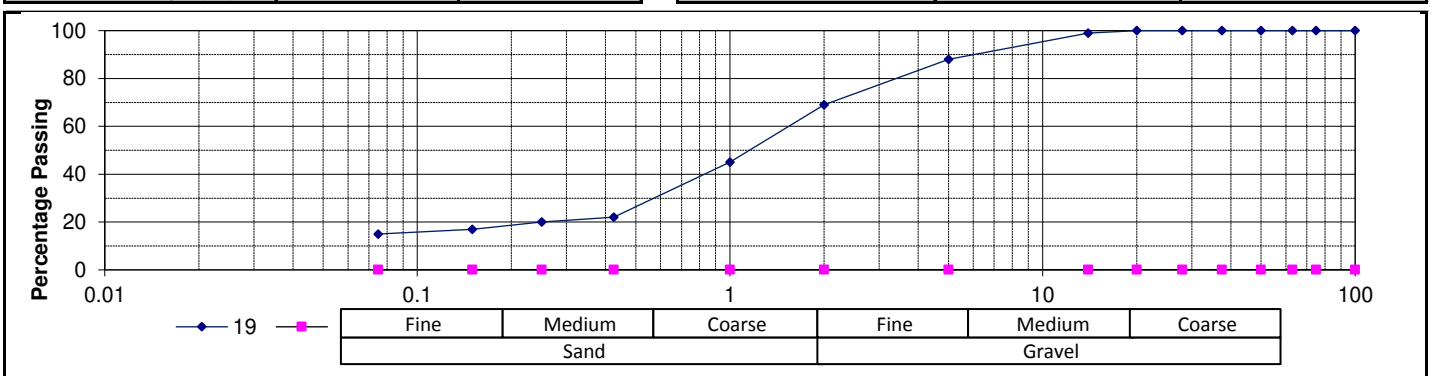


Interpolated CBR Data		
CBR	Mod. AASHTO	
@ 100%		31
@ 98%		29
@ 97%		28
@ 95%		26
@ 93%		24
@ 90%		22
@ SANS3001 Midpoint		28

Soil Mortar Analysis	
Coarse Sand	68
Coarse Fine Sand	3
Medium Fine Sand	4
Fine Fine Sand	3
Silt and Clay	22

Classifications	
HRB (AASHTO)	A-2-6(0)
COLTO	
TRH14	G8

Atterberg Limits		SANS 3001 GR10
Liquid Limit (%)	38	
Plasticity Index (%)	18	
Linear Shrinkage (%)	8.0	





**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acorn City	Date Tested:	4/6/2020
Project No.	2020-B-553	Laboratory Number:	2
Field Sample Reference	TP5	Depth (m):	1.1-1.5

Test No.	1	
Test Type	Collapse Potential	
Remarks	Collapse Potential: 11.75%	

**Specimen-, Preparation- & Test Conditions**

Specimen Type	Undisturbed	
Moulding Dry Density		
Moulding Moisture		
Testing Moisture	Soaked @ 200kPa	

**Equipment Detail**

Machiene No.	OED13	
Ring	No.	H
	Mass (g)	81.6
	Height (mm)	18.94
	Diameter (mm)	70.05

**Specimen Parameters**

Stage	Initial	Final (Unloaded)	Initial	Final (Unloaded)
Relative density (S.G.)	2.650			
Moisture Content (%)	19.7	25.2		
Dry Density (kg/m <sup>3</sup> )	1263	1574		
Void Ratio, e	1.098	0.684		
Degree of Saturation (%)	48	98		

**Test Data**

Test 1																
Cycle	No.	1	2	3	4	5	6	7	8							
Total time	min	1067	4408	1584	1467	1069	1789	3982	2905							
Stress	kPa	10	52	102	202	202	402	102	10							
Strain	%	0.62	3.52	4.37	5.04	16.79	21.80	21.39	19.76							
Void Ratio	e	1.085	1.024	1.006	0.993	0.746	0.641	0.649	0.684							
Mv (1/MPa)		0.000	0.690	0.170	0.067		0.251	0.014	0.178							
t90	min															
Cv	m <sup>2</sup> /year															

Test 2																
Cycle	No.															
Total time	min															
Stress	kPa															
Strain	%															
Void Ratio	e															
Mv (1/MPa)																
t90	min															
Cv	m <sup>2</sup> /year															

The t90 values reported, if any, which are used to calculate the coefficient of consolidation at different loads are selected by the operator conducting the test and checked by the appropriate technical signatories. They may however not reflect an engineer's interpretation of the time settlement graphs and are by no means final.

