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Pienaarsrivier Filling Station

Geotechnical Investigation Report

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DATE: 25 February 2019

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EXECUTIVE SUMMARY

ARQ was appointed by Mr Anton van Vuuren on behalf of Accurate Trading 47 (Pty) Ltd (the Client), to conduct a geotechnical investigation for the proposed Pienaarsrivier Filling Station in the Limpopo Province.

The investigation made provision for a near surface investigation in the form of excavator test pits.

An additional percussion borehole was drilled on site to evaluate the depth of watertable on site.

Recommendations are provided in Section 8.

TABLE OF CONTENTS

1.	Introduction	6
2.	THE SITE	6
3.	GEOLOGY OF THE AREA	7
4.	GENERAL COMMENTS	8
5.	METHOD OF INVESTIGATION	8
	5.1. TEST PITS INVESTIGATION	8
	5.2. Percussion Borehole	8
6.	TESTING LOCALITY AND COORDINATES	8
7.	RESULTS OF THE INVESTIGATION	10
	7.1. Typical soil profile	10
	7.2. CHARACTERISATION OF GEOLOGICAL HORIZONS	10
	7.3. LABORATORY TESTING OF SOIL	11
	7.4. GEOTECHNICAL EVALUATIONS	12
	7.4.1. GRADING ANALYSIS	
	7.4.2. Expansive/Active soils	12
	7.4.3. COLLAPSIBLE SOILS	12
	7.4.4. PH AND CORROSIVITY	12
	7.4.5. MOISTURE CONTENT	13
	7.4.6. COMPACTION AND STRENGTH PROPERTIES	13
	7.4.7. PERMEABILITY	13
	7.5. EXCAVATION CONDITIONS	13
	7.5.1. GROUNDWATER	13
8.	RECOMMENDATIONS	14
	8.1. FOUNDING OF LIGHT STRUCTURES	14
	8.2. ACCESS ROADS AND PARKING	15
	8.2.1. USE OF MATERIAL IN LAYERWORKS	15
	8.2.2. DESIGN OF LAYERWORKS	15
	8.3. TANK FARM	15
	8.3.1. Founding	15
	8.4. Precausionary	15
	8.4.1. CORROSIVE SOILS	15
	8.4.2. Presence of Marl	16
	8.4.3. Drainage	16
9.	CONCLUSION	16
10	GENERAL	16
11	References	16

Table of Figures	
FIGURE 2-1: SITE LOCALITY MARKED BY YELLOW ARROW AS SEEN IN GOOGLE EARTH TM	7
FIGURE 3-1: GEOLOGY OVERLAY AS SEEN IN GOOGLE EARTH.	7
FIGURE 6-1: SITE LAYOUT SHOWING POSITIONS OF TP A TO TP P AND BH01	9
FIGURE 7-1: GRADING CURVE.	12
Table of Tables	
TABLE 6-1: TEST PIT COORDINATES.	
TABLE 6-2: BOREHOLE COORDINATE	
TABLE 7-1: SUMMARY OF TEST PITS PROFILES.	
TABLE 7-2: LABORATORY TESTING.	
TABLE 7-3: SUMMARY OF LABORATORY RESULTS.	11
Appendixes	
APPENDIX A TEST PIT PROFILES	
APPENDIX B PERCUSSION BOREHOLE PROFILE	
APPENDIX C LABORATORY RESULTS	

LIST OF ABBREVIATIONS AND ACRONYMS

ARQ Consulting Engineers (Pty) Ltd

AASHTO American Association of State Highway and Transportation Officials

CBR California Bearing Ratio

COLTO Committee of Land Transport Officials

D Disturbed sample

m metre

MDD/ OMC Moisture-density relationship

NGL Natural Ground Level

PI Plastic Index

SABS South African Bureau of Standards

SAICE South African Institution of Civil Engineers
SANAS South African National Accreditation System

TMH Technical Methods for Highways

TP Test pit

1. Introduction

ARQ was approached by Mr Anton van Vuuren of Accurate Trading 47 (Pty) Ltd, henceforth referred to as the Client, to conduct a geotechnical investigation for the proposed Pienaarsrivier Filling Station in the Limpopo Province.

The site in question comprise ERF 425 (6 895m²) and ERF 426 (7 972m²) with a combined total coverage of 1.4 hectares to be investigated.

The development will consist of:

- A brick building (Service station and Quick Service Restaurant (QSR)),
- Future building,
- Car Dispensary (5 x dispensaries),
- Truck Dispensary (1 x dispensaries),
- Truck Building,
- Cashier cubicle,
- Tank Farm (4 tanks),
- Parking,
- Truck stop area, and
- Access Roads.

The investigation comprised test pits excavated using an excavator (Komatsu PC220) provided by the Client. These test pits were excavated to a maximum depth of approximately 2.4m (where refusal occurred) and were profiled by Madaleen Booysen of ARQ according to industry standards.

The investigation was aimed at providing information with regard to:

- General geology of site,
- Engineering properties of materials encountered,
- Water table and groundwater seepage,
- Suitability of materials for use as fill and layer works,
- Bearing capacity/ suitability for founding in the in-situ soil/soft rock layers,
- Potential expansiveness/collapsibility of the soils,
- Excavatability of the in-situ material, and
- Founding recommendations.

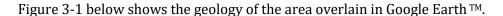
2. THE SITE

The site is located to the west of the N1 at the town of Pienaarsrivier in the Limpopo Province at the approximate co-ordinates; $25^{\circ}12'21.28"S\ 28^{\circ}18'0.23"E$. Refer to Figure 2-1 below for site locality as seen in Google Earth TM.



Figure 2-1: Site locality marked by yellow arrow as seen in Google Earth $^{\text{TM}}$.

3. GEOLOGY OF THE AREA



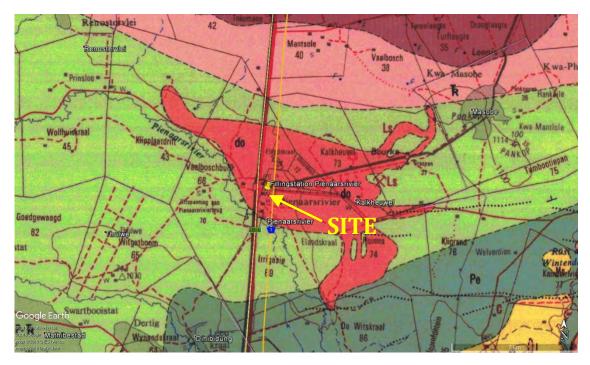


Figure 3-1: Geology overlay as seen in Google Earth.

The 1:250 000 geological map 2528 PRETORIA shows that the site is underlain by dolerite of the Jurassic Period.

The surrounding area is underlain by multi-coloured siltstone, sandstone, marl, mudstone and shale of the Irrigasie Formation, Karoo Supergroup.

4. **GENERAL COMMENTS**

The building layout that the Client provided to ARQ could not be overlain accurately prior to the investigation due to the absence of any visible markers. As such a Client representative was present during the fieldwork to ensure correct placing of ARQ's testing positions according to the Client's latest building design.

5. METHOD OF INVESTIGATION

The investigation was carried out in accordance with SAICE's Site Investigation Code of Practice (2010) and comprised test pits only.

One percussion borehole was drilled on site to establish the depth to watertable.

5.1. TEST PITS INVESTIGATION

Sixteen test pits were excavated to determine in-situ soil conditions and suitability of material for founding as well as to be used as fill or layer works. Test pits were positioned on the footprints of the planned structures as indicated by the Client.

The test pits were profiled according to current methods and procedures (Brink and Bruin, 2002). Samples were taken and tested at a SANAS accredited soils laboratory. Positioning of test pits was undertaken on site, and recorded using a hand-held GPS.

5.2. **PERCUSSION BOREHOLE**

After some concerns were raised that the watertable was not encountered during the excavation of the test pits and additional percussion borehole was drilling on site.

The sole purpose of the borehole was to determine the depth to watertable, as such no samples were logged or evaluated.

6. TESTING LOCALITY AND COORDINATES

Coordinates of the test pits are included in Table 6-1 below.

Table 6-1: Test pit coordinates.

Coordinates						
	South	East				
TP A	25°12'20.40"S	28°17'57.40"E				
TP B	25°12'20.30"S	28°18'00.60"E				
TP C	25°12'20.20"S	28°17'59.20"E				
TP D	25°12'20.20"S	28°17'59.60"E				
TP E	25°12'20.40"S	28°17'55.30"E				
TP F	25°12'19.40"S	28°17'58.40"E				
TP G	25°12'19.40"S	28°17'58.70"E				
TP H	25°12'19.60"S	28°17'59.30"E				
TP I	25°12'19.70"S	28°18'00.20"E				
TP J	25°12'19.10"S	28°17'56.50"E				
TP K	25°12'19.40"S	28°17'56.40"E				
TP L	25°12'19.90"S	28°17'56.00"E				
TP M	25°12'20.30"S	28°18'00.20"E				
TP N	25°12'20.40"S	28°17'58.00"E				
TP O	25°12'19.00"S	28°17'59.20"E				
TP P	25°12'18.90"S	28°17'54.30"E				

Table 6-2: Borehole coordinate.

Coordinates					
	South	East			
BH01	25°12'20.50"S	28°17'59.30"E			

Figure 6-1 overleaf shows positions of test pits in yellow markers and borehole in pink marker, as seen in Google Earth $^{\text{TM}}$.



Figure 6-1: Site layout showing positions of TP A to TP P and BH01.

7. RESULTS OF THE INVESTIGATION

7.1. TYPICAL SOIL PROFILE

A summary of the test pit profiles is presented in Table 7-1, whilst comprehensive soil profiles are included in **Appendix A**.

A site-specific geological characterization is provided in the section below. Disturbed samples were collected from six soil layers (in 5 test pits) which are indicated in Table 7-2.

Table 7-1: Summary of test pits profiles.

Layer	Layer						
Test	Soft to stiff, sandy clay,	Soft to hard rock, sandstone	Refusal/ termination				
pit	Topsoil	and dolerite	teriiiiiatioii				
TP A	0.0-0.6m	0.6-1.5m	Refusal 1.5m				
TP B	0.0-0.5m	0.5-2.0m	Refusal 2.0m				
TP C	0.0-0.6m	0.6-1.8m	Refusal 1.8m				
TP D	0.0-0.6m	0.6-1.4m	Refusal 1.4m				
TP E	0.0-1.1m	1.1-2.4m	Refusal 2.4m				
TP F	0.0-0.7m	0.7-2.0m	Refusal 2.0m				
TP G	0.0-0.5m	0.5-2.1m	Refusal 2.1m				
TP H	0.0-0.6m	0.6-1.7m	Refusal 1.7m				
TP I	0.0-0.6m	0.6-2.1m	Refusal 2.1m				
TP J	0.0-0.8m	0.8-1.8m	Refusal 1.8m				
TP K	0.0-0.5m	0.5-1.7m	Refusal 1.7m				
TP L	0.0-0.7m	0.7-1.8m	Refusal 1.8m				
TP M	0.0-0.5m	0.5-1.9m	Refusal 1.9m				
TP N	0.0-0.6m	0.6-2.0m	Refusal 2.0m				
TP O	0.0-0.8m	0.8-2.1m	Refusal 2.1m				
TP P	0.0-0.45m	0.45-2.4m	Refusal 2.4m				

The following tests were conducted on the layers indicated above by the blue shading.

Table 7-2: Laboratory testing.

Laboratory test conducted	Colour indication
California Bearing Ratio (CBR),	
Maximum Dry Density/Optimum Moisture,	
Foundation Indicators,	
Moisture content	
pH and conductivity	

The percussion borehole profile can be viewed in **Appendix B**.

7.2. CHARACTERISATION OF GEOLOGICAL HORIZONS

The site-specific geology can be characterised as follows:

a) Top soil

• <u>Sandy silty clay</u> - This horizon is generally described as dark brown soft to stiff sandy clay ranging in thicknesses from 0.45-1.1m. Plant roots are expected due to the dense vegetation and as such not specifically mentioned in each profile.

b) Soft to hard rock altered sandstone and dolerite

- <u>Altered sandstone and dolerite</u> Dolerite rock was encountered along with an altered sandstone. The term altered implies some baking of the sandstone was also observed. This may be due to the alteration of the sandstone during the dolerite intrusion. It is believed that the site is located on the gradual contact between the two lithologies and as such a mixture/ combination of the two is present on site with no distinct separation.
- The soft to hard rock was excavated until refusal conditions were encountered by the excavator at a depth between 1.4-2.4m below natural ground level (NGL). The rocks exhibited differential weathering with some staining along joints.

7.3. **LABORATORY TESTING OF SOIL**

Soil samples obtained during investigations were sent to an independent soil laboratory (SGS Matrolab Pretoria) for testing.

A summary of the laboratory test results are provided in Table 7-3 overleaf whilst the comprehensive results are presented in **Appendix C**.

Table 7-3: Summary of laboratory results.

