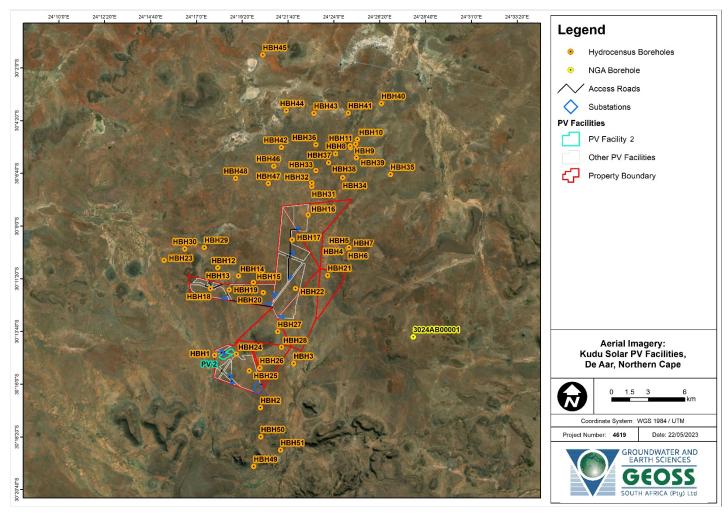


Map 16-2: The study area delineating the study area for the 12 Kudu Solar Facilities, property boundaries, hydrocensus boreholes and the NGA borehole on a 1:50 000 scale topocadastral map (3024AA, 3024AB, 3024AD, 3024BA, 3024BC). Note that this report is focused on Kudu Solar Facility 2.



Map 16-3: Aerial view delineating the study area of the 12 Kudu Solar Facilities, hydrocensus boreholes and the NGA borehole. Note that this report is focused on Kudu Solar Facility 2.

16.4.3 Project Specific Description

16.4.3.1 Climate

The study area experiences a semi-arid climate, with most of the rainfall occurring during February to March. Figure 16-1 shows the monthly average minimum and maximum air temperature distribution and Figure 16-2 shows the monthly median rainfall and evaporation distribution for the study area (Schulze, 2009). The long term (1950 – 2000) mean annual precipitation for the study area is 281 mm/a. The rainfall does not exceed evaporation during the course of the year.

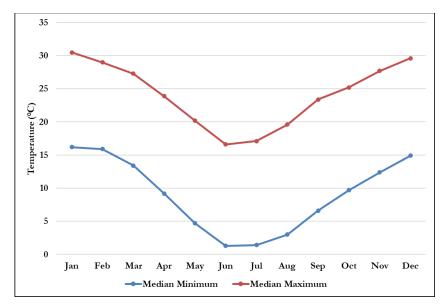


Figure 16-1: Monthly average air temperature for the Kudu Solar Facility study area (Schulze, 2009).

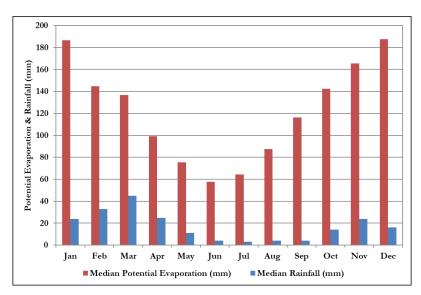


Figure 16-2: Monthly median rainfall and evaporation distribution for the Kudu Solar Facility study area (Schulze, 2009).

16.4.3.2 Regional Geology

The Geological Survey of South Africa (now the Council for Geoscience) has mapped the area at 1:250 000 scale (3024, Colesberg). The geological setting is shown in Map 16-4. The main geology of the area is listed in Table 16-2.

Table 16-2: Geological formations within the study area listed in order of relative age.

Symbol	Formation/Subgroup	Group	Lithology	
Qc	Quaternary Depo	Quaternary Deposit		
Jd	Jurassic Intrusio	Jurassic Intrusion		
Ра	Adelaide Subgroup	Beaufort Group	Blue-grey silty mudstone, subordinate brownish-red mudstone; sandstone	
Pt	Tierberg Formation	Ecca Group	Blue-grey to black shale with carbonate-rich concretions; subordinate siltstone and sandstone in upper part	

The Kudu Solar Facility 2 is mainly underlain by Quaternary alluvium deposits and well-developed calcretes. These quaternary deposits, in turn, overly either dolerite sills and dykes, (Jd) or undifferentiated sediments of the Adelaide Subgroup (Pa) and/or Tierberg Formation (Pt). The Adelaide Subgroup (Pa) comprises interbedded mudstones, siltstones and sandstone, whilst the Tierberg Formation (Pt) consists primarily of shale and sandstone. Both of these units were deposited within a braided river to deltaic setting within the Karoo basin during the Permian Period some 268 to 247 Million years ago (Johnson et al., 2006). These sediments were subsequently intruded during the Jurassic Period by dolerite sills and dykes of the Karoo Dolerite Suite. There are no known large structural geological features in the surrounding area of the proposed project; however, the dolerite sills in the area commonly show extensive jointing as a result of cooling and exhumation (Senger et al., 2015).

16.4.3.3 Regional Hydrogeology

The regional aquifer directly underlying the proposed project study area is classified by the Department of Water Affairs and Forestry (DWAF) (DWAF, 2005) as a fractured aquifer with an average yield potential of 0.5-2.0 L/s (Map 16-5). A fractured aquifer describes an aquifer where groundwater only occurs in narrow fractures within the bedrock. However, based on the geological map and the site-specific information it is known that the Quaternary deposits of alluvium and calcrete form an intergranular aquifer on top of the fractured bedrock. There is no known information about this aquifer. An intergranular aquifer is a primary aquifer and is described as an aquifer in which groundwater is stored within, and flows through open pore spaces in the unconsolidated Quaternary deposits.

Based on the DWAF (2005) mapping of the regional groundwater quality, as indicated by electrical conductivity (EC), the groundwater underlying the Kudu Solar Facility and the surrounding area is in the range of 70 - 300 mS/m. This is considered to be "good to marginal" quality for water (Map 16-6) with respect to drinking water standards.

Both these classifications are based on regional datasets, and therefore only provide an indication of conditions to be expected.

According to research done by Harkness et al. (2018), there is evidence in the southern portion of the Karoo basin that there are several variable aged sources of ground water at different depths. They found that the deeper groundwater was typically more saline, older according to isotope data, and had chemical signatures indicating both ancient meteoric and marine sources. Although separated by confining fine grained units throughout, fracture and joint sets within dolerite sills and dykes potentially act as a conduit for mixing between younger freshwater, and ancient saline aquifers.

16.4.3.4 Aquifer Vulnerability (DRASTIC)

Based on the regional datasets the proposed project overlies a fractured aquifer that possesses water bearing properties due to fracturing. Several methods have been developed to classify an aquifer's vulnerability with The DRASTIC method being applied to this study.

Groundwater vulnerability can be defined as the "tendency for contaminants to reach a specified position in the groundwater system after introduction at some location" (Vrba and Zaporozec, 1994). Key physical parameters which determine groundwater vulnerability include lithology, thickness, effective porosity, groundwater flow direction, age and residence time of water. Generally, the residence time of contaminants in groundwater and the distance that it travels in the aquifer are considered important measures of vulnerability.

There are two main groups of methods for assessing groundwater vulnerability, namely:

- Index or subjective rating methods, and
- Statistical or process-based methods.

The "index or subjective rating method" is relatively easily addressed within a GIS framework. The cell-based layer approach facilitates the assignment of ratings and weights, and rapid achievement of a final result of relative groundwater vulnerability. This approach also means that the algorithm can easily be repeated as new or more detailed data sets are obtained or if ratings and weightings need to be adjusted as a result of a sensitivity analysis for example. The most well-known "index or subjective rating method" is the "DRASTIC" method (Aller et al., 1987). The DRASTIC method of Aller et al. (1987) uses the typical overlay technique often applied in subjective rating methods. The DRASTIC approach is based on four major assumptions:

- The contaminant is introduced at ground surface;
- The contaminant is flushed into the groundwater by precipitation;
- The contaminant has the mobility of water; and
- The area evaluated using DRASTIC is 40.5 ha or larger.

The implication of these assumptions is that DRASTIC should not be used for contaminants that do not have the mobility of water or for point assessment (such as storage tanks). In addition, groundwater conditions in South Africa are dominated by secondary/fracture-controlled flow conditions. The DRASTIC method does not consider local preferential flow paths of fractured aquifer systems particularly well. The DRASTIC method takes into account the following factors:

D	=	depth to groundwater	(9)
R	=	recharge	(8)
Α	=	aquifer media	(8)
S	=	soil type	(4-5
Τ	=	topography	(10)
I	=	impact of the vadose zone	(9)
С	=	conductivity (hydraulic)	(6)

The number indicated in parenthesis at the end of each factor description is the weighting or relative importance at that factor.

Groundwater vulnerability maps developed using the DRASTIC method have been produced in many parts of the world. In spite of the widespread use of DRASTIC, the effectiveness of the method has been met with mixed success due to hydrogeological heterogeneity and the many assumptions that need to be made in determining groundwater vulnerability. In addition, the use of a generic vulnerability map only gives a broad indication of relative vulnerability and in many instances detailed scale, contaminant specific vulnerability assessments are required.

As part of the Groundwater Resources Assessment Project (DWAF, 2005), numerous data sets were produced and this enabled the mapping of groundwater vulnerability at the national scale on a 1 km by 1 km cell (pixel) size basis (Conrad and Munch, 2007). This national scale map indicates the relative vulnerability of groundwater resources throughout the country and provides project planners a clear idea of what level of groundwater protection is required.

The groundwater vulnerability for the study area is shown in Map 16-7. The development area for the Kudu Solar Facility 2 has a **Low to Medium** groundwater vulnerability. It is assumed that the regional data maps relate to the underlying fractured aquifer and not the intergranular aquifer. The intergranular aquifer on top of the fractured aquifer has no protection and therefore any contamination that is introduced on the surface of the intergranular aquifer will infiltrate into the subsurface and can cause contamination of the intergranular aquifer. Therefore, the vulnerability specifically for the intergranular aquifer is considered to be **medium**.

16.4.4 Site Specific and Existing Groundwater Information

16.4.4.1 NGA Database

A desktop assessment was initially carried out within and around the study area to determine if there were any groundwater users in the area. The NGA database provides data on borehole positions, groundwater chemistry and yield, where available. The NGA indicated there is one borehole surrounding the study area (Map 16-2 and Map 16-3). The NGA site is summarized in Table 16-3.

Table 16-3: Summary of NGA borehole.

NGA Label	Latitude (DD, WGS84)	Longitude (DD, WGS84)	Yield (L/s)	Depth (m)	Lithology
3024AB00001	-30.23333	24.46667	0.18	0-39.93 39.93-73.46	Shale Sandstone

The NGA site indicates a borehole has a yield of 0.18 L/s, depth of 73.46 m with a lithology of shale followed by sandstone.

16.4.4.2 Hydrocensus

A representative hydrocensus was conducted on 23 and 24 March 2022 on the farm portions on which the Kudu Solar Facilities 1 - 12 are located (i.e. the study area) and the surrounding farm portions. The hydrocensus boreholes are shown on Map 16-2 and Map 16-3. These boreholes are summarised in Table 16-4. During the hydrocensus data such as borehole depth, water level (WL), pH, total dissolved solids (TDS) and EC were measured.

Table 16-4: Summary of Boreholes in the study area.

Borehole Name	Latitude (DD, WGS84)	Longitude (DD, WGS84)	рН	EC (mS/m)	TDS (mg/L)	WL (mbgl)	Depth (m)
HBH1	-30.2463968	24.2971598	7.4	76	370	-	-
HBH2	-30.2851593	24.3358956	-	-	-	-	-
HBH3	-30.2526869	24.3643247	7.5	91	440	17.75	-
HBH4	-30.1679489	24.4109898	7.1	102	500	8.7	-
HBH5	-30.1675761	24.4118524	-	-	-	8.7	-
HBH6	-30.1676747	24.4112416	-	-	-	-	-
HBH7	-30.1673778	24.4120952	7.5	95	460	9.2	-
HBH8	-30.0936932	24.4136653	6.8	126	1260	6.4	10
HBH9	-30.092446	24.413403	7.5	104	510	8.4	-
HBH10	-30.0875905	24.4194914	7.3	80	390	-	-
HBH11	-30.091018	24.4180866	-	-	-	8.1	-
HBH12	-30.1818617	24.3003232	7.5	94	460	10.1	-
HBH13	-30.181802	24.3002685	-	-	-	-	-
HBH14	-30.1879078	24.3179014	-	-	-	-	-
HBH15	-30.1927376	24.3305225	-	-	-	-	-
HBH16	-30.1431559	24.377371	7.4	100	490	11	-
HBH17	-30.1614565	24.3636659	9.1	64	310	7.25	17
HBH18	-30.1971676	24.2939657	8.4	107	520	11.1	-
HBH19	-30.1980902	24.3098031	7.5	86	420	10.95	-
HBH20	-30.200251	24.33882	9.6	104	520	-	-
HBH21	-30.187906	24.393707	8	58	270	-	-
HBH22	-30.197459	24.366364	7.7	57	280	-	-

Borehole Name	Latitude (DD, WGS84)	Longitude (DD, WGS84)	рН	EC (mS/m)	TDS (mg/L)	WL (mbgl)	Depth (m)
*HBH23	-30.175992	24.2547534	-	-	-	-	-
*HBH24	-30.245532	24.315637	-	-	-	-	-
*HBH25	-30.258001	24.326557	-	-	-	-	-
*HBH26	-30.255856	24.335565	-	-	-	-	-
*HBH27	-30.229251	24.35097	-	-	-	-	-
*HBH28	-30.240724	24.35404	-	-	-	-	-
*HBH29	-30.166797	24.288983	-	-	-	-	-
*HBH30	-30.167743	24.272326	-	-	-	-	-
*HBH31	-30.122051	24.380559	-	-	-	-	-
*HBH32	-30.119526	24.380652	-	-	-	-	-
*HBH33	-30.110477	24.384284	-	-	-	-	-
*HBH34	-30.115827	24.406987	-	-	-	-	-
*HBH35	-30.113626	24.447559	-	-	-	-	-
*HBH36	-30.09143	24.384297	-	-	-	-	-
*HBH37	-30.098216	24.401043	-	-	-	-	-
*HBH38	-30.104676	24.395147	-	-	-	-	-
*HBH39	-30.101161	24.418577	-	-	-	-	-
*HBH40	-30.061157	24.440153	-	-	-	-	-
*HBH41	-30.068085	24.411932	-	-	-	-	-
*HBH42	-30.093241	24.354924	-	-	-	-	-
*HBH43	-30.068237	24.382791	-	ı	-	-	-
*HBH44	-30.06616	24.359238	-	-	-	-	-
*HBH45	-30.024899	24.339597	-	ı	-	-	-
*HBH46	-30.107118	24.348457	-	-	-	-	-
*HBH47	-30.119755	24.343665	-	-	-	-	-
*HBH48	-30.115915	24.315975	-	-	-	-	-
*HBH49	-30.328537	24.329885	-	-	-	-	-
*HBH50	-30.306722	24.336103	-	-	-	-	-
*HBH51	-30.316574	24.352879	-	-	-	-	-

^{*} Could not gain access to borehole due to wet conditions. Farmer indicated location of borehole on a map.

From the information obtained during the hydrocensus it is clear that the boreholes are shallow in the area as all of them were wind pumps. The water is mainly used for domestic use and livestock watering. The boreholes had an EC that ranged from 57 mS/m to 126 mS/m and all of the boreholes were only drilled into the alluvium as the farmers reported that they only drill until they intersect the "ysterklip" which can be assumed to be the shales or dolerites underlying the alluvium.

⁻ Data could not be obtained due to base plate that covered the whole borehole or the information was unavailable.

16.4.4.3 Groundwater Quality

The groundwater quality obtained during the hydrocensus was assessed to establish if it is suitable for the following uses:

- Potable water
- Domestic use which will include washing of dishes and toilet flushing
- Washing of panels
- General construction and concrete batching

16.4.4.3.1 SANS241-1:2015: Drinking water standards

The field parameters that were obtained from boreholes that were tested during the hydrocensus have been classified according to the South African National Standard (SANS) SANS241-1: 2015 standards for domestic water in (Table 16-5). Table 16-6 presents the field chemistry results, colour coded according to the SANS241-1: 2015 drinking water assessment standards.

Table 16-5: Classification table for specific limits for domestic water standards

Acute Health	Chronic Health	Aesthetic	Operational	Acceptable

The limits and associated risks for domestic water as determined by the SANS 241:2015 are as follows, where:

- Health risks: parameters falling outside these limits may cause acute or chronic health problems in individuals.
- Aesthetic risks: parameters falling outside these limits indicate that water is visually, aromatically or palatably unacceptable.
- Operational risks: parameters falling outside these limits may indicate that operational procedures to ensure water quality standards are met may have failed.

Table 16-6: Production borehole results classified according the SANS241-1:2015

Borehole Name	рН	EC (mS/m)	TDS (mg/L)
HBH1	7.4	76	370
HBH3	7.5	91	440
HBH4	7.1	102	500
HBH7	7.5	95	460
HBH8	6.8	126	1260
HBH9	7.5	104	510
HBH10	7.3	80	390
HBH12	7.5	94	460
HBH16	7.4	100	490
HBH17	9.1	64	310

	Borehole Name	рН	EC (mS/m)	TDS (mg/L)
	HBH18	8.4	107	520
	HBH19	7.5	86	420
	HBH20	9.6	104	520
	HBH21	8	58	270
	HBH22	7.7	57	280
SANS241- 1:2015		5-9.5	≤170 Aesthetic	≤1200 Aesthetic

16.4.4.3.2 DWA (1998): Drinking Water Assessment Guide

The field parameters that were obtained have also been classified according to the DWAF (1998) standards for domestic water (as they a little easier to understand). Table 16-7 enables an evaluation of the water quality with regards to the various parameters measured (DWAF, 1998). Table 16-8 presents the water chemistry analysis results colour coded according to the DWAF drinking water assessment standards.

Table 16-7: Classification table for the groundwater results (DWAF, 1998)

Blue	(Class 0)	Ideal water quality - suitable for lifetime use.
Green	(Class I)	Good water quality - suitable for use, rare instances of negative effects.
Yellow	(Class II)	Marginal water quality - conditionally acceptable. Negative effects may occur.
Red	(Class III)	Poor water quality - unsuitable for use without treatment. Chronic effects may occur.
Purple	(Class IV)	Dangerous water quality - totally unsuitable for use. Acute effects may occur.

Table 16-8: Classified production borehole results according to DWAF 1998.

Borehole Name	рН	EC (mS/m)	TDS (mg/L)
HBH1	7.4	76	370
HBH3	7.5	91	440
HBH4	7.1	102	500
HBH7	7.5	95	460
HBH8	6.8	126	1260
HBH9	7.5	104	510
HBH10	7.3	80	390
HBH12	7.5	94	460
HBH16	7.4	100	490
HBH17	9.1	64	310

	Borehole Name	рН	EC (mS/m)	TDS (mg/L)
	HBH18	8.4	107	520
	HBH19	7.5	86	420
	HBH20	9.6	104	520
	HBH21	8	58	270
	HBH22	7.7	57	280
DWAF	Class 0	5-9.5	<70	<450
(1998) Drinking	Class I	4.5-5&9.5-10	70-150	450-1000
Water	Class II	4-4.5&10-10.5	150-370	1000-2400
Assessment	Class III	3-4&10.5-11	370-520	2400-3400
Guide	Class IV	<3&>11	>520	>3400

The available chemistry results (pH, EC and TDS) have been compared SANS241-1: 2015 standards and the DWAF (1998) standards in Table 16-6 and Table 16-8. From this it is seen that the groundwater quality is generally of good quality in terms of pH, EC and TDS. It is possible that the groundwater can be used for potable and domestic purposes with only minor treatment however a full laboratory analysis will be required.

With regards to the cleaning of panels it is understood that a very clean water is required to clean the panels otherwise salts will deposit on the panels. The electric conductivity for the groundwater ranges from 57 to 126 mS/m which is considered to be good to marginal. Although this water quality is relatively good it will not be suitable for panel washing as it will result in salts precipitating on the panels. The salts could be removed from the groundwater by thermal distillation (i.e. boiling since salt has a much higher boiling point than water) or by membrane separation (commonly reverse osmosis). Both of these techniques are possible but financial viability would have to be determined before commissioning as both techniques are costly on a large scale.

In terms of using groundwater for construction purposes and mixing of concrete the SANS 51008:2006 (*Mixing water for concrete document*) was referred to. Both the composition of the water and the application of the concrete needs to be considered. Potable water is considered to be suitable for concrete batching with no testing required. Groundwater is also considered to potentially be suitable for concrete batching; however, it requires testing as some groundwater can be very saline which is not considered to be suitable. Furthermore, the SANS 51008 standards do specify maximum limits for chlorides, sulphates, alkalinity, phosphates, nitrates, lead and zinc. Most of these parameters are currently unknown and therefore it is unclear if the groundwater is suitable for construction and concrete batching.

16.4.4.4 Water level elevation maps

The water level elevations obtained during the hydrocensus were interpolated² to determine the groundwater flow direction. The data is presented in Figure 16-3, and indicates a 99.44% correlation between surface topography (elevation (mamsl)) and groundwater level elevation. Bayesian interpolation is therefore considered an acceptable interpolation technique. The water level elevation map for March 2022 is presented in Map 16-8. From this it is seen that the groundwater flow direction is in a general north westerly direction.

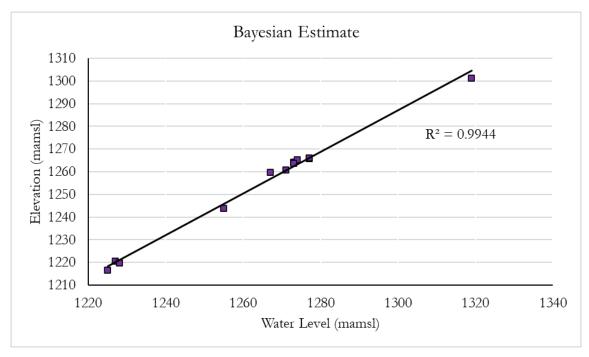
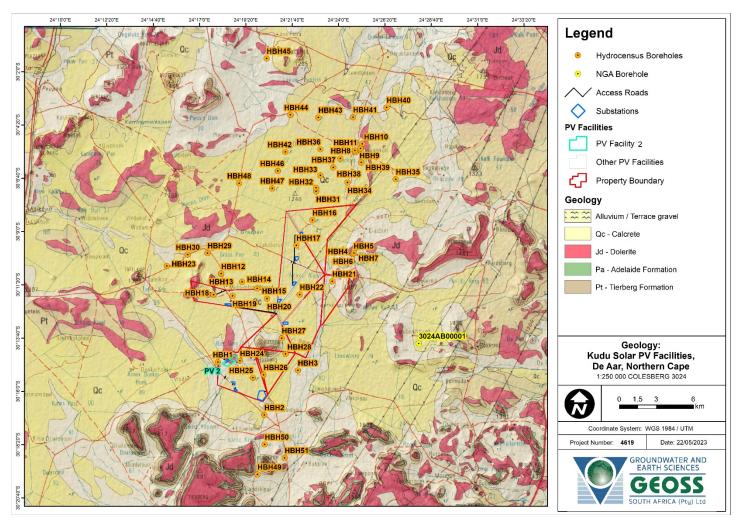
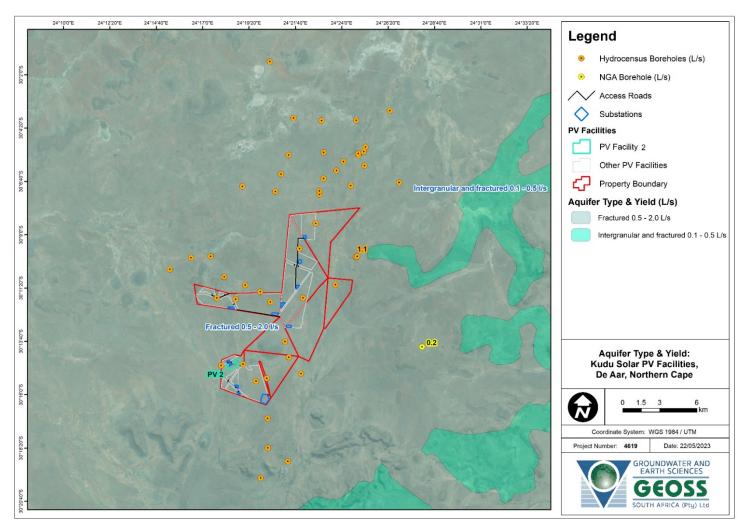


Figure 16-3: Correlation between surface topography and groundwater elevation.

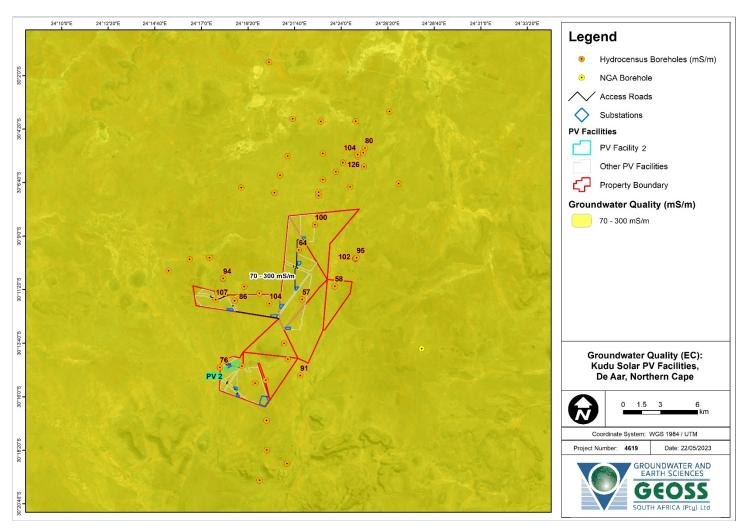
² Bayesian interpolation was used and the output generated was a point grid, which was interpolated in ArcGIS software to create the groundwater elevation surface.



Map 16-4: Geological setting of the study area for the Kudu Solar Facilities. (CGS (1997) map: 1:250 000 scale Colesberg). Note that this report is focused on Kudu Solar Facility 2.

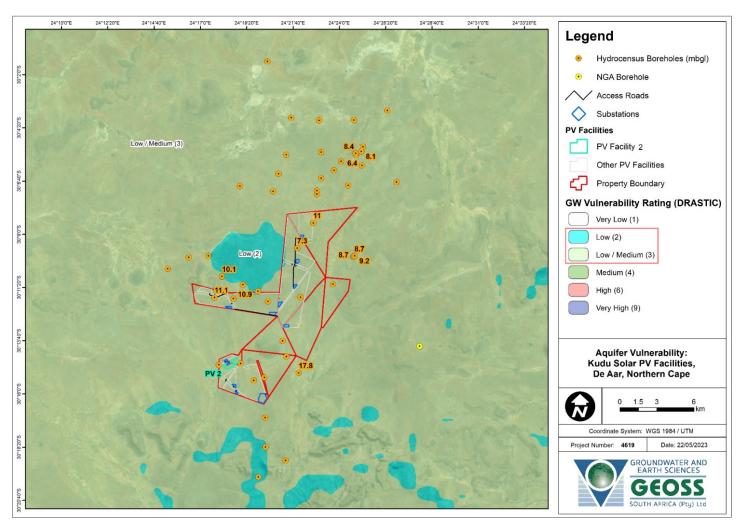


Map 16-5: Regional aquifer yield (DWAF, 2005) and borehole yields (L/s) in the study area for the Kudu Solar Facilities. Note that this report is focused on Kudu Solar Facility 2.