**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acorn City	Date Tested	4/6/2020
Project No.	2020-B-553	Laboratory Number	2
Field Sample Reference	TP5	Depth (m)	1.1-1.5

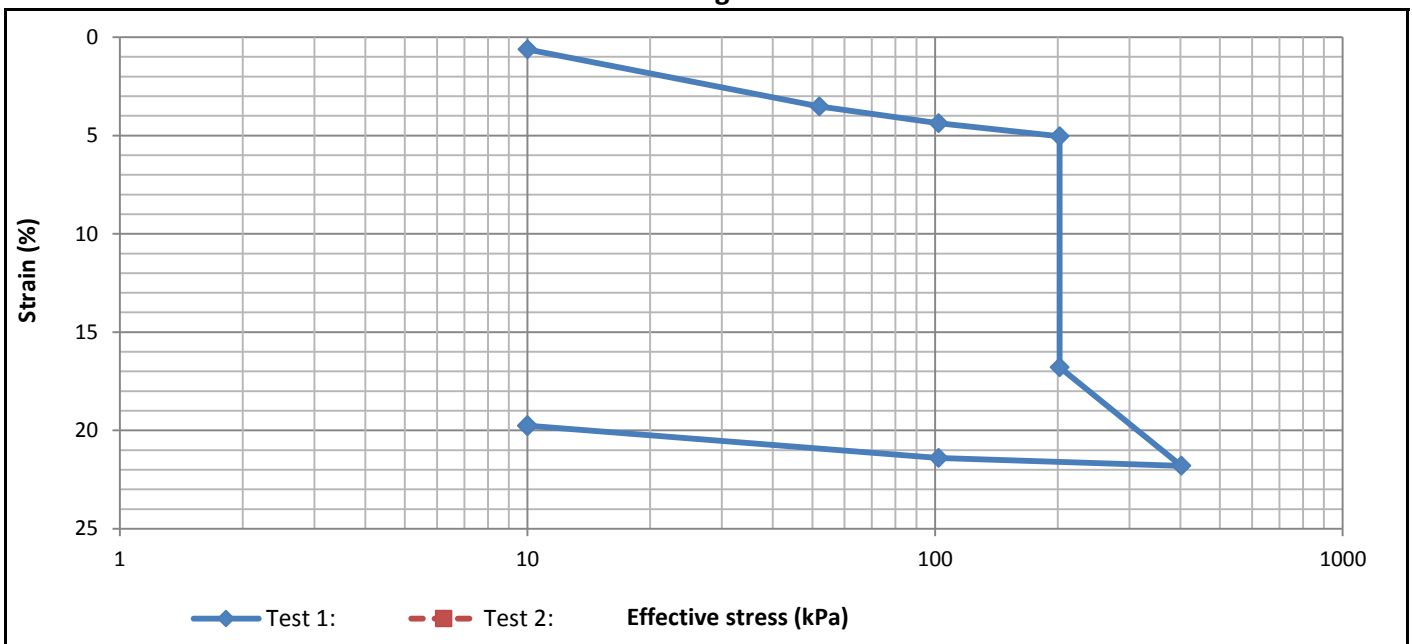
**Test 1: Specimen: Undisturbed , Testing Moisture: Soaked @ 200kPa**

Cycle	1	2	3	4	5	6	7	8									
Stress (kPa)	10	52	102	202	202	402	102	10									
Strain (%)	0.62	3.52	4.37	5.04	16.79	21.80	21.39	19.76									
Void Ratio, e	1.085	1.024	1.006	0.993	0.746	0.641	0.649	0.684									