Sample No.	TP B	TP E	TP G	TP G	TP J	TP I
					·	
Depth (m)	0.5-2.0	1.1-2.4	0.0-0.5	0.5-2.1	0.0-0.8	0.7-1.8
Liquid Limit	53	45	45	50	47	55
Plasticity Index	26	20	22	22	26	24
Plasticity Index of whole sample	8	5	10	4	15	5
Linear shrinkage	11.5	9	10.5	11	13.5	11
Grading modulus	2.01	1.99	1.56	2.28	1.42	2.44
% passing 0.425mm	29	28	51	20	57	19
% passing 0.075mm	19	16	29	12	36	13
Expansiveness rating	Low	Low	Low	Low	Low	Low
AASHTO Classification	A-2-7(1)	A-2-7(0)	A-2-7(2)	A-2-7(0)	A-7-6(4)	A-2-7(0)
pH values	7.9	7.9	7.5	8	7.8	8
Electrical Conductivity (S/m)	0.0862	0.0611	0.0939	0.0523	0.0863	0.0805
Corrosivity	Very corrosive	Very corrosive	Very corrosive	Very corrosive	Very corrosive	Very corrosive
Optimum moisture content (%)	13.5	10.8	15.3	11.4	14.9	9.2
Max Dry Density (kg/m³)	1991	2089	1806	2075	1740	2107
CBR @ 100% Mod AASHTO (%)	11	30	7	15	6	30
CBR @ 95% Mod AASHTO (%)	9	17	6	8	4	24
CBR @ 93% Mod AASHTO (%)	8	13	6	7	3	22
Max swell @ 100% Mod AASHTO (%)	0.7	0.1	1.1	0.7	1.6	0.3
Classification (COLTO)	NC	NC	NC	NC	NC	NC

^{*}NC = Non-Classifiable. All samples were NC due to high a PI.

7.4. **GEOTECHNICAL EVALUATIONS**

Comprehensive geotechnical evaluations are given in the sections below.

It is important to bear in mind that the soil samples collected on site from the layer beneath the top soil, i.e. "soft to hard rock, sandstone and dolerite", was obtained from the soil fines between the broken pieces of rock and as such is merely an indication of the fines portion of this layer which in actual fact comprise mostly rock fragments. .

7.4.1. GRADING ANALYSIS

The grading curve of the material tested can be viewed in Figure 7-1. Specific values can be viewed in the individual laboratory results in **Appendix C**.

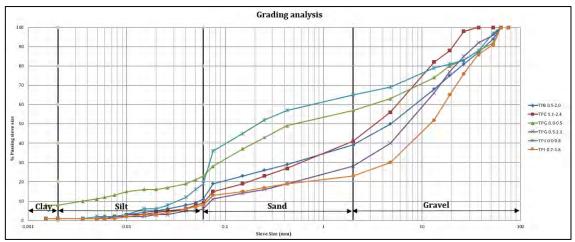


Figure 7-1: Grading curve.

7.4.2. EXPANSIVE/ACTIVE SOILS

Although the finer portion (<0.425mm) of the material tested yielded high Plasticity Index (PI) values, the expansiveness rating of the material, which is a function of the PI of the hole samples vs. the clay fraction of the sample, is low. Therefore expansive soils (i.e. heaving or shrinking) is not expected to be problematic on this site.

7.4.3. COLLAPSIBLE SOILS

A soil with a collapsible fabric may be defined as a soil which can withstand relatively large imposed stresses with minor settlement at a low in-situ moisture content but will exhibit a decrease in volume (which could be of large magnitude) with no increase in the applied stress if wetting-up occurs.

No collapsible structure was identified within the material and thus collapsible material is not expected to be problematic on this site.

7.4.4. PH AND CORROSIVITY

Corrosivity of the material on site was classified as "Very corrosive" with an alkaline pH that ranges from 7.5-8.0 (a pH of 7.0 indicates a completely neutral material) and an electrical conductivity of 0.0523-0.0939 S/m.

7.4.5. MOISTURE CONTENT

From **Table 7-3** it can be seen that the optimum moisture content of the soils tested ranges from 9.2-15.3%.

The material on site was typically described as slightly moist, and it will likely be necessary to add water during the compaction process to bring the material to optimum moisture content.

7.4.6. COMPACTION AND STRENGTH PROPERTIES

CBR tests were conducted according to TMH1 (1986) on representative samples which were subsequently classified according to COLTO (1998). A summary of strength and compaction properties of materials sampled are presented in **Table 7-3**.

None of the materials tested are classifiable according to COLTO due to their high PI values (>12 or >3 \times GM +10). Considering the CBR of the material in isolation (i.e. apart from the PI values rendering the material non-classifiable) the strength of the top soil material is similar to that of a G10 or worse and the strength of the soil portion of the rock layer ranges between that of a G7 to a G9.

7.4.7. PERMEABILITY

The coefficient of permeability depends primarily on the grading and density.

It is possible to estimate the coefficient of permeability for the material at a depth of 0.5-2.4m below NGL by using the empirical method proposed by Hazen. The sieve size allowing 10% of sampled material (by weight) to pass is used as input into Hazen's empirical formulation. The coefficient of permeability was calculated as 3.6×10^{-5} m/s. This value correlates with the typical coefficient of permeability for very fine sands or silts and clay silts (Table 2.1 in Craig's Soil Mechanics, 2004). This is in line with what would be expected.

Therefore, in the absence of permeability specific testing it is proposed that the in-situ permeability of the material surrounding the top of the tank will be approximately 3.6×10^{-5} m/s, and will decrease with depth as more competent rock is encountered.

7.5. **EXCAVATION CONDITIONS**

Based on SABS 1200, "soft" excavation conditions can be expected up to depths of between 1.4m and 2.4m beneath natural ground level.

Although the depth of the investigation was limited to a maximum depth of 2.4m, it is estimated that "intermediate" excavation conditions can be expected in the sandstone bedrock immediately below the "soft" excavation conditions. It is possible that the sandstone bedrock becomes more competent with depth and that at some level "hard" excavation conditions occur, however due to the limited depth of this investigation no more detail can be provided on this.

7.5.1. GROUNDWATER

No water table or seepage was encountered in any test pits.

A percussion borehole was drilled on site with the singular purpose of locating the watertable if encountered within 10m below NGL.

The drilling conducted was concluded without additional fluid being added during the drilling process. The watertable encountered during the drilling proses was located at 9m below NGL.

The site was subjected to heavy rains during the day leading up to the drilling and two days thereafter. The amount of rain received during the period of 13 February 2019 to 15 February 2019 can be obtained from the South African Weather Service, at a cost. However as the closest measuring station is some 36km away the relevance of the data cannot be ensured.

The standing watertable was measured 48 hours after the drilling was completed instead of the usual 24 hours as ARQ thought it prudent to evaluate the rise of watertable along with the rain encountered. The watertable measured after 48 hours was at 5.5m below NGL.

8. RECOMMENDATIONS

The recommendations given in this report are based on the near-surface geotechnical investigation conducted on site and a single percussion borehole (watertable depth only).

8.1. **FOUNDING OF LIGHT STRUCTURES**

The following founding methods are recommended for the light structures:

Option 1:

Remove the top soil and found the light structures (single storey buildings) on very soft to soft rock dolerite or sandstone. Strip or pad footings can be used and the foundations should be designed such as not to exceed allowable bearing pressures of 250kPa. Based on the test pits this founding depth will vary between ± 0.5 m and 1.1m below NGL (average depth ± 0.7 m).

Option 2:

Remove the top soil until very soft rock or harder dolerite or sandstone is encountered (as per the depths described in Option 1). Then backfill the excavation with G7 quality material or better compacted in maximum 150mm layers to minimum 93% of its Mod AASHTO maximum dry density at 0 to +2% of its optimum moisture content. The light structures can then be founded on strip or pad footings on the G7 material at a minimum depth of 0.5m below ground level. The foundations should be designed such as not to exceed allowable bearing pressures of 150kPa. The plan dimensions of the excavation must be equal to the width of the foundation plus a width equal to the thickness of the G7 backfill. For pad footings both plan dimensions (length and width) of the excavation must be increased by a length equal to the thickness of the G7 backfill layer.

Option 3:

If higher allowable bearing pressures are required the top soil and very soft rock must be removed and the structures founded on pad or strip footings on the soft rock (maximum

allowable bearing pressure of 500 kPa) or on medium hard rock or harder (maximum allowable bearing pressures of 1 MPa).

Please note:

All foundations should be inspected by a competent geotechnical engineer/engineering geologist prior to concrete in order to verify that the founding conditions are in agreement with the recommendations given in this report.

8.2. ACCESS ROADS AND PARKING

8.2.1. USE OF MATERIAL IN LAYERWORKS

The topsoil material above the bedrock was found to be non-classifiable (i.e. worse than G10) and is therefore unsuitable for use in layerworks The two samples tested from this material have a subgrade rating (based on their AASHTO classification) of good and poor respectively. This material's consistency was however often described as "soft" in the test pits and therefore, together with the fact that 1 out of 2 samples have a poor subgrade rating, is considered to be a fair to poor subgrade material. The material may however be used for landscaping or rehabilitation purposes.

The soil material sampled from the rock layer underlying the topsoil was non-classifiable and is therefore unsuitable for use in layerworks. It does however have a good to excellent rating as a subgrade.

As all of the material sampled was non-classifiable and therefore not suitable for use in layerworks it is recommended that the Client import material for use in layerworks from a commercial source.

8.2.2. DESIGN OF LAYERWORKS

Due to the load requirements and vibration impacts of the fuel tankers it is recommended that the Client appoint a specialist Pavement/ Road Engineer to design the layerworks required.

8.3. TANK FARM

8.3.1. FOUNDING

Based on information received from the Client the base of the tank farm will be placed 4.5m below NGL. As the test pits refused above this level it is believed that medium hard rock or harder (allowable bearing capacity of 1MPa) will be present at the proposed tank base level for founding.

The rock strength should be verified by a competent geotechnical engineer/ engineering geologistonce the excavation for the tank farm has reached the proposed founding level.

8.4. **PRECAUSIONARY**

8.4.1. CORROSIVE SOILS

The material on site was evaluated to be "Very Corrosive". It is recommended that the Client take adequate preventative measures (e.g. sufficient cover to steel reinforcement, adequate

concrete mix design)in order to ensure that the material do not corrode the concrete, steel reinforcement, tanks, pipes or any other underground services.

8.4.2. PRESENCE OF MARL

Although no marl rock was encountered during the investigation, the possible presence of the rock in the surrounding area should not be overlooked.

It is recommended that the Client take precautionary measures during construction and for the lifetime of the development to ensure that any calcite minerals present on site are not dissolved due to improper drainage or maintenance of the development.

8.4.3. DRAINAGE

It is essential that proper site drainage and plumbing/services precautions be taken to prevent saturation of underlying materials, e.g.. proper down pipes which eject away from the proposed structure must be installed in conjunction with a concrete or a paved apron with a width of at least 1m.

9. CONCLUSION

The investigation undertaken has revealed valuable information relating to the soil and rock profile on site as well as the engineering properties of the materials.

10. GENERAL

The comments and recommendations contained within this report are based on a limited number of tests and observations which ARQ believe are representative. However, conditions at variance with those described in this report should not be overlooked.

11. REFERENCES

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APPENDIX A TEST PIT PROFILES

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Test Pit: TP A

Test	Pit: T	P A		
			Client:	MDV Development
		P	roject:	PienaarsrivierFilling Station - 8536
Date Profiled:			rofiled:	2019/01/30
Coordinates:			inates:	25°12'20.4 "S, 28°17'57.4 "E
	Elevation:			1045 m
		Profil	led By:	Madaleen Booysen
		ater		
Œ	ing	×	_	option and the state of the sta
Depth (m)	Sampling	Ground Water	Symbol	Description
Ĭ	Š	Ō	\(\(\oldsymbol{S} \)	
				SOFT TO STIFF, SANDY SILTY CLAY Slightly moist, dark brown, soft to stiff, sandy silty clay
0.1 -				Topsoil
0.2 -				
0.3 -				
0.5				
0.4 -				
0.5 -				
0.6 -				(0.6 m)
			×	SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock,
0.7 -			×	altered sandstone and dolerite
0.8 -			×	
0.9 -			×	
			×	
1.0 -			×	
1.1 -				
1.2 -			×	
			×	
1.3 -			×	
1.4 -			×	
1.5 -			×	(1.5 m)
				Refused On: Hard rock sandstone and dolerite
1.6 -				
1.7 –				
1.8 -				
1.9 -				
1.9				
2.0 -				
2.1 -				
2.2 -				
2.2				
				EXCAVATOR
	Ur		Sides:	
			etusal: Table:	1.5 m on Hard rock sandstone and dolerite
		vvater	i abie:	Page 1 of 16