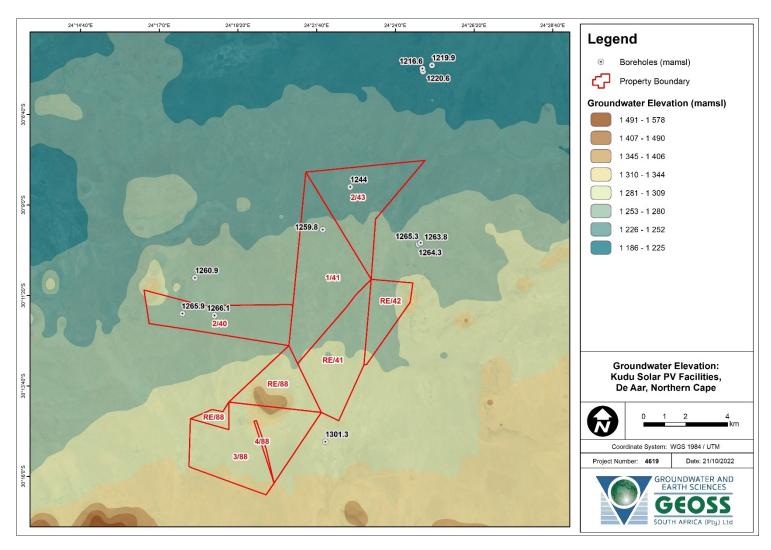


Map 16-6: Regional groundwater quality (mS/m) from DWAF (2005) and borehole groundwater quality (EC in mS/m) in the study area for the Kudu Solar Facilities.

Note that this report is focused on Kudu Solar Facility 2.



Map 16-7: Vulnerability rating (DWAF, 2005) and groundwater depths (mbgl) in the study area for the Kudu Solar Facilities. Note that this report is focused on Kudu Solar Facility 2.



Map 16-8: Groundwater contour map based on the March 2022 field measurements in the study area. Note that this report is focused on Kudu Solar Facility 2.

16.4.5 Identification of Environmental Sensitivities

16.4.5.1 Sensitivities identified by the National Web-Based Environmental Screening Tool

Part of the terms of reference for the Kudu Solar Facility was to identify sensitivities by the National Web-Based Environmental Screening Tool. However, it is important to note that there are no dedicated Geohydrology or Groundwater themes on the National Web-based Environmental Screening Tool (Screening Tool) (as of May 2023), therefore the environmental sensitivity of the proposed project area as identified by the Screening Tool is not applicable. As such, no site sensitivity verification report is required. Furthermore, there is no dedicated assessment protocol prescribed for Geohydrology or Groundwater. Therefore, the specialist assessment has been undertaken in compliance with Appendix 6 of the NEMA EIA Regulations of 2014.

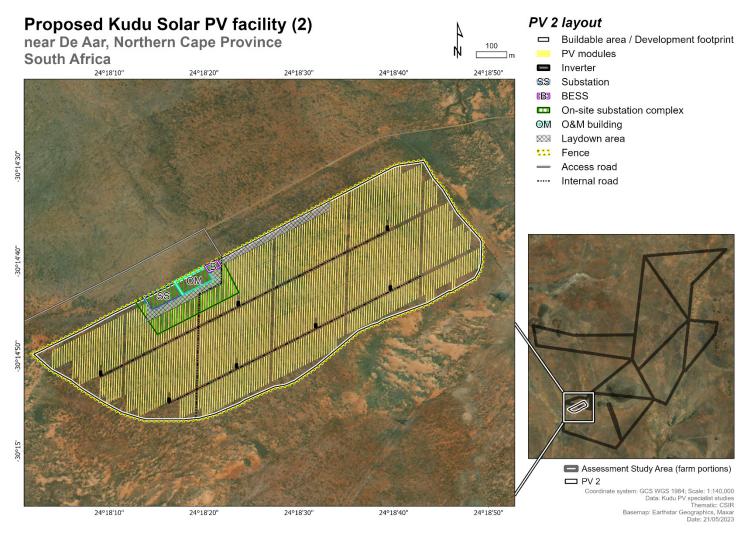
16.4.5.2 Specialist Sensitivity Analysis and Verification

As there is no sensitivity assessment protocol for Groundwater or Geohydrology, the following sensitivity analysis is based primarily on the results from the DRASTIC approach outlined in section 16.4.2. From this analysis a geospatial model was created, which shows that the entire site sits within a low/medium ground water vulnerability rating, with the overlying alluvium being tentatively given a medium vulnerability rating. Furthermore, the site is situated above a fractured aquifer with relatively low yield of 0.5 to 2.0 l/s. Overlying the fractured aquifer is an intergranular aquifer made up of Cenozoic alluvium and carbonate palaeosols. This aquifer has no protection, with the result that any contamination introduced on the surface can infiltrate into the subsurface and potentially contaminate this aquifer. However, this is coupled with a low permeability of the unsaturated layer, which allows for a significant attenuation capacity. The sensitivity across the entire development is, therefore, similarly classified as "medium" with respect to all activities associated with the proposed development. This classification as "medium" sensitivity does not represent a constraint and does not represent an area to be avoided from a groundwater sensitivity perspective. Accordingly, no buffer areas have been identified save for a 50m buffer around borehole sites with respect to BESS construction/installation. Additional information on the impacts associated with the BESS are discussed in the following sections. Currently no site alternatives have been identified as these would be located within a similarly classed sensitivity area.

The major receptors with respect to ground water within the region are limited to livestock and the occupants of the surrounding farms. The principal activity within the region is the farming of livestock, which relies almost completely on the underground water resource. Any deterioration in either groundwater quality or groundwater level will negatively impact on these receptors.

16.4.5.3 Sensitivity Analysis Summary Statement

As indicated above, following the identification of sensitivities during the Scoping Phase, the Project Developer considered such sensitivities and formulated the Revised Scoping Buildable Areas. The Revised Scoping Buildable Areas led to the identification of the development footprints and detailed layouts in the EIA Phase. The development footprint and detailed layout are considered suitable from a Geohydrological perspective, as the sensitivities identified above (i.e. BESS placement to be outside of 50 m from identified boreholes) have been taken into consideration. The development footprint and detailed layout are shown in Map 16.9. Changes to the detailed layouts are deemed acceptable if the changes remain within the approved buildable areas / development footprints and area assessed during the Scoping and EIA Process with nogo sensitive areas avoided.



Map 16-9: Detailed Layout of Kudu Solar Facility 2

16.5 Issues, Risks and Impacts

16.5.1 Identification of Potential Impacts/Risks

The potential impacts on groundwater due to the proposed project activities are listed below:

- Lowering of the groundwater level due to abstraction during the construction and operational phases (9 000 m³/a for the Construction Phase and 1 000 m³/a for the Operational Phase for this PV project).
- Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages during the construction and decommissioning phases.
- Potential impact on groundwater quality as a result of cleaning agents used for cleaning the solar panels during the operational phase.
- Potential impact on groundwater quality as a result of electrolyte that will be used for the BESS.

Any construction activities such as the excavation and installation of foundations and piling (narrow diameter holes for foundation purposes) will have minimal to no impact on the groundwater of the site or region, as the groundwater level is approximately >5 mbgl.

The potential impacts identified during the Scoping and EIA are:

Construction Phase

- Potential impact 1: Potential lowering of the groundwater level from construction requirements.
- Potential impact 2: Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages.

Operational Phase

- Potential impact 3: Potential lowering of the groundwater level from operational requirements.
- Potential impact 4: Potential impact on groundwater quality as a result of using cleaning agents for cleaning the solar panels.
- Potential impact 5: Groundwater quality deterioration as a result of electrolyte that will be used for the BESS.

Decommissioning Phase

- Potential impact 6: Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages.
- Potential impact 7: Potential lowering of the groundwater level from decommissioning requirements.

Although the project description does not state the anticipated water use during decommissioning phase, from previous experience on similar projects it is unlikely that water use for the decommissioning phase will exceed that of the construction phase. This impact is,

therefore, assessed according to anticipated water usages similar to that of the construction phase.

Cumulative Impacts

- Cumulative Impact 1: Potential lowering of groundwater level during the construction, operational and decommissioning phase for all 12 of the Kudu PV facilities.
- Cumulative Impact 2: Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages from the construction and the decommissioning phase for all 12 Kudu facilities.
- Cumulative Impact 3: Potential of impact on groundwater quality as a result of using cleaning agents for cleaning the solar panels during the operational phase for all the 12 Kudu facilities.
- Cumulative Impact 4: Potential impact on groundwater quality as a result of electrolyte that will be used for the BESS.
- Cumulative Impact 5: Other wind and solar, and EGI projects within a 30 km radius.

No indirect impacts are identified.

16.5.2 Summary of Issues identified during the Public Consultation Phase

The following represents a summary of the main issues identified during the Public Consultation Phase during Scoping. Many of the stakeholders shared the same concerns including:

- Increased abstraction of groundwater due to the proposed development may deplete the groundwater resources in the area.
- Increased abstraction may lower the groundwater table to depths lower than the average windpump depth of 50 to 80 meters.
- Whether the cumulative water requirements are serviceable by the aquifer and does not exceed the potential recharge.
- What the Water Use Licence Requirements are for groundwater uses related to the proposed project.

Table 16-9 shows a more detailed representation of these concerns with reference to specific comments made by stakeholders. All of these comments are addressed in the subsequent sections of this assessment.

Table 16-9: Table showing a summary of the main comments received from stakeholders during the Public Consultation Phase during Scoping with key responses

Comment	Commenter	Response
Queries on the water usage of the project.	Adjacent and/or nearby landowners and Interested and Affected Parties (I&APs)	Note that each Kudu Solar Facility will require the following water volumes. This specifically applies to Kudu Solar Facility 1, 2, 3, 4, 6, 9, 10, and 12. Each facility listed here will require the amount of water below:
		 Approximately 9 000 m³ of water is estimated to be required per year for the construction phase.
		 Approximately 1 000 m³ of water is estimated to be required per year for the operational phase.
		The following water usage applies to <u>Kudu Solar Facilities 5, 7, 8 and 11</u> each (i.e. each facility listed here will require the amount of water below):
		 Approximately 18 000 m³ of water is estimated to be required per year for the construction phase.
		 Approximately 2 000 m³ of water is estimated to be required per year for the operational phase.
		For all the proposed Kudu Solar Facilities, water requirements during the decommissioning phase are unknown at this stage, however it is unlikely to exceed the water requirements of the construction phase.
		Water required for the construction, operational and decommissioning phases will either be sourced from the following sources (<u>in order of priority and likelihood</u>):
		 Local municipality i.e. most likely trucked in or made available for collection at the Local Municipal Water Treatment Plant via a metered standpipe;
		 Investigation into a third-party water supplier which may include private services companies. This would most likely be trucked in; Existing boreholes on site to source groundwater (if available and if suitable); or

Comment	Commenter	Response
Comment	Commenter	Response New boreholes that will be drilled on site to source groundwater (if available and if suitable), which will be subject to complete geohydrological testing and an assessment, as well as a Water Use Licence Application process, as well as the necessary Environmental Assessment process (if required). This will be undertaken as a separate process, once more detailed information becomes available, outside of the current Application for EA for the Solar PV Facility and associated infrastructure. Therefore the use of existing boreholes on site to source groundwater (if available and if suitable) is only one of the potential water sources (and it is only the third most likely option, as noted above. Water from the municipality is the first option in terms of viability but consideration of other options is vital). A hydrocensus was undertaken as part of this Geohydrology Assessment in order to visit selected boreholes and landowners to obtain information such as yields and to measure the field chemistry to assess the groundwater quality (pH, total dissolved solids (TDS) and electrical conductivity (EC)). An analysis of the hydrocensus chemistry results was also undertaken in terms of the SANS 241-1: 2015 and the Department of Water Affairs and Forestry (DWAF) (1998) Standards. Based on this, the groundwater quality in the study area is generally of good quality in terms of pH, TDS and EC. It is possible that the groundwater can be used for potable and domestic purposes with only minor treatment however a full laboratory analysis will be required. With regards to the cleaning of panels, salts could be removed from the groundwater by thermal distillation (i.e. boiling since salt has a much higher boiling point than water) or by membrane separation (commonly reverse osmosis). Both of these techniques are possible but financial viability would have to be determined before commissioning as both techniques are costly on a large scale. Water pipelines may need to be constructed to transfer groundwater from existing
		transported by trucks from the boreholes to the site. Groundwater may also need to be stored on site in suitable containers or reservoir tanks during the construction and operational phases. Ground water storage may trigger the need for a Water Use Licence if there is more than 2000 m³ stored on the site per year in an open container.

Comment	Commenter	Response
		These responses are expanded within Section 16.3 and Section 16.6 of this chapter.
Requests for information on the measures in place to test the availability of water resources.	 Adjacent and/or nearby landowners and I&APs 	As noted above, a hydrocensus was conducted to confirm the quality of various existing boreholes in the region. However, no drill records or yield test data exists for production or wind pump boreholes to clarify yields and geological logs. Therefore, estimations for groundwater supply capacity for the area are based on regional datasets. For each PV Facility, the anticipated demands are less than the regional yield potential of the underlying aquifer $(0.5-2.0 \text{ L/s})$. This is considered appropriate for a study undertaken as part of an EIA Process.
		The study area is located mainly within quaternary catchment D33B with small sections within quaternary catchment D62F. Both of these quaternary catchments form part of the Lower Orange Water Management Area in the Northern Cape. The groundwater General Authorisation (GA) for both of the catchments is 45 m³/ha/a (published on 2 September 2016, in GG 40243, GN 538 (i.e. Revision of GA for the taking and storing of water). If the proposed projects are timed and planned appropriately with regards to groundwater use, all the water can be obtained from groundwater, with the use being Generally Authorised.
		The impact of the proposed abstraction on groundwater is predicted to be of low significance, with effective implementation of mitigation actions (i.e. to adhere to the borehole's safe yield and to monitor water levels and flow).
		These responses are expanded on in Section 16.4, Section 16.8 and Section 16.6 of this chapter.
Requests for information regarding Water Use Licence Requirements for boreholes.	Adjacent and/or nearby landowners and I&APs	As noted above, for all the proposed Kudu Solar Facilities, the potential sources of water, in order of priority and likelihood, include the: Local municipality, third-party water supplier, existing boreholes or drilled boreholes on site. Therefore, the use of existing boreholes on site to source groundwater is only one of the potential water sources (and it is only the third most likely option, as noted above. Water from the municipality is the first option in terms of viability but consideration of other options is vital).

Comment	Commenter	Response
		In terms of measurements, the Geohydrology Assessment undertook a hydrocensus of the existing boreholes in the area and an analysis of the data, and based on this, the groundwater quality in the study area is generally of good quality in terms of pH, TDS and EC.
		The study area is located mainly within quaternary catchment D33B with small sections within quaternary catchment D62F. Both of these quaternary catchments form part of the Lower Orange Water Management Area in the Northern Cape. The groundwater GA for both of the catchments is 45 m³/ha/a (published on 2 September 2016, in GG 40243, GN 538 (i.e. Revision of GA for the taking and storing of water)). If the proposed projects are timed and planned appropriately with regards to groundwater use, all the water can be obtained from groundwater, with the use being Generally Authorised. Registration of the usage in terms of the GA with the Department of Water and Sanitation (DWS) would be required.
		These responses are expanded on in Section 16.3, Section 16.4, Section 16.6, and Section 16.8 of this chapter.
Requests for information regarding the impact of the development on groundwater resources.	Adjacent and/or nearby landowners and I&APs and I&APs	This Geohydrology Assessment provides feedback on the suitability of the groundwater for usage during the construction and operational phases of the project, and also identifies various potential impacts of the proposed project on the geohydrology, as noted below:
		Construction Phase:
		 Potential lowering of the groundwater level.
		 Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages.
		Operational Phase
		o Potential lowering of the groundwater level.
		Potential impact on groundwater quality as a result of using cleaning
		 agents for cleaning the solar panels. Potential impact on groundwater quality as a result of electrolyte that will be used for the BESS.

Comment	Commenter	Response
Queries on the sustainability of groundwater	Adjacent and/or nearby landowners	Decommissioning Phase O Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages. All the impacts have been rated with a low to very low significance with the implementation of mitigation measures. All mitigation measures have been captured in the Environmental Management Programme (EMPr). These responses are expanded on in Section 16.3, Section 16.6, and Section 16.9 of this chapter. The impact of the usage of the ground water during the relevant project phases is
withdrawal for the maintenance of the development.	and I&APs and I&APs	addressed in this Geohydrology Assessment, along with the identification of various management actions to address such usage of water, which have been carried over to the EMPr, which is legally binding once approved. Any historical groundwater monitoring by the DWS should be sourced and assessed during all phases of development (once Environmental Authorisation is obtained, should it be granted), and a monitoring program should be instated (water level, chemistry and volumes abstracted). This has been included in the EMPr. These responses are expanded on in Section 16.9 of this chapter.
Queries on the effect of windpump/boreholes on the supply of drinking water to sheep, cattle, and game farm activities.	Adjacent and/or nearby landowners and I&APs and I&APs	This Geohydrology Assessment assessed the impact of the water required for the proposed development on the environment. With appropriate sighting and management measures groundwater impact on existing users can be entirely mitigated. The assessment has identified the lowering of groundwater levels as a result of over-abstraction as a potential impact, of low significance, with the implementation of recommended mitigation measures (i.e. adhere to the borehole's safe yield and to monitor water levels and flow; and boreholes must be correctly yield tested according to the National Standard (SANS 10299-4:2003, Part 4 – Test pumping of water boreholes). This includes a Step Test, Constant Discharge Test and recovery monitoring). This has been included as a requirement in the EMPr. In addition, an appropriate monitoring program will need to be instated to ensure over abstraction of groundwater is not taking place, and/or to ensure that no contamination

Comment	Commenter	Response
		of groundwater is taking place. This will allow the Environmental Control Officer / Environmental Manager of the proposed project (appointed post EA should authorisation be granted, and the proposed project progresses to the commencement phase) to determine the observed effect on the groundwater resources in the area. These responses are expanded on within Section 16.9 within this chapter.
Comment regarding the majority of existing windpumps and boreholes being just adequate for sheep; and the impact on water levels due to the drought season.	Adjacent and/or nearby landowners and I&APs	Testing of boreholes, that are planned to be used, will be required to determine if the yields can actually deliver the required volumes. In addition, droughts are seasonal and will occur. The more information that is collected (e.g. monitoring prior to construction) the more certainty there will be on the actual observed effect on the proposed development on the groundwater resources. Therefore, groundwater monitoring is crucial for the protection of the regional groundwater resources.
Comment regarding the ground water being slow running.	Adjacent and/or nearby landowners and I&APs	These responses are expanded on within Section 16.9 within this chapter. As noted above, this will need to be scientifically yield tested. The impact of the usage of groundwater has been assessed in this Geohydrology Assessment.
Comments regarding groundwater moving from south to north.	Adjacent and/or nearby landowners and I&APs	These responses are expanded on within Section 16.9 within this chapter. The comment is agreed with, based on the available information. Groundwater movement is driven by gravity and (generally speaking) flows from high elevations to low elevations. These responses are expanded on within Section 16.4 within this chapter.
Comments regarding the depth of the water surface in this area, and its gradual sinking over time and as drought seasons approach.	Adjacent and/or nearby landowners and I&APs	This can only be confirmed by instatement of an appropriate monitoring program. The requirements for such a program have been documented in the EMPr. These responses are expanded on within Section 16.9 within this chapter.
Feedback on the depth of the borehole (and link to the dolerite bank) and the history around the boreholes.	Adjacent and/or nearby landowners and I&APs	Anecdotal evidence suggests that many of the boreholes were drilled using 'stamper boor' apparatus. It appears this is the average depth of the boreholes (50 – 80 m) in the region. It is agreed that boreholes are typically shallow in the region. This is not to say there is absolutely no water deeper than the average depth of the boreholes in the region. Only several deep boreholes could prove this.

Comment	Commenter	Response			
		These responses are expanded on within Section 16.4 within this document			
Comment regarding status of the ground water (i.e. fossil water and stored	 Adjacent and/or nearby landowners and I&APs 	This could be confirmed by isotopic dating of the ground water. There is evidence in the southern portion of the Karoo basin that there are several sources of ground water			
underground for many years).	iandowners and texal 3	at variable depths, with variable ages. Deeper groundwater was typically found to saline, and older (Harkness et al., 2018). However, this is not within the scope of current assessment, nor is it required in order to assess the overall impacts of growater usage associated with the proposed project.			
		These responses are expanded on within Section 16.4 within this chapter.			
Comment regarding the supplement of ground water (i.e. slow and occurs only once every few years).	 Adjacent and/or nearby landowners and I&APs 	This can be confirmed by yield testing boreholes in the area and implementing monitoring to observe actual effects of groundwater removal/abstraction. The impact of the usage of groundwater has been assessed in this Geohydrology Assessment			
		These responses are expanded on within Section 16.9 within this chapter.			

Comments related to geohydrology impacts associated with the proposed project were raised by Interested and Affected Parties during the review period of the Draft EIA Report. These comments are similar to those submitted and considered during the Scoping Phase, and therefore similar responses apply. Comments were raised in terms of recommendations for groundwater monitoring and in terms of water use licence applications and general authorisations; queries on the water use licence requirements for the project, the amount of groundwater to be used, water availability and drought related concerns, sustainability of groundwater usage, concerns around not distributing the development over a larger area thereby distributing the impact of groundwater abstraction and increasing sustainable abstraction, groundwater flow, and chemical pollution of grazing land. Responses have been provided in Appendix H.7 of the Final EIA Report.

16.6 Impact Assessment

16.6.1 Potential Impacts during the Construction Phase

The impact table for the Construction Phase is presented in Table 16-11.

16.6.1.1 Impact 1: Groundwater impact as a result of over-abstraction from construction requirements

During the construction phase the project plans to use 9 000 m³/a (0.29 L/s) (Table 16-10). This requirement is within the expected capacity of the aquifer (0.5-2.0 L/s) therefore the risk associated to this impact is considered to be low. It must be noted that the study area is known to experience extreme droughts and therefore even though the construction groundwater demand is within the yield potential of the aquifer, adherence to the mitigation measures during the construction phase is vital.

The status of this impact is rated as negative with a local spatial extent and a short-term duration (i.e. for the construction phase). The consequence and probability of the impact are respectively rated as substantial and likely. The reversibility of the impact is rated as high and the irreplaceability is rated low. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of prevention / mitigation actions (i.e. to adhere to the borehole's safe yield and to monitor water levels and flow etc.), the impact of the proposed abstraction on groundwater is predicted to be of low significance.

Table 16-10: Extent and water requirements of the Kudu Solar Facility 2

Solar Facility	Size (MWac)	Construction Requirement (m³)	Operational Requirement (m³)
2	50	9000	1000

Impact 2: Potential Impact on Groundwater Quality as a result of Accidental Oil Spillages or Fuel Leakages

If there is an accidental oil spill or fuel leakage during the construction phase, then the low permeability of the unsaturated zone will provide significant attenuation capacity. The status of this impact (for the construction phase) is rated as negative with a site-specific spatial extent and short-term duration. The consequence and probability of the impact are respectively rated as slight and extremely unlikely. The reversibility of the impact is rated as high and the irreplaceability is rated as low. The significance of the impact without the implementation of mitigation measures is rated as very low.

A precautionary approach must be implemented and reasonable measures must be undertaken to prevent oil spillages and fuel leakages from occurring. During the construction phase, vehicles must be regularly serviced and maintained to check and ensure there are no leakages. Any engines that stand in one place for an excessive length of time must have drip trays. Diesel fuel storage tanks, if required, should be above ground on an impermeable concrete surface in a bunded area. Construction vehicles and equipment should also be refuelled on an impermeable surface. A designated area should be established at the construction site camp for this purpose, if

off-site refuelling is not possible. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, and reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.

With effective implementation of these prevention / mitigation actions, the impact of the project on groundwater as a consequence of accidental oil spillages and fuel leakages is predicted to be of very low significance.

Table 16-11: Impact Summary Tables: Construction Phase

Impact	Impact C	Criteria	Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
			C	ON	ISTRUCTION PHASE		
Lowering of	Status	Negative			Adhere to the borehole's safe yield and to monitor		
Lowering of	Spatial Extent	Local			water levels and flow.		
groundwater levels as a	Duration	Short Term		•	Boreholes must be correctly yield tested according to		High
result of	Consequence	Substantial	Moderate	-	the National Standard (SANS 10299-4:2003, Part 4 – Test pumping of water boreholes). This includes a Step Test, Constant Discharge Test and recovery monitoring.	Low	
over-	Probability	Likely					
abstraction	Reversibility	High					
aboli action	Irreplaceability	Low					
1	Status	Negative		t	Vehicles must be regularly serviced and maintained		
	Spatial Extent	Site Specific			to check and ensure there are no leakages. Any engines that stand in one place for an excessive length of time must have drip trays. Diesel fuel storage tanks, if required, should be above ground on an impermeable surface in a bunded area. Vehicles		
1	Duration	Short Term					
1	Consequence	Slight					
Accidental	Probability	Extremely Unlikely		an impermeable surface in a bunded area. Vehicles and equipment should also be refuelled on an			
oil	Reversibility	High					
spillage / fuel leakage	Irreplaceability	Low	Very Low		impermeable surface. A designated area should be established at the construction site camp for this purpose, if off-site refuelling is not possible. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, and reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes	Very Low	High

16.6.2 Potential Impacts during the Operational Phase

The impact table for the Operational Phase is presented in Table 16-12.

16.6.2.1 Impact 1: Groundwater impact as a result of over-abstraction from operational requirements

During the operational phase the peak requirement is estimated to be 1 000 m 3 /a (0.032 L/s) for the PV Facility (Table 16-10). Therefore, the groundwater requirement for the operational phase is within the yield potential of the underlying aquifer (0.5 – 2.0 L/s). It must be noted that the study area is known to experience extreme droughts and therefore even though the operational groundwater demand is within the yield potential of the aquifer, adherence to the mitigation measures during the operational phase is vital.

The status of this impact is rated as negative with a local spatial extent and a long-term duration (i.e. for the life of the project). The consequence and probability of the impact are respectively rated as substantial and likely. The reversibility of the impact is rated as high and the irreplaceability is rated low. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of prevention / mitigation actions (i.e. to adhere to the borehole's safe yield and to monitor water levels and flow), the impact of the proposed abstraction on groundwater is predicted to be of low significance.

16.6.2.2 Impact 2: Potential impact on groundwater quality as a result of using cleaning agents

The low permeability of the unsaturated zone will provide significant attenuation capacity. The status of this impact (for the operational phase) is rated as negative with a site-specific spatial extent and long-term duration (i.e. for the life of the project). The consequence and probability of the impact are respectively rated as slight and extremely unlikely. The reversibility of the impact is rated as high and the irreplaceability is rated as low. The significance of the impact without the implementation of mitigation measures is rated as very low. Recommended mitigation measures include using environmentally safe cleaning agents that breakdown naturally and do not cause adverse effects. With adherence to the proposed mitigation measures the significance of this impact would also be rated as very low.

16.6.2.3 Impact 3: Potential impact on groundwater quality as a result of electrolyte that will be used for the BESS

The proposed development will require a BESS at the facility. There are usually electrolytes of an environmentally harmful chemical composition that are used within the BESS, especially for Redox Flow BESS (whereas Lithium Ion BESS are solid state containerized systems). With any chemical storage there is always a risk of contamination to soils and groundwater. The status of this impact (for the operational phase) is rated as negative with a site-specific spatial extent and long-term duration (i.e. for the life of the project). The consequence and probability of the impact are respectively rated as substantial and very unlikely. The reversibility of the impact is rated as high and the irreplaceability is rated as low. The significance of the impact without the implementation of mitigation measures is rated as low. It is recommended that all BESS's are placed a minimum of 50m from any borehole and include effective bunding and secondary containment structures. With adherence to the proposed mitigation measures the significance of this impact would be rated as very low.

Table 16-12: Impact Summary Tables: Operational Phase

Impact	Impact Cr	iteria	Significance and Ranking (Pre- Mitigation)		Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
			0	PER	RATIONAL PHASE		
	Status	Negative			Adhere to the borehole's safe yield and to		
Lowering of	Spatial Extent	Local			monitor water levels and flow.		
groundwater	Duration	Long Term			Boreholes must be correctly yield tested		
levels as a	Consequence	Substantial	Moderate		according to the National Standard (SANS	Low	High
result of over-	Probability	Likely			10299-4:2003, Part 4 – Test pumping of water boreholes). This includes a Step Test, Constant Discharge Test and recovery monitoring.		
abstraction	Reversibility	High					
	Irreplaceability	Low					
	Status	Negative	Very Low		Use environmentally safe cleaning agents that breakdown naturally and do not cause adverse V effects.		High
Potential impact	Spatial Extent	Site Specific					
on groundwater	Duration	Long Term					
quality as a	Consequence	Slight				Very Low	
result of using cleaning agents	Probability	Extremely Unlikely				·	
	Reversibility	High					
	Irreplaceability	Low					
	Status	Negative			Ensure that all electrolyte or chemicals stored or		
Potential impact	Spotial Extent	Site			used on site have secondary containment		
on groundwater	Spatial Extent	Specific			systems in place with reliable leak detection,		
quality as a	Duration	Long Term			annunciation in place. Ensure that all chemicals		
result of	Consequence	Substantial	Low		are handled on concrete bunded surfaces and	Very Low	High
electrolyte that will be used for	Probability	Very Unlikely			not on bare soil. Any waste products produced from the BESS systems should be removed and disposed of appropriately.		-
the BESS	Reversibility	High					
	Irreplaceability	Low					

Impact	Impact Criteria	Significance and Ranking (Pre- Mitigation)	Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level		
	OPERATIONAL PHASE						
			Waste water produced by fire hydrants should not be allowed to runoff into the environment. It is recommended that all BESS's are placed a minimum of 50m from any borehole.				