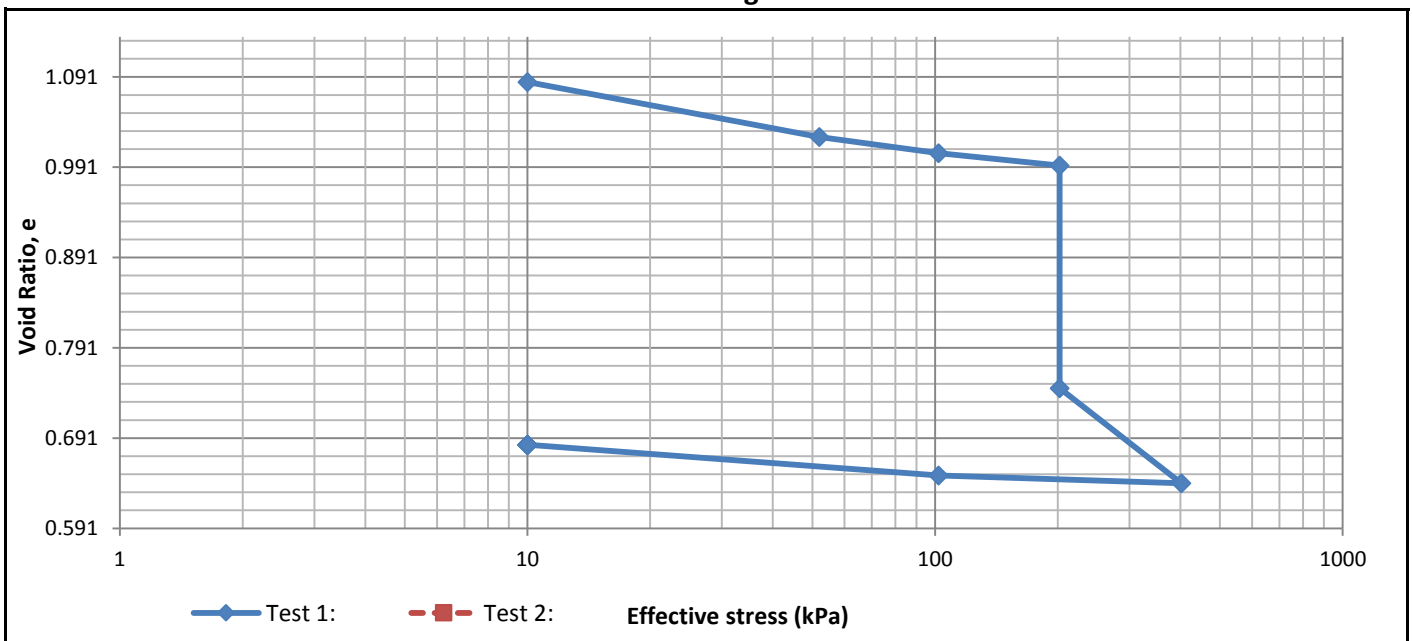
**Test 2:**

Cycle																	
Stress (kPa)																	
Strain (%)																	
Void Ratio, e																	