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Test Pit: TP B

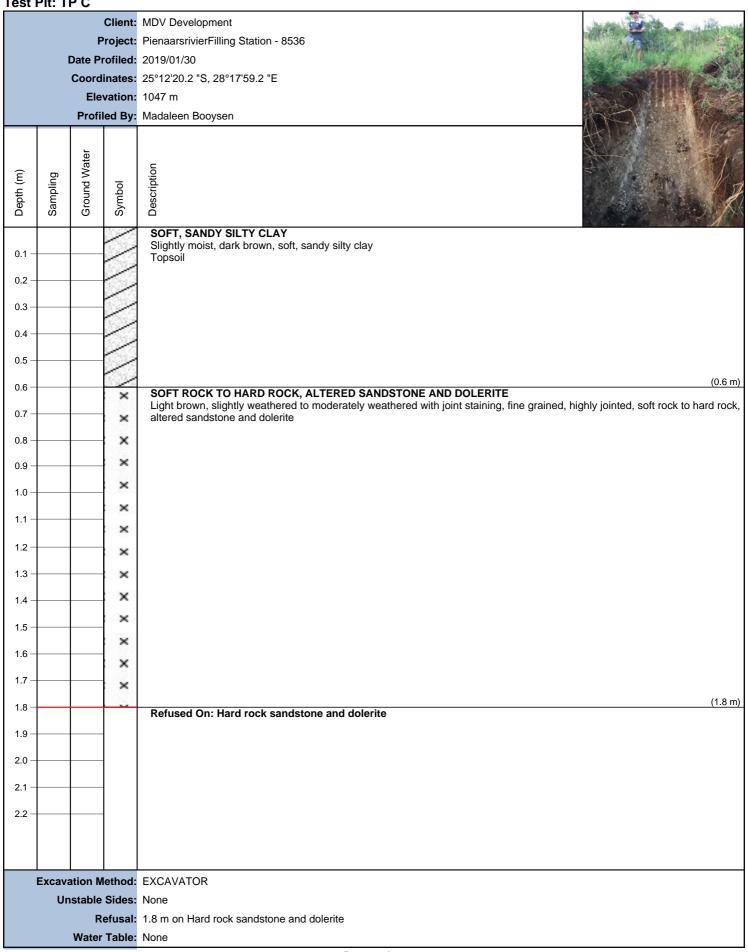
Test F	Pit: T	<u> </u>		
			Client:	MDV Development
Project			roject:	PienaarsrivierFilling Station - 8536
Date Profiled			ofiled:	2019/01/30
		Coord	inates:	25°12'20.3 "S, 28°18'00.6 "E
		Ele	vation:	1044 m
		Profil	led By:	Madaleen Booysen
Depth (m)	Sampling	Ground Water	Symbol	SOFT, SANDY SILTY CLAY
0.1				Slightly moist, dark brown, soft, sandy silty clay Topsoil
				100001
0.2				
0.3				
0.4				
				(0.5.77)
0.5			×	SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE (0.5 m)
0.6			×	Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock, altered sandstone and dolerite
0.7 -			×	
1 1			×	
0.8 —			×	
0.9 —			7 1. A. SON POLICE OF	
1.0 —			×	
1.1 -			×	
1 1			×	
1.2 -	D		×	
1.3 —			×	
1.4 —			×	
1.5 —			×	
1.5			×	
1.6 —			×	
1.7 —			×	
1.8 —			×	
			×	
1.9 –			×	
2.0				Refused On: Hard rock sandstone and dolerite
2.1 —				
2.2				
2.2				
	_			EVOLVATOR
				EXCAVATOR Nace
	Un		Sides:	
				2 m on Hard rock sandstone and dolerite
		vvater	Table:	Page 2 of 16

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Test Pit: TP C



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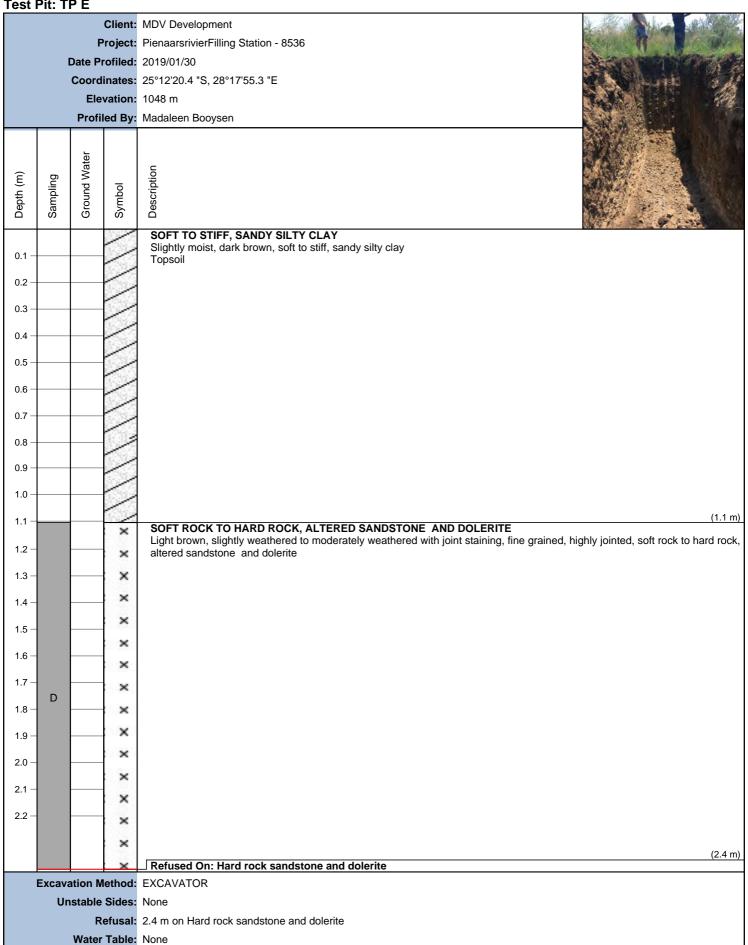
Client: MOV Development Project: Planastrivier Filling Station - 8636 Date Profiled: 2010/30 Coordinates: 2512.20.21 S, 281750.6 TE Elevation: 1038 Profiled By: Macialeen Bionysen Soft: SANDY SILTY CLAY Display moles, dark frown, soft, sandy silty clay Class Coordinates: 2512.20.21 S, 281750.6 TE Elevation: 1038 Soft: SANDY SILTY CLAY Display moles, dark frown, soft, sandy silty clay Class Coordinates: 2512.20.21 S, 281750.6 TE Elevation: 1038 Soft: SANDY SILTY CLAY Display moles, dark frown, soft, sandy silty clay Class Coordinates: 2512.20.21 S, 281750.6 TE Elevation: 1038 Soft: SANDY SILTY CLAY Display moles, dark frown, soft, sandy silty clay Class Coordinates: 2512.20.21 S, 281750.6 TE Elevation: 1038 Soft: Rock To HARD ROCK, ALTERED SANDSTONE AND DOLERITE Ulyth trown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock allowed sandstone and dolerite Excavation Method: EXCAVATOR Unstable Sides No. 1038 Unstable Sides No. 1038 Soft: Rock To Hard rock sandstone and dolerite Excavation Method: EXCAVATOR Unstable Sides No. 1038 Unstable Sides No. 1038	Test	Pit: T	P D		
Date Profiled Scientification: 1038 m Profiled By: Madaleen Booysen Soft SAMDY SILTY CLAY Sliphly most, dark brown, soft, sandy silty diay Topposil Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathlested or moderately weathlested with joint staming, fine grained, highly jointed, soft rock to hard rock altered sameterne and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathlested or moderately weathlested with joint staming, fine grained, highly jointed, soft rock to hard rock altered sameterne and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathlested with joint staming, fine grained, highly jointed, soft rock to hard rock altered sameterne and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light Took Sandstone and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light Took Sandstone and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light Took Sandstone and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light Took Sandstone and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light Took Sandstone and delette Soft Took TO HARD ROCK ALTERED SANDSTONE AND DOLERITE Light Took Sandstone and delette Soft Took Took Took Took Sandstone and delette Soft Took Took Took Took Sandstone and delette Soft Took Sandstone Sandstone and delette Soft Took Sandstone Sandstone and delette Soft Took Sandstone Sandstone Sandstone Sandstone and delette Soft Took Sandstone San				Client:	MDV Development
Coordinates: 25/12/20, 2**0, 28*17:59.6 °E Elevation: Profiled By: Madeleen Booysen Coordinates: 25/12/20, 2**0, 28*17:59.6 °E Coordinates: 25/12/20, 28*17:59.6 °E Coordi			Р	roject:	PienaarsrivierFilling Station - 8536
Elevation: 1038 m Profiled By: Maclaleen Booysen Section Profiled By: Maclaleen Booysen	Date Profiled:			ofiled:	2019/01/30
Profiled By: Maddleon Booysen George Fig. Fi	Coordinates:			inates:	25°12'20.2 "S, 28°17'59.6 "E
SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERTE 1.0	Elevation			vation:	1038 m
SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERTE 1.0			Profil	ed By:	Madaleen Booysen
Slightly moist, dark brown, soft, sandy silty clay Topsoil Soft ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite Refused On: Hard rock sandstone and dolerite Exeavation Method: Unstable Sides: None Water Tables Slightly moist, dark brown, soft, sandy silty clay Topsoil (I.4 m.)	Depth (m)	Sampling	Ground Water	Symbol	
0.8	0.1 —				Slightly moist, dark brown, soft, sandy silty clay
0.6	0.2 -			/	
Soft ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite Refused On: Hard rock sandstone and dolerite Excavation Method: Unstable Sides: Refused: Refused: 1.4 m on Hard rock sandstone and dolerite Refused: 1.4 m on Hard rock sandstone and dolerite Refused: 1.4 m on Hard rock sandstone and dolerite Water Table: None	0.3 —				
Soft ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite Refused On: Hard rock sandstone and dolerite Excavation Method: Unstable Sides: Refused: Refused: 1.4 m on Hard rock sandstone and dolerite Refused: 1.4 m on Hard rock sandstone and dolerite Refused: 1.4 m on Hard rock sandstone and dolerite Water Table: None	04-				
SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite Refused On: Hard rock sandstone and dolerite Excavation Method: 2.0 2.1 2.2 Excavation Method: Carcal Soft Rock To HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite (1.4 m) Refused On: Hard rock sandstone and dolerite Excavation Method: Carcal Soft Rock To HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite (1.4 m) Refused On: Hard rock sandstone and dolerite Excavation Method: Carcal Soft Rock To HARD ROCK, ALTERED SANDSTONE AND STAINING, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite (1.4 m) Refused On: Hard rock sandstone and dolerite Excavation Method: Carcal Soft Rock Soft Rock Sandstone and dolerite Water Table: None					
SOFT ROCK TO HARR ROCK, ALTERED SANDSTONE AND DOLERTE Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite *** *** ** ** ** ** ** ** **	0.5 –				
Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite Light brown, slightly weathered with joint staining, fine grained, highly jointed, soft rock to hard rock altered sandstone and dolerite Refused On: Hard rock sandstone and dolerite Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	0.6 -			×	SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE
1.0	0.7 —				Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock,
1.0	0.8 -			×	
Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	0.9 -			×	
1.1	1.0			×	
Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	1.0 -			×	
Excavation Method: EXCAVATOR Unstable Sides: None Refused On: Hard rock sandstone and dolerite Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	1.1 —			×	
1.3 Refused On: Hard rock sandstone and dolerite 1.5 Refused On: Hard rock sandstone and dolerite 1.7 Refused On: Hard rock sandstone and dolerite 2.0 Land Refused On: Hard rock sandstone and dolerite Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	1.2 -			×	
Refused On: Hard rock sandstone and dolerite 1.5 1.6 1.7 1.8 1.9 2.0 2.1 2.2 Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	1.3 –				
Excavation Method: Unstable Sides: Refused Un: Hard rock sandstone and dolerite Excavation Method: Unstable Sides: Refusal: Water Table: None Refusal: None	1.4 —			×	(1.4 m)
Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None					Refused On: Hard rock sandstone and dolerite
1.7 1.8 1.9 2.0 2.1 2.2 Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	1.5 -				
Excavation Method: Unstable Sides: Refusal: Water Table: None Line Sides: None None None None None None	1.6 -				
Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	1.7 —				
2.0 2.1 2.2 Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	1.8 -				
2.0 2.1 2.2 Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	19-				
2.1 2.2 Excavation Method: EXCAVATOR Unstable Sides: None Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None					
Excavation Method: Unstable Sides: Refusal: Water Table: None EXCAVATOR None 1.4 m on Hard rock sandstone and dolerite None	2.0 –				
Excavation Method: Unstable Sides: Refusal: Water Table: None EXCAVATOR None 1.4 m on Hard rock sandstone and dolerite None	2.1 —				
Unstable Sides: Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None	2.2 -				
Unstable Sides: Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None					
Refusal: 1.4 m on Hard rock sandstone and dolerite Water Table: None		Excava	ation M	ethod:	EXCAVATOR
Water Table: None		Ur	stable	Sides:	None
			R	efusal:	1.4 m on Hard rock sandstone and dolerite
			Water	Table:	None

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Test Pit: TP E



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Test Pit: TP F

Test F	Pit: T	<u> </u>											
			Client:	MDV Development									
		P	roject:	PienaarsrivierFilling Station - 8536									
	I	Date Pr	ofiled:	2019/01/30									
		Coord	inates:	25°12'19.4 "S, 28°17'58.4 "E									
		Ele	vation:	1048 m									
		Profil	ed By:	: Madaleen Booysen									
Depth (m)	Sampling	Ground Water	Symbol	Operation of the control of the cont									
0.1				Slightly moist, dark brown, soft, sandy silty clay Topsoil									
				Topson									
0.2													
0.3													
0.4													
0.5													
0.6													
0.7				(0.7 m)									
			×	SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered to moderately weatheredwith joint staining, fine grained, highly jointed, soft rock to hard rock,									
0.8			×	altered sandstone and dolerite									
0.9			×										
1.0 —			×										
1.1 —			×										
1.1			×										
1.2			×										
1.3 —			×										
1.4 —			×										
			×										
1.5													
1.6			×										
1.7			×										
			×										
1.8 —			×										
1.9			×										
2.0			×	Refused On: Word rock conditions and delegits									
24				Refused On: Hard rock sandstone and dolerite									
2.1 —													
2.2 —													
E				EXCAVATOR									
	Un		Sides:										
				2 m on Hard rock sandstone and dolerite									
		water	Table:	None Page 6 of 16									