16.6.3 Potential Impacts during the Decommissioning Phase

The impact table for the Decommissioning Phase is presented in Table 16-13.

16.6.3.1 Impact 1: Potential Impact on Groundwater Quality as a result of Accidental Oil Spillages or Fuel Leakages

During the decommissioning phase the main impact is linked to the potential for accidental oil spillages due to the machinery that will be used to decommission the site. The same applies as in the construction phase, therefore, if there is an accidental oil spill or fuel leakage during the decommissioning phase the low permeability of the unsaturated zone will provide significant attenuation capacity. The status of this impact (for the decommissioning phase) is rated as negative with a site-specific spatial extent and short-term duration. The consequence and probability of the impact are respectively rated as slight and extremely unlikely. The reversibility of the impact is rated as high and the irreplaceability is rated as low. The significance of the impact without the implementation of mitigation measures is rated as very low. A precautionary approach must be implemented and reasonable measures must be undertaken to prevent oil spillages and fuel leakages from occurring. During the decommissioning phase, vehicles must be regularly serviced and maintained to check and ensure there are no leakages. Any engines that stand in one place for an excessive length of time must have drip trays. Diesel fuel storage tanks, if required, should be above ground on an impermeable concrete surface in a bunded area. Vehicles and equipment should also be refuelled on an impermeable surface. A designated area should be established at the site camp for this purpose, if off-site refuelling is not possible. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, and reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes. With effective implementation of these prevention / mitigation actions, the impact of the project on groundwater as a consequence of accidental oil spillages and fuel leakages is predicted to be of very low significance.

16.6.3.2 Impact 2: Groundwater impact as a result of over-abstraction from decommissioning requirements

Although water requirements during the decommissioning phase were not specificized, it is unlikely that they will exceed the water requirements of the construction phase. As such, this potential impact has been evaluated at a potential maximum requirement of 9 000 m³/a (0.29 L/s). This requirement is within the expected capacity of the aquifer (0.5-2.0 L/s) therefore the risk associated to this impact is considered to be low. It must be noted that the study area is known to experience extreme droughts and therefore even though the construction groundwater demand is within the yield potential of the aquifer, adherence to the mitigation measures during the decommissioning phase is vital.

The status of this impact is rated as negative with a local spatial extent and a short-term duration (i.e. for the decommissioning phase). The consequence and probability of the impact are respectively rated as substantial and likely. The reversibility of the impact is rated as high and the irreplaceability is rated low. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of prevention / mitigation actions (i.e. to adhere to the borehole's safe yield and to monitor water levels and flow etc.), the impact of the proposed abstraction on groundwater is predicted to be of low significance.

Table 16-13: Impact Summary Tables: Decommissioning Phase

Impact	Impact Cı	riteria	Significance and Ranking (Pre-Mitigation)	Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level			
	DECOMMISSIONING PHASE								
	Status								
	Spatial Extent	Site Specific		to check and ensure there are no leakages. Any engines that stand in one place for an excessive					
	Duration	Short Term		length of time must have drip trays. Diesel fuel					
	Consequence	Slight		storage tanks, if required, should be above ground on an impermeable surface in a bunded area. Vehicles and equipment should also be refuelled on an impermeable surface. A designated area should be					
Accidental oil	Probability	Extremely Unlikely							
spillage /	Reversibility	High	Very Low		Very Low	High			
spillage / fuel leakage	Irreplaceability	Low	very Low	established at the site camp for this purpose, if off- site refuelling is not possible. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, and reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.					
Lauranina of	Status	Negative		Adhere to the borehole's safe yield and to monitor					
Lowering of	Spatial Extent	Local		water levels and flow.					
groundwater levels as a	Duration	Short Term		 Boreholes must be correctly yield tested according to 					
result of	Consequence	Substantial	Moderate	the National Standard (SANS 10299-4:2003, Part 4	Low	High			
over-	Probability	Likely		 Test pumping of water boreholes). This includes a 					
abstraction	Reversibility	High		Step Test, Constant Discharge Test and recovery					
	Irreplaceability	Low		monitoring.					

16.6.4 Potential Cumulative Impacts

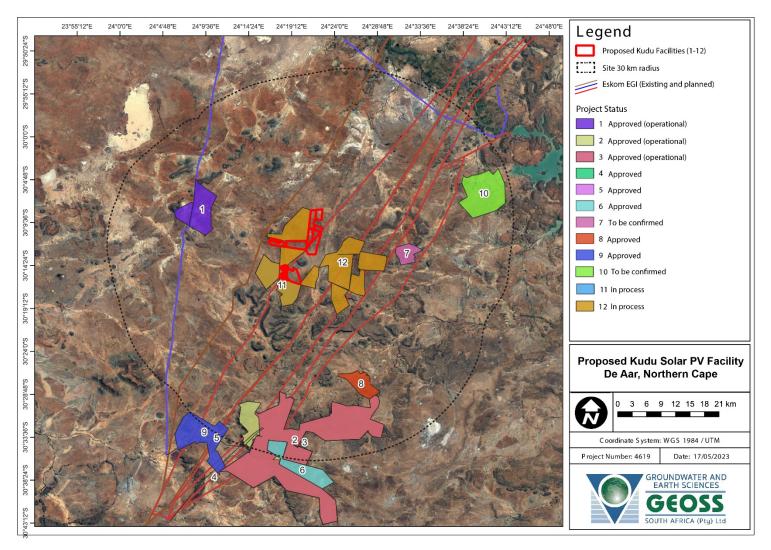
The cumulative impacts of the proposed Kudu Solar Facility and other approved and in process renewable energy facilities and electricity grid infrastructure (EGI) within a 30 km radius from the study area are presented in this section. The cumulative impacts identified include the impacts related to the construction, operational and decommissioning phases across proposed Kudu Solar Facility. In general, the impacts during the different phases of the project are quite similar, therefore, their intensities increase as the project progresses resulting in a higher probability for the impact to occur.

According to information collected by the CSIR from the Renewable Energy EIA Database and the South African Heritage Resources Information System (SAHRIS) (~February 2023), 12 other renewable energy facilities and EGI have been approved, or in the process of approval in terms of the NEMA EIA Regulations, that are located with a 30 km radius from the Kudu Solar Facilities (Map 16-10). Three of these renewable energy facilities are already existing and operational. In addition, approximately 10 existing Eskom power lines fall within the 30 km radius of the proposed project, with three Eskom planned power line projects, as shown in Map 16-10. Failing to implement effective mitigation measures throughout the lifespan of projects might cause the intensity of different identified impacts to increase. Appendix F of this chapter contains Table 16-19 covering the details of approved projects within a 30 km radius of the proposed Kudu Solar Facility as provided by the CSIR.

The types of impacts of these developments are nearly identical to each other, with the main cumulative effect being an increase in impact duration and likelihood for the construction, operational, and decommissioning phase. These increases are especially exacerbated for the construction phase, in the case that construction of all the proposed developments within a 30km radius occurs simultaneously. Of special concern is the cumulative effect of the proposed Odyssey and Crossroads Green Energy Cluster projects which fall within a 10 km radius of the Kudu Project. It must be reiterated that these projects are still in their Environmental Assessment Phases. The cumulative impact of all these developments during the operational phase should be quite low as long as the proposed mitigation measures and appropriate ground water monitoring is implemented.

The cumulative impacts include all the potential impacts discussed in section 16.6.1, 16.6.2, 16.6.3 and the potential impacts of other wind and solar, and EGI projects within a 30km radius, see Map 16-10 and Appendix F of this chapter. As such, the cumulative impacts are:

- Potential lowering of groundwater level during the construction and operational phase for all 12 of the proposed Kudu Solar PV facilities, Odyssey, and Crossroads projects.
- Potential of impact on groundwater quality as a result of accidental oil spillages or fuel leakages from the construction and the decommissioning phases for the proposed 12 Kudu Solar PV facilities, Keren Energy Odyssey, and Crossroads projects.
- Potential of impact on groundwater quality as a result of using cleaning agents for cleaning the solar panels during the operational phases for all 12 proposed Kudu Solar PV facilities, Keren Energy Odyssey, and Crossroads projects
- Potential impact on groundwater quality as a result of electrolyte that will be used for the BESS).
- Other wind and solar, and EGI projects within a 30 km radius.



Map 16-10: Map showing the proposed Kudu Solar PV Facility in relation to other local authorised, in process or operational renewable projects

16.6.4.1 Impact 1: Groundwater impact as a result of over-abstraction from construction, operation, and decommissioning requirements

As an overview and as noted above, water requirements for individual facilities divided based on their capacities (MWac) are as follows (Table 16-14):

- Kudu Solar Facilities 1, 2, 3, 4, 6, 9, 10 and 12 (i.e. those projects up to 150 MWac):
 - Construction Phase: 9 000 m³/a/facility (~0.29 L/s/facility).
 - Operational Phase: 1 000 m³/a/facility (~0.03 L/s/facility.
- Kudu Solar Facility 5, 7, 8 and 11 (i.e. those projects with a capacity of more than 150 MWac but up to 350 MWac):
 - Construction Phase: 18 000 m³/a/facility (~0.60 L/s/facility).
 - Operational Phase: 2 000 m³/a/facility (~0.06 L/s/facility).

During the construction phase, cumulatively across all facilities (1 to 12) this equates to 144 000 m³/a (~4.6 L/s) (Table 16-14). Thus, if all facilities are developed during the same year the proposed groundwater abstraction is higher than the yield potential of the underlying aquifer (0.5 – 2.0 L/s). However, it is unlikely that all 12 facilities will be developed in the same year and additionally, the extent over which the water will be required (and likely abstracted), is expected to reduce the volume required from any single borehole. Adherence to mitigation measures during the construction phase is vital. As mentioned earlier in the report, the use of existing boreholes to source groundwater (if available and suitable) is only the third most likely water use option. Water sourced from the municipality is the first option in terms of viability, but consideration of other options is vital.

During the operational phase, cumulatively across all facilities (1 to 12) this equates to 16 000 m 3 /a (\sim 0.5 L/s) (Table 16-14). Therefore, the groundwater requirement for the operational phase of all 12 projects is within the yield potential of the underlying aquifer (0.5 – 2.0 L/s). It must be noted that the study area is known to experience extreme droughts and therefore even though the operational groundwater demand is within the yield potential of the aquifer, adherence to the mitigation measures during the operational phase is vital.

Due to the large spatial extent (30 km radius), most of the other authorised facilities are more than 10 km from the Kudu Solar Facilities and will likely have little influence on the Kudu Solar Facility. This includes the associated power lines which have a low enough water requirement as to not greatly impact the geohydrological conditions of the region.

Of special concern would be the cumulative impact of the adjacent Odyssey and Crossroads Green Energy Cluster projects which, although still in the EIA phase, are within a 10 km radius of the Kudu Solar Project. Although no data on the expected water usage of the Crossroads and Odyssey projects was interrogated, generalised water requirements for Solar PV projects suggest that there is a much higher risk of over abstraction should all these projects be constructed simultaneously, as opposed to one at a time. In the event that construction of the Keren Energy Odyssey, Crossroads, and Kudu projects occurs simultaneously the cumulative impact is regarded as moderate significance without the implementation of mitigation measures. This impact has a variable duration dependent on whether the proposed sites are constructed simultaneously (short

term) or in several phases (medium term). In the event of multiple projects being constructed at the same time, the monitoring program needs to be strictly adhered to so as to prevent over abstraction. By adhering to the proposed mitigation measures the impact can be regarded as low significance.

During the operational phases the cumulative water use should still be below the regional groundwater yield; however, this interpretation is only based on generalised water requirements for Solar PV facilities.

For the operational phase, the impact is also rated as moderate significance before mitigation and low significance with mitigation, with the same mitigation measures discussed above.

Similar impact ratings have been provided for the decommissioning phase as for the operational phase.

Table 16-14: Summary of anticipated water requirements of solar facilities during construction and operational phases.

Facility	Size (MWac)	Construction (m3/a)	Operational (m3/a)	Construction (L/s)	Operational (L/s)
1	50	9000	1000	0,285	0,032
2	50	9000	1000	0,285	0,032
3	50	9000	1000	0,285	0,032
4	50	9000	1000	0,285	0,032
6	150	9000	1000	0,285	0,032
9	150	9000	1000	0,285	0,032
10	150	9000	1000	0,285	0,032
12	150	9000	1000	0,285	0,032
Cumulat	ive <150 MWac	72000	8000	2,283	0,254
5	350	18000	2000	0,571	0,063
7	350	18000	2000	0,571	0,063
8	350	18000	2000	0,571	0,063
11	330	18000	2000	0,571	0,063
Cumula	tive >150 <350 MWac	72000	8000	2,283	0,254
Cı	umulative	144000	16000	4,566	0,507

16.6.4.2 Impact 2: Potential Impact on Groundwater Quality as a result of Accidental Oil Spillages or Fuel Leakages during the construction and decommissioning phases

If there is an accidental oil spill or fuel leakage during any of the project phases, then the low permeability of the unsaturated zone will provide significant attenuation capacity. This potential cumulative impact is mainly limited to the construction and decommissioning phase of the development. The status of this impact is rated as negative with a site-specific spatial extent and a variable duration dependent on whether the proposed sites are constructed and decommissioned simultaneously (short term) or in several phases (medium term). The consequence and probability of the impact are respectively rated as slight and unlikely (phased construction/decommissioning)

to likely (simultaneous construction/decommissioning). The reversibility of the impact is rated as high and the irreplaceability is rated as low. The significance of the impact without the implementation of mitigation measures is rated as very low.

The mitigation measures for this impact are the same as that discussed above for the construction and decommissioning phases.

With effective implementation of these prevention / mitigation actions, the impact of the project on groundwater as a consequence of accidental oil spillages and fuel leakages is predicted to be of very low significance.

16.6.4.3 Impact 3: Potential impact on groundwater quality as a result of using cleaning agents during the operational phase

The low permeability of the unsaturated zone will provide significant attenuation capacity. The status of this impact is limited mostly to the operational phase, and is rated as negative with a site-specific spatial extent and long-term duration (i.e. for the life of the project). The consequence and probability of the impact are respectively rated as slight and unlikely. The reversibility of the impact is rated as high and the irreplaceability is rated as low. The significance of the impact without the implementation of mitigation measures is rated as very low. Recommended mitigation includes using an environmentally safe cleaning agent that breakdown naturally and do not cause adverse effects. With adherence to the proposed mitigation measures the significance of this impact would also be rated as very low.

16.6.4.4 Impact 4: Potential impact on groundwater quality as a result of electrolyte that will be used for the BESS during the operational phase

The status of this impact is limited primarily to the operational phase, and is rated as negative with a site-specific spatial extent and long-term duration (i.e. for the life of the project). The consequence and probability of the impact are respectively rated as substantial and unlikely. The reversibility of the impact is rated as high and the irreplaceability is rated as low. The significance of the impact without the implementation of mitigation measures is rated as moderate. It is recommended that all BESS's are placed a minimum of 50m from any borehole and include effective bunding and secondary containment structures. With adherence to the proposed mitigation measures the significance of this impact would be rated as low.

16.6.4.5 Concluding Cumulative Summary: Potential impacts during the construction, operational, and decommissioning phases of other wind and solar, and EGI projects within a 30 km radius.

When including each of the Kudu PV clusters as separate entities, a total of 22 renewable power projects are either operational, proposed, or in the environmental approval phase within a 30 km radius of the Kudu Solar PV 2 (see Appendix F). Of these only the Cross Roads Green Energy Cluster and Keren Energy Odyssey Solar PV Facilities (environmental approval in process for both) are within 10 km radius of the Kudu Solar Facility (should Environmental Authorisations be granted). Accordingly, only these projects would be considered to have an appreciable cumulative impact on the underlying aquifer. Both these projects are solar PV projects and, therefore, have very similar impacts to those of the Kudu Solar Facility, namely over abstractions of groundwater, and potential aquifer contamination from oil spills, solar panel cleaning agents, and electrolytes from associated BESS infrastructure. The mitigations for each of these impacts is discussed in the subsections above.

16.6.4.6 Impact Summary Tables: Cumulative Impacts

Impact	Impad	ct Criteria	Significance and Ranking (Pre-	Potential mitigation measures	Significance and Ranking (Post-	Confidence
			Mitigation)		Mitigation)	Level
			CO	NSTRUCTION PHASE		
	Status	Negative		Adhere to the borehole's safe yield and to monitor		
Lowering of	Spatial Extent	Local		water levels and flow. Boreholes must be correctly		
groundwater levels as a	Duration	Short Term to Medium Term		yield tested according to the National Standard (SANS 10299-4:2003, Part 4 – Test pumping of	Low	
result of	Consequence	Substantial	Moderate	water boreholes). This includes a Step Test,		High
over-	Probability	Likely		Constant Discharge Test and recovery monitoring.		
abstraction	Reversibility	High		 A monitoring program needs to be adhered to so as to determine and remain below safe abstraction 		•
	Irreplaceability	Low		rates.		
	Status	Negative		 Vehicles must be regularly serviced and maintained 		
	Spatial Extent	Site Specific		to check and ensure there are no leakages. Any		
	Duration	Short term to Medium Term		engines that stand in one place for an excessive length of time must have drip trays. Diesel fuel		
	Consequence	Slight	1	storage tanks, if required, should be above ground		
	Probability	Unlikely to Likely		on an impermeable surface in a bunded area.		
Accidental	Reversibility	High		Vehicles and equipment should also be refuelled on an impermeable surface. A designated area should		
oil spillage / fuel leakage	Irreplaceability	Low	Very Low	be established at the construction site camp for this purpose, if off-site refuelling is not possible. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, and reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.	Very Low	High

Impact	Impact Criteria		Significance and Ranking (Pre- Mitigation)	Potential mitigation measures	Significance and Ranking (Post- Mitigation)	Confidence Level			
	OPERATIONAL PHASE								
	Status	Negative		 Adhere to the borehole's safe yield and to monitor 					
Lowering of	Spatial Extent	Local		water levels and flow. Boreholes must be correctly					
groundwater	Duration	Long Term		yield tested according to the National Standard					
levels as a	Consequence	Substantial] ., , ,	(SANS 10299-4:2003, Part 4 – Test pumping of					
result of	Probability	Likely	Moderate	water boreholes). This includes a Step Test,	Low	High			
over-	Reversibility	High		 Constant Discharge Test and recovery monitoring. A monitoring program needs to be adhered to so as to determine and remain below safe abstraction rates. 					
abstraction	Irreplaceability	Low							
Potential	Status	Negative							
impact on	Spatial Extent	Site Specific	Very Low						
groundwater	Duration	Long Term		 Use environmentally safe cleaning agents that breakdown naturally and do not cause adverse effects. 					
quality as a	Consequence	Slight			Very Low	High			
result of	Probability	Unlikely			,	9			
using	Reversibility	High							
cleaning agents	Irreplaceability	Low							
	Status	Negative		Ensure that all electrolyte or chemicals stored or					
Potential	Spatial Extent	Site Specific		used on site have secondary containment systems					
impact on	Duration	Long Term		in place with reliable leak detection, annunciation in					
groundwater	Consequence	Substantial		place. Ensure that all chemicals are handled on					
quality as a	Probability	Unlikely		concrete bunded surfaces and not on bare soil.					
result of	Reversibility	High	Moderate	Any waste products produced from the BESS	Low	High			
electrolyte that will be used for the BESS	Irreplaceability	Low		systems should be removed and disposed of appropriately. Waste water produced by fire hydrants should not be allowed to runoff into the environment. It is recommended that all BESS's are placed minimum of 50m from any borehole.		-			

Impact	Impact Criteria		Significance and Ranking (Pre- Mitigation)	Potential mitigation measures	Significance and Ranking (Post- Mitigation)	Confidence Level
	DECOMMISSIONING PHASE					
	Status Negative Spatial Extent Site Specific Short to Medium Term		Vehicles must be regularly serviced and maintained to check and ensure there are no leakages. Any engines that stand in one place for an excessive length of time must have drip trays. Diesel fuel storage tanks, if required, should be above ground			
Accidental oil	Consequence Probability	Slight Unlikely to Likely		on an impermeable surface in a bunded area. Vehicles and equipment should also be refuelled on		High
	Reversibility	High	Very Low	an impermeable surface. A designated area should	Very Low	
spillage / fuel leakage	Irreplaceability	Low	Very Low	be established at the site camp for this purpose, if off-site refuelling is not possible. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, and reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.	very Low	riigii
	Status	Negative		 Adhere to the borehole's safe yield and to monitor 		
Lowering of	Spatial Extent	Local		water levels and flow. Boreholes must be correctly		
groundwater levels as a	Duration	Short Term to Medium Term		yield tested according to the National Standard (SANS 10299-4:2003, Part 4 – Test pumping of		
result of	Consequence	Substantial	Moderate	water boreholes). This includes a Step Test,	Low	High
over-	Probability	Likely		Constant Discharge Test and recovery monitoring.		
abstraction	Reversibility	High		A monitoring program needs to be adhered to so as		
	Irreplaceability	Low		to determine and remain below safe abstraction rates.		

16.6.5 No-go Alternatives

The potential groundwater impacts of the No-go alternative for the proposed Kudu PV Solar Facility 2 are also considered. Presently, the sites proposed for development is used mainly for agricultural purposes, i.e. open fields for grazing of various types of livestock. In the scenario that the PV facility did not go ahead it would be expected that these activities would continue and represents the baseline against which other impacts can be compared.

The farm portions where Kudu PV Solar Facility 2 is proposed does not currently utilize significant volumes of groundwater and small-scale abstraction is predominantly for domestic purposes. As such the No-go alternative does not represent a risk to groundwater or aquifer depletion.

However, as noted above, there is a low water demand in the study area and a large spatial extent; and the impacts relating to the use of ground water are not considered to be very significant, especially if the projects are planned and phased suitably.

16.6.6 Battery Energy Storage System

As noted above, Lithium-Ion BESS and Redox Flow BESS were both considered for the proposed project. For Redox Flow BESS, various chemical compositions are likely, such as Vanadium. Refer to Chapter 15 of this EIA Report for a High-Level Safety, Health and Environment Risk Assessment, which provides high level information on the safety, health and environmental risks of the BESS technologies.

Both BESS technologies have been considered in this assessment. The risks associated with each individual technology is such that, with strict adherence to the appropriate mitigation measures, both technologies will have little risk to the local hydrogeological system. Furthermore, no fatal flaws of either technology with respect to the geohydrological system have been identified. Considering this, both Lithium Ion BESS and Redox Flow BESS are considered suitable and no preference is given to either one.

16.7 Impact Assessment Summary

The overall impact significance findings, following the implementation of the proposed mitigation measures are shown in Table 16-15.

Table 16-15: Overall Impact Significance

Phase	Overall Impact Significance (Pre-Mitigation)	Overall Impact Significance (Post Mitigation)
Construction	Moderate to Very Low	Low-Very Low
Operational	Moderate to Very Low	Low-Very Low
Decommissioning	Very Low	Very Low
Nature of Impact	Overall Impact Significance (Pre-Mitigation)	Overall Impact Significance (Post Mitigation)
Cumulative - Construction	Moderate to Very Low	Low-Very Low
Cumulative - Operational	Moderate to Very Low	Low-Very Low
Cumulative - Decommissioning	Very Low	Very Low

The cumulative demands of simultaneous construction (\sim 4.6 L/s) for all twelve planned Kudu Solar Facilities exceeds the regional yield potential of the underlying aquifer (0.5 – 2.0 L/s). The will also likely be the case should construction of the surrounding Keren Energy Odyssey Solar PV Facilities and the Crossroads Green Energy Cluster occur at the same time as construction of the Kudu Solar Facilities. In the event that construction of the above-mentioned projects occurs at the same time, adherence to the recommended mitigation measures should be strictly followed to prevent over abstraction.

The cumulative impacts on groundwater quality due to the construction and operation of the PV facilities for the Kudu Solar Facility are considered Low to Very Low, provided that responsible construction practices are adopted, and the proposed mitigation measures are utilized; for example, use of environmentally cleaning agents.

16.8 Legislative and Permit Requirements

The NWA is administered by the DWS and is the main legislation for managing water resources in South Africa. The purpose of the NWA is to provide a framework for the equitable allocation and sustainable management of water resources. Both surface and groundwater sources are redefined by the Act as national resources which cannot be owned by any individual, and rights to which are not automatically coupled to land rights, but for which prospective users must apply for authorization and register as users. The NWA also provides for measures to prevent, control and remedy the pollution of surface and groundwater sources.

The proposed project is located mainly within quaternary catchment D33B with small sections within quaternary catchment D62F. Both of these quaternary catchments from part of the Lower Orange Water Management Area in the Northern Cape. The groundwater General Authorisation (GA) for both of the catchments is 45 m³/ha/a (published on 2 September 2016, in Government Gazette 40243, Government Notice (GN) 538 (i.e. Revision of General authorisation for the taking and storing of water)). The farm portions with the associated hectares and allowable abstraction under GA is presented in Table 16-16. The allowable abstraction under the GA is capped at 40 000

m³/a per farm portion and therefore the majority of the farm portions are capped at 40 000 m³/a due to the size.

The total allowable volume of groundwater the project can abstract within the GA is 234 650 m³/a which is higher than the peak requirement during the construction phase of 144 000 m³/a for all 12 Kudu Solar Facilities (Table 16-16). Therefore, if the project is planned appropriately with regards to groundwater use, all the water can be obtained from groundwater, with the use being Generally Authorised. Registration of the usage in terms of the GA with DWS would be required. Alternatively, to source all the water from the Remaining Extent of Portion 3 of the Farm Bas Berg No. 88, a Water Use License Application will be required to meet the demands of the construction period. In the case of water storage, a total of 2000 m³/a can be stored on the property in an open container.

Table 16-16: Farm portions affected by the proposed Kudu Solar Facilities; relevant portion highlighted in blue.

Farm Portion Name	Size (ha)	Kudu Solar 1	Kudu Solar 2	Kudu Solar 3	Kudu Solar 4	Kudu Solar 5	Kudu Solar 6	Kudu Solar 7	Kudu Solar 8	Kudu Solar 9	Kudu Solar 10	Kudu Solar 11	Kudu Solar 12	Allowable abstraction under GA (m3/a)	Anticipated requirement during construction m3/a
Remaining Extent of Farm Bas Berg No. 88 (Two Sections)	770	(75%) of 9000 m³/a	50% of 9000 m³/a											34 650	11 250
Remaining Extent of Portion 3 of the Farm Bas Berg No. 88	7687	25% of 9000 m ³ /a	50% of 9000 m³/a	100% of 9000 m ³ /a	100% of 9000 m³/a	100% of 18000 m³/a								40 000	42 750
Remaining extent of Portion 2 (Middel Plaats) (a portion of Portion 1) of the farm Grasspan No. 40	1054						100% of 9000 m³/a	100% of 18000 m ³ /a						40 000	27 000
Portion 1 (Wolve Kuil West) of the farm Annex Wolve Kuil No. 41	1707								75% of 18000 m³/a	100% of 9000 m ³ /a	100% of 9000 m ³ /a	75% of 18000 m³/a		40 000	45 000
Remaining extent of the farm Annex Wolve Kuil No. 41	1128								25% of 18000 m ³ /a					40 000	4 500
Portion 2 of the farm Wolve Kuil No. 43	1238											25% of 18000 m³/a	100% of 9000 m ³ /a	40 000	13 500
		-	-										Total	234 650	144 000

16.9 Environmental Management Programme Inputs

Potential environmental impacts pertaining to local groundwater resources have been considered in this EIA. In order to ensure safe and sustainable management of the groundwater resources in the area, several management inputs will be required. These inputs are, however, not required as part of the EIA phase and will <u>only be required</u> once the final operational conditions of the project are confirmed <u>post environmental authorisation</u>. Phase 1 will be required to determine if the groundwater is of a suitable quality and quantity; and Phase 2 will only be required if the groundwater quality and quantity are confirmed suitable for use. Additional information is provided below.