**Strain Log Stress**



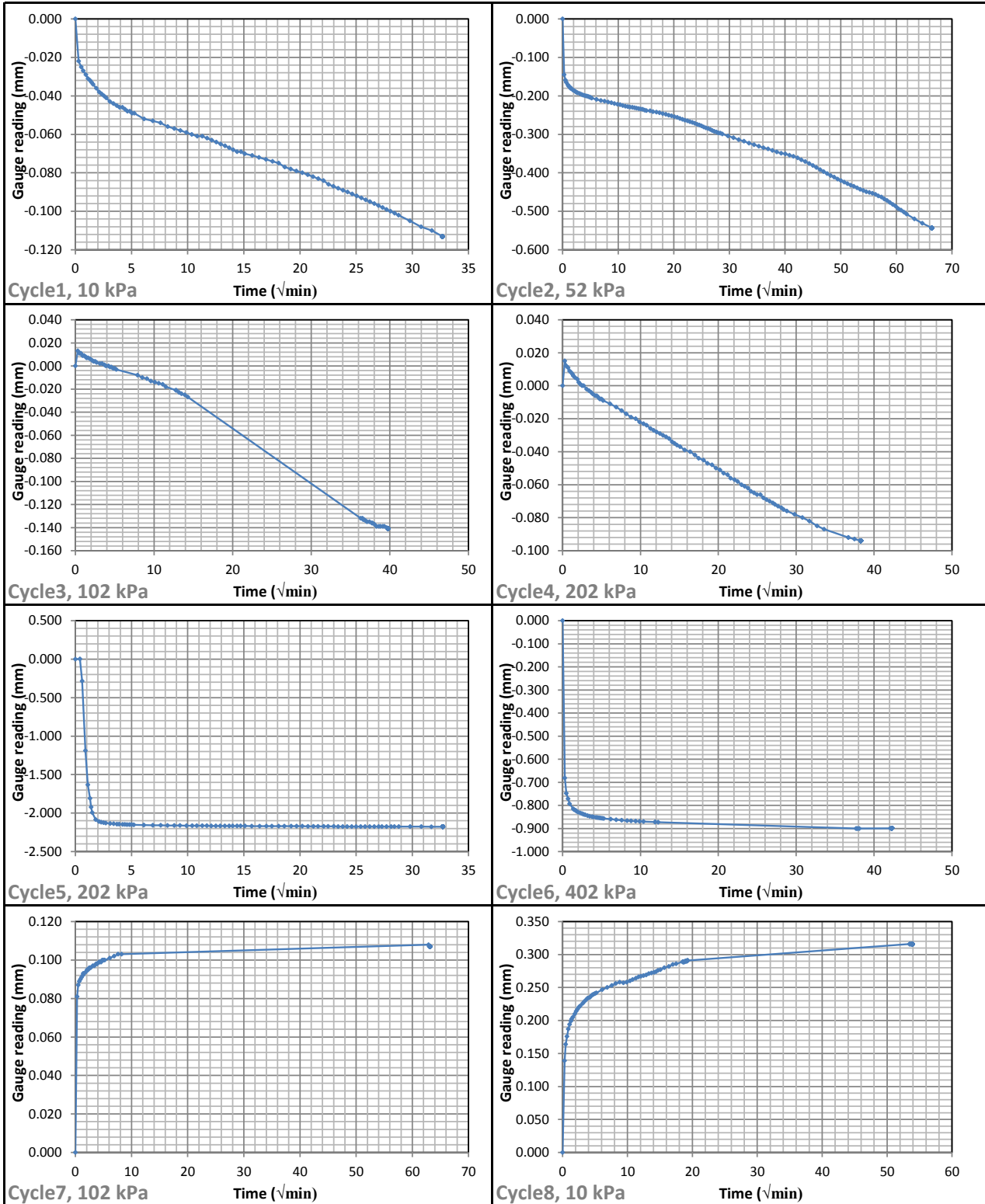
**Void Ratio Log Stress**



**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acorn City	Date Tested:	4/6/2020
Project No.	2020-B-553	Laboratory Number:	2
Field Sample Reference	TP5	Depth (m):	1.1-1.5

**Test 1 - Consolidation vs Square Root Time**



**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acron City	Date Tested:	4/6/2020
Project No.	2020-B-553	Laboratory Number:	11
Field Sample Reference	TP19	Depth (m):	0.5-1.6

Test No.	1	
Test Type	Collapse Potential	
Remarks	Collapse Potential: 2.81%	

**Specimen-, Preparation- & Test Conditions**

Specimen Type	Undisturbed	
Moulding Dry Density		
Moulding Moisture		
Testing Moisture	Soaked @ 200kPa	

**Equipment Detail**

Machiene No.	OED14	
Ring	No.	F
	Mass (g)	75.8
	Height (mm)	19.02
	Diameter (mm)	69.82

**Specimen Parameters**

Stage	Initial	Final (Unloaded)	Initial	Final (Unloaded)
Relative density (S.G.)	2.650			
Moisture Content (%)	21.9	26.4		
Dry Density (kg/m <sup>3</sup> )	1390	1522		
Void Ratio, e	0.906	0.741		
Degree of Saturation (%)	64	94		

**Test Data**

Test 1																
Cycle	No.	1	2	3	4	5	6	7	8							
Total time	min	1078	4184	3058	6856	246.5	2652	1347	299.3							
Stress	kPa	10	52	102	202	202	402	102	10							
Strain	%	0.32	2.13	3.20	3.71	6.51	10.03	9.72	8.68							
Void Ratio	e	0.900	0.866	0.845	0.835	0.782	0.715	0.721	0.741							
Mv (1/MPa)		0.000	0.431	0.215	0.050		0.176	0.010	0.113							
t90	min															
Cv	m <sup>2</sup> /year															

Test 2																
Cycle	No.															
Total time	min															
Stress	kPa															
Strain	%															
Void Ratio	e															
Mv (1/MPa)																
t90	min															
Cv	m <sup>2</sup> /year															

The t90 values reported, if any, which are used to calculate the coefficient of consolidation at different loads are selected by the operator conducting the test and checked by the appropriate technical signatories. They may however not reflect an engineer's interpretation of the time settlement graphs and are by no means final.

**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acron City	Date Tested	4/6/2020
Project No.	2020-B-553	Laboratory Number	11
Field Sample Reference	TP19	Depth (m)	0.5-1.6