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Test Pit: TP G

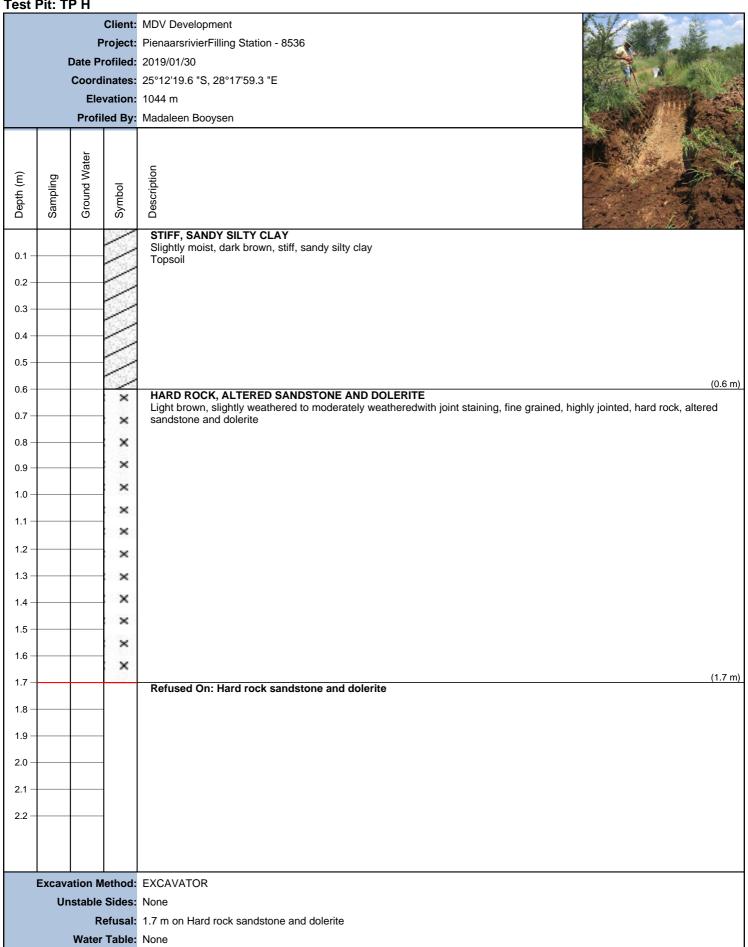
Test F	Pit: T	PG												
			Client:	MDV Development										
		Р	roject:	PienaarsrivierFilling Station - 8536										
	I	Date Pr	ofiled:	2019/01/30										
		Coordi	inates:	25°12'19.4 "S, 28°17'58.7 "E										
		Elev	vation:	1047 m										
		Profil	ed By:	: Madaleen Booysen										
		ter												
<u> </u>	g	Wa		tion										
Depth (m)	Sampling	Ground Water	loqu	Description										
Dep	San	Gro	Symbol	Des										
\vdash				SOFT, SANDY SILTY CLAY										
0.1 -				Slightly moist, dark brown, soft, sandy silty clay										
1 1				Topsoil										
0.2 —														
0.3	D													
1 1														
0.4														
0.5				SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE (0.5 m)										
			×	Light brown, slightly weathered to moderately weatheredwith joint staining, fine grained, highly jointed, soft rock to hard rock,										
0.6 —			×	altered sandstone and dolerite										
0.7 —			×											
0.8			×											
1 1			×											
0.9 —			×											
1.0 —														
1.1 -			×											
'''			×											
1.2 -			×											
1.3 -	D		×											
1 1			×											
1.4 —			×											
1.5 —			×											
1.6														
1.0			×											
1.7 –			×											
1.8			×											
,			×											
1.9 —			×											
2.0 —														
2.1			×	(2.1 m)										
2.1				Refused On: Hard rock sandstone and dolerite										
2.2														
E	Excava	tion M	ethod:	EXCAVATOR										
			Sides:											
		R	efusal:	2.1 m on Hard rock sandstone and dolerite										
			Table:											
				Page 7 of 16										

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Test Pit: TP H

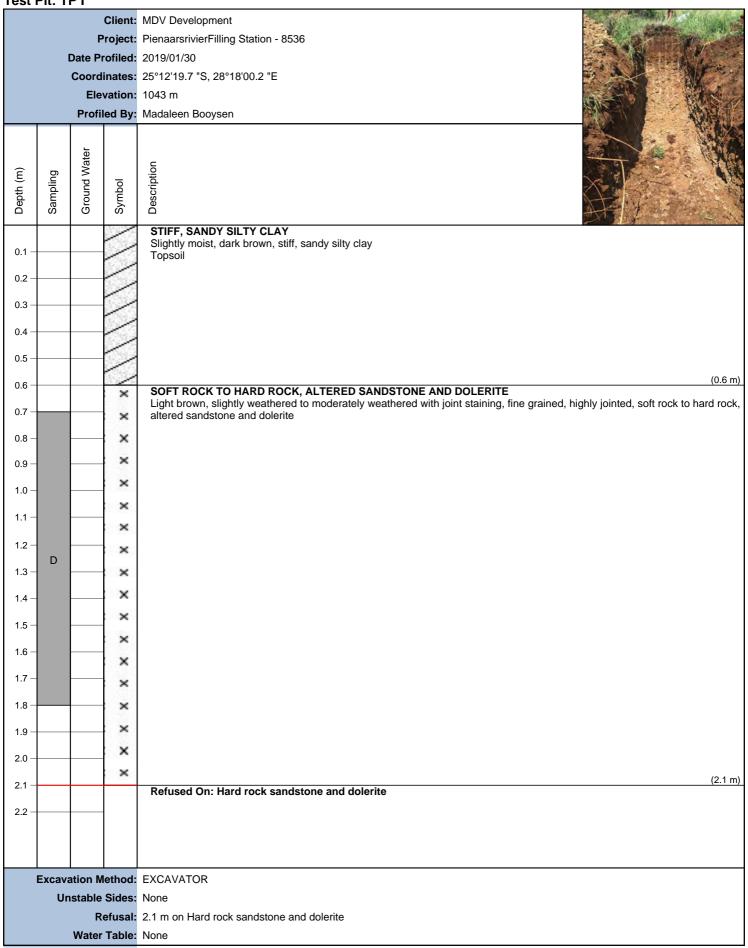


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Test Pit: TP I

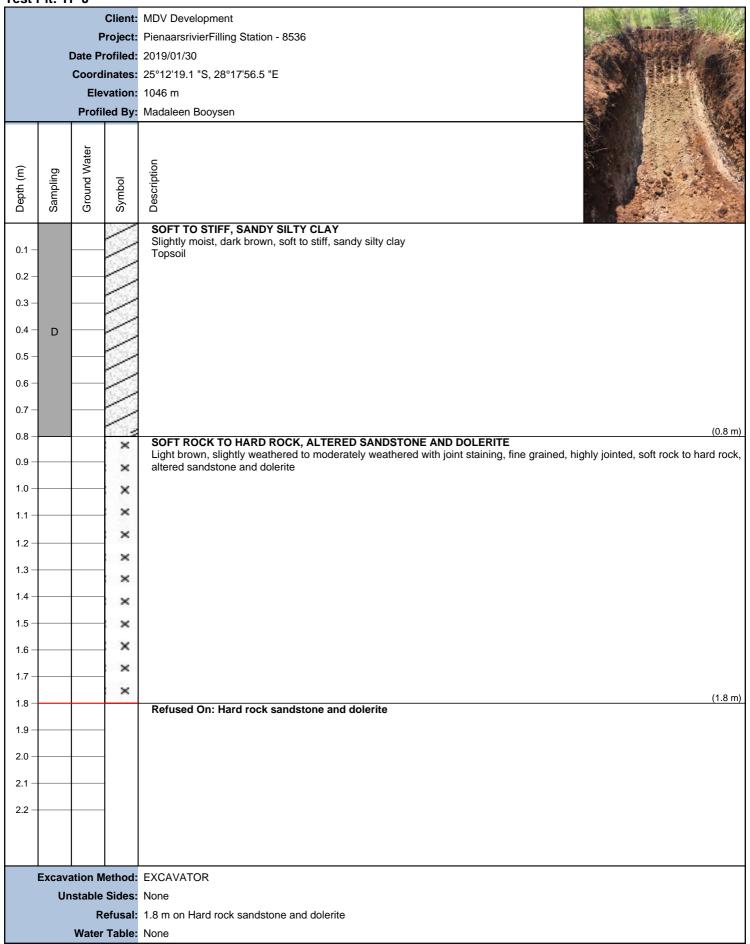


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Test Pit: TP J



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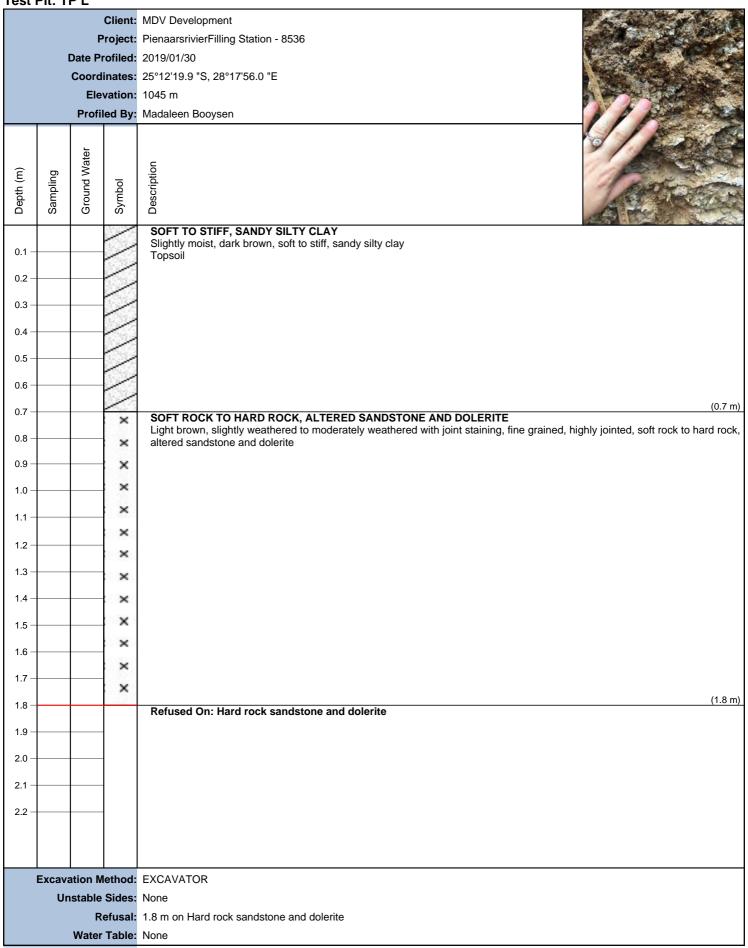
Test I	Pit: T	PΚ		
			Client:	MDV Development
		F	Project:	PienaarsrivierFilling Station - 8536
		Date P	rofiled:	2019/01/30
		Coord	inates:	25°12'19.4 "S, 28°17'56.4 "E
				1046 m
		Profi	led By:	Madaleen Booysen
Oepth (m)	Sampling	Ground Water	Symbol	STIFF, SANDY SILTY CLAY Slightly moist, dark brown, stiff, sandy silty clay
0.1 - 0.2 - 0.3 - 0.4 -				Topsoil
0.4				
0.5 —			×	SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE (0.5 m)
0.6 —			×	Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock, altered sandstone and dolerite
0.7 —			×	
0.8 —			×	
0.9 —			×	
			×	
1.0 —			×	
1.1 —			×	
1.2 —			×	
1.3 —			×	
1.4 —			×	
1.5 —			×	
1.5			×	
1.6 —			×	
1.7 —				Refused On: Hard rock sandstone and dolerite (1.7 m)
1.8 —			-	
1.9 —				
2.0 —				
2.1 —				
2.2 —			-	
	Excava	ation N	lethod:	EXCAVATOR
	Ur	stable	Sides:	None
				1.7 m on Hard rock sandstone and dolerite
		Water	Table:	None

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Test Pit: TP L

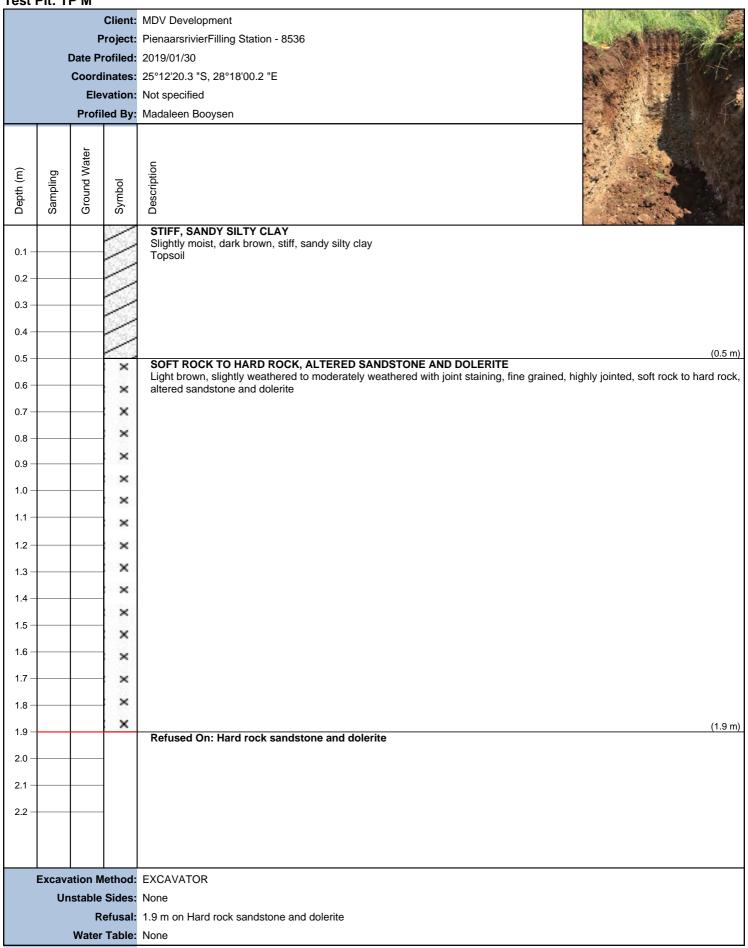


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Test Pit: TP M



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Test Pit: TP N

Test F	Pit: T	<u> </u>												
			Client:	MDV Development										
		P	roject:	PienaarsrivierFilling Station - 8536										
	ı	Date Pi	ofiled:	2019/01/30										
		Coord	inates:	25°12'20.4 "S, 28°17'58.0 "E										
		Ele	vation:	1046 m										
		Profil	led By:	Madaleen Booysen										
Depth (m)	Sampling	Ground Water	Symbol	Description										
0.1 —				SOFT, SANDY SILTY CLAY Slightly moist, dark brown, soft, sandy silty clay										
0.1				Topsoil										
0.2 —														
0.3 —														
0.4 —														
0.5 —														
0.6				(0.6 m)										
0.6 —			×	SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock,										
0.7 —			×	altered sandstone and dolerite										
0.8 —			×											
0.9 —			×											
0.9			×											
1.0 —														
1.1 —			×											
			×											
1.2 —			×											
1.3 —			×											
1.4 —			×											
1.4			×											
1.5 —														
1.6 —			×											
4.7			×											
1.7 —			×											
1.8 —			×											
1.9 —			×											
			×	(2 m)										
2.0 —				Refused On: Hard rock sandstone and dolerite										
2.1 —														
2.2 —														
2.2														
	Evecus	tion !	othe d	EXCAVATOR										
			Sides:											
	UII			2 m on Hard rock sandstone and dolerite										
			Table:											
		TTALEI	Table.	Page 14 of 16										