Phase 1: Determining if the groundwater is of a suitable quality and quantity:

- Undertake a full laboratory analysis to confirm that the groundwater can be used for potable and domestic purposes, and determine the treatment required. This Geohydrology Assessment has confirmed that the groundwater is generally of good quality in terms of pH, EC and TDS.
- 2. The water quality is not considered suitable for panel washing as it will result in salts precipitating on the panels. The salts could be removed from the groundwater by thermal distillation (i.e. boiling since salt has a much higher boiling point than water) or by membrane separation (commonly reverse osmosis). Confirm what mechanisms could be used to remove the salts from the groundwater for panel cleaning. This will entail undertaking a financial viability investigation / feasibility study.
- 3. Undertake necessary tests to confirm if the groundwater is suitable for construction and concrete batching.
- 4. Conduct scientific yield tests to determine sustainable abstraction volumes from boreholes that are to be utilised.

Phase 2: Once the groundwater quality and quantity are determined more accurately and confirmed it is suitable for use the follow steps are required for sustainable management:

- 1. Acquire any historical monitoring data for the region.
- 2. Determine the volume of groundwater abstracted by farmers annually prior to construction by flow meters.
- 3. Ensure water saving techniques are instated and adhered to.
- 4. Ensure that proper bunding and secondary containment measures are in place for BESS facilities and are designed by an appropriate competent person.
- 5. Ensure that environmentally safe cleaning agents that breakdown naturally and do not cause adverse effects are used.
- In the event that the entire Kudu Solar Facility development is constructed simultaneously, adherence to the recommended mitigation measures should be strictly followed to prevent over-abstraction.
- 7. Instate an appropriate monitoring program including monitoring of groundwater quality, water levels (ideally by water level loggers and hand readings using a dip meter), and abstracted volumes. These data should be reported on at the least biannually.

8. Yield test all monitoring boreholes according to SANS 10299-4:2003, Part 4 – Test pumping of water boreholes. This includes a Step Test, Constant Discharge Test and recovery monitoring.

16.9.1 Proposed Monitoring Plan:

It is recommended that at least three boreholes in the vicinity of each cluster of projects be allocated for monitoring purposes. These can either be existing boreholes, or newly drilled monitoring boreholes as this will allow for monitoring of the groundwater quality and groundwater levels across the affected area. The optimum position of the monitoring boreholes should be based on availability of open space surrounding the planned buildable area; however, it is recommended that one borehole be located up-gradient of the affected area to monitor background values and the other two boreholes be downgradient of the affected area. Three general monitoring sites are presented in Table 16-17, however these are in an idealised scenario and any existing boreholes in the vicinity of the proposed sites can be utilised for monitoring purposes. Furthermore, one or more monitoring boreholes should present within 100 meters of notable contamination points (i.e. BESS and refuelling stations) as well as near project specific groundwater abstraction points. The borehole water level (if present) and the groundwater quality should be monitored on a monthly basis during construction phase and then on a quarterly basis during operational phase, so as to determine seasonal fluctuation. The implementation of the groundwater monitoring programme will be important for assessing any impacts of the Kudu Solar Facility on groundwater and the environment.

It is recommended that groundwater monitoring be undertaken at the proposed site in accordance with guidelines set out in the publication by DWAF (1998). The various aspects of the monitoring are presented in this section, along with relevant recommendations.

Table 16-17:	General locations for pr	oposed monitoring points.

Site_ID	Latitude (DD, WGS84)	Longitude (DD, WGS84)
K1M_01	-30,23785	24,30997
K1M_02	-30,26389	24,29734
K1M_03	-30,27589	24,33460

In the case that new monitoring boreholes are drilled, the drilling should be supervised by a geohydrologist and drill samples should be collected every 1 metre and logged. Additional information should also be collected such as the depth of water strikes, associated water strike yields and groundwater quality. This is crucial information for the optimal design of the boreholes. The driller should be supervised to ensure all site requirements are met. A graphical representation of a proposed borehole construction is presented in Figure 16-4; the exact construction will, however, be unique for the borehole. It is not anticipated that multiple aquifers will be present in the bedrock. The inner diameter of the uPVC casing must not be less than 110 mm.

A gravel pack should be installed with an annulus of about 12 mm. The boreholes should be developed with compressed air for at least two hours upon completion along with an airlift test to

estimate the yield of the borehole. Each borehole must be protected with a concrete block or a protected manhole if there is traffic in the area. Each borehole also needs a permanent plate glued to the lid containing the details pertaining to the borehole. A bentonite plug of at least 500 mm needs to be installed at the top of the hole to prevent ingress of surface water.

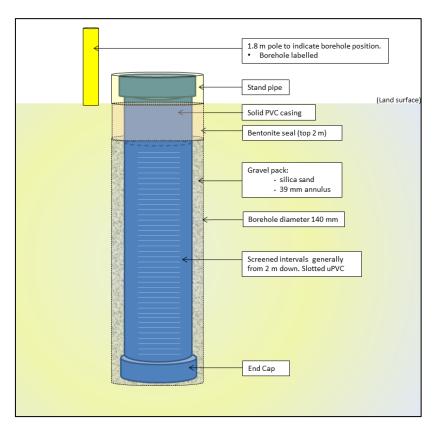


Figure 16-4: Schematic representation of the proposed general borehole construction.

16.9.1.1 Groundwater Level Monitoring

Groundwater level measurements are recommended for the monitoring boreholes at the study site. A dip meter can be used to measure the water level below the top of the borehole collar/casing height (mbch). The height of the collar/casing height must then also be measured (m). The water level (metres below ground level (mbgl)) can then be calculated by subtracting the collar/casing height from the water level (mbch). The value must be recorded along with the date and time of measurement. An interface meter can be used during monitoring to detect the presence of non-aqueous phase liquids (if present).

16.9.1.2 Groundwater Quality Monitoring

It is preferable to use a low volume sampling pump in most monitoring boreholes. Prior to sampling, the groundwater should be pumped through a flow-through cell until field chemistry parameters have stabilised.

16.9.1.3 Sample Collection, Preservation and Submission

Sample bottles must be labelled with the site name, borehole name and date. At the time of sampling, field chemistry parameters must be measured and recorded. These include electrical conductivity (EC), oxidation reduction potential (ORP), pH, temperature and dissolved oxygen (DO). During sampling, disposable nitrile gloves should be worn to minimise the transfer of any potential contaminants. Nitrile gloves should be dedicated to a sampling location and disposed of after use. Samples must be collected in an appropriate sampling container and preserved in the correct manner prior to submission to an accredited laboratory for the analysis parameters. The sample method and preservation must be discussed with the laboratory prior to sampling.

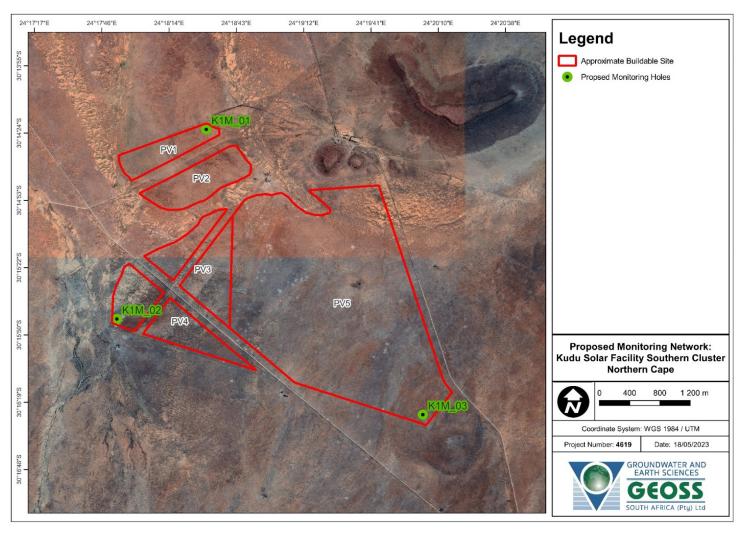
16.9.1.4 Monitoring Frequency and Parameter Analysis

In order to best understand and monitor the site, it is recommended that monthly water level measurements be taken to determine seasonal fluctuation during the construction period, after which water level measurements can be taken at quarterly intervals during the operational phase. Further to this, water quality measurements should be taken on a quarterly basis during the construction phase, after which water quality measurement can be taken on a bi-annual basis during the operational phase. The monitoring schedule can be reviewed and revised upon the start of the decommissioning phase. Table 16-18 indicates the potential parameters for the analysis.

Table 16-18: Proposed groundwater monitoring parameters and their recommended frequency.

Parameter	Frequency							
	K1M_01	K1M_02	K1M_03					
Groundwater Level	Monthly (Construction Phase)	Monthly (Construction Phase)	Monthly (Construction Phase)					
	Quarterly (Operational Phase)	Quarterly (Operational Phase)	Quarterly (Operational Phase)					
рН	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)					
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)					
Electrical conductivity (EC)	Quarterly (Construction Phase)	Quarterly (Construction Phase) Bi-	Quarterly (Construction Phase) Bi-					
	Bi-annually (Operational Phase)	annually (Operational Phase)	annually (Òperational Phase)					
Total Dissolved Solids (TDS)	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)					
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)					
Alkalinity	Quarterly (Construction Phase) Bi-	Quarterly (Construction Phase) Bi-	Quarterly (Construction Phase)					
	annually (Operational Phase)	annually (Operational Phase)	Bi-annually (Operational Phase)					
Total Organic Carbon (TOC)	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)					
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)					
Benzene	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)					
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)					
Toulene	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)					
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)					
Ethylene	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)					
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)					
Xylene	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)					

Parameter	Frequency								
i urumoto.	K1M_01	K1M_02	K1M_03						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Gasoline Range Organics	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
(GRO)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Extractible Petroleum	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
Hydrocarbons (EPH)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Volatile Organic Compounds	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
(VOC)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Cd	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Cr	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Cu	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Fe	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Ni	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
Zn	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						
V	Quarterly (Construction Phase)	Quarterly (Construction Phase)	Quarterly (Construction Phase)						
	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)	Bi-annually (Operational Phase)						



Map 16-11: Proposed monitoring borehole locations from an aerial view.

16.10 Final Specialist Statement and Authorisation Recommendation

16.10.1 Statement and Reasoned Opinion

The Geohydrology Assessment conducted for the Kudu Solar PV 2 facility came to the following main conclusions:

- The anticipated demands of this facility are less than the regional yield potential of the underlying aquifer (0.5 2.0 L/s).
- HBH1 and HBH24 are potentially viable sources of groundwater for the development of Solar Facility 2. The use of this/these borehole/s would/will depend on the operational requirements of the facility, negotiations with the landowners and proximity to the facility.
- The demand for the facility could potentially be met by abstraction from Remaining Extent of Portion 3 of the Farm Bas Berg No. 88 under General Authorisation. However, if Solar Facilities 2, 3, 4 and 5 are constructed at the same time, cumulatively, the water demands during the construction period will exceed the available GA volume of the farm portion. Therefore, groundwater exploration (including hydrocensus, lineament mapping and geophysics) on adjacent properties should be undertaken for additional supply to meet the demands. Alternatively, to source all the water from this farm portion, a Water Use License Application will be required to meet the demands of the construction period.
- The cumulative demands of construction (~4.6 L/s) for all twelve planned Kudu Solar Facilities (if developed simultaneously) exceeds the regional yield potential of the underlying aquifer (0.5 – 2.0 L/s). Since yield information was not available during the undertaking of the hydrocensus, estimations for groundwater supply capacity for the area are based on regional datasets.
- The study site has been classified as overlying low yielding aquifer with a groundwater vulnerability classification of "low/medium" to medium and a sensitivity rating of "medium" with no areas that need to be avoided.
- Both the potential individual and cumulative impacts from the construction, operation, and decommissioning phases for of the development are considered as Low to Very Low with appropriate mitigation.

Given these conclusions it is the opinion of the specialist that development of the proposed Kudu Solar Facility be authorised to proceed given that proper mitigation measures highlighted within this document are implemented during each phase of the project to suppress the intensity of identified impacts.

16.10.2 EA Condition Recommendations

From the impact assessment it is evident that the development will have a very low to low impact on the local geohydrological system as long as the recommended mitigation measures are adhered to. As such, the project is authorised to continue from a geohydrological perspective on condition of implementation of the following recommendations:

- In the case that multiple projects are constructed simultaneously, adherence to recommended mitigation measures should be strictly followed to prevent over abstraction.
- Phase two of the monitoring plan is to be discussed and evaluated in the event that groundwater is to be used in the project.
- The proposed monitoring plan should be followed with a special focus on groundwater level monitoring to ensure that the aquifer is not over abstracted and falls to levels below historic borehole depths.
- All proposed impact mitigation measures are to be implemented during the development of the project. These include the use of environmentally safe cleaning agents, the construction of BESS facilities 50m from any boreholes along with appropriate bunding and secondary containment, and the recommended precautionary approaches aimed at preventing oil spills and fuel leaks.

16.11 References

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APPENDICES

APPENDIX A - SPECIALIST EXPERTISE

<u>CURRICULUM VITAE – LOUIS JONK</u>

GENERAL

Nationality: South African

Profession: Geotechnical Specialist

Specialization: Soil classification for engineering purposes. Groundwater exploration and

sampling.

Position in firm: Geotechnical Geologist at GEOSS – South Africa (Pty) Ltd.

Date commenced: 09 January 2023

Year of birth & ID #: 1993 – 9307215060088

Language skills: English (good – speaking, reading, and writing)

Afrikaans (good - speaking, reading, and writing).

KEY SKILLS

- Geotechnical investigations
- Compilation of factual reports.
- Field mapping.
- Soil and rock profiling.
- Material classification and material use determination.
- Supervision of geotechnical contractors.
- ArcGIS, QGIS, Python, FLAC/SLOPE; HotPlot

EDUCATIONAL AND PROFESSIONAL STATUS

Qualifications

2018	M.Sc. (Geology – Cum Laude)	University of the Stellenbosch, South Africa
2015	B.Sc. Hons. (Earth Science)	University of the Stellenbosch, South Africa
2014	B.Sc. (Geology: Earth Science)	University of the Stellenbosch, South Africa

EMPLOYMENT RECORD

Jan 2023 to present GEOSS South Africa (Pty) Ltd, South Africa
April 2020 to Dec 2022 Council for Geoscience South Africa

April 2018 to March 2020 Iziko Museums of South Africa

<u>CURRICULUM VITAE – SHANE TEEK</u>

GENERAL

Nationality: South African

Profession: Geotechnical Specialist & Hydrogeologist

Specialization: Soil classification for engineering purposes. Groundwater exploration and

sampling.

Position in firm: Geotechnical Geologist & Hydrogeologist at GEOSS – South Africa (Pty) Ltd.

Date commenced: 17 July 2021

Year of birth & ID #: 1994 – 9404135162084

Language skills: English (good – speaking, reading, and writing)

Afrikaans (good - speaking, reading, and writing).

KEY SKILLS

- Geotechnical investigations
- Compilation of factual reports.
- Field mapping.
- Soil and rock profiling.
- Material classification and material use determination.
- Supervision of geotechnical contractors.
- Groundwater geophysics and conducting hydrocensus studies.
- Groundwater development borehole drilling and test pumping supervision and analysis.
- Groundwater monitoring development and analysis of groundwater level and quality data.
- Groundwater management sustainable aquifer development and management.
- Groundwater contamination assessments.
- ArcGIS, QGIS, Python, FLAC/SLOPE, Midas GTS NX.

EDUCATIONAL AND PROFESSIONAL STATUS

Qualifications

2021	M.Eng. (Civil Engineering – Cum Laude)	University of the Stellenbosch, South Africa
2016	B.Sc. Hons. (Earth Science)	University of the Stellenbosch, South Africa
2015	B.Sc. (Geology: Earth Science)	University of the Stellenbosch, South Africa

Memberships

- Geological Society of South Africa Member No. 970413
- South African Council for National Scientific Professions (SACNASP) Mem. No. 126397/20
- Founding member of the UNESCO Groundwater Youth Network (GWYN)

EMPLOYMENT RECORD

July 2021 to present	GEOSS South Africa (Pty) Ltd, South Africa
Jan 2020 to June 2021	Geotechnics Africa Western Cape, South Africa
Feb 2019 to July 2019	Polytechnique Montréal, Canada
Jan 2017 to Dec 2017	Remote Exploration Services, South Africa.

<u>CURRICULUM VITAE – DALE BARROW</u>

GENERAL

Nationality: South African Profession: Hydrogeologist

Firm: GEOSS South Africa (Pty) Ltd Position: Director and Hydrogeologist

Specialization: Groundwater exploration, development, management and monitoring

including numerical modelling. Hydrogeological impact studies and

assessment of groundwater - surface water interaction.

Date commenced: February 2008

Year of birth & ID #: 1985 – 851205 5227 082

Language skills: English (mother tongue), Afrikaans (average)

KEY SKILLS

Qualifications

- Project Management
- Hydrogeological technical input on projects
- Groundwater surface water interaction assessment
- Groundwater exploration (aerial photo interpretation, resistivity, magnetic and EM34 geophysical surveys for borehole siting purposes, geological conceptualization)
- Groundwater development borehole drilling and test pumping supervision and analysis.
- Groundwater monitoring –development and analysis of groundwater level and quality data.
- Groundwater management sustainable aquifer development and management.
- Numerical modelling of groundwater flow and mass transport.
- Groundwater component of Catchment Management Strategies and other Groundwater Resource Directed Measures.
- Groundwater contamination assessments.
- GIS / WISH and GW Vistas and typical software skills.

EDUCATIONAL AND PROFESSIONAL STATUS

Q G G III I	<u> </u>				
2017	MBA (Cum Laude)	University of Stellenbosch, South Africa			
2010	M.Sc. (Geohydrology)	University of the Free State, South Africa			
2007	B.Sc. (Hons) Structural Geology	University of Stellenbosch, South Africa			
2006	B.Sc. Geology – Applied Earth Science	University of Stellenbosch, South Africa			
<u>Course</u>	<u>'S</u>				
2019	Water Governance in South Africa: IWRM, the	NWA, and water use authorizations, focusing			
	on WULAs and IWWMPs. WISA accredited. Carin Bosman (CBSS)				
2016	SPRING Software Modelling Course				
2015	European Management Residency in Economics and Business (Maastricht University School				
	of Business and Economics)				
2013	Aquifer Firm Yield; Wellfield Design; Wellfield costing				
2010	Introduction to QGIS (GISSA)				
2010	Presentation Skills (Elsabé Daneel productions cc)				
2009	Introduction to Isotope Hydrology in Southern Africa (GSSA)				
2009	Aquifer Mechanics (IGS-UOFS)				

ENVIRONMENTAL IMPACT ASSESSMENT REPORT: Scoping and Environmental Impact Assessment (EIA)
Process for the Proposed Development of a Solar Photovoltaic (PV) Facility (Kudu Solar Facility 2) and
associated infrastructure, near De Aar, Northern Cape Province

2009	Groundwater Chemistry (IGS-UOFS)
2009	Groundwater Geophysics (IGS-UOFS)
2009	Groundwater Modelling (IGS-UOFS)
2009	Groundwater Management (IGS-UOFS)

Memberships

- Groundwater Division of the Geological Society of South Africa
- South African Council for National Scientific Professions (SACNASP) Mem. No. 400289/13

EMPLOYMENT RECORD

1 February 2008 to present:	GEOSS – Geohydrological and Spatial Solutions International (Pty)
	Ltd, Stellenbosch
23 July 2018 - November 2019	Design and part time lecturing of the Hydrogeology course for 3 rd year
	students at Stellenbosch University

APPENDIX B - SPECIALIST STATEMENT OF INDEPENDENCE



DETAILS OF THE SPECIALIST, DECLARATION OF INTEREST AND UNDERTAKING UNDER OATH

File Reference Number:
NEAS Reference Number:
Date Received:

(For official us	e only)	4-2
DEA/EIA/		

Application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

PROJECT TITLE

Scoping and Environmental Impact Assessment Processes for the Proposed Development of 12 Solar Photovoltaic (PV) Facilities and associated infrastructure (i.e. Kudu Solar Facility 1 - 12), near De Aar, Northern Cape

Kindly note the following:

- This form must always be used for applications that must be subjected to Basic Assessment or Scoping & Environmental Impact Reporting where this Department is the Compelent Authority.
- This form is current as of 01 September 2018. It is the responsibility of the Applicant / Environmental Assessment Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the The latest available Departmental templates are available at Competent Authority. https://www.environment.gov.za/documents/forms.
- A copy of this form containing original signatures must be appended to all Draft and Final Reports submitted to the department for consideration.
- All documentation delivered to the physical address contained in this form must be delivered during the official Departmental Officer Hours which is visible on the Departmental gate.
- All EIA related documents (includes application forms, reports or any EIA related submissions) that are faxed; emailed; delivered to Security or placed in the Departmental Tender Box will not be accepted, only hardcopy submissions are accepted.

Departmental Details

Postal address:

Department of Environmental Affairs

Attention: Chief Director: Integrated Environmental Authorisations

Private Bag X447

Pretoria

0001

Physical address:

Department of Environmental Affairs

Attention: Chief Director: Integrated Environmental Authorisations

Environment House

473 Steve Biko Road

Arcadia

Queries must be directed to the Directorate: Coordination, Strategic Planning and Support at:

Email: EIAAdmin@environment.gov.za

Details of Specialist, Declaration and Undertaking Under Oath

Page 1 of 3

SPECIALIST INFORMATION

Specialist Company Name:	GEOSS SOUTH AFRICA (PT	Y) LTD				
B-BBEE	Contribution level (Indicate 1	3	Percentage	110%		
	to 8 or non-compliant)		Procuremen	t		
		<u></u>	recognition			
Specialist name:	SHANE TEEK					
Specialist Qualifications:	MEng – Civil Engineering					
Professional	SACNASP: 126397					
affiliation/registration:						
Physical address:	Unit 12, Techno Stell Bldg, 09 Quantum Street, Techno Park, Stellenbosch					
Postal address:	PO Bo12412, Die Boord, Stellenbosch					
Postal code:	7613	Cell	: 0	9 183 7782		
Telephone:	021 880 1079	Fax	:n/	a		
E-mail:		_				

2. DECLARATION BY THE SPECIALIST

I, SHANE TEEK, declare that -

- I act as the independent specialist in this application;
- I will perform the work relating to the application in an objective manner, even if this results in views and findings
 that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act,
 Regulations and any guidelines that have relevance to the proposed activity;
- I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information. In my possession that
 reasonably has or may have the potential of influencing any decision to be taken with respect to the application by
 the competent authority; and the objectivity of any report, plan or document to be prepared by myself for
 submission to the competent authority;
- all the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of regulation 48 and is punishable in terms of section 24F of the Act.

Signature of the Specialist

GEOSS SOUTH AFRICA (PTY) LTD

Name of Company:

28 November 2022

Date

Details of Specialist, Declaration and Undertaking Under Oath

Page 2 of 3

3. UNDERTAKING UNDER OATH/ AFFIRMATION
I, <u>SHANE TEEK</u> , swear under oath / affirm that all the information submitted or to be submitted for the purposes of this application is true and correct.
State
Signature of the Specialist
GEOSS SOUTH AFRICA (PTY) LTD
Name of Company
28 November 222
Date Samantha Schoeman ACMA 1-7 Fucus 6N 13 Schoongelegen Ste, Helderwe, 3130 Signature of the Commissioner of Oaths
29/11/2027
Date



DETAILS OF THE SPECIALIST, DECLARATION OF INTEREST AND UNDERTAKING UNDER OATH

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File Reference Number:	
NEAS Reference Number:	DEA/EIA/
Date Received:	

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PROJECT TITLE

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 Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the
 Competent Authority. The latest available Departmental templates are available at
 https://www.environment.gov.za/documents/forms.
- A copy of this form containing original signatures must be appended to all Draft and Final Reports submitted to the department for consideration.
- All documentation delivered to the physical address contained in this form must be delivered during the official Departmental Officer Hours which is visible on the Departmental gate.
- All EIA related documents (includes application forms, reports or any EIA related submissions) that are faxed; emailed; delivered to Security or placed in the Departmental Tender Box will not be accepted, only hardcopy submissions are accepted.

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Department of Environmental Affairs

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Private Bag X447

Pretoria

0001

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Department of Environmental Affairs

Attention: Chief Director: Integrated Environmental Authorisations

Environment House

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Email: EIAAdmin@environment.gov.za

Details of Specialist, Declaration and Undertaking Under Oath

Page 1 of 3

1. SPECIALIST INFORMATION

Specialist Company Name:	GEOSS SOUTH AFRICA (PTY) LTD				
B-BBEE	Contribution level (indicate 1 to 8 or non-compliant)	3	Percent Procure recognit	ment	110%
Specialist name:	DALE BARROW				
Specialist Qualifications:	MSc in Hydrogeology				
Professional	SACNASP: 400289/13				
affiliation/registration:					
Physical address:	Unit 12, Techno Stell Bldg, 09 Quantum Street, Techno Park, Stellenbosch				
Postal address:	PO Box 12412, Die Boord, Stellenbosch				
Postal code:	7613	Cel	l;	074 172 28	62
Telephone:	021 880 1079	Fax	C.	n/a	
E-mail:	dbarrow@geoss.co.za				

2. DECLARATION BY THE SPECIALIST

I, Dale Barrow, declare that -

- 1 act as the independent specialist in this application;
- I will perform the work relating to the application in an objective manner, even if this results in views and findings
 that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act,
 Regulations and any guidelines that have relevance to the proposed activity;
- . I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information in my possession that
 reasonably has or may have the potential of influencing any decision to be taken with respect to the application by
 the competent authority; and the objectivity of any report, plan or document to be prepared by myself for
 submission to the competent authority;
- · all the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of regulation 48 and is punishable in terms of section 24F of the Act.



Signature of the Specialist

GEOSS SOUTH AFRICA (PTY) LTD

Name of Company:

07 July 2023

Date

Details of Specialist, Declaration and Undertaking Under Oath

Page 2 of 3

3. UNDERTAKING UNDER OATH/ AFFIRMATION	
, <u>Dale Barrow</u> , swear under oath / affirm that all the information submitted or to be submitted for the purposes of this application is true and correct.	e
Signature of the Specialist	
GEOSS SOUTH AFRICA (PTY) LTD	
Name of Company	
07 July 2023	
Date	
Le .	
Signature of the Commissioner of Oaths	
07 July 2023	
Date -	

Ex officio COMMISSIONER OF OATHS (RSA)
Samantha Schoaman ACMA – 1-7FUWGN
The Boulevard Office Park, Block B
Ground Floor, Searle Street, Woodstock, 7925

Details of Specialist, Declaration and Undertaking Under Oath

Page 3 of 3



DETAILS OF THE SPECIALIST, DECLARATION OF INTEREST AND UNDERTAKING UNDER OATH

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(For official use only)	
DEA/EIA/	

Application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

PROJECT TITLE

Scoping and Environmental Impact Assessment Processes for the Proposed Development of 12 Solar Photovoltaic (PV) Facilities and associated infrastructure (i.e. Kudu Solar Facility 1 - 12), near De Aar, Northern

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- 3. A copy of this form containing original signatures must be appended to all Draft and Final Reports submitted to the department for consideration.
- 4. All documentation delivered to the physical address contained in this form must be delivered during the official Departmental Officer Hours which is visible on the Departmental gate.
- 5. All EIA related documents (includes application forms, reports or any EIA related submissions) that are faxed; emailed; delivered to Security or placed in the Departmental Tender Box will not be accepted, only hardcopy submissions are accepted.