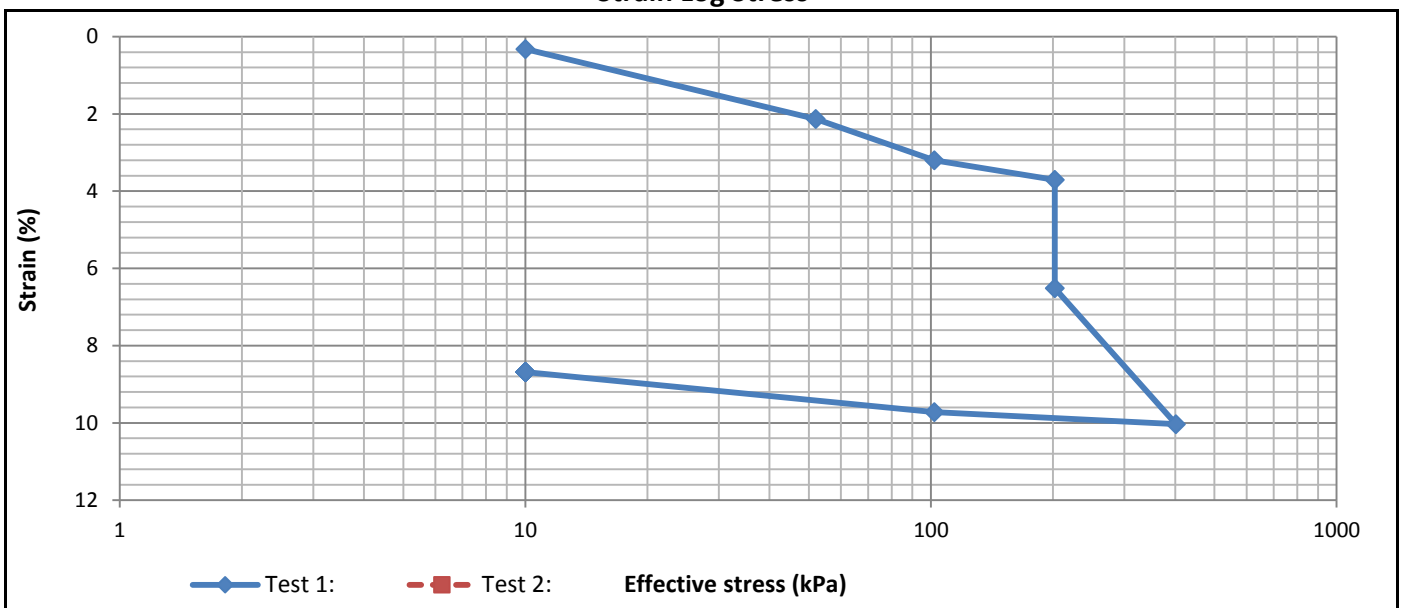
**Test 1: Specimen: Undisturbed , Testing Moisture: Soaked @ 200kPa**

Cycle	1	2	3	4	5	6	7	8						
Stress (kPa)	10	52	102	202	202	402	102	10						
Strain (%)	0.32	2.13	3.20	3.71	6.51	10.03	9.72	8.68						
Void Ratio, e	0.900	0.866	0.845	0.835	0.782	0.715	0.721	0.741						