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Test Pit: TP O

Test P	it: TF	0													
				MDV Development											
			_	PienaarsrivierFilling Station - 8536											
				2019/01/30											
				25°12'19.0 "S, 28°17'59.2 "E											
				1045 m											
		Profile	ed By:	Madaleen Booysen											
Depth (m)	Sampling	Ground Water	Symbol	Description											
0.1				STIFF, SANDY SILTY CLAY Slightly moist, dark brown, stiff, sandy silty clay											
0.1				Topsoil											
0.2															
0.3 —															
0.4															
0.5															
0.5															
0.6															
0.7															
0.8			×	(0.8 m) SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE											
0.9			×	Light brown, slightly weathered to moderately weathered with joint staining, fine grained, highly jointed, soft rock to hard rock, altered sandstone and dolerite											
1.0			×	ancred sandstone and dolenic											
1.1			×												
			×												
1.2			×												
1.3 —			×												
1.4 —			×												
1.5 —			×												
1.6			×												
1.6			×												
1.7			×												
1.8			×												
1.9			×												
2.0			×												
0.4			×	(2.1 m)											
2.1				Refused On: Hard rock sandstone and dolerite											
2.2															
E	xcava	tion M	ethod:	EXCAVATOR											
	Un	stable	Sides:	None											
		Re	efusal:	2.1 m on Hard rock sandstone and dolerite											
		Water	Table:	None											

Tel: +27 (0) 12 348 6668 Fax: +27 (0) 12 348 6669 6 Daventry Street Lynnwood Manor 0081



www.arq.co.za arq@arq.co.za P.O.Box 76379 Lynnwood Ridge 0040

Test Pit: TP P

Client: MDV Development Project: PienaarsrivierFilling Station - 8536 Date Profiled: 2019/01/30 Coordinates: 25°12'18.9 "S, 28°17'54.3 "E Elevation: 1048 m Profiled By: Madaleen Booysen **Ground Water** Description Depth (m) Sampling Symbol VERY SOFT TO SOFT, SANDY SILTY CLAY Slightly moist, dark brown, very soft to soft, sandy silty clay 0.1 Topsoil 0.2 0.3 0.4 (0.45 m) SOFT ROCK TO HARD ROCK, ALTERED SANDSTONE AND DOLERITE × 0.5 Light brown, slightly weathered to moderately weathered, fine grained, highly jointed, soft rock to hard rock, altered sandstone × and dolerite 0.6 × × 0.8 × 0.9 × 1.0 × 1.1 × 1.2 × 1.3 × 1.4 × 1.5 × 1.6 × 1.7 × 1.8 × 1.9 \times × 2.0 × 2.1 × 2.2 × × (2.4 m) Refused On: Hard rock sandstone and dolerite **Excavation Method: EXCAVATOR** Unstable Sides: None Refusal: 2.4 m on Hard rock sandstone and dolerite Water Table: None

APPENDIX B PERCUSSION BOREHOLE PROFILE

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www.arq.co.za arq@arq.co.za P.O.Box 76379 Lynnwood Ridge 0040

Sheet: 1 of 1

Percussion Log: BH01

Client: MDV Development

Project: PienaarsrivierFilling Station - 8536

Date Profiled: 2019/02/13

Coordinates: 25°12'20.5 "S, 28°17'59.3 "E

Elevation: Not specified

Profiled By: Madaleen Booysen

Date Drilled: 2019/02/13

m/s;u	1 :	minu	utes	s/m)		Cavity	1 1 1 1 0.1	Soft	0.9 1 1 0.5		N	None	Slightly	Medium	Total	Water Found	Wet	Moist	S Dry Su	Water Applied	2 Depth (m)	boo5 > >	Medium	Jood Jood	None	♦ ♦ ♦ Symbol	Description Notes: Material was not analysed as per arangement, as watertable depth was the solitary concern.
31 54 14 14 14 14 14 15 14 15 15	1 :	2	3	4	5	Cavity	1 1 1 1 1	Soft	0.9	0.5	R R R R R R	None	Slightly	Medium	Total		Wet	-	✓ ✓	Water App	1 2	√ √	Medium	Poor	None	Symbol	Notes: Material was not analysed as per arangement, as watertable depth was the solitary concern.
31 54 14 14 14 14 14 15 14 15 15							1 1 1 1		0.9	0.5	R R R R R R					→		✓ 	✓		1 2	✓				Š.	Notes: Material was not analysed as per arangement, as watertable depth was the solitary concern.
14 16 19 14 22 54 21							1 1 1		1	0.5	R R R R R					¥н			✓							[+×̈+]	watertable depth was the solitary concern.
4 22 54							1		1	0.5	R R R R					> 11					3	✓					
9 4 2 4 1							1		1	0.5	R R R R					Y 1-			./		_	<u> </u>				* <u>`</u> *	
4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4							_		1	0.5	R R R					¥-			v		4	✓					
2 4 1							0.1		1	0.5	R R I								✓		5	✓				$T_{\wedge}T_{\perp}$	
4									1	_	R								✓		6	✓				$T_{\wedge}T_{\perp}$	
1									_	_	ı								✓		7	✓				~~	
_									0.5	_	_								✓		8	✓					
										1	IR	-							✓		9	✓				$\left[\begin{array}{c} \times \\ \times \end{array}\right]$	
									1		+``							✓			10	✓				**	(10
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Notes: Standing watertable was measured 48 hour after drilling at 5.5m. The area experienced heavy rain during the 3 days prior to measurement of water table.

APPENDIX C LABORATORY RESULTS





SGS MATROLAB (PTY) LTD

- CIVIL ENGINEERING SERVICES -Reg.No.: 2003/021980/07 - VAT. Reg.No.: 4040210587

a SANAS Accredited Testing Laboratory, No. T0025

: A9/272

: 500-2000

: TPB

: 53

: 26

: 8.00

: 2.13

: 8

256 Brander Street, Jan Niemand Park, Pretoria. P.O Box 912387, Silverton, 0127

Tel. : (012) 800 1299 Fax : (012) 800 3043

Fax : (012) 800 3043 Email : bennie.vanniekerk@sgs.com

TEST RESULTS

ARQ CONSULTING ENGINEERS

P.O BOX 76379 LYNNWOOD RIDGE

0040

Sample No. Hole No.

Liquid Limit (%)

Plasticity Index

PI of Whole Sample

Grading Modulus

Depth

Activity

Attention: Madaleen Booysen

Linear Shrinkage (%) : 11.5

Unified Soil Classificati: GC

Heave Classification : LOW

Percentage (<0.002) : 1.0

Moisture Content (%): 10.4

P.R.A. Classification : A-2-7(1)

Project : Pienaarsrivier Filling Station

Your Ref

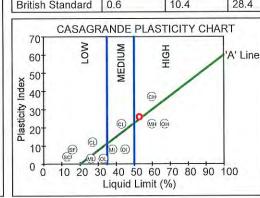
: 8536

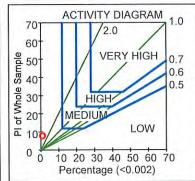
Our Ref Date Reported : PL/26628 : 18.02.2019

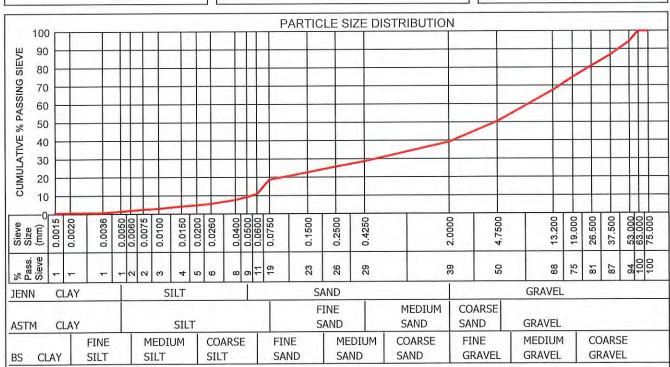
FOUNDATION INDICATOR (ASTM: D422)

Material Description : Light brown SILTY SAND

Sand (%) Gravel (%) Classification Clay (%) Silt (%) 60.6 SILTY SAND 1.4 7.9 30.1 Jennings SILTY SAND 31.6 49.6 Astm 1.4 17.4 SILTY SAND 10.4 28.4 60.6 British Standard 0.6







Remarks: Sampled by client.

FORM: A6

4.4.0(SGS)(2016.08.31)

/S Daynoth





SGS MATROLAB (PTY) LTD
- CIVIL ENGINEERING SERVICES Reg.No.: 2003/021980/07 - VAT. Reg.No.: 4040210587

a SANAS Accredited Testing Laboratory, No. T0025

: TPE

: 45

: 20

: 5

: 5.00

: 2.17

: 1100-2400

256 Brander Street, Jan Niemand Park, Pretoria.

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Email : bennie.vanniekerk@sgs.com

TEST RESULTS

ARQ CONSULTING ENGINEERS

P.O BOX 76379 LYNNWOOD RIDGE

0040

Sample No. Hole No.

Liquid Limit (%)

Plasticity Index

Depth

Activity

Attention: Madaleen Booysen

Linear Shrinkage (%): 9.0

Unified Soil Classificati: SC

Heave Classification : LOW

Percentage (<0.002) : 1.0

Moisture Content (%) : 6.5

P.R.A. Classification : A-2-7(0)

PI of Whole Sample

Grading Modulus

Project: Pienaarsrivier Filling Station

Your Ref

: 8536 : PL/26628

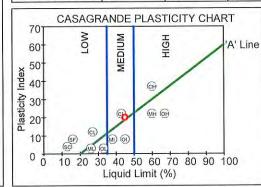
Date Reported : 18.02.2019

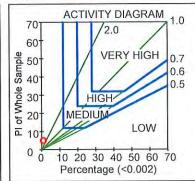
FOUNDATION INDICATOR (ASTM: D422)

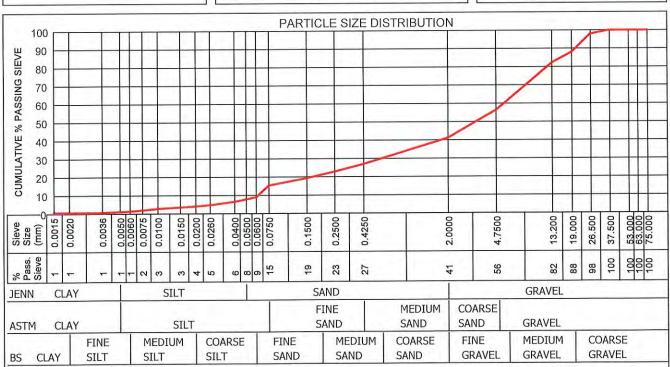
: A9/273 Material Description : Light yellow brown SILTY SAND

Our Ref

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	1.0	6.7	33.5	58.8	SAND
Astm	1.0	14.3	41.0	43.7	SILTY SAND
British Standard	0.5	8.5	32.1	58.8	SILTY SAND







Remarks: Sampled by client.