Departmental Details

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Department of Environmental Affairs Attention: Chief Director: Integrated Environmental Authorisations Private Bag X447 Pretoria 0001

Physical address:

Department of Environmental Affairs Attention: Chief Director: Integrated Environmental Authorisations **Environment House** 473 Steve Biko Road

Arcadia

Queries must be directed to the Directorate: Coordination, Strategic Planning and Support at: Email: ElAAdmin@environment.gov.za

Details of Specialist, Declaration and Undertaking Under Oath

Page 1 of 3

 SPECIALIST INFORMATIC 	M
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Specialist Company Name:	GEOSS South Africa (I	Ptv) Lt	d.						
B-BBEE	Contribution level (indicate 1 to 8 or non-compliant)			Percen Procure recogn	ement	110%			
Specialist name:	Louis Jonk								
Specialist Qualifications:	B.Sc. (Hons) – Earth Sciences; M.Sc - Geology								
Professional affiliation/registration:	SACNASP 121278; GSSA 969970; PSSA								
Physical address:	Unit 12, Techno Stell Stellenbosch	Bldg	09	Quant	um Stre	et, Techno Park,			
Postal address:	PO Box 12412, Die Boore	d, Stell	enbos	ch					
Postal code:	7613		Cell:		078 802	8447			
Telephone:	021 880 1079		Fax:		n/a				
E-mail:	ljonk@geoss.co.za	-							

2. DECLARATION BY THE SPECIALIST.

I, Louis Jonk, declare that -

- I act as the independent specialist in this application;
- I will perform the work relating to the application in an objective manner, even if this results in views and findings that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act,
 Regulations and any guidelines that have relevance to the proposed activity;
- I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information in my possession that
 reasonably has or may have the potential of influencing any decision to be taken with respect to the application by
 the competent authority; and the objectivity of any report, plan or document to be prepared by myself for
 submission to the competent authority;
- all the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of regulation 48 and is punishable in terms of section 24F of the Act.

	•	

Page 2 of 3

3. UNDERTAKING UNDER OATH/ AFFIRMATION	
, Louis Jonk swear under oath / affirm that all the	ne information submitted or to be
submitted for the purposes of this application is true and correct.	
Signature of the Specialist	
GEOSS SOUTH AFRICA (PTY) LTD	
Name of Company	
07 July 2023 Date 17	
Jane X	
Signature of the Commissioner of Oaths	
07 July 2023	
Date	
Ex officie COMMISSIONER OF DATHS (RSA) Samantha Schoeman ACMA – 1-7FUWGN The Boulevard Office Park, Block B Ground Floar, Searle Street, Woodstock, 7925	
etails of Specialist, Declaration and Undertaking Under Oath	

APPENDIX C: SITE SENSITIVITY VERIFICATION

Geohydrology themes do not exist on the National Web-based Environmental Screening Tool (Screening Tool) (as of May 2023); therefore, the environmental sensitivity of the proposed project area as identified by the Screening Tool is not applicable. For this reason, no site sensitivity verification report is required. Furthermore, there is no dedicated assessment protocol prescribed for conducting a Geohydrological Assessment. Therefore, this specialist assessment has been undertaken in compliance with Appendix 6 of the National Environmental Management Act (Act 107 of 1998, as amended) (NEMA) Environmental Impact Assessment (EIA) Regulations of 2014. Details of the site visit are indicated below:

Date of Site Visit	23-24 March 2022
Specialist Name	Christel van Staden and Dale Barrow
Professional Registration Number	Cand.Sci.Nat: 122591 and Pr.Sci.Nat: 400289/13
Specialist Affiliation / Company	GEOSS

All relevant desktop information, consultation with landowners, and previous assessments undertaken by the author in the study area have been taken into consideration during the undertaking of this specialist assessment.

The site sensitivity verification was undertaken using the following means:

- (a) desk top analysis, using satellite imagery; geological maps and hydrogeological and geotechnical reports and databases where possible and applicable.
- (b) preliminary on-site inspection; and drive over.
- (c) collected water samples, field chemistry and water levels where possible and relevant; assessed site conditions to determine whether literature information is generally confirmed.

APPENDIX D - IMPACT ASSESSMENT METHODOLOGY

The impact assessment includes:

- the nature, status, significance and consequences of the impact and risk;
- the extent and duration of the impact and risk;
- the probability of the impact and risk occurring;
- the degree to which impacts and risks can be mitigated;
- the degree to which the impacts and risks can be reversed; and
- the degree to which the impacts and risks can cause loss of irreplaceable resources.

Terminology used in impact assessment can overlap. To avoid ambiguity, please note the following clarifications (that are based on NEMA and the EIA Regulations):

- The term environment is understood to have a broad interpretation that includes both the natural (biophysical) environment and the socio-economic environment. The term socioecological system is also used to describe the natural and socio-economic environment and the interactions amongst these components.
- Significance = Consequence x Probability, which means that significance is equivalent to risk.
- The impact can have a positive or negative status. The significance of a negative impact may be called a risk, and the significance of a positive impact may be called an opportunity.

The following principles are to underpin the application of this methodology:

- Transparent and repeatable process specialists are to describe the thresholds and limits they apply in their assessment, wherever possible.
- Adapt parameters to context (where justified) the methodology proposes some thresholds (e.g. for spatial extent, in Step 3 below), however, if the nature of the impact requires a different definition of the categories of spatial extent, then this can be provided and described.
- Combination of a quantitative and qualitative assessment where possible, specialists are to provide quantitative assessments (e.g. areas of habitat affected, decibels of noise, number of jobs), however, it is recognised that not all impacts can be quantified, and then qualitative assessments are to be provided.

As per the DFFE Guideline 5: Assessment of Alternatives and Impacts, the following methodology is applied to the prediction and assessment of impacts and risks. Potential impacts and risks have been rated in terms of the direct, indirect and cumulative:

- Direct impacts are impacts that are caused directly by the activity and generally occur at the same time and at the place of the activity. These impacts are usually associated with the construction, operation or maintenance of an activity and are generally obvious and quantifiable.
- Indirect impacts of an activity are indirect or induced changes that may occur as a result of the activity. These types of impacts include all the potential impacts that do not manifest immediately when the activity is undertaken or which occur at a different place as a result of the activity.
- Cumulative impacts are impacts that result from the incremental impact of the proposed activity on a common resource when added to the impacts of other past, present or reasonably foreseeable future activities. Cumulative impacts can occur from the collective

impacts of individual minor actions over a period of time and can include both direct and indirect impacts.

The impact assessment methodology includes the aspects described below.

- <u>Step 1</u>: Nature of impact/risk The type of effect that a proposed activity will have on the environment.
- Step 2: Status Whether the impact/risk on the overall environment will be:
 - o Positive environment overall will benefit from the impact/risk;
 - Negative environment overall will be adversely affected by the impact/risk; or
 - Neutral environment overall not be affected.
- Step 3: Qualitatively determine the consequence of the impact/risk by identifying the a) SPATIAL EXTENT; b) DURATION; c) REVERSIBILITY; AND d) IRREPLACEABILITY.
 - o A) Spatial extent The size of the area that will be affected by the impact/risk:
 - Site specific;
 - Local (<10 km from site);
 - Regional (<100 km of site);</p>
 - National: or
 - International (e.g. Greenhouse Gas emissions or migrant birds).
 - B) Duration The timeframe during which the impact/risk will be experienced:
 - Very short term (instantaneous);
 - Short term (less than 1 year);
 - Medium term (1 to 10 years);
 - Long term (the impact will cease after the operational life of the activity (i.e. the impact or risk will occur for the project duration)); or
 - Permanent (mitigation will not occur in such a way or in such a time span that the impact can be considered transient (i.e. the impact will occur beyond the project decommissioning)).
 - C) Reversibility of the Impacts the extent to which the impacts/risks are reversible assuming that the project has reached the end of its life cycle (decommissioning phase):
 - High reversibility of impacts (impact is highly reversible at end of project life i.e. this is the most favourable assessment for the environment);
 - Moderate reversibility of impacts;
 - Low reversibility of impacts; or
 - Impacts are non-reversible (impact is permanent, i.e. this is the least favourable assessment for the environment).
 - D) Irreplaceability of Receiving Environment/Resource Loss caused by impacts/risks the degree to which the impact causes irreplaceable loss of resources assuming that the project has reached the end of its life cycle (decommissioning phase):

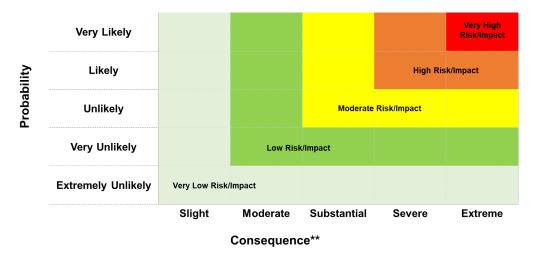
- High irreplaceability of resources (project will destroy unique resources that cannot be replaced, i.e. this is the least favourable assessment for the environment);
- Moderate irreplaceability of resources;
- Low irreplaceability of resources; or
- Resources are replaceable (the affected resource is easy to replace/rehabilitate, i.e. this is the most favourable assessment for the environment).

Some of the criteria are quantitative (e.g. spatial extent and duration) and some may be described in a quantitative or qualitative manner (e.g. reversibility and irreplaceability). The specialist then combines these criteria in a qualitative manner to determine the **consequence**.

The consequence terms ranging from slight to extreme must be calibrated per Specialist Study so that there is transparency and consistency in the way a risk/impact is measured. For example, from a biodiversity and ecology perspective, the consequence ratings could be defined according to a reduction in population or occupied area in relation to Species of Conservation Concern (SCC) status, ranging from slight consequence for defined areas of Least Concern, to extreme consequence for defined areas that are Critically Endangered. For example, from a social perspective, a slight consequence could refer to small and manageable impacts, or impacts on small sections of the community; a moderate consequence could refer to impacts which affect the bulk of the local population negatively or may produce a net negative impact on the community; and an extreme consequence could refer to impacts which could result in social or political violence or institutional collapse.

- **Consequence** The anticipated consequence of the risk/impact is generally defined as follows:
 - Extreme (extreme alteration of natural or socio-economic systems, patterns or processes, i.e. where environmental or socio-economic functions and processes are altered such that they permanently cease);
 - Severe (severe alteration of natural or socio-economic systems, patterns or processes, i.e. where environmental or socio-economic functions and processes are altered such that they temporarily or permanently cease);
 - Substantial (substantial alteration of natural or socio-economic systems, patterns or processes, i.e. where environmental or socio-economic functions and processes are altered such that they temporarily or permanently cease;
 - Moderate (notable alteration of natural or socio-economic systems, patterns or processes, i.e. where the natural or socio-economic environment continues to function but in a modified manner; or
 - Slight (negligible and transient alteration of natural or socio-economic systems, patterns or processes, i.e. where natural systems/environmental or socio-economic functions, patterns, or processes are not affected in a measurable manner, or if affected, that effect is transient and the system recovers).
- **Step 4**: Rate the **probability** of the impact/risk using the criteria below:
 - o **Probability** The probability of the impact/risk occurring:
 - Extremely unlikely (little to no chance of occurring);
 - Very unlikely (<30% chance of occurring);

- Unlikely (30-50% chance of occurring)
- Likely (51 90% chance of occurring); or
- Very Likely (>90% chance of occurring regardless of prevention measures).
- <u>Step 5</u>: Use both the **consequence** and **probability** to determine the **significance** of the identified impact/risk (qualitatively as shown in Figure 16.5). Significance definitions and rankings are provided below:



**[Qualitatively determined based on Spatial Extent, Duration, Reversibility and Irreplaceability]

Figure 16-5: Guide to assessing risk/impact significance as a result of consequence and probability.

- Significance Will the impact cause a notable alteration of the environment?
 - Very low (the risk/impact may result in very minor alterations of the environment and can be easily avoided by implementing appropriate mitigation measures, and will not have an influence on decision-making);
 - Low (the risk/impact may result in minor alterations of the environment and can be easily avoided by implementing appropriate mitigation measures, and will not have an influence on decision-making);
 - Moderate (the risk/impact will result in moderate alteration of the environment and can be reduced or avoided by implementing the appropriate mitigation measures, and will only have an influence on the decision-making if not mitigated);
 - High (the risk/impact will result in major alteration to the environment even with the implementation on the appropriate mitigation measures and will have an influence on decision-making); and
 - Very high (the risk/impact will result in very major alteration to the environment even with the implementation on the appropriate mitigation measures and will have an influence on decision-making (i.e. the project cannot be authorised unless major changes to the engineering design are carried out to reduce the significance rating)).

ENVIRONMENTAL IMPACT ASSESSMENT REPORT: Scoping and Environmental Impact Assessment (EIA)
Process for the Proposed Development of a Solar Photovoltaic (PV) Facility (Kudu Solar Facility 2) and
associated infrastructure, near De Aar, Northern Cape Province

With the implementation of mitigation measures, the residual impacts/risks are ranked as follows in terms of significance:

- *Very low = 5;*
- Low = 4;
- Moderate = 3;
- High = 2; and
- Very high = 1.

The specialists must provide a written supporting motivation of the assessment ratings provided.

- <u>Step 6</u>: Determine the **Confidence Level** The degree of confidence in predictions based on available information and specialist knowledge:
 - o Low;
 - o Medium; or
 - o High.

APPENDIX E - COMPLIANCE WITH THE APPENDIX 6 OF THE 2014 EIA REGULATIONS (AS AMENDED)

	ements of Appendix 6 (Specialist Reports) of Government Notice Environmental Impact Assessment (EIA) Regulations of 2014, as ed)	Section where this has been addressed in the Specialist Report
	specialist report prepared in terms of these Regulations must contain - details of -	Appendix A.
	i. the specialist who prepared the report; and	
	ii. the expertise of that specialist to compile a specialist report including a curriculum vitae;	
b)	a declaration that the specialist is independent in a form as may be specified by the competent authority;	Appendix B
c)	an indication of the scope of, and the purpose for which, the report was prepared;	Section 16.1.1
cA) an	indication of the quality and age of base data used for the specialist report;	Sections 16.2.1 and 16.2.2
	description of existing impacts on the site, cumulative impacts of the ed development and levels of acceptable change;	Section 16.4 and Section 16.6.4
d)	the duration, date and season of the site investigation and the relevance of the season to the outcome of the assessment;	Section 16.2.2
e)	a description of the methodology adopted in preparing the report or carrying out the specialised process inclusive of equipment and modelling used;	Section 16.2
f)	details of an assessment of the specific identified sensitivity of the site related to the proposed activity or activities and its associated structures and infrastructure, inclusive of a site plan identifying site alternatives;	Section 16.4.3 and Section 16.4.6
g)	an identification of any areas to be avoided, including buffers;	Section 16.4.6
h)	a map superimposing the activity including the associated structures and infrastructure on the environmental sensitivities of the site including areas to be avoided, including buffers;	Section 16.4.6
i)	a description of any assumptions made and any uncertainties or gaps in knowledge;	Section 16.2.2
j)	a description of the findings and potential implications of such findings on the impact of the proposed activity or activities;	Section 16,4 and 16,5
k)	any mitigation measures for inclusion in the EMPr;	Section 16.9
l)	any conditions for inclusion in the environmental authorisation;	Section 16.10.2
m)	any monitoring requirements for inclusion in the EMPr or environmental authorisation;	Section 16.10.2
n)	a reasoned opinion- i. whether the proposed activity, activities or portions thereof should be authorised;	Section 16.10.1
(IA) I	egarding the acceptability of the proposed activity or activities; and ii. if the opinion is that the proposed activity, activities or portions thereof should be authorised, any avoidance, management and mitigation measures that should be included in the EMPr, and where applicable, the closure plan;	
0)	a description of any consultation process that was undertaken during the course of preparing the specialist report;	Section 16.2.3
p)	a summary and copies of any comments received during any consultation process and where applicable all responses thereto; and	Section 16.5.2
q)	any other information requested by the competent authority.	

Requirements of Appendix 6 (Specialist Reports) of Government Notice R326 (Environmental Impact Assessment (EIA) Regulations of 2014, as amended)	Section where this has been addressed in the Specialist Report
(2) Where a government notice by the Minister provides for any protocol or minimum information requirement to be applied to a specialist report, the requirements as indicated in such notice will apply.	Note: Part A of the Assessment Protocols published in GN 320 on 20 March 2020 are not applicable as there are no dedicated Geohydrology or Groundwater themes on the National Web-based Environmental Screening Tool (Screening Tool) (as at May 2023). Section 16.4.5 and Appendix C

APPENDIX F - OTHER RENEWABLE ENERGY PROJECTS WITHIN 30 KM OF THE KUDU SOLAR PV FACILITY

Table 16-19: Approved renewable energy projects, located within 30 km of the proposed Kudu Solar Facility.

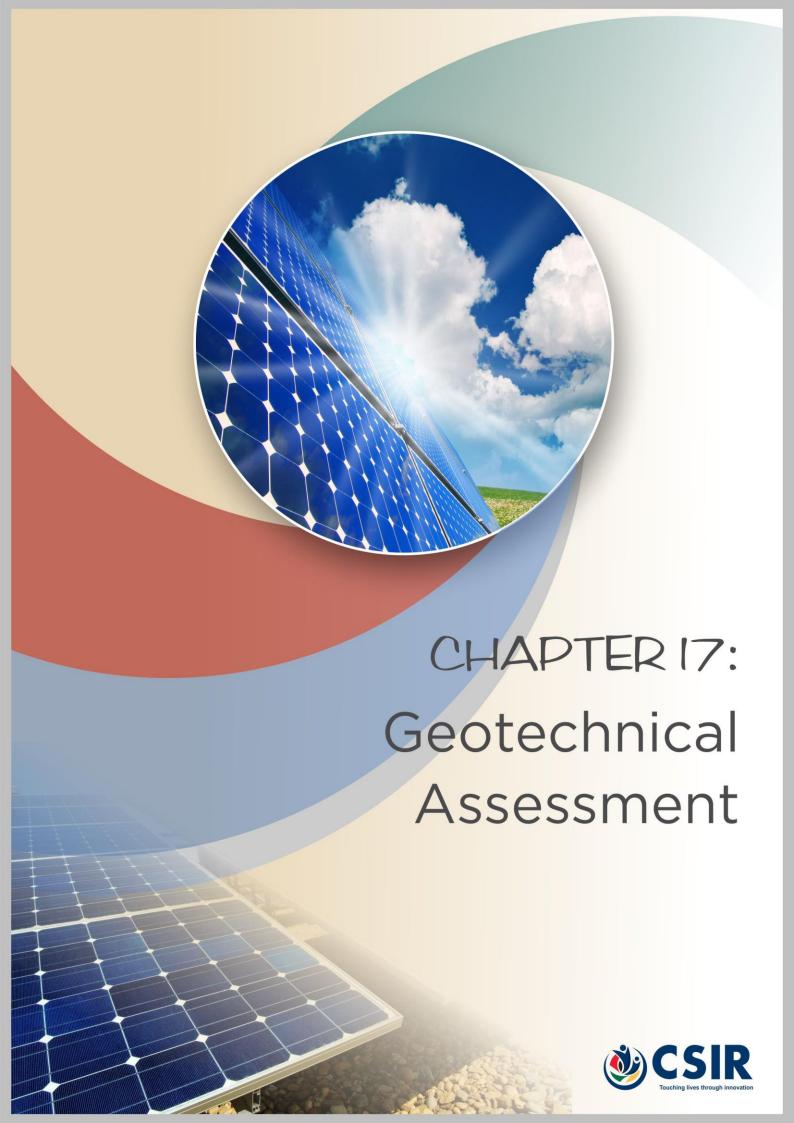
CSIR No.	DFFE REFERENCE	TECHNO- LOGY	MW/ KV	STATUS		PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
1	12/12/20/225812/12/20/2258/1	Solar PV	75	Approved and Preferred Bidder (Operational)	•	The Proposed Establishment of Photovoltaic (Solar Power) Farms in the Northern Cape Province - Kalkbult	2010	Scoping and EIA	Scatec Solar SA Pty Ltd	Sustainable Development Projects cc
2	 12/12/20/2463/1 12/12/20/2463/1/2 12/12/20/2463/1/A2 12/12/20/2463/1/AM3 12/12/20/2463/1/AM4 12/12/20/2463/1/AM5 	Onshore Wind	140	Approved and Preferred Bidder (Operational)	•	Longyuan Mulilo De Aar 2 North Wind Energy Facility Longyuan Mulilo De Aar Maanhaarberg Wind Energy Facility The Wind Energy Facility (North and South) situated on the Plateau Near De Aar, Northern Cape Province	2010 and 2014	Scoping and EIA and Amendment	Longyuan Mulilo De Aar 2 South (Pty)	Aurecon South Africa (Pty) Ltd and Holland and Associates Environmental Consultants
3	12/12/20/2463/212/12/20/2463/2/AM2	Onshore Wind	100	Approved and Preferred Bidder (Operational)	•	Longyuan Mulilo De Aar Maanhaarberg Wind Energy Facility The Wind Energy Facility (North and South) Situated On The Plateau Near De Aar, Northern Cape Province	2010 and 2014	Scoping and EIA and Amendment	Mulilo Renewable Energy (Pty) Ltd	Aurecon South Africa (Pty) Ltd
4	• 14/12/16/3/3/1/1166 14/12/16/3/3/1/1166/AM3 14/12/16/3/3/1/1166/AM4	Transmis sion line	132	Approved	•	Basic Assessment for the proposed construction of a 132 kV transmission line corridor adjacent to the existing Eskom transmission line from Longyuan Mulilo De	2010 and 2014	Basic Assessment	Longyuan Mulilo De Aar 2 North (Pty) Ltd	Aurecon South Africa (Pty) Ltd

CSIR No.	DFFE REFERENCE	TECHNO- LOGY	MW/ KV	STATUS		PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	ЕАР
						Aar 2 North Wind Energy Facility (WEF) to the Hydra Substation in De Aar, Northern Cape				
5	• 14/12/16/3/3/1/785	Transmis sion line	132	Approved	•	Proposed construction of two 132kV transmission lines from the South & North Wind Energy Facilities on the Eastern Plateau (De Aar 2) near De Aar, Northern Cape.	2010	Basic Assessment	Mulilo Renewable Energy (Pty) Ltd	Aurecon South Africa (Pty) Ltd
6	 14/12/16/3/3/2/278 14/12/16/3/3/2/278/1 14/12/16/3/3/2/278/2 	Onshore Wind	118	Approved	•	Proposed Castle Wind Energy Facility Project, located near De Aar, Northern Cape	2010 and 2014	Scoping and EIA	Castle Wind Farm (Pty) Ltd	Aurecon South Africa (Pty) Ltd; and Savannah Environmental Consultants (Pty) Ltd
7	 14/12/16/3/3/2/564 14/12/16/3/3/2/564/AM1 14/12/16/3/3/2/564/AM2 	Solar PV	75	To be confirmed	•	Proposed Swartwater 75MW solar PV power facility in Petrusville within Renosterburg Local Municipality, Northern Cape	2010 and 2014	Scoping and EIA and Amendment	AE-AMD Renewable Energy (Pty) Ltd	USK Environmental and Waste Engineering (Pty) Ltd
8	• 14/12/16/3/3/2/740	Solar PV	300	Approved	•	Proposed 300MW Solar Power Plant in Phillipstown area in Renosterberg Local Municipality	2010	Scoping and EIA	To be confirmed	Tshikovha Environmental and Communication Consultants
9	• 14/12/16/3/3/2/744	Solar PV	0	Approved	•	Proposed PV facility on farm Jakhalsfontein near De Aar	2010	Scoping and EIA	Solar Capital (Pty) Ltd	Eco Compliance (Pty) Ltd
10	• 14/12/16/3/3/2/739	Solar PV	70 - 100	To be confirmed	•	Proposed 70 - 100 MW Solar Power Plant in Petrusville	2010	Scoping and EIA	To be confirmed	Tshikovha Environmental and Communication Consultants
11	Not issued yet (it is understood that the	Solar PV	800 (Max	Pre- Application	•	The Proposed Keren Energy Odyssey Solar PV Facilities	2014	Scoping and EIA	Keren Energy Group Holdings	EnviroAfrica cc

CSIR No.	DFFE REFERENCE	TECHNO- LOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
	project is still within the pre-application stage)		imu m)		(Odyssey Solar 1, Odyssey Solar 2, Odyssey Solar 3, Odyssey Solar 4, Odyssey Solar 5, Odyssey Solar 6, Odyssey Solar 7 And Odyssey Solar 8)				
12	To be confirmed	Solar PV	3050	Scoping	The Proposed Development of the Crossroads (formally referred to as the Hydra B) Green Energy Cluster of Renewable Energy Facilities and Grid Connection Infrastructure, Pixley Ka Seme District Municipality, Northern Cape Province. The Cluster entails the development of up to 21 solar energy facilities, with the Scoping and EIA Processes consisting of three phases. Phases 1, 2 and 3 consist of 9, 6 and 6 solar facilities, respectively. The Phase 1 Scoping and EIA Processes were launched in January 2023.	2014	Scoping and EIA	Akuo Energy Afrique	Savannah Environmental Consultants (Pty) Ltd
Study area shown on map	 14/12/16/3/3/2/2244 14/12/16/3/3/2/2245 14/12/16/3/3/2/2246 14/12/16/3/3/2/2247 14/12/16/3/3/2/2248 14/12/16/3/3/2/2249 14/12/16/3/3/2/2250 14/12/16/3/3/2/2251 14/12/16/3/3/2/2252 14/12/16/3/3/2/2252 	Solar PV	2180	Scoping and EIA Process underway	Proposed Development of 12 Solar Photovoltaic (PV) Facilities (Kudu Solar Facility 1 to 12) and associated infrastructure, near De Aar, Northern Cape Province	2014	Scoping and EIA	Kudu Solar Facility 1 (Pty) Ltd to Kudu Solar Facility 12 (Pty) Ltd	CSIR

CSIR No.	DFFE REFERENCE	TECHNO- LOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
	14/12/16/3/3/2/225414/12/16/3/3/2/2255								
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	220	Existing Power Line	HYDRA ROODEKUIL 2	-	-	-	-
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	132	Existing Power Line	HYDRA ROODEKUIL 1	-	-	-	-
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	765	Existing Power Line	BETA HYDRA 2	-	-	-	-
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	400	Existing Power Line	HYDRA PERSEUS 3	-	-	-	-
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	220	Existing Power Line	VAN DER KLOOF ROODEKUIL 2	-	-	-	-
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	220	Existing Power Line	VAN DER KLOOF ROODEKUIL 1	-	-	-	-
Shown on map as	• N/A	Transmis sion Line	400	Existing Power Line	BETA HYDRA 1	-	-	-	-

CSIR No.	DFFE REFERENCE	TECHNO- LOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
Existing HV Lines									
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	400	Existing Power Line	HYDRA PERSEUS 2	-	-	-	-
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	132	Existing Power Line	KALKBULT/KAREEBOSCH PAN 1	-	-	-	-
Shown on map as Existing HV Lines	• N/A	Transmis sion Line	132	Existing Power Line	ROODEKUIL/ORANIA 1	-	-	-	-
Shown on map as Planned HV Lines	• N/A	Transmis sion Line	765	Planned Power Line	 Perseus to Gamma 2nd 765 kV line Cape Corridor Phase 4: 2nd Zeus-Per-Gam-Ome 765kV Line 	-	-	-	-
Shown on map as Planned HV Lines	• N/A	Transmis sion Line	765	Planned Power Line	 Relocate Beta-Hydra 765kV line to form Perseus-Hydra 1st 765kV line Cape Corridor Phase 2: Zeus - Hydra 765kV Integration 	-	-	-	-
Shown on map as Planned HV Lines	• N/A	Transmis sion Line	765	Planned Power Line	 Perseus to Gamma 2nd 765 kV line Cape Corridor Phase 4: 2nd Zeus-Per-Gam-Ome 765kV Line 	-	-	-	-



GEOTECHNICAL ASSESSMENT:

Scoping and Environmental Impact Assessment (EIA)
Process for the Proposed Development of a Solar
Photovoltaic Facility (Kudu Solar Facility 2) and associated
infrastructure, near De Aar, Northern Cape Province

Report prepared for:	Report prepared by:
CSIR – Environmental Management Services	Hardy Luttig, Shane Teek & Dale
P O Box 320	Barrow
Stellenbosch	GEOSS South Africa (Pty) Ltd
7599	P.O. Box 12412
South Africa	Die Boord, Stellenbosch 7613
	Stellenbosch, South Africa
	7600

Version 0: 13 April 2023



This report summarises the results from a desktop specialist study which aimed to project a high-level overview of envisaged risks from a geotechnical standpoint, and provide broad recommendations for high-level designs. The following conclusions can be drawn from the investigation:

- 1. Based on the findings of this geotechnical desktop study, development should proceed provided the mitigation measures are implemented.
- 2. Increased soil erosion and contamination may transpire as an impact of the proposed development, and this may persist for the life of the project. However, the impact of this is expected to be very low to low significance during all phases of the development (i.e., construction, operation and decommissioning).
- 3. Published data for the area, e.g., geological map, is generally confirmed by fieldwork undertaken by GEOSS in the area. However, variable soil and rock conditions will exist across the site, broadly these have been divided as follows:
 - a. Zone A Karoo Sandstones and mudstones
 - b. Zone B Karoo dolerite
 - c. Zone C Areas of thicker soil cover (generally within drainage channels)
- 4. It is anticipated that conventional foundations can be employed for all structures. Karoo mudrock and sandstone should be avoided when selecting aggregates for concrete mixes.
- 5. The footprint of each proposed structure would have to be investigated prior to compilation of final design.
- 6. Owing to the variable geologic and soil conditions across the proposed development area, the subgrade conditions will vary across the site. Dolerite has been proven to perform well as an aggregate for wearing courses in other areas of the Karoo. Dolerite has also been incorporated as an aggregate in concrete mixes.
- 7. The excavatability of the stratum on site are anticipated to be variable, based on material composition and texture, the degree of weathering, and the nature of discontinuities within the rock and/or soil mass.
- 8. The seismicity in the region should be considered during design.
- 9. Road cuttings and drainage systems should be designed by an appropriately qualified professional.
- Detailed geotechnical investigations will need to be undertaken prior to construction. Such investigations would not be required to fulfil the requirements of the EIA process. However, it would be necessary prior to construction.