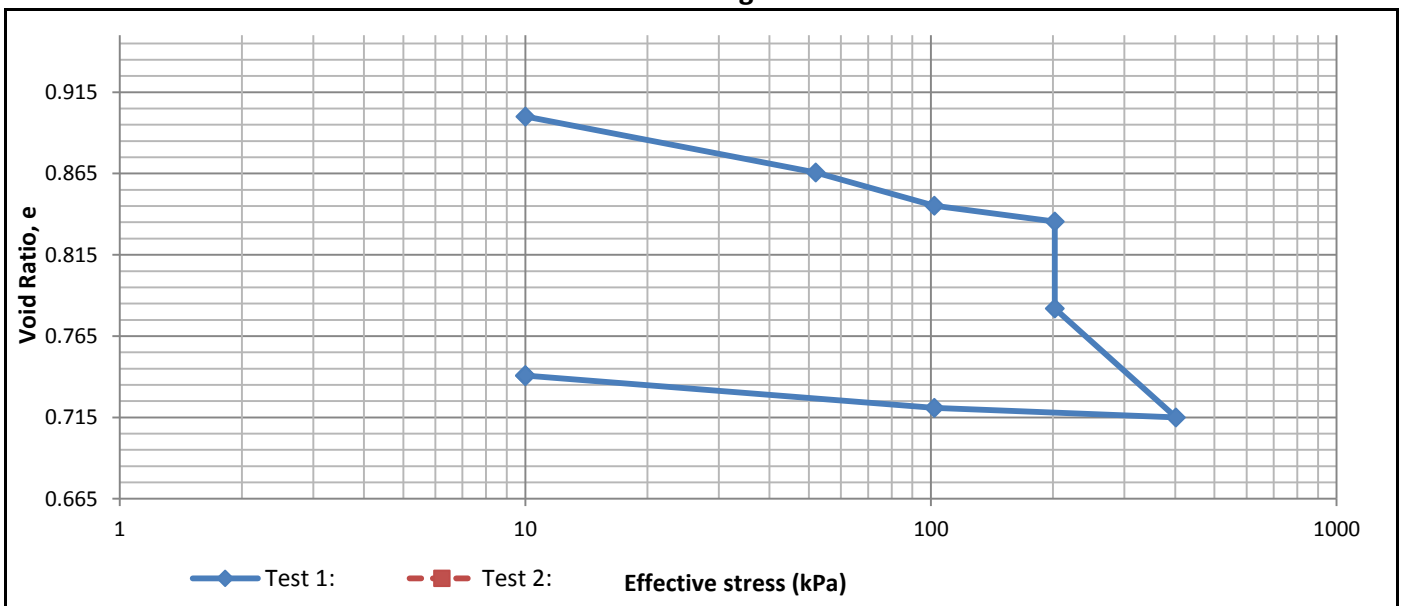
**Test 2:**

Cycle														
Stress (kPa)														
Strain (%)														
Void Ratio, e														

**Strain Log Stress**



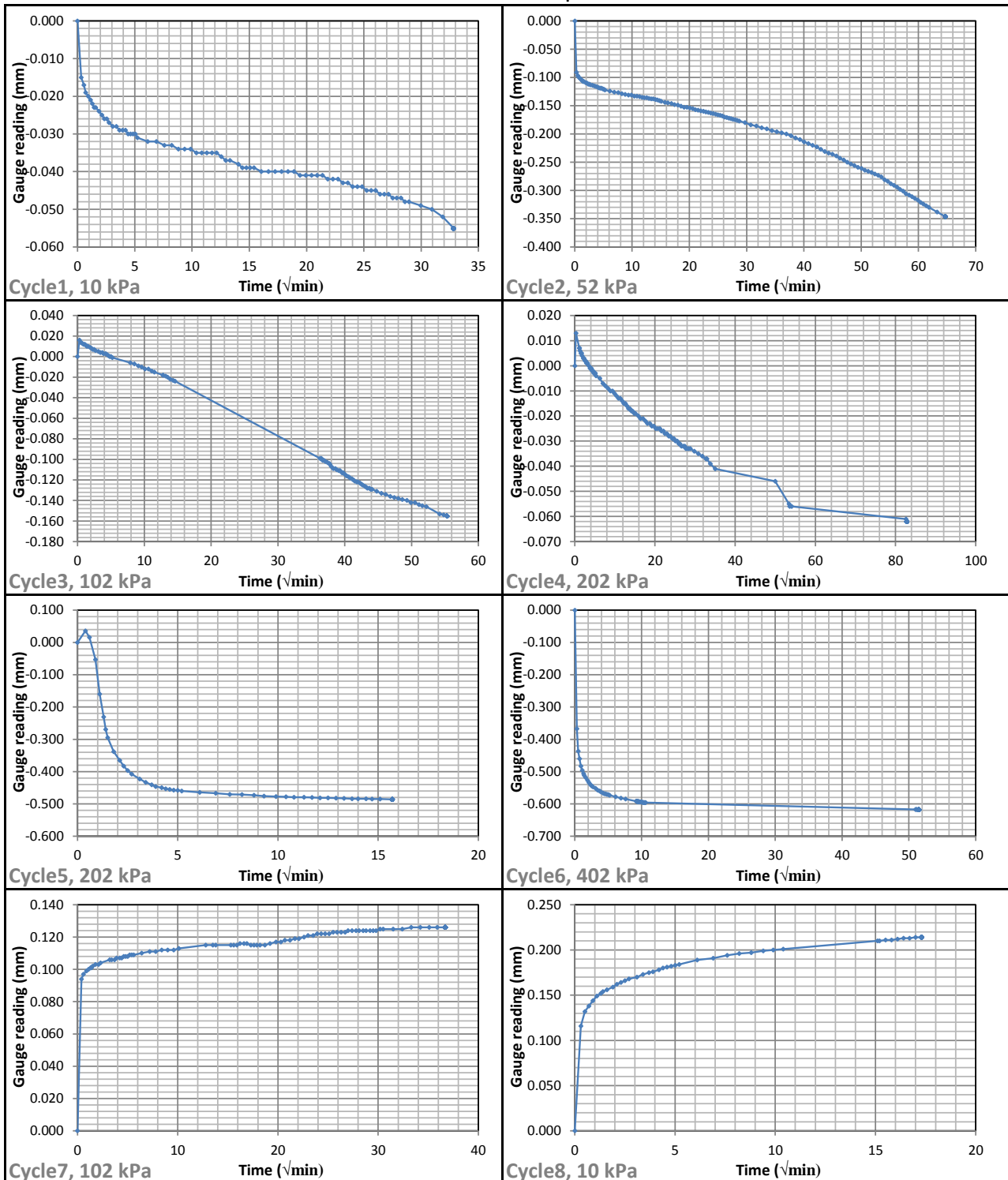
**Void Ratio Log Stress**



**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acron City	Date Tested:	4/6/2020
Project No.	2020-B-553	Laboratory Number:	11
Field Sample Reference	TP19	Depth (m):	0.5-1.6