FORM: A6

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TEST RESULTS

ARQ CONSULTING ENGINEERS

P.O BOX 76379 LYNNWOOD RIDGE

0040

Attention: Madaleen Booysen

Project: Pienaarsrivier Filling Station

Your Ref : 8536

Our Ref : PL/26628

Date Reported : 18.02.2019

FOUNDATION INDICATOR (ASTM: D422)

 Sample No.
 : A9/274

 Hole No.
 : TPG

 Depth
 : 0-500

 Liquid Limit (%)
 : 44

 Plasticity Index
 : 21

Linear Shrinkage (%) : 10.5 PI of Whole Sample : 10

P.R.A. Classification : A-2-7(1)

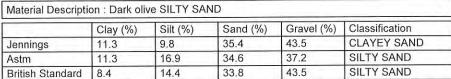
Unified Soil Classificati: SC

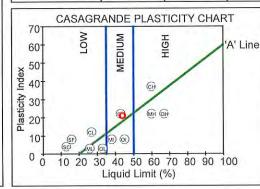
Activity : 1.25

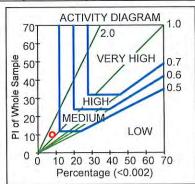
Heave Classification : LOW
Grading Modulus : 1.66

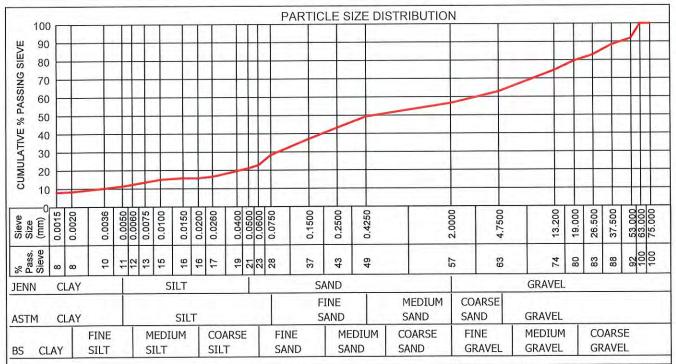
Percentage (<0.002) : 8.0

Moisture Content (%) : 12.0









Remarks: Sampled by client.

FORM: A6

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: A9/275

: TPG : 500-2100

: 50

: 22

: 4.00

: 2.42

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Fax (012) 800 3043 Email : bennie.vanniekerk@sgs.com

TEST RESULTS

ARQ CONSULTING ENGINEERS

P.O BOX 76379 LYNNWOOD RIDGE

0040

Sample No.

Liquid Limit (%)

Plasticity Index

PI of Whole Sample

Grading Modulus

Hole No.

Depth

Activity

Attention: Madaleen Booysen

Linear Shrinkage (%) : 11.0

P.R.A. Classification : A-2-7(0)

Unified Soil Classificati: GW-GM

Heave Classification : LOW

Percentage (<0.002) : 1.0

Moisture Content (%) : 6.2

Project: Pienaarsrivier Filling Station

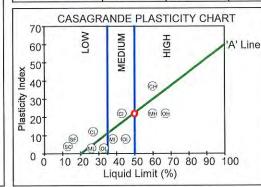
Your Ref : 8536

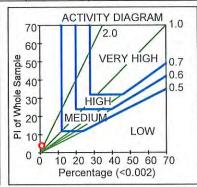
: PL/26628 Our Ref : 18.02.2019 Date Reported

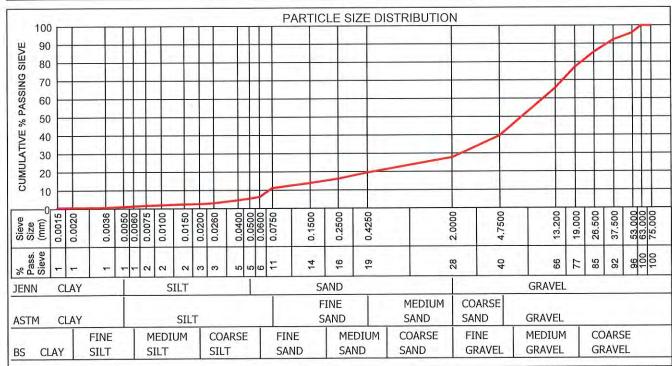
FOUNDATION INDICATOR (ASTM: D422)

Material Description : Light yellow brown SILTY SAND

	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification
Jennings	1.0	4.4	22.4	72.2	SAND
Astm	1.0	10.2	28.4	60.5	SILTY SAND
British Standard	0.6	5.8	21.4	72.2	SILTY SAND







Sampled by client. Remarks:

FORM: A6

4.4.0(SGS)(2016.08.31)





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: A9/276

: TPJ

: 47

: 26

: 15

: 15.00

: 1.42

: 0-800

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(012) 800 3043 Fax

: bennie.vanniekerk@sgs.com

TEST RESULTS

ARQ CONSULTING ENGINEERS

P.O BOX 76379 LYNNWOOD RIDGE

0040

Sample No.

Liquid Limit (%)

Plasticity Index

PI of Whole Sample

Grading Modulus

Hole No.

Depth

Activity

Attention: Madaleen Booysen

Linear Shrinkage (%): 13.5

Unified Soil Classificati: SC

Heave Classification : LOW

Percentage (<0.002) : 1.0

Moisture Content (%): 10.2

P.R.A. Classification : A-7-6(4)

Project : Pienaarsrivier Filling Station

Your Ref

: 8536

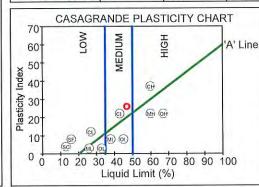
Our Ref Date Reported : PL/26628

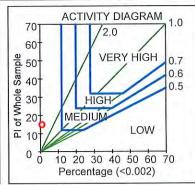
: 18.02.2019

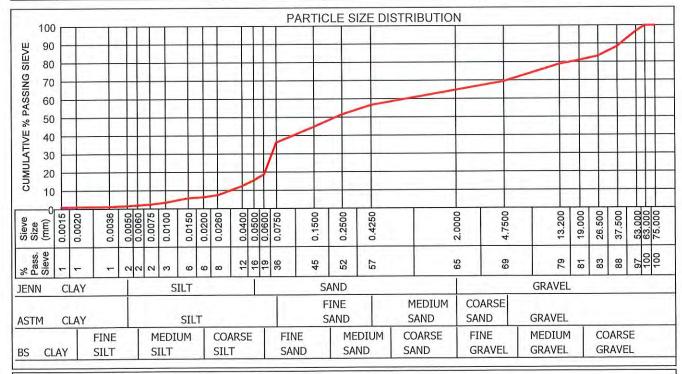
FOUNDATION INDICATOR (ASTM: D422)

Material Description : Dark brown SILTY SAND

Waterial Description . Dark brown GLTT GARD									
	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification	_1!			
Jennings	1.6	14.0	49.2	35.2	SILTY SAND				
Astm	1.6	34.6	33.2	30.6	SILTY SAND				
British Standard	1.1	17.8	45.9	35.2	SILTY SAND				







Sampled by client. Remarks:

FORM: A6

4.4.0(SGS)(2016.08.31)





- CIVIL ENGINEERING SERVICES -Reg.No.: 2003/021980/07 - VAT. Reg.No.: 4040210587

a SANAS Accredited Testing Laboratory, No. T0025

: A9/293

: TPI

: 55

: 24

: 5

: 5.00

: 2.45

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(012) 800 3043 Email : bennie.vanniekerk@sgs.com

TEST RESULTS

ARQ CONSULTING ENGINEERS

P.O BOX 76379 LYNNWOOD RIDGE

0040

Sample No.

Liquid Limit (%)

Plasticity Index

PI of Whole Sample

Grading Modulus

Hole No.

Depth

Activity

Attention: Madaleen Booysen

Linear Shrinkage (%): 11.0

Unified Soil Classificati: GM

Heave Classification : LOW

Percentage (<0.002) : 1.0

Moisture Content (%) : 12.5

Project: Pienaarsrivier Filling Station

Your Ref : 8536

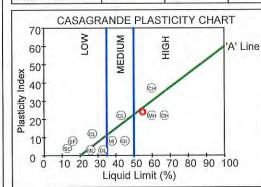
: PL/26628 Our Ref Date Reported : 18.02.2019

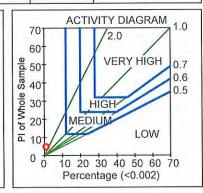
FOUNDATION INDICATOR (ASTM: D422)

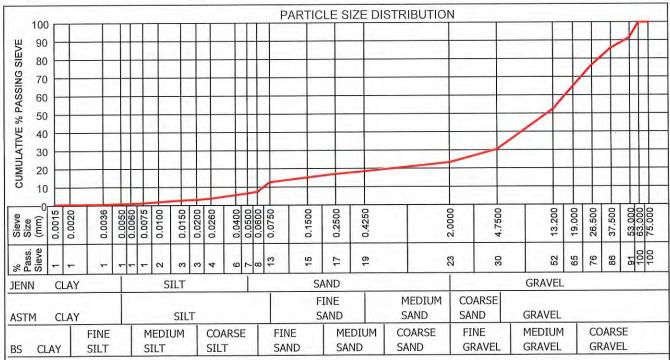
Material Description: Yellowish brown SILTY SAND

Material Beechpter : Tellemen Brenn CIET : C. WIE									
The same and the	Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Classification				
Jennings	0.8	5.8	16.7	76.6	SILTY SAND	_1			
Astm	0.8	11.9	17.7	69.6	SILTY SAND				
British Standard	0.6	7.0	15.8	76.6	SILTY SAND				









Sampled by client. Remarks:

FORM: A6

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256 Brander street, Jan Niemand Park,

Pienaarsrivier Filling Atation

Pretoria.

P.O. BOX 912387 SILVERTON 0127

Tel. : 012-800 1299 Fax. : 012-800 3034 Email : lizette.breiting@sgs.com

TEST RESULTS

CLIENT:

ARQ CONSULTING ENGINEERS

ADDRESS:

P.O BOX 76379 LYNNWOOD RIDGE

Attention:

Your Ref: 8536 Our Ref: PL/26628 18.02.2019 Date Reported:

Project:

0040 Madaleen Booysen

		PROPE	RTIES OF AGO	GREGATE AND SAN	ID		
			Lab no	A9/272	A9/273	A9/274	A9/275
Test description	Sample Description Source Additional Info Client Ref No	Test method	UOM	Light brown TPB (500-2000)	Light yellow brown TPE (1100-2400)	Dark oilve	Light yellow brown TPG (500-2100)
рН		SANS 5854	рН	7.9	7.9	7.5	8.0
Conductivity		SANS 6240	S/m	0.0862	0.0611	0.0939	0.0523

Remarks: Sampled by client.

Test covered, not part of scope of accreditation

for SGS Matrolab (Pty) Ltd. Technical Signatory: B. van Niekerk/L. Breiting

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Pretoria. P.O. BOX 912387 SILVERTON 0127

Tel. : 012-800 1299 Fax. : 012-800 3034 Email : lizette.breiting@sgs.com

TEST RESULTS

CLIENT:

ARQ CONSULTING ENGINEERS

ADDRESS:

Attention:

P.O BOX 76379 LYNNWOOD RIDGE

0040

Madaleen Booysen

Pienaarsrivier Filling Atation Project:

8536

Your Ref: Our Ref: PL/26628a

18.02.2019 Date Reported:

		PROPE	RTIES OF AGG	REGATE AND SAI	ND	
			Lab no	A9/276	A7/293	
Test description	Sample Description Source Additional Info Client Ref No	Test method	UOM	Dark brown TPJ (0-800)	Yellowish brown TPI (700-1800)	
Н		SANS 5854	рН	7.8	8.0	
Conductivity		SANS 6240	S/m	0.0863	0.0805	

Remarks: Sampled by client.

Test covered, not part of scope of accreditation

for SGS Matrolab (Pty) Ltd. Technical Signatory: B. van Niekerk/L. Breiting

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Tel: +27 (0)12 800 1299 Fax: +27 (0)12 800 3601

E-mail: info@matrolab.co.za Website: www.matrolab.co.za Reg No.: 2003/029180/07 – VAT Reg No.: 4040210587

Order No.



a SANAS Accredited Testing Laboratory, No. T0025

ARQ CONSULTING ENGINEERS (PTY) LTD Client

PO BOX 76379 Address

LYNNWOOD RIDGE

0040

Attention

Madaleen Booysen

Facsimile

Project

E-mail

Pienaarsrivier Filling Station

Project No. : 2019-S-177

Date Received

Date Reported

Client Reference :

01/02/2019

PL-26628

Date Tested 31/01/2019 - 18/02/2019

18/02/2019

Report Status

FINAL

1 of 19 Page

Herewith please find the test report(s) pertaining to the above project. All tests were conducted in accordance with prescribed test method(s). Information herein consists of the following:

Test(s) conducted / Item(s) measured	Qty.	Test Method(s)	Authorized By**	Page(s)
Moisture Density Relationship	6.000	SANS 3001: GR30		2-11
Atterberg Limits < 0.425mm	6.000	SANS GR10,GR11,GR12		2-11
Sieve Analysis 0.075mm	6.000	SANS 3001: GR1, GR2		2-11
California Bearing Ratio (CBR)	6.000	SANS 3001: GR40		2-11
Foundation Indicators	6.000	ASTM: D422		12-17
PH & Conductivity	6.000	SANS 5854,6240		18-19
	11 1			

SGS MATROLAB

a SANASAccredited Testing Laboratory, No. T0025

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Results only have bearing on the samples tested.

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**All results are authorized electronically by approved managers and/or technical signatories.

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Tel: +27 (0)12 800 1299 Fax: +27 (0)12 800 3601
E-mail: info@matrolab.co.za Website: www.matrolab.co.za
Reg No.: 2003/029180/07 – VAT Reg No.: 4040210587



31/01/2019 Date Received ARQ CONSULTING ENGINEERS (PTY) LTD Client 18/02/2019 Date Reported Pienaarsrivier Filling Station Project Page No.