11. GEOSS has endeavoured to highlight and characterise all potential geotechnical risks that are presented by the site that has been proposed for development. However, due to the anisotropic (variable) nature of earth materials, each point on the site will present results that differ. For this reason, it is considered of the utmost importance that the foundation excavations be inspected prior to casting to ensure that soil with an adequate bearing capacity is obtained beneath each footing, and/or piling conditions be assessed. These works should be carried out by an appropriately qualified individual, during construction of the facility.



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Abbreviations			
AASHTO	American Association of State Highway and Transportation Officials		
BH	Borehole		
CBR	California bearing ratio		
CGS	Council for Geoscience		
CSIR	Council for Scientific and Industrial Research		
DWS	Department of Water Affairs and Sanitation		
EAM	Engineering and Asset Management		
EC	electrical conductivity		
EOH	End of Hole		
g	Gravity		
L/s	litres per second		
LL	Liquid Limit		
LS	Linear Shrinkage		
LSSG	Lower selected sub-grade		
m	metres		
MCCSSO	Moisture content, colour, consistency, structure, soil type, and origin.		
MDD	Maximum Dry Density		
mm	millimetre		
MOD	Modified AASHTO		
mS/m	milli-Siemens per metre		
NGA	National Groundwater Archive		
NHBRC	National Home Builders Registration Council		
OMC	Optimum moisture content		
PI	Plasticity Index		
TLB	Tractor loader backhoe		
UFST	Underground Fuel Storage Tanks		
USSG	Upper selected sub-grade		



Definitions	
Aquifer	a geological formation, which has structures or textures that hold water or permit appreciable water movement through them [from National Water Act (Act No. 36 of 1998)]
Electrical conductivity	the ability of groundwater to conduct electrical current due to the presence of charged ionic species in solution (Freeze and Cherry, 1979)
Fractured aquifer	Describes an aquifer where groundwater only occurs in narrow fractures within the bedrock
Geologic materials	Primarily rock and soil (synonymous with Geological)
Geotechnical zone	Region where similar geotechnical conditions are anticipated.
Groundwater	Water found in the subsurface in the saturated zone below the water table or piezometric surface, i.e., the water table marks the upper surface of groundwater systems.
Intergranular aquifer (or primary aquifer)	An aquifer in which groundwater is stored within and flows through open pore spaces in the unconsolidated granular Quaternary deposits
Lithology/lithologies	A specific rock type, e.g., sandstone, shale or granite etc.
Pedocrete	Superficial deposits, not of sedimentary origin, which have formed through either weathering residues, or cementation or replacement of existing soils (by precipitates derived from soil-water and or groundwater), or a combination of such processes. Several chemical agents replace or cement, e.g., calcium carbonates (calcrete) and/or iron oxides (ferricrete)

17. GEOTECHNICAL ASSESSMENT

This chapter includes the Geotechnical Specialist Assessment that was prepared by GEOSS South Africa, as part of the Scoping and Environmental Impact Assessment (EIA) Process for the proposed development of the Kudu Solar Facility 2 and associated infrastructure, near De-Aar, Northern Cape Province (Map 17-1). Kudu Solar Facility 2 forms part of a cluster of 12 Solar Photovoltaic (PV) projects proposed by the Project Developer.

17.1 Introduction

17.1.1 Scope, Purpose and Objectives of this Specialist Report

The primary objective of the desktop assessment is to summarise the area's geology, including the likely distribution of potential geotechnical challenges related to the underlying geology. Provide geotechnical impact assessment of the proposed development on the receiving environment, e.g., providing mitigation measures to limit impacts of concentrated runoff generated by hard surfaces resulting in increased soil erosion.

This chapter only addresses Kudu Solar Facility 2 (hereafter referred to as the "Kudu Solar Facility" or "proposed project").

17.1.2 Details of Specialist

This specialist assessment has been undertaken by Hardy Luttig, Shane Teek, and Dale Barrow of GEOSS South Africa. Hardy Luttig obtained a Bachelor degree in Earth Science and a Masters in Geotechnical Engineering at the University of Stellenbosch. Shane Teek is registered as a candidate with the SACNASP, with Registration Number 126397. Dale Barrow is registered as a professional with the SACNASP, with Registration Number 400829/13. A curriculum vitae is included for all parties in Appendix A of this Specialist Assessment.

In addition, a signed specialist statement of independence is included in Appendix B of this Specialist Assessment.

17.1.3 Terms of Reference

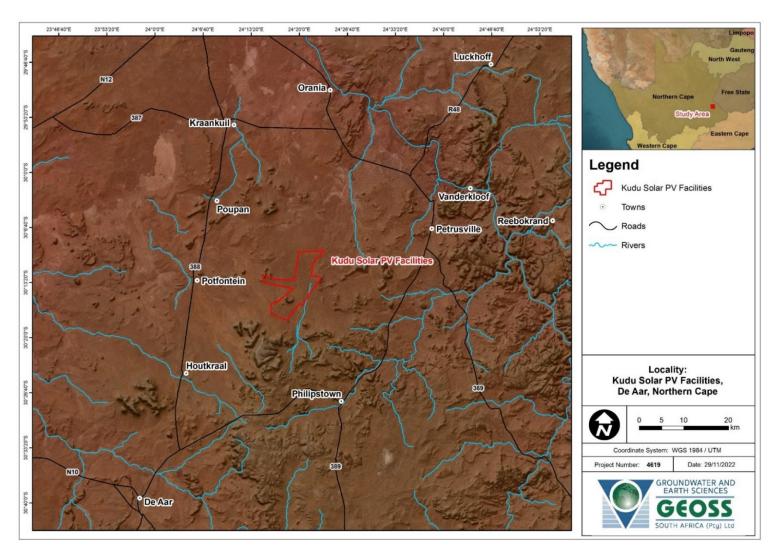
The Terms of Reference for the geotechnical desktop specialist study are as follows:

- Compile and review available geological and geotechnical information for the region, including the anticipated soil conditions.
- Determine whether problem soils are likely to be encountered within the study area.
- A general discussion of possible and likely engineering characteristics of the respective geological materials.
- Identify possible development constraints that may be present across the study area, e.g., topographical constraints, major discontinuities, or shallow groundwater conditions (permanent or non-permanent).

- An evaluation of the seismic potential of the area based on available published literature.
- Provide commentary on any potentially sensitive areas across the site, such as ridges, outcrops and exposures.
- Provide broad recommendations that may be used to guide the geotechnical design and plan future investigations within the study area.
- Specification of set-backs or buffers (if any), and provide clear reasons for these recommendations.
- Provide review input on the preferred infrastructure layout following the sensitivity analysis and layout identification.
- Summarise, classify and categorise geotechnical risks that may arise due to the development and provide relevant mitigation measures to manage said risks.
- Provide spatial mapping of geotechnical zones where similar environmental conditions are expected.
- Provide spatial mapping of slope classification, where development is most to least favourable, based on Stiff et al. (1996).
- Identify and assess the potential direct, indirect and cumulative impacts of the proposed development on the receiving environment from a geotechnical perspective.
- A description of assumptions and limitations used.
- Identification of additional protocols, licensing and/or permitting requirements that are relevant to the project and the implications thereof, if any.
- Provide recommendations with regards to potential monitoring programmes.
- Determine mitigation and/or management measures, which could be implemented to as far as
 possible, reduce the effect of negative impacts and enhance the effect of positive impacts. Also,
 identify best practice management actions, monitoring requirements, and rehabilitation guidelines
 for all identified impacts, for inclusion in the Environmental Management Programme (EMPr).
- Review the Generic EMPr for Substations (GN 435) and confirm if there are any specific environmental sensitivities or attributes present on the site and any resultant site-specific impact management outcomes and actions that need to be included.
- Provide a reasoned opinion indicating the acceptability of the proposed development and a recommendation if the development should go ahead or not.

17.1.4 Proposed Development

The proposed development includes all components of the Kudu Solar Facility, e.g., the erection of PV tables for the generation of solar power, associated electrical infrastructure (above and/or below the surface), ancillary structures for site security and/or transformers, battery energy storage system(s) (BESS), as well as access tracks/roads and boundary fences.



Map 17-1: Locality map showing the location of the proposed Kudu Solar Facility and surrounds.

17.2 Approach and Methodology

The following approach and methodology were followed for this desktop geotechnical assessment:

- Task 1: Obtain all data relevant to the project (i.e., previous geotechnical reports), and search the internal GEOSS database (including relevant information pertinent to the study area). Review/acquire geological, geotechnical, and hydrogeological maps for the area. Review any reports that have been compiled for the study area. Compile a project GIS.
- Task 2: Conduct a literature review. Compile geotechnical impact assessment using the methodology presented in Appendix D of this assessment chapter. Draw from data gathered during the site visit undertaken by GEOSS during the separate Hydrogeological study (Chapter 16 of this EIA Report), during which time the geotechnical and geological conditions were generally confirmed visually.
- Task 3: Compile and analyse the data using geotechnical methods and address the questions raised in the project objectives. Document findings in the desktop geotechnical report.

17.2.1 Information Sources

The information sources used in this study are listed in Table 17-1.

Table 17-1: Information sources used to assess the Geotechnical conditions for the proposed Kudu Solar Facility.

Data / Information	Source	Date	Туре	Description
Geological Map	Council for Geosciences	1997	Spatial	1:250 000 scale Geological Map Series of 3024 Colesberg
[Geotechnical] Engineering Geology of Southern Africa: The Karoo Sequence Volume 3	A. B. A. Brink	1983	Literature	Engineering properties of rocks and soils of the Karoo Supergroup
Climatology and Geohydrology	Cape Farm Mapper	2009	Database	SA Atlas of Climatology and Geohydrology; obtained from Western Cape Government Agriculture
Groundwater recharge and vulnerability mapping	Conrad J. and Munch Z.	2007	Spatial	A National scale approach to groundwater recharge and vulnerability mapping
Hydrogeological map series	Department of Water Affairs and Forestry	2005	Spatial	Hydrogeological map series of the republic of South Africa
NGA Database	NGA	14 April 2022	Database and Spatial	Spatial delineation of NGA registered boreholes

17.2.2 Assumptions, Knowledge Gaps and Limitations

The following is important to note regarding the completion of this project:

- A site visit was not undertaken during the geotechnical desktop study. However, the services performed by GEOSS South Africa (Pty) Ltd are consistent with the level of care and skill ordinarily exercised by the geotechnical unit and/or members of the geotechnical profession practising under similar conditions in the locality of the project. This report is therefore considered to fulfil the scope of the present investigation, and third party information has been utilised in good faith in compilation of this report.
- The duration of the construction phase and decommissioning phase is assumed to be approximately one and a half years, and one year respectively.
- The interpretation of the site conditions is based on the available information (from literature and experience in the region). Professional judgement (analysis of available data) is considered to provide sufficient confidence to meet the objectives of this specialist desktop geotechnical study.
- Earth materials are, by nature, variable. Therefore, reasonable variance between the conditions and properties described and actual site conditions are expected. Recommendations provided are suitable for the purposes of this investigation, but are provisional in nature and will need to be confirmed by intrusive on-site investigations prior to construction.
- Third-party information (e.g., literature) has been utilised in good faith.
- Cumulative impacts are assessed by adding effects expected from this proposed development to existing and proposed developments with similar impacts in a 30 km radius. The current and proposed developments that were considered for cumulative impacts are discussed and displayed in Section 17.6.4.
- The cumulative impacts of the construction period are expected to be staggered, i.e., as one development's construction period is complete, the next commences, prolonging the cumulative impacts of the construction period. A similar approach has been adopted for the operation and decommissioning phases.
- It must be noted that there are no areas on site that should be avoided from a geotechnical sensitivity perspective. However, areas of moderate to steep topography would likely render development financially unfeasible (Map 17-5). Further, the Digital Elevation Model (DEM) used to generate the slope map (Map 17-5) indicated anomalous elevation values that run along the length of the overhead transmission lines. Based on the available evidence, these anomalous elevation values are considered erroneous.
- No responsibility will be accepted for consequences arising out of the fact that actual conditions vary from those presented/inferred. Engineering recommendations provided in this report are preliminary and must be confirmed through further intrusive investigations. The information must be verified by the undertaking of a detailed geotechnical site investigation. Such investigations would not be required to fulfil the requirements of the EIA process. However, it would be necessary prior to construction.
- There is no specific Assessment Protocol devised for Geotechnical Assessments, and the Screening Tool does not include any layers or themes for geotechnical conditions (as at May 2023). Therefore, the report needs to comply with Appendix 6 of the 2014 National Environmental Management Act (Act 107 of 1998, as amended) (NEMA) EIA Regulations (as amended). Appendix E of this chapter contains a table complying with Appendix 6 of the 2014 NEMA EIA Regulations (as amended).

17.2.3 Consultation Processes Undertaken

During the undertaking of the geohydrological¹ and geotechnical site verification process, all landowners were contacted to ensure that GEOSS was able to locate their boreholes and inspect the landforms across their properties. This was mainly to ensure consent was granted; this was achieved telephonically by Christel Van Staeden of GEOSS South Africa.

17.3 Description of Project Aspects relevant to this Geotechnical Specialist Assessment

The project applicant intends to construct several solar panel arrays across the proposed development area of Kudu Solar Facility. To do so, construction will be required, which typically entails the following:

- 1. Stripping and clearing of vegetation, where necessary, within the approved development footprint to facilitate the construction and/or establishment of infrastructure. Note that vegetation is planned to be trimmed within the PV array area (and not removed completely);
- 2. Levelling and grading of the site.
- 3. Excavation of foundation trenches and/or installation [method dependent on conditions] of pile foundation systems for the solar panel arrays and related infrastructure.

The above activities generally affect the surrounding environment as follows:

- Displacement of geological materials.
- · Contamination of geological materials.
- Generation of construction and demolition waste.

To date, apart from the construction of farmhouses and the erection of boundary and subcamp fences for farming purposes; little disturbance of the subsoils and rocks in the area proposed for development has taken place.

17.4 Baseline Environmental Description

17.4.1 Study Area Definition

The study area for the proposed Kudu Solar Facilities 1 to 12 is the full extent of the eight affected farm properties on which the proposed PV Facilities will be constructed. The full extent of these properties has been assessed in this study in order to identify environmental sensitivities and no-go areas. The total **study area** for Kudu Solar Facilities 1 to 12 is approximately 8 150 hectares (ha).

At the commencement of this Scoping and EIA Process, the **Original Scoping Buildable Areas** which fall within the study area were identified by the Project Developer following the completion of high-level environmental screening based on the Screening Tool.

¹ Note that a separate Geohydrology Assessment is included in Chapter 16 of this EIA Report

Following the identification of sensitivities during the Scoping Phase, the Project Developer considered such sensitivities and formulated the **Revised Scoping Buildable Areas**. The **Revised Scoping Buildable Areas** were used to inform the design of the layout, and further assessed during this EIA Phase of the project in order to identify the preferred development footprint of the proposed project on the approved site as contemplated in the accepted Scoping Report. The development footprint is where the actual development will be located, i.e. the footprint containing the PV solar arrays and associated infrastructure.

For simplicity, the maps contained within this report include all boundaries of the study area. However, each report is focused on a single component of the investigation, e.g., Kudu Solar Facility 2.

17.4.2 General Description

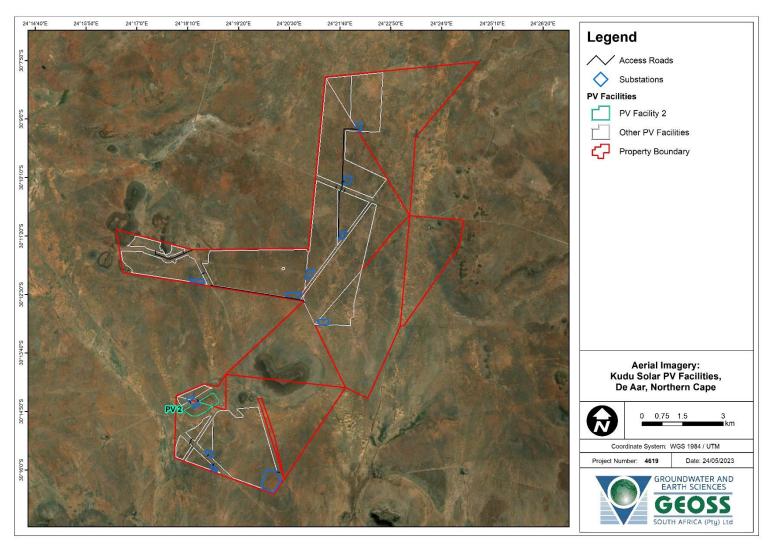
The nearest town to the proposed project is De Aar, approximately 60 km to the southwest. The landscape in the surrounding area is arid, with transported sands occurring widely along plains with dolerite sills (generally northwest of the study area) and mudstone, shale and sandstones (generally southeast of the study area) outcropping in areas of higher elevation. It is understood that the farms in the area are mainly used for livestock farming purposes.

Receptors that could be impacted by changes in the geotechnical conditions of the study area include (but are not limited to):

- Destruction/alteration of endemic fauna and flora environment due to displacement of geologic materials, e.g., removal of soils and/or rocks on site.
- Reduced food for livestock and inhabitants of the farms, decreased crop yields (although uncommon in this region) due to erosion and contamination, and consequential soil loss.

Acceptable levels of change in terms of geotechnical conditions would generally be characterised by safe tolerable levels. For the EIA process this would include identification of fatal flaws and levels of change via desktop study. This information can be later refined after EA with data based on observations made during the structural design phase which includes intrusive investigations, detailed designs, design verifications and calculations. This would also include applicable norms and standards deemed relevant by the geotechnical professional.

Map 17-2 presents relevant boundaries of the study area with solar facility boundaries superimposed on the aerial imagery, and Map 17-3 presents the solar facility and land portion boundaries overlain on the geological map.



Map 17-2: Aerial view delineating the study area of the 12 Kudu Solar Facilities (Google, 2022). Note that this report is focused on Kudu Solar Facility 2.

17.4.3 Project Specific Description

17.4.3.1 Climate

The study area experiences a semi-arid climate, with most of the rainfall occurring during February to March. Figure 17-1 shows the monthly average minimum and maximum air temperature distribution and Figure 17-2 shows the monthly average rainfall and evaporation distribution for the study area (Schulze, 2009). The long-term (1950 – 2000) average annual precipitation for the study area is 281 mm/a. The rainfall does not exceed evaporation during the course of the year.

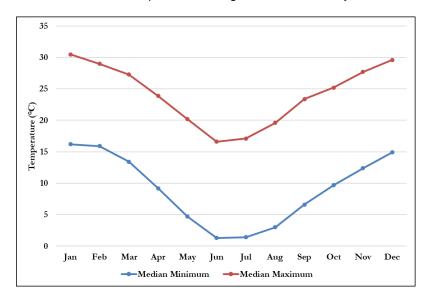


Figure 17-1: Monthly average air temperature distribution for the Kudu Solar Facility study area (Schulze, 2009)

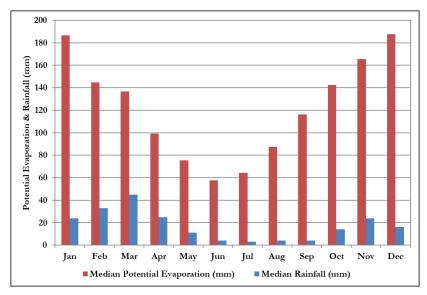


Figure 17-2: Monthly average rainfall and potential evaporation distribution for the Kudu Solar Facility study area (Schulze, 2009).

17.4.3.2 Weinert 'N' Value

The present and past climate is a useful indicator of the typical soil conditions that may be encountered on a particular site (Weinert, 1975). Weinert (1975) developed a general model to categorise the climate of southern Africa based on what he termed the 'N'-value (Figure 17-3). The Weinert 'N'-value for the project area is greater than 5 (Brink, 1983). For areas where Weinert 'N'-values exceed five (5), transported soils vary in thickness, and residual soils are anticipated to be shallow, and where pedocretes are developed they are expected to be calcrete and less commonly silcrete.

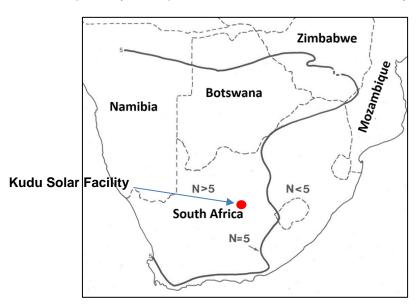


Figure 17-3: Climatic 'N' value = 5 plotted for southern Africa (after Weinert, 1967).

17.4.3.3 Regional Geology

The Geological Survey of South Africa (now the Council for Geoscience) has mapped the area at 1:250 000 scale (3024, Colesberg). The geological setting is shown in Map 17-3. The main geology of the area is listed in Table 17-2.

Table 17-2: Geological formation within the study area.

Symbol	Formation	Group	Lithology
~~	Quaternary Depos	sit	Alluvium / Terrace Gravel
Qc	,	Calcrete	
Jd	Jurassic Intrusion		Dolerite
Pa	Adelaide Subgroup	Beaufort Group	Blue-grey silty mudstone, subordinate brownish-red mudstone; sandstone
Pt	Tierberg Formation	Ecca Group	Blue-grey to black shale with carbonate-rich concretions; subordinate siltstone and sandstone in upper part

The Kudu Solar Facility 2 is mainly underlain by Quaternary alluvium deposits and well-developed calcretes. These quaternary deposits, in turn, overly either dolerite sills and dykes (Jd) or undifferentiated sediments of the Adelaide Subgroup (Pa) and/or Tierberg Formation (Pt). The Adelaide Subgroup (Pa) comprises interbedded mudstones, siltstones and sandstone, and the Tierberg Formation (Pt) consists primarily of shale and sandstone. Both of these units were deposited within a braided river to deltaic setting within the Karoo basin during the Permian Period some 268 to 247 million years ago (Johnson et al., 2006). These sediments were subsequently intruded during the Jurassic Period by dolerite sills and dykes of the Karoo Dolerite Suite. There are no known large structural geological features in the surrounding area of the proposed project; however, the dolerite sills in the area commonly show extensive jointing as a result of cooling and exhumation.

The site has been broadly classified into three zones of similar anticipated geological and geotechnical characteristics (Zones A, B and C). The zones are presented in Map 17-4, and are expanded upon in subsequent sections. Supporting information and literature on the anticipated engineering characteristics for materials anticipated for soils and rocks in geotechnical zones are presented in **Appendix G of this chapter**.

17.4.3.4 Geotechnical Properties and Engineering Geology

Sandstones and mudstones (Zone A)

Problems with slope stability may be experienced where sandstones and shales/mud rocks of the Karoo Supergroup are closely intercalated, as weathering of the fine-grained rocks may result in undercutting (Brink, 1983). Porewater pressure may develop at the interface between sand- and mud-/siltstones (Brink, 1983). Where sandstones are thickly bedded and highly jointed, joint-controlled block and wedge failures can potentially occur (Brink, 1983).

Dolerite (Zone B)

The end of the Karoo age was terminated by the intrusion of dolerite dykes and sills into the Karoo sedimentary rocks. The intrusive dolerites only had a limited thermal metamorphism effect on the surrounding Karoo sediments, as a rule of thumb, causing changes to the host lithology of equivalent thickness to the dyke itself (Brink, 1983).

During the late 1960s and early 1970s, several tests were undertaken to determine the strength properties of dolerite rock. The general description of dolerite was as follows, bluish-grey, very hard to extremely hard rock, variably fine- and medium-grained, variably jointed and fractured, with calcite, chlorite and zeolite minerals present on the joint and fracture surfaces in varying amounts (Brink, 1983). Of relevance to this assessment, dolerite rocks are considered erosion resistant.

Quaternary sediments (Zone C)

Quaternary sediments in the region include alluvium and terrace gravels (CGS, 1991). The geotechnical characteristics of such materials are variable in nature. Typical construction constraints with such materials include a potentially collapsible grain structure associated with sandy sediments, and challenging excavation conditions associated with terrace gravels, particularly where boulders are encountered. Often, transported soils of mixed origin may be potentially collapsible (Brink, 1983). Moreover, alluvium, depending on several factors, can be potentially expansive. The potential geotechnical problems would have to be investigated during the field investigations. Calcrete has been mapped in the area. Calcrete could be investigated as a construction material for incorporation in the construction of the proposed development. The reserves of calcrete would have to be proven on-site.

Expected soil profile

In the region between Orange River and Beaufort West, the sandstones and mudrocks of the Karoo supergroup often dip gently. The topography is generally undulating, and areas of strong relief are usually present where intrusive dolerite sills create a capping characterised by a landscape of mesas and buttes. According to Brink (1983), the hillslopes of such topography, here and in most arid areas of the world, usually display up to four soil profiles (Figure 17-4).

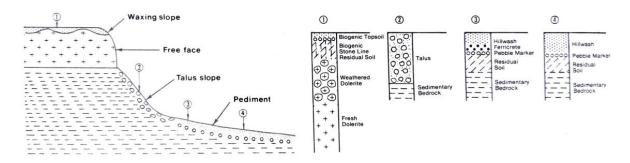


Figure 17-4: Elements of typical Karoo hillslopes and anticipated soil profiles (Brink, 1982)

Slope Classification

The topography is the region that has been classified in terms of development based on classes suggested by Stiff et al. (1996), see Map 17-5. A digital elevation model (DEM, 2018) has been used to determine slope gradients, which have been classified in terms of development potential in the region where development is to take place. The majority of the region is classified as "most favourable" and "intermediate" due to the generally flat nature of the site. A northeast trending linear feature of "least favourable" development potential (red) has been determined to be an overhead transmission line, i.e., a powerline (Map 17-5).

Seismicity

It is common practice to design structures for seismic loads when the nominal peak acceleration exceeds a 0.1 g once every 475 years (Retief and Dunaiski, 2009). Retief and Dunaisk (2009) delineated such regions in southern Africa, the approximate position of the proposed Kudu Solar Facility is shown in red on Figure 17-5 relative to these regions. The region surrounding Kudu Solar Facility, although generally low, is shown to have a nominal peak ground of more than 0.1 g; therefore, seismic loads should be considered when designing structures in this area.

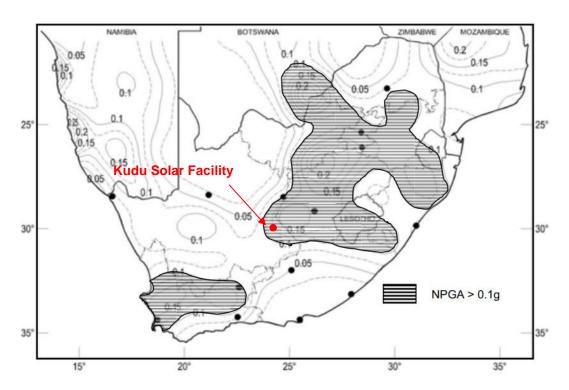
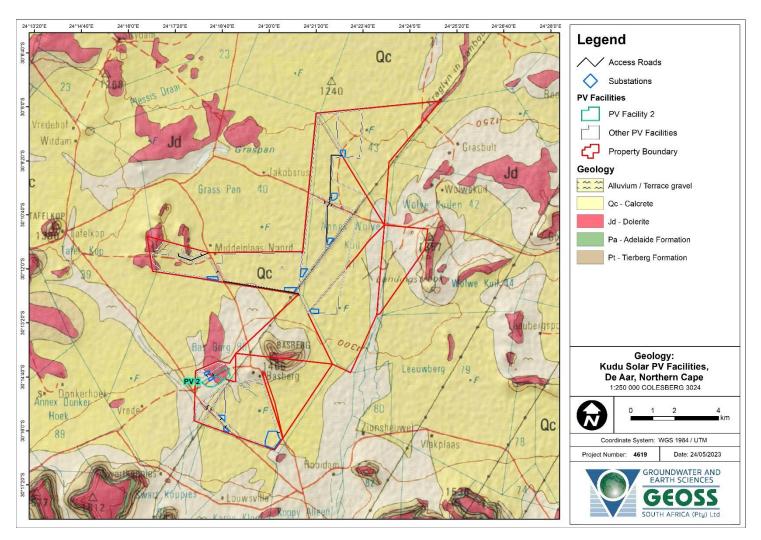


Figure 17-5: Zones in South Africa with nominal peak ground acceleration (NPGA) of more than 0.1 g for 10% in 50 years probability showing approximate position of the Kudu Solar Facility (after Retief and Dunaiski, 2009).