**Test 1 - Consolidation vs Square Root Time**



**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acorn City	Date Tested:	4/6/2020
Project No.	2020-B-553	Laboratory Number:	14
Field Sample Reference	TP23	Depth (m):	0.5-1.6

Test No.	1	
Test Type	Collapse Potential	
Remarks	Collapse Potential: 13.41%	

**Specimen-, Preparation- & Test Conditions**

Specimen Type	Undisturbed	
Moulding Dry Density		
Moulding Moisture		
Testing Moisture	Soaked @ 200kPa	

**Equipment Detail**

Machiene No.	OED15	
Ring	No.	15
	Mass (g)	84.5
	Height (mm)	19.15
	Diameter (mm)	69.84

**Specimen Parameters**

Stage	Initial	Final (Unloaded)	Initial	Final (Unloaded)
Relative density (S.G.)	2.650			
Moisture Content (%)	13.5	21.8		
Dry Density (kg/m <sup>3</sup> )	1305	1652		
Void Ratio, e	1.030	0.604		
Degree of Saturation (%)	35	96		

**Test Data**

Test 1																
Cycle	No.	1	2	3	4	5	6	7	8							
Total time	min	1067	4184	1444	1600	1069	1781	2916	1325							
Stress	kPa	10	52	102	202	202	402	102	10							
Strain	%	0.68	2.03	2.43	3.46	16.87	22.03	21.82	21.00							
Void Ratio	e	1.016	0.989	0.981	0.960	0.688	0.583	0.587	0.604							
Mv (1/MPa)		0.000	0.322	0.080	0.103		0.258	0.007	0.089							
t90	min															
Cv	m <sup>2</sup> /year															

Test 2																
Cycle	No.															
Total time	min															
Stress	kPa															
Strain	%															
Void Ratio	e															
Mv (1/MPa)																
t90	min															
Cv	m <sup>2</sup> /year															

The t90 values reported, if any, which are used to calculate the coefficient of consolidation at different loads are selected by the operator conducting the test and checked by the appropriate technical signatories. They may however not reflect an engineer's interpretation of the time settlement graphs and are by no means final.

**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acorn City	Date Tested	4/6/2020
Project No.	2020-B-553	Laboratory Number	14
Field Sample Reference	TP23	Depth (m)	0.5-1.6

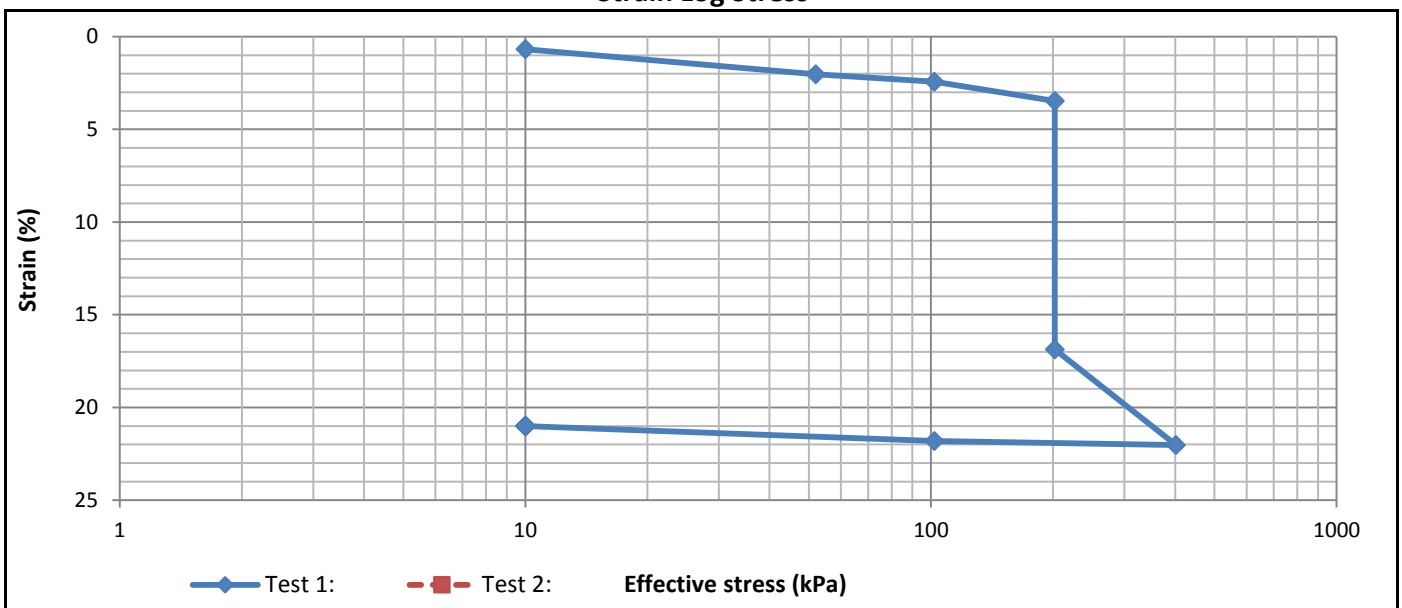
**Test 1: Specimen: Undisturbed , Testing Moisture: Soaked @ 200kPa**