Project No : 2019-	-S-177						Page N				of	
	N	/IATERIA	ALS	TES	STR	EPO	ORT					
Laboratory Number Field Number Client Reference Depth (m)		A9/272 8536 500-2000										
Position		TPB										
Coordinates	X											
Description		Light brow	n									
Additional information	6	Sampled by c	lient.									
Calcrete/Crushed Stabilizing Agent		Natural										
	Sieve Analys	is (Wet prepar	ation)					SANS	S 3001:	GR1, (GR2	
	100 mm	100	-									
	75 mm	100										- [
D	63 mm	100										- 1
Percentage Passing	50 mm	94										
as	37.5 mm	87										
ω Ω	28 mm	81										
a D	20 mm	75										
ţ	14 mm	68										
Ď.	5 mm	51										
<u>a</u>	2 mm	51										
	0.425 mm	29										
La Carrier	0.075 mm	19										
Grading Modulus	40076-040	2.01	- 2									
0			Soil Mo	ortar A	nalysis							
Coarse Sand	2.0-0.425	43										
Coarse Fine Sand	0.425-0.250	6										
Medium Fine Sand	0.250-0.150	6										
Fine Fine Sand	0.150-0.075	8										
Silt and Clay	< 0.075	37										
Oilt and Olay		berg Limits	-					SANS	GR10	,GR11,	GR12	
Liquid Limit	%	53		V -			-					
Plasticity Index	%	26										
Linear Shrinkage	%	11.5										
Maximu	m Dry Density		oisture	Conte	ent			SA	ANS 30	01: GR	30	
Max. Dry Density	kg/m³	1991								1000		
Optimum Moisture	%	13.5										
CBR SANS 3001:					ITS							
Test Type		CBR UCS (%) (kPa)	ITS (kPa)	CBR (%)	UCS (kPa)	ITS (kPa)	CBR (%)	UCS (kPa)	ITS (kPa)	CBR (%)	UCS (kPa)	ITS (kPa)
nterpolated Data	100% O 10 98% H 10 97% V 10 95% V 10 93% P 10 90% W 10 O effort 11 SHTO effort	11.3 10.4 9.9 9.1 8.4 7.4					, ,					
En es		1 427/41		ssificat	ions					1		
HRB		A-2-7(1)										
COLTO TRH14		G9										
LIMILAT												



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esting Laboratory, No. 70025 Reg No.: 2003/0 ARQ CONSULTING ENGINEERS (PTY) LTD

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Project Pienaarsrivier Filling Station Date Reported

18/02/2019

2019-S-177 Project No. :

Page No.

4 of 4

Laboratory No.	A9/272 🔷	W.
Field Number		
Client Reference	8536	
Depth (m)	500-2000	
Position	TPB	
Coordinates X Y		
Description	Light brown	
Additional information	Sampled by client.	
Calcrete/Crushed		
Stabilizing Agent	Natural	

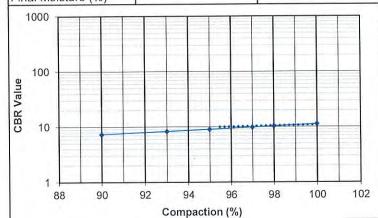
Sieve A	nalysis (Wet prepa	ration)	SANS 3001: GR1, GR2
	100 mm	100	
	75 mm	100	
	63 mm	100	
пg	50 mm	94	
Passing	37.5 mm	87	
	28 mm	81	
Percentage	20 mm	75	
nta	14 mm	68	
Se	5 mm	51	
Je.	2 mm	51	
	0.425 mm	29	
	0.250 mm	26	
	0.150 mm	23	
	0.075 mm	19	
Grading M	lodulus	2.0	

Soli Wortar Analysis						
Coarse Sand	43					
Coarse Fine Sand	6					
Medium Fine Sand	6					
Fine Fine Sand	8					
Silt and Clay	37					

Atterberg Limits	SANS GR10,GR11,GR12	
Liquid Limit (%)	53	
Plasticity Index (%)	26	
Linear Shrinkage (%)	11.5	

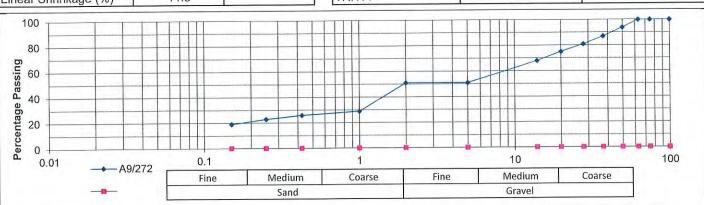
Laboratory No. A9/272		A9/272	
Maximum Dr	y Density & Optimum	SANS 3001: GR30	
MDD	kg/m ³	1991	
ОМС	%	13.5	
California Bearing Ratio			SANS 3001: GR40

		Comp	action	Data		
Moisture	%		14.6			
Dry Density	kg/m ³	1972	1879	1780		
Compaction	%	100.0	95.3	90.3		
		Pene	tration I	Data		
La Trans	2.50 mm	11	10	7		
CBR at	5.00 mm	12	10	9		
	7.50 mm	12	10	9		
Swell	%	0.7	0.9	1		
Final Moistur	e (%)					
1000					-1-1	



		Inter	polated CBR Data	
@	100%	0	11	
@	98%	Ī	10	
~ @	97%	ASI	10	
8 @	95%	∢	9	
0 @	93%	Mod	8	
@	90%	Σ	7	
@	SANS3001 Mid	dpoint	10	
			Classifications	

Classifications	
A-2-7(1)	
G9	-
	A-2-7(1)





HRB COLTO

TRH14

Project

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Page No. of Project No 2019-S-177 MATERIALS TEST REPORT A9/273 Laboratory Number Field Number 8536 Client Reference Depth (m) 1100-2400 TPE Position X Coordinates Light yellow brown Description Additional information Sampled by client. Calcrete/Crushed Natural Stabilizing Agent SANS 3001: GR1, GR2 Sieve Analysis (Wet preparation) 100 mm 100 75 mm 100 100 63 mm Percentage Passing 50 mm 100 100 37.5 mm 98 28 mm 20 mm 89 14 mm 83 57 5 mm 2 mm 57 0.425 mm 28 16 0.075 mm 1.99 Grading Modulus Soil Mortar Analysis 51 2.0-0.425 Coarse Sand 8 Coarse Fine Sand 0.425-0.250 Medium Fine Sand 0.250-0.150 6 Fine Fine Sand 0.150-0.075 7 < 0.075 28 Silt and Clay SANS GR10, GR11, GR12 Atterberg Limits Liquid Limit 45 % 20 Plasticity Index % Linear Shrinkage % 9 SANS 3001: GR30 Maximum Dry Density & Optimum Moisture Content 2089 Max. Dry Density kg/m³ 10.8 Optimum Moisture UCS ITS SANS 3001: GR40 CBR UCS ITS UCS ITS CBR UCS ITS CBR CBR UCS ITS CBR Test Type (kPa) (kPa) (kPa) (kPa) (%) (kPa) (kPa) (%) (kPa) (kPa) (%) (%) @100% 29.6 **AASHTO** nterpolated 23.4 @ 98% 20.8 @ 97% 16.5 @ 95% Mod. 13 @ 93% 9.2 @ 90% Value @ Mod. AASHTO effort Swell (%) @ Mod. AASHTO effort 0.1 Classifications

A-2-7(0)



Project

Project No.

Pienaarsrivier Filling Station

2019-S-177

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Page No.

Laboratory No.	A9/273 🔷	
Field Number		
Client Reference	8536	
Depth (m)	1100-2400	
Position	TPE	
Coordinates X Y		
Description	Light yellow brown	
Additional information	Sampled by client.	
Calcrete/Crushed		
Stabilizing Agent	Natural	

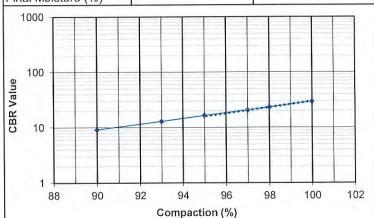
Sieve A	nalysis (Wet prepa	SANS 3001: GR1, GR2	
	100 mm	100	
	75 mm	100	
	63 mm	100	
рп	50 mm	100	
Passing	37.5 mm	100	
Ра	28 mm	98	
ge	20 mm	89	E1 (1)
ta	14 mm	83	
Percentage	5 mm	57	
Jec	2 mm	57	
	0.425 mm	28	
	0.250 mm	24	
	0.150 mm	20	
	0.075 mm	16	
Grading M	1odulus	2.0	

Soil Mortar Analysis				
Coarse Sand	51			
Coarse Fine Sand	8			
Medium Fine Sand	6			
Fine Fine Sand	7			
Silt and Clay	28			

Atterberg Limits	SANS GR10	,GR11,GR12
Liquid Limit (%)	45	
Plasticity Index (%)	20	
Linear Shrinkage (%)	9.0	

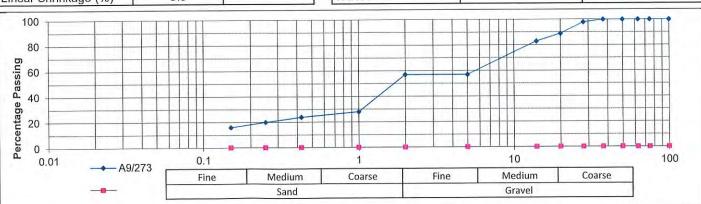
Laboratory No. A9/273		A9/273	
Maximum Dry	Density & Optimun	SANS 3001: GR30	
MDD	kg/m ³	2089	
ОМС	%	10.8	
(California Bearing	Ratio	SANS 3001: GR40

		Comp	action	Data	
Moisture	%		10.8		
Dry Density	kg/m ³	2090	1985	1889	
Compaction	%	100.0	95.0	90.4	
		Pene	tration I	Data	
	2.50 mm	30	16	10	
CBR at	5.00 mm	27	19	16	
	7.50 mm	26	22	15	
Swell	%	0.1	0.3	1	
Final Moistur	e (%)				



			Inte	erpolated CBR Data	
	@	100%	0	30	
	@	98%	도	23	
	@	97%	AS	21	
CBR	@	95%	₹.	17	
0	@	93%	Mod	13	
	@	90%	Σ	9	
	@	SANS3001 M	lidpoint	22	

Classifications					
HRB (AASHTO)	A-2-7(0)				
COLTO					
TRH14	G9				





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Page No. of Project No 2019-S-177

Project No : 2019-	-S-177		erest seems. N	A I 6				Page N				of	
		MAT		ALS		STR	REP(ORI					
Laboratory Number Field Number Client Reference Depth (m)		A9/274 8536 0-500				A9/275 8536 00-2100							
Position			TPG			TPG				1			
Coordinates	X												
Description		Da	ark olive	e	Light	yellow b	rown						
Additional information		Sampl	ed by c	lient.	Samp	led by c	lient.						
Calcrete/Crushed Stabilizing Agent			Vatural		= 1	Natural							
	Sieve Analys	is (Wet		ation)					SAN	S 3001:	GR1, (GR2	
	100 mm		100			100							
	75 mm		100			100							
ם	63 mm		100			100							
Percentage Passing	50 mm		92	1		96				1			
ag	37.5 mm		89			92							
Φ	28 mm		84			85				\			
ag	20 mm		81			77							
eni	14 mm		76			66							
Ō	5 mm		64		40								
ď	2 mm		64			40							
	0.425 mm		51			20							
	0.075 mm		29			12							
Grading Modulus	33300		1.56	- L		2.28							
Ordang Wodalas				Soil M	ortar A	nalysis							
Coarse Sand	2.0-0.425		20			50							
Coarse Fine Sand	0.425-0.250		9		8								
Medium Fine Sand	0.250-0.150		10		6								
Fine Fine Sand	0.150-0.075		14		7								
Settle of the Control of the Settle of the Control	< 0.075		46		29								
Silt and Clay		hara Li			25				SANS	GR10	,GR11,	GR12	
Liquid Limit	%	rberg Limits 45			50				0,1110		, = ,		
Liquid Limit	%		22	, III	22								
Plasticity Index	%		10.5		11								
Linear Shrinkage	n Dry Density	& Onfir		oisture					SA	NS 30	01: GR	30	
	kg/m ³	o Optil	1806	Jistuit	Conte	2075			- Or			- F	
Max. Dry Density	ку/III %		15.3			11.4							
Optimum Moisture CBR SANS 3001:		S	10.0			ITS							
Test Type	CITTO DE	CBR	UCS	ITS	CBR	UCS	ITS	CBR	UCS	ITS (LDa)	CBR	UCS	ITS (kDa)
nterpolated Data		(%) 6.9 6.5 6.4 6 5.7 5.2	(kPa)	(kPa)	(%) 15 11.8 10.5 8.2 6.5 4.5	(kPa)	(kPa)	(%)	(kPa)	(kPa)	(%)	(kPa)	(kPa)
				Cla	ssificat								
HRB			A-2-7(2)			A-2-7(0)							
COLTO TRH14			G10			G10							



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2019-S-177 Project No. :

Page No. of

CALIFORNIA BEARING RATIO	(CBR)	& ROAD	INDICATOR	REPORT
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Laboratory No.	A9/274 🔷	A9/275
Field Number		
Client Reference	8536	8536
Depth (m)	0-500	500-2100
Position	TPG	TPG
Coordinates X Y		
Description	Dark olive	Light yellow brown
Additional information	Sampled by client.	Sampled by client.
Calcrete/Crushed		
Stabilizing Agent	Natural	Natural

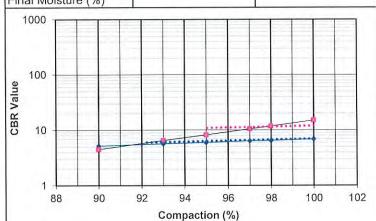
	JJ		
	nalysis (Wet prepa	aration)	SANS 3001: GR1, GR2
	100 mm	100	100
	75 mm	100	100
	63 mm	100	100
Вu	50 mm	92	96
SS	37.5 mm	89	92
Percentage Passing	28 mm	84	85
o O	20 mm	81	77
nta	14 mm	76	66
Se	5 mm	64	40
Je C	2 mm	64	40
	0.425 mm	51	20
	0.250 mm	45	17
	0.150 mm	39	15
	0.075 mm	29	12
Grading M	lodulus	1.6	2.3