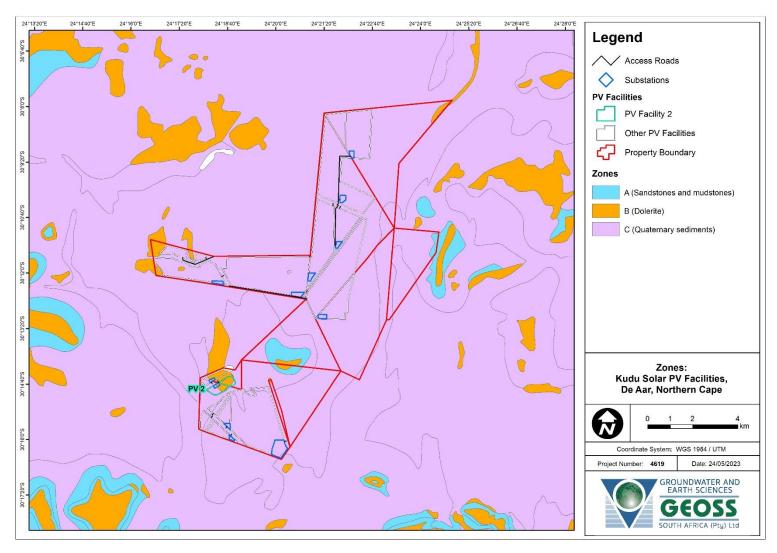
Regional Hydrogeology

The regional aquifer directly underlying the proposed project is classified by the Department of Water Affairs and Forestry (DWAF) (DWAF, 2005) as a fractured aquifer with an average yield potential of 0.5 – 2.0 L/s. However, based on the geological map and the site-specific information, it is known that the Quaternary Deposits of alluvium and calcrete form an intergranular aquifer on top of the fractured bedrock. There is no known published information about this aquifer.

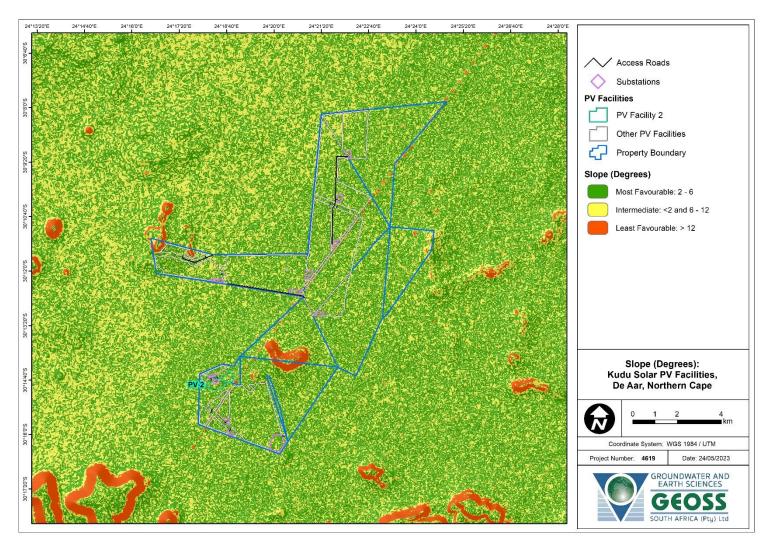
Based on the DWAF (2005) mapping of the regional groundwater quality, as indicated by electrical conductivity (EC), the groundwater underlying the Kudu Solar Facility and the surrounding area is in the range of 70 - 300 mS/m. This is considered to be "good to marginal" quality for water with respect to drinking water standards. Both these classifications are based on regional datasets and therefore only indicate conditions to be expected.



Map 17-3: Geological setting of the study area for the 12 Kudu Solar Facilities. Note that this report is focused on Kudu Solar Facility 2.



Map 17-4: Broad geotechnical zones across the study area. Note that this report is focused on Kudu Solar Facility 2.



Map 17-5: Regional slope classification based on Stiff et al. (1996). Note that this report is focused on Kudu Solar Facility 2.

17.4.4 Identification of Environmental Sensitivities

17.4.4.1 Sensitivities identified by the National Web-Based Environmental Screening Tool

Part of the terms of reference for the Kudu Solar Facility was to identify sensitivities by the National Web-Based Environmental Screening Tool. However, it is important to note that there are no dedicated Geotechnical themes on the National Web-based Environmental Screening Tool (Screening Tool) (as of May 2023); therefore, the environmental sensitivity of the proposed project area as identified by the Screening Tool is not applicable. For this reason, no site sensitivity verification report is required, and no map can be made available. Furthermore, no dedicated assessment protocol is prescribed for conducting a Desktop Geotechnical Assessment. Therefore, this specialist assessment has been undertaken in compliance with Appendix 6 of the NEMA EIA Regulations of 2014.

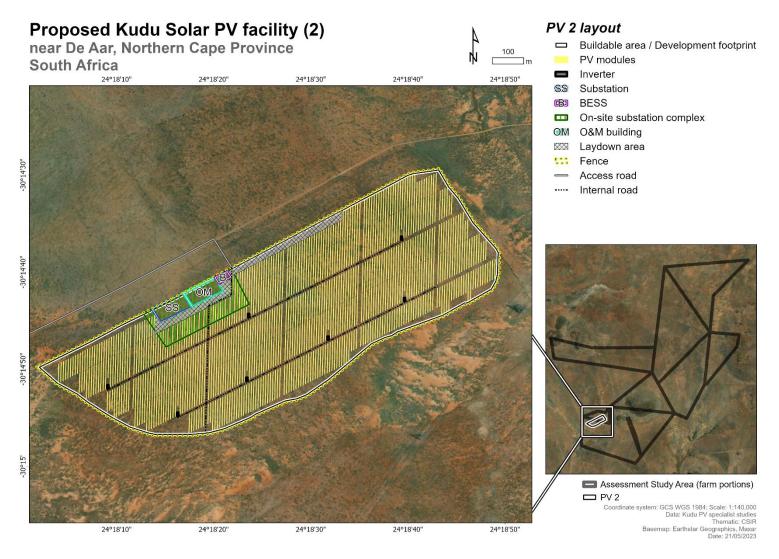
17.4.4.2 Specialist Sensitivity Analysis and Verification

The construction of infrastructure for the proposed solar facility will require several activities, e.g., stripping of vegetation (where required), excavation of foundation trenches etc., to take place (as described in Section 17.1.4 and Section 17.3) which will disturb the soils and rocks underlying the site. In areas of the study area where steeper topography is present, deeper excavations or more extensive site levelling may be required for construction to take place. The boundary of Kudu Solar Facility has been superimposed on the slope classifications and is indicated on (Map 17-5). In areas classed as "least favourable", steep slopes are expected; these will likely need to be dealt with by excavation where necessary. Here relevant mitigation measures will need to be adopted; these are expanded on in the section "Impact Assessment".

17.4.4.3 Sensitivity Analysis Summary Statement

No site sensitivity information is available for the study area and there are no areas on site that should be avoided from a geotechnical sensitivity perspective. However, areas of moderate to steep topography would likely render development financially unfeasible. GEOSS had previously undertaken a site sensitivity verification during the groundwater specialist assessment, the details of which are indicated in **Appendix C of this chapter (Site Sensitivity Verification)**. The information collected during the groundwater specialist assessment generally confirms the geotechnical information available for the lithologies in the area.

As indicated above, following the identification of sensitivities during the Scoping Phase, the Project Developer considered such sensitivities and formulated the Revised Scoping Buildable Areas. The Revised Scoping Buildable Areas led to the identification of the development footprints and detailed layouts in the EIA Phase. The development footprint and detailed layout are considered suitable from a geotechnical perspective. The development footprint and detailed layout are shown in Map 17-6. Changes to the detailed layouts are deemed acceptable if the changes remain within the approved buildable areas / development footprints and area assessed during the Scoping and EIA Process with no-go sensitive areas avoided.



Map 17-6: Detailed layout of Kudu Solar Facility 2.

17.5 Issues, Risks and Impacts

17.5.1 Identification of Potential Impacts/Risks

Potential impacts during construction, operational, and decommissioning phases are listed in this section.

Potential impacts on the geotechnical conditions as a consequence of the proposed development are as follows for the construction phase:

- Impact 1: Displacement of geologic materials.
- Impact 2: Contamination of subsoils and loss of topsoil.

Potential impacts on the geotechnical conditions as a consequence of the proposed development are as follows for the operational phase:

- Impact 1: Increased unnatural hard surfaces yielding increased runoff, potentially increasing erosion.
- Impact 2: Contamination of subsoils and loss of topsoil.

Potential impacts on the geotechnical conditions as a consequence of the proposed development are as follows for the decommissioning phase:

- Impact 1: Increased unnatural hard surfaces yielding increased runoff, potentially increasing erosion.
- Impact 2: Contamination of subsoils and loss of topsoil.

It is important to mention that the phases, construction, operation and decommissioning include all infrastructure-related components of the proposed development. The components of the proposed development are elaborated on in the Section 17.1.4 and Section 17.3.

Cumulative Impacts

- Impact 1 Displacement of geologic materials.
- Impact 2 Contamination of geologic materials.
- Impact 3 Increased unnatural hard surfaces yielding increased runoff, potentially increasing erosion.

A possible positive indirect impact could be the accumulation of topsoil in low-lying areas surrounding the site.

17.5.2 Summary of Issues identified during the Public Consultation Phase

No issues were raised during the Scoping Phase regarding geotechnical impacts.

17.6 Impact Assessment

The impact of the proposed project on the geological and/or geotechnical environment will predominantly relate to the impact/effect that the development will have on the soils / rock units beneath the site through topsoil stripping, excavations for foundations (where required), trenching, the construction of access tracks and associated light infrastructure. Bulk earthworks, where required, particularly in areas of steeper topography, for the construction of platforms and access tracks, and may generate a significant impact on the soils and rocks where such construction activities take place. For example, in such areas, removal of large quantities of rock may be required.

A primary concern in terms of potential environmental impacts associated with geotechnical works is displacement of geologic materials, e.g., increased soil erosion on site due to stripping of vegetation during the construction phase of the project. Removal of vegetation reduces infiltration, thereby increasing runoff yielding increased erosion. Further, compaction during earthworks reduces rainwater infiltration and increase surface runoff and increase erosion. The construction of paved and/or hard-surfaced areas increases runoff and often localises discharge of stormwater, which may lead to increased erosion and consequently loss of topsoil. Disturbance of the soil may extend beyond the footprint of the structures should such conditions persist for long periods of time, e.g., more than ten years.

Coupled with the potential for the displacement of geologic materials is the risk of soil contamination from on-site activities. Conventional construction and earthworks make use of construction equipment, which with poor maintenance, cause leakages and result in refuelling spillages during construction and/or decommissioning.

Potential risks associated with the operational phase mainly include erosion and contamination of geologic materials. This could be mitigated and managed by adopting appropriate drainage designs.

The above is discussed in subsequent sections with particular reference to possible activities and phases of development.

17.6.1 Potential Impacts during the Construction Phase

The impact table for the Construction Phase is presented in Table 17-3.

17.6.1.1 Impact 1: Displacement of Geologic Material: Removal of rocks and other geologic materials for site levelling and grading, resulting in loss of geologic materials, e.g., topsoil removal/loss, and potentially the destruction of habitats of endemic species.

Stripping of topsoil, general site levelling, and the removal of rocks is common during the initial stages of the construction phase. The loss of geologic material, the disturbance of naturally intact soil, and the removal of vegetation might all result in soil erosion. The status of this impact is rated as negative with a local spatial extent and a short-term duration (i.e., for the construction phase). The consequence and probability of the impact are respectively rated as moderate and very likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as low. With effective implementation of mitigation actions, the impact is predicted to be of very low significance. The mitigation measures are listed in the table below.

17.6.1.2 Impact 2: Contamination of geologic materials as a consequence of the construction activities by earthworks machinery and other apparatus.

Construction involves heavy machinery and apparatus especially during earth work activities. This might include graders, bulldozers, rollers, excavators, water trucks and, concrete mixers. This type of equipment requires regular greasing and operates with hydraulic fluid and diesel which might potentially cause contamination of geological materials. The status of this impact is rated as negative with a local spatial extent and a short-term duration (i.e. for the construction phase). The consequence and probability of the impact are respectively rated as moderate and very likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as low. With effective implementation of mitigation actions, the impact is predicted to be of very low significance. The mitigation measures are listed in the table below.

17.6.1.3 Impact Summary Tables: Construction Phase

Table 17-3: Impact Summary Tables: Construction Phase

Impact	Impact Criteria		Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post- Mitigation)	Confidence Level
			CONS	STR	UCTION PHASE		
Impact 1 Displacement of geologic materials	Status Spatial Extent Duration Consequence Probability Reversibility Irreplaceability	Negative Local Short term Moderate Very likely Moderate Moderate	Low		Favour dolerite as an aggregate (as opposed to Karoo sandstones and mudstones). Subject to investigation. Any road cuttings should be designed by an appropriately qualified professional. Drainage in the region should be designed and managed appropriately. Investigate and confirm the geotechnical suitability of each structure (or other appropriate level of investigation) prior to construction (i.e., determine that soil with an adequate bearing capacity is obtained beneath each footing). Such investigations would not be required to fulfil the requirements of this Environmental Impact Assessment (EIA) process. However, it would be necessary prior to construction. Only strip vegetation necessary for the next phase of construction. Install temporary drainage to divert stormwater away from active construction activities, where required. Stormwater Management Plan must be developed in the preconstruction phase. It should detail the stormwater structures and management interventions that must be installed to manage the increase of surface water flow directly into any natural systems (in consultation with suitably qualified professionals). Effective stormwater management must include effective	Very Low	Medium

Impact	Impact Criteria	Significance and Ranking (Pre-Mitigation)	Potential mitigation measures	Significance and Ranking (Post- Mitigation)	Confidence Level
			 stabilisation (e.g., gabions and Reno mattresses) of exposed soil. Suitable stormwater management systems must be installed along roads and other areas and be monitored during the first few months of use. Any erosion/sedimentation must be resolved through any additional interventions that may be necessary (e.g., extension, energy dissipaters, spreaders, etc.). Where impacted through construction-related activities, all sloped areas must be stabilised to ensure proper rehabilitation is affected and erosion is controlled. Sloped areas stabilised using designed structures or vegetation as specified in the design to prevent erosion of embankments. The contract design specifications must be adhered to and implemented strictly. Any rehabilitation should be scheduled to ensure rehabilitation can take place at the optimal time for vegetation establishment. Where earthwork is being undertaken near any watercourses, slopes must be stabilised using suitable materials, e.g., sandbags or geotextile fabric, to prevent sand and rock from entering the channel. Appropriate rehabilitation and re-vegetation measures for any disturbed watercourse banks must be implemented timeously. In this regard, the banks should be appropriately and incrementally stabilised as soon as development allows. 		

Table 17-3: Impact Summary Tables: Construction Phase (cont.)

Impact	Impact Ci	riteria	Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level		
CONSTRUCTION PHASE									
Impact 2 Contamination of geologic materials	Status Spatial Extent Duration Consequence Probability Reversibility Irreplaceability	Negative Local Short term Moderate Very likely Moderate Moderate	Low		During the execution of the works, appropriate measures to prevent pollution and contamination of the riparian environment must be implemented, e.g. including ensuring that construction equipment is well maintained. Provision must be made for refuelling at the storage area by protecting the soil with an impermeable groundcover. Where dispensing equipment is used, a drip tray must be used to ensure small spills are contained. Where refuelling away from the dedicated refuelling station is required, a mobile refuelling unit must be used. Appropriate ground protection such as drip trays must be used. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilt material, as reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.	Very Low	Medium		

17.6.2 Potential Impacts during the Operational Phase

The impact table for the Operational Phase is presented in Table 17-4.

17.6.2.1 Impact 1: Increased unnatural hard surfaces yielding increased runoff, potentially increasing erosion.

The operational phase will partially consist of access point/s and internal roads. This involves newly constructed road layers effectively creating unnatural hard surfaces. This might also include earth/concrete drains to divert water away from access points/roads. In return this might yield increased runoff effectively increasing erosion. The status of this impact is rated as negative with a local spatial extent and a long-term duration. The consequence and probability of the impact are respectively rated as moderate and likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as low. With effective implementation of mitigation actions, the impact is predicted to be of very low significance. The mitigation measures are listed in the table below.

17.6.2.2 Impact 2: Contamination of geologic materials as a consequence of typical maintenance activities, as example, washing of solar panels, or spillages associated with battery energy storage facilities.

During the operational phase, geologic material might potentially be contaminated as a consequence of maintenance activities and/or spillages. For optimal functionality of the solar facility, solar panels must be free from dust deposits and any obstruction from the solar panel face. Washing and maintaining of solar panels might result in chemical contamination of geologic materials. Further chemical contamination may transpire from spillages by the BESS as these facilities potentially contain either flow based batteries or solid state batteries. The status of this impact is rated as negative with a local spatial extent and a short-term duration. The consequence and probability of the impact are respectively rated as moderate and very likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as low. With effective implementation of mitigation actions, the impact is predicted to be of very low significance. The mitigation measures are listed in the table below.

17.6.2.3 Impact Summary Tables: Operational Phase

Table 17-4: Impact Summary Tables: Operational Phase

Impact	Impact C	criteria	Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
				0	PERATIONAL PHASE		
Impact 1 Increased unnatural hard surfaces	Status Spatial Extent Duration Consequence Probability Reversibility Irreplaceability	Negative Local Long term Moderate Likely Moderate Moderate	Low	1. 2. 3.	Install drainage to divert stormwater away from activities, roads/tracks, structures, where required. Generic management for typical infrastructure of the proposed development, including: Stormwater Management Plan must be developed in the preconstruction phase and should detail the stormwater structures and management interventions that must be installed to manage the increase of surface water flows directly into any natural systems, where possible and lawful. Effective stormwater management must include effective stabilisation (e.g., gabions and Reno mattresses) of exposed soil etc. Suitable stormwater management systems must be installed along roads and other areas and monitored during the first few months of use. Any erosion / sedimentation must be resolved through any additional interventions that may be necessary (e.g., extension, energy dissipaters, spreaders, etc.). Sloped areas stabilised using design structures or vegetation as specified in the design to prevent erosion of embankments. No regular maintenance activities to take place outside of the authorised footprint and all	Very Low	Medium

Table 17-4: Impact Summary Tables: Operational Phase (cont.)

Impact	Impact C	riteria	Significance and Ranking (Pre-Mitigation)	Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
				OPERATIONAL PHASE		
Impact 2	Status	Negative	Low	During the execution of the operations,	Very Low	Medium
	Spatial Extent	Local		appropriate measures to prevent pollution and		
Contamination	Duration	Short term		contamination of the riparian environment must be implemented e.g. including ensuring that		
of geologic	Consequence	Moderate				
materials	Probability	Very likely		construction equipment is well maintained;		
	Reversibility Moderate		Provision must be made for refuelling at the storage area by protecting the soil with an			
	Irreplaceability	Moderate		impermeable groundcover/bunding. Where dispensing equipment is used, a drip tray must be used to ensure small spills are contained. Where refuelling away from the dedicated refuelling station is required, a mobile refuelling unit must be used. Appropriate ground protection such as drip trays must be used. Electrolyte spillage to be mitigated through leak detection, double containment and suitably designed bunding for the structure, approved by a qualified professional. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, as reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.		

17.6.3 Potential Impacts during the Decommissioning Phase

The impact table for the Decommissioning Phase is presented in Table 17-5.

17.6.3.1 Impact 1: Increased unnatural hard surfaces yielding increased runoff, potentially increasing erosion.

Access points, internal road and sufficient drainage will continue to form part of the decommissioning phase. Unnatural hard surfaces will potentially be present continuously yielding runoff causing erosion. The status of this impact is rated as negative with a local spatial extent and a short-term duration. The consequence and probability of the impact are respectively rated as slight and likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as very low. With effective implementation of mitigation actions, the impact is predicted to be of very low significance. The mitigation measures are listed in the table below.

17.6.3.2 Impact 2: Contamination and disturbance of geologic materials as a consequence of typical decommissioning activities.

Similar to the construction phase, dismantling of the facility will potentially involve the use of heavy machinery. On going maintenance of equipment and refuelling activities increase the risk of spillages which might potentially cause contamination of geological material. The status of this impact is rated as negative with a local spatial extent and a short-term duration. The consequence and probability of the impact are respectively rated as slight and likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as very low. With effective implementation of mitigation actions, the impact is predicted to be of very low significance. The mitigation measures are listed in the table below.

17.6.3.3 Impact Summary Tables: Decommissioning Phase

Table 17-5: Impact Summary Tables: Decommissioning Phase

Impact	Impact C	Criteria	Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
			DE	CO	MMISSIONING PHASE		
Impact 1	Status	Negative	Very low	•	Only drive and park vehicles where necessary.	Very Low	Medium
,	Spatial Extent	Local		•	Land rehabilitation to near natural state, i.e.,	,	
Increased	Duration	Short term			removal of foundations and backfilling of any		
unnatural hard	Consequence	Slight			resultant voids within the soil, as well as removal of hard surfaced areas. Replacement soil should		
surfaces	Probability	Likely			be sourced locally to ensure homogeneity.		
Reversibility	Reversibility	Moderate			Reinstate natural topography where cut-to-fill		
	Irreplaceability	Moderate			embankments have been constructed. Implement generic environmental management procedures for infrastructure.		
Impact 2	Status	Negative	Very low	appropriate measures to prevent pollution and contamination of the riparian environment must be implemented e.g., including ensuring that equipment is well maintained; Provision must be made for refuelling at the		Very Low	Medium
	Spatial Extent	Local					
Contamination	Duration	Short term					
of geologic	Consequence	Slight					
materials	Probability	Likely					
	Reversibility	Moderate			storage area by protecting the soil with an		
	Irreplaceability	Moderate			impermeable groundcover. Where dispensing equipment is used, a drip tray must be used to ensure small spills are contained. Where refuelling away from the dedicated refuelling station is required, a mobile refuelling unit must be used. Appropriate ground protection such as drip trays must be used. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, as reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.		

17.6.4 Cumulative Impacts

The cumulative impacts of the proposed Kudu Solar Facility and other approved and in process renewable energy facilities and electricity grid infrastructure (EGI) within a 30 km radius from the study area are presented in this section. The cumulative impacts identified include the impacts related to the construction, operational and decommissioning phases across the proposed Kudu Solar Facility. In general, the impacts during the different phases of the project are quite similar therefore, their intensities increase as the project progresses resulting in a higher probability for the impact to occur.

According to information collected by the CSIR from the Renewable Energy EIA Database and the South African Heritage Resources Information System (SAHRIS) (~February 2023), 12 other renewable energy facility clusters and EGI have been approved, or in the process of approval in terms of the NEMA EIA Regulations, that are located within a 30 km radius from the Kudu Solar Facilities Map 17-7. Three of these renewable energy facilities are already existing and operational. In addition, approximately 10 existing Eskom power lines fall within the 30 km radius of the proposed project, with three Eskom planned power line projects, as shown in Map 17-7. Failing to implement effective mitigation measures throughout the lifespan of projects might cause the intensity of different identified impacts to increase. **Appendix F** of this chapter contains APPENDIX F - APPROVED RENEWABLE ENERGY PROJECTS

Table covering the details of approved, existing and in process projects within a 30 km radius of the proposed Kudu Solar Facility as provided by the CSIR.

The types of impacts of these developments are nearly identical to each other, with the main cumulative effect being an increase in impact severity for construction, operational, and decommissioning phase. This increase in cumulative severity will be especially exacerbated for the construction phase, in the case that construction of all the proposed developments within a 30km radius occurs simultaneously. The cumulative impact of all these developments during the operational phase should be quite low as long as the proposed mitigation measures and appropriate erosion monitoring is implemented.

Livestock farming is the main activity in the developable area of the proposed project. It is therefore crucial that the footprint of the proposed Kudu Solar Facility does not exceed its borders and negatively impact neighbouring agricultural activities. However, note that an Agricultural Compliance Statement has been undertaken as part of this EIA Process, which adequately addresses agricultural impact. Refer to Chapter 6 of the EIA Report for the Agricultural Compliance Statement. The intensity of the identified cumulative impacts should be suppressed by implementing effective mitigation measures to minimise (1) the contamination of geological materials and (2) the displacement of geological materials.

The cumulative impacts and mitigation measures for the Construction, Operational and Decommissioning Phases are contained in Table 17-6, Table 17-7, and Table 17-8, respectively.

Overall, the risk that impacts associated with removal, displacement, and contamination of geological material beyond this project site is very low as long as the appropriate mitigation measures are

implemented. Furthermore, the risk of this project receiving cumulative impacts from the surrounding developments is also quite low, providing appropriate mitigation measures are followed.

17.6.5 Potential Cumulative Impacts during the Construction Phase

17.6.5.1 Impact 1: Displacement of Geologic Material: Removal of rocks and other geologic materials for site levelling and grading, resulting in loss of geologic materials, e.g., topsoil removal/loss, and potentially the destruction of habitats of endemic species.

Refer to the description of the impact above for the construction phase. The status of this impact is rated as negative with a regional spatial extent and a medium-term duration. The consequence and probability of the impact are respectively rated as substantial and very likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of mitigation actions, the impact is predicted to be of low significance. The mitigation measures are listed in the table below.

17.6.5.2 Impact 2: Contamination of geologic materials as a consequence of the construction activities by earthworks machinery and other apparatus.

Refer to the description of the impact above for the construction phase. The status of this impact is rated as negative with a regional spatial extent and a medium-term duration. The consequence and probability of the impact are respectively rated as substantial and very likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of mitigation actions, the impact is predicted to be of low significance. The mitigation measures are listed in the table below.

17.6.6 Potential Impacts during the Operational Phase

17.6.6.1 Impact 1: Increased unnatural hard surfaces yielding increased runoff, potentially increasing erosion.

Refer to the description of the impact above for the operational phase. The status of this impact is rated as negative with a regional spatial extent and a long-term duration. The consequence and probability of the impact are respectively rated as substantial and very likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of mitigation actions, the impact is predicted to be of low significance. The mitigation measures are listed in the table below.

17.6.6.2 Impact 2: Contamination of geologic materials as a consequence of typical maintenance activities, as example, washing of solar panels, or spillages associated with battery energy storage facilities.

Refer to the description of the impact above for the operational phase. The status of this impact is rated as negative with a regional spatial extent and a medium-term duration. The consequence and probability of the impact are respectively rated as substantial and very likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the

implementation of mitigation measures is rated as moderate. With effective implementation of mitigation actions, the impact is predicted to be of low significance. The mitigation measures are listed in the table below.

17.6.7 Potential Impacts during the Decommissioning Phase

17.6.7.1 Impact 1: Increased unnatural hard surfaces yielding increased runoff, potentially increasing erosion.

Refer to the description of the impact above for the decommissioning phase. The status of this impact is rated as negative with a local spatial extent and a short-term duration. The consequence and probability of the impact are respectively rated as substantial and likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of mitigation actions, the impact is predicted to be of low significance. The mitigation measures are listed in the table below.

17.6.7.2 Impact 2: Contamination and disturbance of geologic materials as a consequence of typical decommissioning activities.

Refer to the description of the impact above for the decommissioning phase. The status of this impact is rated as negative with a local spatial extent and a short-term duration. The consequence and probability of the impact are respectively rated as substantial and likely. The reversibility and irreplaceability of the impact are rated as moderate. The significance of the impact without the implementation of mitigation measures is rated as moderate. With effective implementation of mitigation actions, the impact is predicted to be of low significance. The mitigation measures are listed in the table below.