Cycle	1	2	3	4	5	6	7	8						
Stress (kPa)	10	52	102	202	202	402	102	10						
Strain (%)	0.68	2.03	2.43	3.46	16.87	22.03	21.82	21.00						
Void Ratio, e	1.016	0.989	0.981	0.960	0.688	0.583	0.587	0.604						

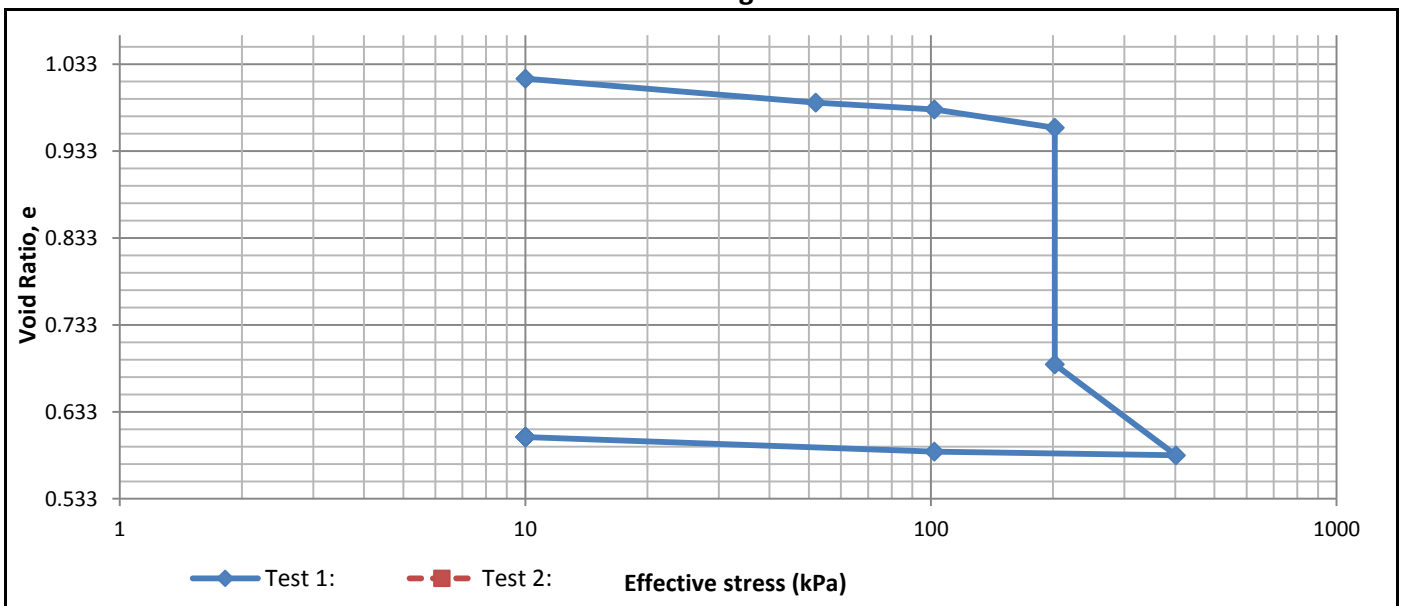
**Test 2:**

Cycle														
Stress (kPa)														
Strain (%)														
Void Ratio, e														

**Strain Log Stress**



**Void Ratio Log Stress**





**CONSOLIDATION TEST RESULTS - BS 1377: Part 5**

Project	Acorn City	Date Tested:	4/6/2020
Project No.	2020-B-553	Laboratory Number:	14
Field Sample Reference	TP23	Depth (m):	0.5-1.6

**Test 1 - Consolidation vs Square Root Time**