Soil N	Iortar Analysis	
Coarse Sand	20	50
Coarse Fine Sand	9	8
Medium Fine Sand	10	6
Fine Fine Sand	14	7
Silt and Clav	46	29

Atterberg Limits	SANS GR10,GR11,GR12					
Liquid Limit (%)	45	50				
Plasticity Index (%)	22	22				
Linear Shrinkage (%)	10.5	11.0				

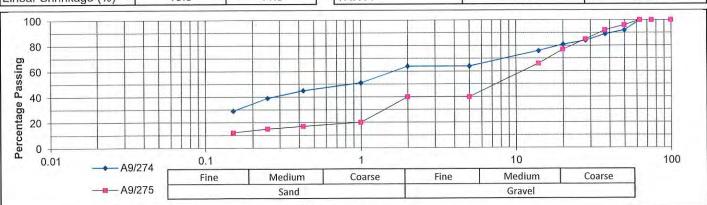
Laboratory No.		A9/274	A9/275
Maximum Dr	y Density & Optimun	n Moisture Content	SANS 3001: GR30
MDD	kg/m ³	1806	2075
OMC	%	15.3	11.4
(California Bearing	Ratio	SANS 3001: GR40

	2 42 12 20 124 2.3. 0.00						
		Comp	action I	Data			
Moisture	%		15.5			11.2	
Dry Density	kg/m ³	1865	1718	1641	2080	1975	1886
Compaction	%	100.0	92.1	88.0	100.0	95.0	90.7
		Pene	tration [Data			
	2.50 mm	7	6	5	12	11	5
CBR at	5.00 mm	6	5	4	15	14	12
	7.50 mm	5	5	4	19	18	16
Swell	%	1.1	1.2	1.5	0.7	0.9	1.2
Final Moistur	e (%)						



		Interpo	lated CBR Dat	ia
@	100%	Э	7	15
@	98%	Ē	7	12
0	97%	ž	6	11
CBR (®)	95%	₹.	6	8
0 @	93%	Mod	6	7
@	90%	Σ	5	5
@	SANS3001 Mid	lpoint	6	11

	Classifications								
HRB (AASHTO)	A-2-7(2)	A-2-7(0)							
COLTO									
TRH14	G10	G10							





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Project No	: 2019-9	S-177						F	Page N	0.			of	
			MAT	ERI	ALS	TE:	STR	EP(ORT					
Laboratory Field Numb Client Refe	er			A9/276 8536 0-800										-
Depth (m)														
Position				TPJ										
Coordinate	S	X												
Description	i .		Da	ark brow	n									
Additional i	nformation		Samp	led by c	lient.									
Calcrete/Co Stabilizing	Agent			Natural										
		Sieve Anal			ation)					SAN	S 3001:	GR1,	GR2	
		100 mi	CO	100										
		75 mi		100										
D D		63 mi		100										
SS		50 mi		97										
Passing		37.5 mi		89										
e e		28 mi		84										
Percentage		20 mi		82										
Se		14 m		80										
e e		5 m 2 m	m	70 65										
О.			100	57										
		0.425 m	Charles Inc.	36										
O I' M	- abote -	0.075 m	m	1.42										
Grading M	odulus				Soil Me	ortar A	nalysis							
Coarse Sa	nd	2.0-0.425	J	12										
Coarse Fir		0.425-0.25		8										
Medium Fi		0.250-0.15		10										
Fine Fine S		0.150-0.07		13										
Silt and Cl		< 0.075		56										
	/		erberg L	imits						SANS	GR10	,GR11,	GR12	
Liquid Lim	it	%		47										
Plasticity I		%		26										
Linear Shr	inkage	%		13.5										
	Maximum	Dry Densi	ty & Opt	imum N	oisture	Conte	ent			SA	ANS 30	01: GR	30	
Max. Dry [Density	kg/m³		1740										
Optimum I		%		14.9										
CBR S/	ANS 3001:	GR40	JCS	1100	ITO	000	ITS	ITO	ODD	1100	ITC	CDD	LICC	ITC
Test Type			CBR (%)	UCS (kPa)	ITS (kPa)	CBR (%)	UCS (kPa)	ITS (kPa)	CBR (%)	UCS (kPa)	ITS (kPa)	CBR (%)	UCS (kPa)	ITS (kPa)
75		100% 0	5.8											-
ate		98%	4.9		-				-					
rpola		97%	4.5											
Interpolated Data		98% H97% VAV 95% P0 WAY 990% WAY P0 W	3.8	-	-						-			
프		93%	3.1		-						-			-
V-1. ~ · ·		0070	2.4				-							
	od. AASHTO		1.6									-		
Swell (%) (Mod. AASI	110 enort	1.0	1	Cla	ssifica	tions				1			-
HRB				A-7-6(4)		Jointa								
COLTO				1										
TRH14														



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Project No. : 2019-S-177 Page No.

Laboratory No.	A9/276 ◆	
Field Number		
Client Reference	8536	
Depth (m)	0.0-0.8	
Position	TPJ	
Coordinates X Y		
Description	Dark brown	
Additional information	Sampled by client.	
Calcrete/Crushed		
Stabilizing Agent	Natural	

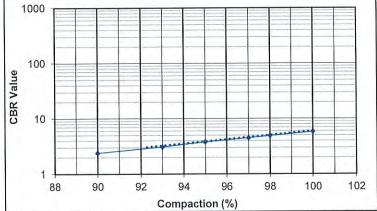
Sieve A	nalysis (Wet prepa	SANS 3001: GR1, GR2	
	100 mm	100	
	75 mm	100	
	63 mm	100	
рп	50 mm	97	
Passing	37.5 mm	89	
D a	28 mm	84	
ge	20 mm	82	
nta	14 mm	80	
Percentage	5 mm	70	
) el	2 mm	65	
	0.425 mm	57	
	0.250 mm	52	
	0.150 mm	45	
	0.075 mm	36	
Grading M	odulus	1.4	

Soil Mortar Analysis			
Coarse Sand	12		
Coarse Fine Sand	8		
Medium Fine Sand	10		
Fine Fine Sand	13		
Silt and Clay	56		

Atterberg Limits	SANS GR10,GR11,GR12			
Liquid Limit (%)	47			
Plasticity Index (%)	26			
Linear Shrinkage (%)	13.5			

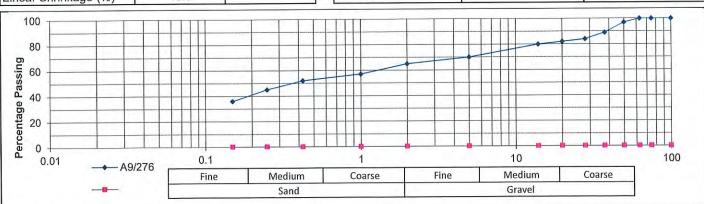
Laborator	y No.		
Maximum Dr	y Density & Optimum	SANS 3001: GR30	
MDD	kg/m ³	1740	
OMC	%	14.9	
(California Bearing	SANS 3001: GR40	

		Comp	action	Data		
Moisture	%		14.8			
Dry Density	kg/m ³	1745	1607	1521		
Compaction			92.1	87.2		
		Pene	tration I	Data		
1	2.50 mm	6	3	2		
CBR at	5.00 mm	7	3	2		
	7.50 mm	6	3	2		
Swell %		1.6	1.9	2		
Final Moistur	e (%)					
1000					_	_
1000						



			Inte	rpolated CBR Data	
	@	100%	0	6	
	@	98%	도	5	
~	@	97%	ASI	5	
CBR	@	95%	⋖.	4	
0	@	93%	Mod	3	
	@	90%	2	2	
	@	SANS3001 M	lidpoint	4	

	Classifications	
HRB (AASHTO)	A-7-6(4)	
COLTO		
TRH14		





HRB COLTO

TRH14

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31/01/2019 18/02/2019

Project No		6-177	g Otatio					ı	Page N	0.			of	
			MAT	ERI	ALS	TE	STR	REP	ORT					
aboratory	Number			A9/293										
Field Numl														
Client Refe				8536										
Depth (m)			7	00-1800										
Position				TPI										
Obliton		X												
Coordinate	es	Ŷ												
Description	1		Yello	wish bro	own									
Additional	information		Samp	led by c	lient.									
Calcrete/C	rushed													
Stabilizing	Agent			Natural										
		Sieve Analy			ation)					SAN	S 3001:	GR1, (GR2	
		100 mm		100										
		75 mm		100										
Б		63 mm		100										
Percentage Passing		50 mm		92										
ag		37.5 mm		86										
0		28 mm		77										
tag		20 mm		66	- 71									
en		14 mm		53										
erc		5 mm		31										
Δ.		2 mm												
		0.425 mm		19										
		0.075 mm	1	13										
Grading M	lodulus			2.44										
					Soil M	ortar A	nalysis							
Coarse Sa		2.0-0.425		21				-						
Coarse Fire		0.425-0.250		8		0			-					
Medium F		0.250-0.150	_	7										
Fine Fine		0.150-0.075		11										
Silt and Cl	lay	<0.075	rberg L	53						SANS	GR10	,GR11,	GR12	
Liquid Lim	i+	%	iberg L	55						O/ ii ve	JOILIO	,01111,	01112	
Liquid Lim Plasticity I		%		24										
Linear Sh		%		11										
Lilleal Olli	Maximum	Dry Densit	/ & Onfi		oistur	e Conte	ent			SA	ANS 30	01: GR	30	
Max. Dry		kg/m ³	, G. G. P. I.	2107										
Optimum		%		9.2										
	ANS 3001: 0		cs				ITS							
Test Type			CBR	UCS	ITS	CBR	UCS	ITS	CBR	UCS (kDa)	ITS	CBR (%)	UCS (kPa)	ITS (kPa)
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		1000/	(%)	(kPa)	(kPa)	(%)	(kPa)	(kPa)	(%)	(kPa)	(kPa)	(70)	(NI-a)	(Ma)
σ	@100% O	30.2					-							
Interpolated Data		98%	27.7											
		97% S	26.5 24.2			-					-	-		
D		95%	22.2			-		-			-			
<u>-</u>		98% 97% 95% PO W 90% W	19.4					-						
Value @ M	യ 1od. AASHTO	0070	13.4											
	@ Mod. AASH		0.3											
SWEII (%) (w IVIOU. AAST	n O Giloit	0.0		Cla	ssifica	tions	1						
Lunn			_	A-2-7/0\	Cia	Some	110115							

A-2-7(0)



SGS MATROLAB (PTY) LTD

- CIVIL ENGINEERING SERVICES -

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Reg No.: 2003/029180/07 - VAT Reg No.: 4040210587

esti<mark>ng Laboratory, No. 10025. Reg No.: 2003/0</mark> ARQ CONSULTING ENGINEERS (PTY) LTD

Date Received

31/01/2019

Pienaarsrivier Filling Station Project

Date Reported

18/02/2019

Project No. :

Client

2019-S-177

Page No. of

Laboratory No.	A9/293 🔷	
Field Number		
Client Reference	8536	
Depth (m)	700-1800	
Position	TPI	
Coordinates X Y		
Description	Yellowish brown	
Additional information	Sampled by client.	
Calcrete/Crushed		
Stabilizing Agent	Natural	

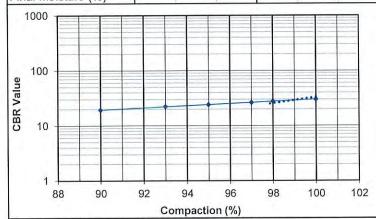
Clubinzing	7 190111	7.55,640,00	
Sieve A	nalysis (Wet prepa	aration)	SANS 3001: GR1, GR2
	100 mm	100	
	75 mm	100	
	63 mm	100	
рп	50 mm	92	
Passing	37.5 mm	86	
	28 mm	77	V .
Percentage	20 mm	66	
nta	14 mm	53	
Se C	5 mm	31	
Je.	2 mm	24	
	0.425 mm	19	
	0.250 mm	17	
	0.150 mm	15	
	0.075 mm	13	
Grading M	odulus	2.4	

Soil N	Nortar Analysis	
Coarse Sand	21	
Coarse Fine Sand	8	
Medium Fine Sand	7	
Fine Fine Sand	11	
Silt and Clay	53	

Atterberg Limits	SANS GR10,GR11,GR12
Liquid Limit (%)	55
Plasticity Index (%)	24
Linear Shrinkage (%)	11.0

Laboratory No.		A9/293		
Maximum Dry Density & Optimum Moisture Content			SANS 3001: GR30	
MDD	kg/m ³	2107		
OMC	%	9.2		
	o ur Desire	Dette	CANC 2004, CD40	

California Bearing Ratio				3AN3 3001. GR40	
		Comp	action	Data	
Moisture %			9.6		
Dry Density	kg/m ³	2105	2058	1911	
Compaction %		100.0	97.8	90.8	
		Pene	tration I	Data	
	2.50 mm	33	25	20	
CBR at	5.00 mm	42	33	22	
	7.50 mm	44	36	22	
Swell	%	0.3	0.4	0.6	
Final Moistur	e (%)				
1000					
0. 1					



			Inte	rpolated CBR Data	
	@	100%	0	30	
	@	98%	ASHT	28	
	@	97%	AS	27	
SBR	@	95%	₹.	24	
O	@	93%	Mod	22	
	@	90%	Σ	19	
	@	SANS3001 M	idpoint	29	

Classifications				
HRB (AASHTO)	A-2-7(0)			
COLTO				
TRH14	G8			