17.6.7.3 Impact Summary Tables: Cumulative Impacts

Table 17-6: Cumulative Impact Summary Tables: Construction Phase

Impact	Impact C	Criteria	Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
				СО	NSTRUCTION PHASE		
Impact 1	Status	Negative	Moderate	•	Only strip vegetation necessary for the next	Low	Medium
	Spatial Extent	Regional			phase of construction.		
Displacement	Duration	Medium-		•	Install temporary drainage to divert stormwater		
of geologic		term			away from active construction activities, where		
materials	Consequence	Substantial			required.		
matorialo	Probability	Very likely		•	Stormwater Management Plan must be		
	Reversibility	Moderate			developed in the preconstruction phase. It		
	Irreplaceability	Moderate			should detail the stormwater structures and management interventions that must be installed to manage the increase of surface water flows directly into any natural systems (in consultation with suitably qualified professionals). Effective stormwater management must include effective stabilisation (e.g., gabions and Reno mattresses) of exposed soil. Suitable stormwater management systems must be installed along roads and other areas and be monitored during the first few months of use. Any erosion/sedimentation must be resolved through any additional interventions that may be necessary (e.g., extension, energy dissipaters, spreaders, etc). Where impacted through construction-related activities, all sloped areas must be stabilised to ensure proper rehabilitation is affected and erosion is controlled. Sloped areas stabilised using designed structures or vegetation as specified in the		

Impact	Impact Criteria	Significance and Ranking (Pre-Mitigation)	Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
			design to prevent erosion of embankments. The contract design specifications must be adhered to and implemented strictly. Any rehabilitation should be scheduled to ensure rehabilitation can take place at the optimal time for vegetation establishment. Where earthwork is being undertaken in near any watercourses, slopes must be stabilised using suitable materials, e.g. sandbags or geotextile fabric, to prevent sand and rock from entering the channel. Appropriate rehabilitation and re-vegetation measures for any disturbed watercourse banks must be implemented timeously. In this regard, the banks should be appropriately and incrementally stabilised as soon as development allows.		

Table 17-6: Cumulative Impact Summary Tables: Construction Phase (cont.)

Impact	Impact C	Criteria	Significance and Ranking (Pre-Mitigation)	Potential mitigation measures	Significance and Ranking Post-Mitigation)	Confidence Level
			C	CONSTRUCTION PHASE		
Impact 2 Contamination of geologic materials	Status Spatial Extent Duration Consequence Probability Reversibility Irreplaceability	Negative Regional Mediumterm Substantial Very likely Moderate Moderate	Moderate	 During the execution of the works, appropriate measures to prevent pollution as contamination of the riparian environment must be implemented, e.g., including ensuring the construction equipment is well maintained. Provision must be made for refuelling at the storage area by protecting the soil with a impermeable groundcover. Where dispensite equipment is used, a drip tray must be used ensure small spills are contained. Where refuelling away from the dedicate refuelling station is required, a mobile refuelling unit must be used. Appropriate ground protection such as drip trays must be used. If spillages occur, they should be contained and removed as rapidly as possible, we correct disposal procedures of the spillages. 	ad state of the control of the contr	Medium

Table 17-7: Cumulative Impact Summary Tables: Operational Phase

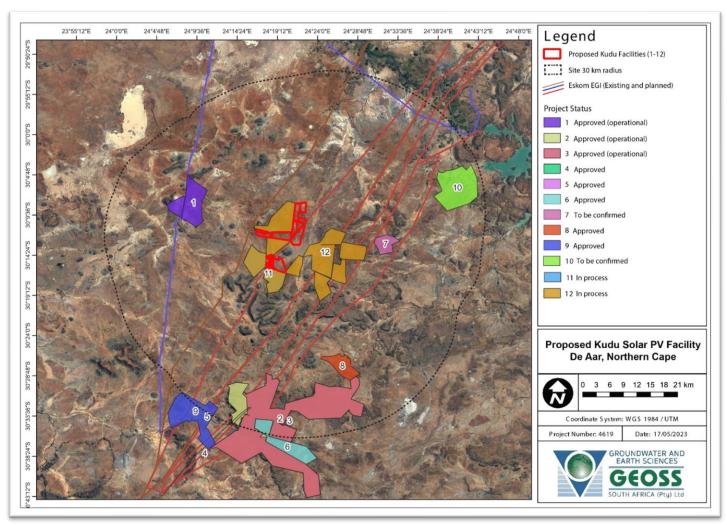
Impact	Impact C	Criteria	Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post- Mitigation)	Confidence Level			
OPERATIONAL PHASE										
Impact 1 Increased unnatural hard surfaces	Status Spatial Extent Duration Consequence Probability Reversibility Irreplaceability	Negative Regional Long-term Substantial Very likely Moderate Moderate	Moderate	1. 2. 3.	Install drainage to divert stormwater away from activities, roads/tracks, structures, where required. Generic management for typical infrastructure of the proposed development, including: Stormwater Management Plan must be developed in the preconstruction phase and should detail the stormwater structures and management interventions that must be installed to manage the increase of surface water flows directly into any natural systems, where possible and lawful. Effective stormwater management must include effective stabilisation (gabions and Reno mattresses) of exposed soil etc. Suitable stormwater management systems must be installed along roads and other areas and monitored during the first few months of use. Any erosion / sedimentation must be resolved through any additional interventions that may be necessary (e.g., extension, energy dissipaters, spreaders, etc.). Sloped areas stabilised using design structures or vegetation as specified in the design to prevent	Low	Medium			
				4.	erosion of embankments. No regular maintenance activities to take place outside of the authorised footprint and all vehicles to remain on authorised roads and tracks.					

Table 17-7: Cumulative Impact Summary Tables: Operational Phase (cont.)

Impact	Impact C	riteria	Significance and Ranking (Pre-Mitigation)		Potential mitigation measures	Significance and Ranking (Post-Mitigation)	Confidence Level
				OI	PERATIONAL PHASE		
Impact 2	Status	Negative	Moderate		During the execution of the operations,	Low	Medium
	Spatial Extent	Regional			appropriate measures to prevent pollution and		
Contamination	Duration	Medium-			contamination of the riparian environment must		
of geologic		term			be implemented e.g., including ensuring that		
materials	Consequence	Substantial			construction equipment is well maintained.		
Probability Very likely		•	Provision must be made for refuelling at the				
	Reversibility Moderate			storage area by protecting the soil with an			
	Irreplaceability	Moderate			impermeable groundcover/bunding. Where dispensing equipment is used, a drip tray must be used to ensure small spills are contained. Where refuelling away from the dedicated refuelling station is required, a mobile refuelling unit must be used. Appropriate ground protection such as drip trays must be used. Electrolyte spillage to be mitigated through double containment and suitably designed bunding for the structure, approved by a qualified professional. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, as reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for auditing purposes.		

Table 17-8: Cumulative Impact Summary Tables: Decommissioning Phase

Impact	Impact C	Criteria	Significance and Ranking (Pre- Mitigation)	Potential mitigation measures	Significance and Ranking (Post- Mitigation)	Confidence Level
			DE	ECOMMISSIONING PHASE		
Impact 1 Increase of unnatural hard surfaces	Status Spatial Extent Duration Consequence Probability Reversibility Irreplaceability	Negative Local Short term Substantial Likely Moderate Moderate	Moderate	 Only drive and park vehicles where necessary. Land rehabilitation to near natural state, i.e., removal of foundations and backfilling of any resultant voids within the soil, as well as removal of hard surfaced areas. Replacement soil should be sourced locally to ensure homogeneity. Reinstate natural topography where cut-to-fill embankments have been constructed. Implement generic environmental management procedures for infrastructure. 	Low	Medium
Impact 2 Contamination of geologic materials	Status Spatial Extent Duration Consequence Probability Reversibility Irreplaceability	Negative Local Short term Substantial Likely Moderate Moderate	Moderate	 During the execution of the decommissioning, appropriate measures to prevent pollution and contamination of the riparian environment must be implemented e.g., including ensuring that equipment is well maintained; Provision must be made for refuelling at the storage area by protecting the soil with an impermeable ground cover. Where dispensing equipment is used, a drip tray must be used to ensure small spills are contained. Where refuelling away from the dedicated refuelling station is required, a mobile refuelling unit must be used. Appropriate ground protection such as drip trays must be used. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, as reported. Proof of disposal (waste disposal slips or waybills) should be obtained and retained on file for 	Low	Medium



Map 17-7: Approved renewable energy projects within a 30 km radius from the proposed Kudu Solar Facility.

17.6.8 No-go Alternatives

In terms of the no-go alternative, if the proposed development does not go ahead, there will be no need for displacement and/or loss of topsoil in the area. However, to date, apart from the construction of farmhouses and the erection of boundary and subcamp fences for farming purposes; little disturbance of the subsoils and rocks in the area proposed for development has taken place. For this reason, the no-go alternative is considered of low significance. However, as noted above, the potential impacts of the proposed project from a geotechnical perspective are not considered to be very significant, especially if the recommended mitigation measures are adopted.

17.6.9 Battery Energy Storage System

Lithium-Ion BESS and Redox Flow BESS were both considered for the proposed project. For Redox Flow BESS, various chemical compositions are likely, such as Vanadium. Refer to Chapter 15 of this EIA Report for a High-Level Safety, Health and Environment Risk Assessment, which provides high level information on the safety, health and environmental risks of the BESS technologies.

Both Lithium Ion and Redox Flow BESS technologies have been assessed. It is important to note that the choice of technology will not be influenced by geotechnical factors, thus both options are considered suitable from a geotechnical standpoint.

17.7 Impact Assessment Summary

The overall impact significance findings, following the implementation of the proposed mitigation measures are shown in the Table 17-9.

Table 17-9: Overall Impact Significance (Post Mitigation)

Phase	Overall Impact Significance
Construction	Very Low
Operational	Very Low
Decommissioning	Very Low
Nature of Impact	Overall Impact Significance
Cumulative - Construction	Low
Cumulative - Operational	Low
Cumulative - Decommissioning	Low

The overall impact significance for all three phases of the Kudu Solar PV 2 Facility is considered very low, with the cumulative impacts for all of the Kudu Facilities and other relevant projects within a 30 km radius rated considered as Low, provided that responsible construction practises are adopted, and the proposed mitigation measures are utilized; for example, correct culvert design.

17.8 Legislative and Permit Requirements

This section has been divided as follows, based on the impacts that may transpire during the construction, operation and decommissioning phases of the proposed development:

- Loss of geological materials.
- Removal of geologic materials.
- Contamination of geologic materials as a consequence of typical maintenance activities.

From a permitting perspective, mining and quarrying on the proposed site is likely seen as a listed activity in terms of the NEMA, as amended. However, existing and permitted borrow pits will be used for the proposed projects, where necessary. Furthermore, where there may be existing services on the proposed development site and an excavation/wayleave permit may be required.

The norms and references given below are not exhaustive.

17.8.1 Loss of geologic materials (soil erosion)

Relevant legislation and guidelines pertaining to soil conservation, particularly soil erosion includes:

- Conservation of Agricultural Resources Act, 1983 (Act No 43 of 1983).
- Environmental Conservation Act, 1998 (Act No 73 of 1989).
- National Forestry Act, 1998 (Act No 84 of 1998, as amended).
- National Environmental Management Act, 1998 (Act No 107 of 1998), as amended.
- The Department of Water Affairs and Forestry, February 2005. Environmental Best Practice Specifications: Construction Integrated Environmental Management Sub-Series No. IEMS 1.6. Third Edition. Pretoria.

17.8.2 Contamination of geologic materials

Relevant literature pertaining to contamination of soil, includes:

- National Environmental Management: Waste Act, 2008 (Act No 59 of 2008).
- National Water Act, 1998 Act No 36 of 1998) Section 19.

17.9 Environmental Management Programme Inputs

From a Geotechnical point of view there are three main impacts caused by the different stages of the proposed development:

- 1. Displacement of geologic materials
- 2. The creation of unnatural hard surfaces
- 3. Contamination of geologic materials

From the impact assessment it can be anticipated that by displacing geological materials the existing soil conditions are disturbed and natural vegetation removed potentially causing soil erosion. Another impact that might further escalate erosion is the creation of unnatural hard surfaces i.e., road surfaces and stormwater drainage. Finally, potential contamination of geological material might be caused by spillages/leakages and maintenance procedures. Mitigating and monitoring of these impacts during the different phases of the project forms a vital part in the success of the development. Failing to implement mitigation and monitoring measures, the intensity of the different impacts may rise. All mitigation measures recommended in this assessment are included in the project EMPr. Listed below are the main EMPr inputs and management actions.

Construction Phase

The development of a stormwater management plan prior to the construction phase by a qualified professional is recommended. Suitable systems must preferably be installed along roads and other areas in order to divert water away from zones where the solar infrastructure is to be constructed. These systems should be monitored throughout the first few months of the construction phase during which any erosion/sedimentation should be resolved. It is recommended that rehabilitation commence soon after construction at the optimal time for vegetation establishment.

Provision should be made during refuelling operations to protect soil by means of impermeable ground cover. If spillages occur, they should be contained and removed as rapidly as possible with the correct disposal procedures. Ideally proof of disposal should be obtained and retained on file for auditing purposes.

Operational Phase

Similarly, to the construction phase it is recommended that a stormwater management plan to be implemented. It should preferably be designed by a qualified professional. This phase will potentially contain unnatural hard surfaces in the form of access roads, road layers, earth/concrete drains and, foundations. Similar to the construction phase, water should preferably be diverted away from road layers and erected structures.

It is recommended that similar mitigations and provisions with regards to spillages/leakages from the construction phase to be implemented during the operational phase. Additionally, proper designed bunding structures and double containment to be implemented at BESS to mitigate potential electrolyte spillage. It is recommended that the design should be approved by a qualified professional. Furthermore, maintenance of solar panels to be closely monitored and the use of hazardous chemical products to be avoided when solar panels are cleaned.

Decommissioning Phase

The main impacts are increased unnatural hard surfaces and the contamination of geological material. It is recommended that the natural topography to be reinstated and that rehabilitation of the land should take place to near natural state which might include but is not limited to the removal of foundations and hard surfaced areas followed by the backfilling of resultant voids. To ensure homogeneity, material utilised for backfilling and reinstating should be locally sourced. Implementation of generic environmental management procedures for infrastructure is highly recommended.

Appropriate measures should be in place to prevent pollution and contamination of the riparian zone e.g., well maintained equipment. Provision should be made during refuelling operations to protect soil by means of impermeable ground cover. If spillages occur, they should be contained and removed as rapidly as possible with the correct disposal procedures. Ideally proof of disposal should be obtained and retained on file for auditing purposes.

17.10 Final Specialist Statement and Authorisation Recommendation

17.10.1 Statement and Reasoned Opinion

Soil and rock conditions vary across the proposed Kudu Solar Facility study area resulting in the likely variation of geotechnical properties that might be encountered. These variations might influence foundation conditions, foundation designs, drainage properties, excavatability of soil and rock mass, and the occurrence of problem soils. It is, therefore, vital that an intrusive geotechnical study be undertaken prior to the development of Kudu Solar Facility to confirm the anticipated geotechnical conditions identified in this report.

The proposed Kudu Solar Facility may impact the environment by means of increased soil erosion and the contamination of geological material. It is understood that the main land use of the proposed development is livestock farming and it is therefore crucial that the potential impacts do not exceed the proposed footprints/buildable areas of Kudu Solar Facility. Although the impacts from neighbouring renewable facilities are notably similar to those of Kudu Solar Facility, cumulatively the intensity of these impacts can potentially increase if proper mitigation measures are not implemented. Proper designed mitigation measures should be implemented at all the Kudu Solar facilities to successfully suppress the intensities of impacts in order to achieve a low post mitigation significance.

Based on the geotechnical analysis conducted, it is recommended that the proposed Kudu Solar Facility be authorized, as no fatal flaws were found during this desktop assessment. However, it is crucial to implement appropriate mitigation measures at every phase of the project to minimize the intensity of the identified impacts.

The following conclusions are made:

- 1. Based on the findings of this geotechnical desktop study, development should proceed provided the mitigation measures are implemented.
- Increased soil erosion and contamination may transpire as an impact of the proposed development, and this may persist for the life of the project. However, the impact of this is expected to be very low to low significance.
- 3. Published data for the area, e.g., geological map, is generally confirmed by fieldwork undertaken by GEOSS in the area. However, variable soil and rock conditions will exist across the site, broadly these have been divided as follows:
 - Zone A Karoo Sandstones and mudstones
 - Zone B Karoo dolerite
 - Zone C Areas of thicker soil cover (generally within drainage channels)
- 4. It is anticipated that conventional foundations can be employed for all structures. Karoo mudrock and sandstone should be avoided when selecting aggregates for concrete mixes.
- 5. The footprint of each proposed structure would have to be investigated prior to compilation of final design.
- 6. Owing to the variable geologic and soil conditions across the proposed development area, the subgrade conditions will vary across the site. Dolerite has been proven to perform well as an aggregate for wearing courses in other areas of the Karoo. Dolerite has also been incorporated as an aggregate in concrete mixes.
- 7. The excavatability of the stratum on site are anticipated to variable, based on material composition and texture, the degree of weathering, and the nature of discontinuities within the rock and/or soil mass.
- 8. The seismicity in the region should be considered during design.
- 9. Road cuttings and drainage systems should be designed by an appropriately qualified professional.
- 10. Detailed geotechnical investigations will need to be undertaken prior to construction. Such investigations would not be required to fulfil the requirements of the EIA process. However, it would be necessary prior to construction.
- 11. GEOSS has endeavored to highlight and characterise all potential geotechnical risks that are presented by the site that has been proposed for development. However, due to the anisotropic (variable) nature of earth materials, each point on the site will present results that differ. For this reason, it is considered of the utmost importance that the foundation excavations be inspected prior to casting to ensure that soil with an adequate bearing capacity is obtained beneath each footing, and/or piling conditions be assessed. These works should be carried out by an appropriately qualified individual, during construction of the facility.

17.10.2EA Condition Recommendations

From the impact assessment it is evident that the development will have a very low to low impact significance on the local soil conditions and geology. As such, the project is authorised to continue from a geotechnical impact perspective with the following recommendations:

- The removal of vegetation should be kept to a minimum and only removed where necessary.
- A stormwater management plan should be developed prior to the construction phase by an accredited professional.
- The management plan should be managed throughout the duration of the project to successfully mitigate potential soil erosion.
- Rehabilitation of soil and geological material to commence during the construction phase, if possible, alternatively following the construction phase to allow successful re-vegetation.
- Authorised vehicles to only use proposed access points and roads and keep within the footprint of the facility.
- The land should be reinstated to natural or near natural conditions following decommissioning.
- Machinery and equipment to be maintained throughout the project.
- Ground protection measures to be implemented during maintenance and refuelling operations.
- Suitably designed bunding structures, double containment and leak detection to be implemented at BESS facilities.
- Spillages to be removed and contained as rapidly as possible.

17.11 References

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APPENDICES

APPENDIX A - SPECIALIST EXPERTISE

<u>CURRICULUM VITAE – HARDY LUTTIG</u>

GENERAL

Nationality: South African

Profession: Geotechnical / Engineering Geologist

Specialization: Soil classification for engineering purposes. Groundwater exploration and

sampling.

Date commenced 09 January 2023

Year of birth & ID #: 1993 – 930725 514 60 86

Language skills: Afrikaans (mother tongue, good - speaking, reading and writing),

English (good - speaking, reading and writing)

KEY SKILLS

- Geotechnical site investigation and site assessment.
- Field mapping
- Rock & soil profiling
- Material classification and material use determination.
- Hydrocensus studies
- Borehole drilling supervision and analysis
- Groundwater monitoring development and analysis of groundwater level and quality data.
- ArcGIS, QGIS

EDUCATIONAL AND PROFESSIONAL STATUS

Qualifications

2018	MEng (Geotechnical Engineering)	University of Stellenbosch, South Africa
2015	PDIP (Geotechnical Engineering)	University of Stellenbosch, South Africa
2014	B.Sc Earth Science	University of Stellenbosch, South Africa

EMPLOYMENT RECORD

January 2023 to present GEOSS South Africa (PTY) Ltd

January 2019 to December 2022 Martin & East (PTY) Ltd

January 2018 to October 2018 Ndodana Consulting Engineers (PTY) Ltd

<u>CURRICULUM VITAE – SHANE TEEK</u>

GENERAL

Nationality: South African

Profession: Geotechnical Specialist & Hydrogeologist

Specialization: Soil classification for engineering purposes. Groundwater exploration and

sampling.

Position in firm: Geotechnical Geologist & Hydrogeologist at GEOSS – South Africa (Pty) Ltd.

Date commenced: 17 July 2021

Year of birth & ID #: 1994 – 9404135162084

Language skills: English (good – speaking, reading, and writing)

Afrikaans (good - speaking, reading, and writing).

KEY SKILLS

- Geotechnical investigations
- Compilation of factual reports.
- Field mapping.
- Soil and rock profiling.
- Material classification and material use determination.
- Supervision of geotechnical contractors.
- Groundwater geophysics and conducting hydrocensus studies.
- Groundwater development borehole drilling and test pumping supervision and analysis.
- Groundwater monitoring development and analysis of groundwater level and quality data.
- Groundwater management sustainable aquifer development and management.
- Groundwater contamination assessments.
- ArcGIS, QGIS, Python, FLAC/SLOPE, Midas GTS NX.

EDUCATIONAL AND PROFESSIONAL STATUS

Qualifications

2021	M.Eng. (Civil Engineering – Cum Laude)	University of the Stellenbosch, South Africa
2016	B.Sc. Hons. (Earth Science)	University of the Stellenbosch, South Africa
2015	B.Sc. (Geology: Earth Science)	University of the Stellenbosch, South Africa

Memberships

- Geological Society of South Africa Member No. 970413
- South African Council for National Scientific Professions (SACNASP) Mem. No. 126397/20
- Founding member of the UNESCO Groundwater Youth Network (GWYN)

EMPLOYMENT RECORD

July 2021 to present	GEOSS South Africa (Pty) Ltd, South Africa
Jan 2020 to June 2021	Geotechnics Africa Western Cape, South Africa
Feb 2019 to July 2019	Polytechnique Montréal, Canada
Jan 2017 to Dec 2017	Remote Exploration Services, South Africa.

CURRICULUM VITAE – DALE BARROW

GENERAL

Nationality: South African Profession: Hydrogeologist

Firm: GEOSS South Africa (Pty) Ltd Position: Director and Hydrogeologist

Specialization: Groundwater exploration, development, management and monitoring including

numerical modeling. Hydrogeological impact studies and assessment of

groundwater - surface water interaction.

Date commenced: February 2008

Year of birth & ID #: 1985 - 851205 5227 082

Language skills: English (mother tongue), Afrikaans (average)

KEY SKILLS

Qualifications

- Project Management
- Hydrogeological technical input on projects
- Groundwater surface water interaction assessment
- Groundwater exploration (aerial photo interpretation, resistivity, magnetic and EM34 geophysical surveys for borehole siting purposes, geological conceptualization)
- Groundwater development borehole drilling and test pumping supervision and analysis.
- Groundwater monitoring –development and analysis of groundwater level and quality data.
- Groundwater management sustainable aquifer development and management.
- Numerical modelling of groundwater flow and mass transport.
- Groundwater component of Catchment Management Strategies and other Groundwater Resource Directed Measures.
- Groundwater contamination assessments.
- GIS / WISH and GW Vistas and typical software skills.

EDUCATIONAL AND PROFESSIONAL STATUS

Qualific	alions					
2017 2010	MBA (Cum Laude) M.Sc. (Geohydrology)	University of Stellenbosch, South Africa University of the Free State, South Africa				
2010	B.Sc (Hons) Structural Geology	University of Stellenbosch, South Africa				
2007	B.Sc Geology – Applied Earth Science	University of Stellenbosch, South Africa				
2000	B.Go Goology 7.ppiled Editif Goleride	Offiverally of Oteneribosoff, Oodiff Affica				
Course	es					
2019	Water Governance in South Africa: IWRM, the	NWA, and water use authorizations, focusing				
	on WULAs and IWWMPs. WISA accredited. Car	rin Bosman (CBSS)				
2016	SPRING Software Modelling Course					
2015	European Management Residency in Economic	s and Business (Maastricht University School				
	of Business and Economics)					
2013	Aquifer Firm Yield; Wellfield Design; Wellfield co	esting				
2010	Introduction to QGIS (GISSA)					
2010	Presentation Skills (Elsabé Daneel productions cc)					
2009	Introduction to Isotope Hydrology in Southern Af	rica (GSSA)				
2009	Aquifer Mechanics (IGS-UOFS)					
2009	Groundwater Chemistry (IGS-UOFS)					

ENVIRONMENTAL IMPACT ASSESSMENT REPORT: Scoping and Environmental Impact Assessment (EIA)
Process for the Proposed Development of a Solar Photovoltaic (PV) Facility (Kudu Solar Facility 2) and
associated infrastructure, near De Aar, Northern Cape Province

2009 Groundwater Geophysics (IGS-UOFS)
2009 Groundwater Modelling (IGS-UOFS)
2009 Groundwater Management (IGS-UOFS)

Memberships

- Groundwater Division of the Geological Society of South Africa
- South African Council for National Scientific Professions (SACNASP) Mem. No. 400289/13

EMPLOYMENT RECORD

1 February 2008 to present: GEOSS – Geohydrological and Spatial Solutions International (Pty)

Ltd, Stellenbosch

23 July 2018 - November 2019 Design and part time lecturing of the Hydrogeology course for 3rd year

students at Stellenbosch University

APPENDIX B - SPECIALIST STATEMENT OF INDEPENDENCE



DETAILS OF THE SPECIALIST, DECLARATION OF INTEREST AND UNDERTAKING UNDER OATH

ile Reference Number: IEAS Reference Number:	(For official use only)
ile Reference Number:	
VEAS Reference Number:	DEA/EIA/
Date Received:	

Application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

PROJECT TITLE

Scoping and Environmental Impact Assessment Processes for the Proposed Development of 12 Solar Photovoltaic (PV) Facilities and associated infrastructure (i.e. Kudu Solar Facility 1 - 12), near De Aar, Northern Cape

Kindly note the following:

- This form must always be used for applications that must be subjected to Basic Assessment or Scoping & Environmental Impact Reporting where this Department is the Competent Authority.
- This form is current as of 01 September 2018. It is the responsibility of the Applicant / Environmental Assessment
 Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the
 Competent Authority. The latest available Departmental templates are available at
 https://www.environment.gov.za/documents/forms.
- A copy of this form containing original signatures must be appended to all Draft and Final Reports submitted to the department for consideration.
- All documentation delivered to the physical address contained in this form must be delivered during the official Departmental Officer Hours which is visible on the Departmental gate.
- All EIA related documents (includes application forms, reports or any EIA related submissions) that are faxed; emailed; delivered to Security or placed in the Departmental Tender Box will not be accepted, only hardcopy submissions are accepted.

Departmental Details

Postal address:

Department of Environmental Affairs Attention: Chief Director: Integrated Environmental Authorisations Private Bag X447 Pretoria

0001

Physical address:

Department of Environmental Affairs
Attention: Chief Director: Integrated Environmental Authorisations
Environment House
473 Steve Biko Road

Queries must be directed to the Directorate: Coordination, Strategic Planning and Support at: Email: ElAAdmin@environment.gov.za

Details of Specialist, Declaration and Undertaking Under Oath

Page 1 of 3

SPECIALIST INFORMATION

Specialist Company Name:	GEOSS South Africa (F	Ptv) L	td.		
B-BBEE	Contribution level (indicate 1 to 8 or non-compliant)	3	Percer Procur recogn	ement	110%
Specialist name:	Hardy Luttig				
Specialist Qualifications:	B.Sc. Earth Sciences; MEng Civil (Geotechnical Engineering)				
Professional affiliation/registration:	SACNASP (Pending)				
Physical address:	Unit 12, Techno Stell Stellenbosch	Bldg	, 09 Quant	tum Stree	t, Techno Park,
Postal address:	PO Box 12412, Die Boord, Stellenbosch				
Postal code:	7613		Cell:	082 397 7182	
Telephone:	021 880 1079		Fax:	n/a	
E-mail:	hluttig@geoss.co.za				

2. DECLARATION BY THE SPECIALIST

I, Hardy Luttig, declare that -

- I act as the independent specialist in this application;
- I will perform the work relating to the application in an objective manner, even if this results in views and findings
 that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act,
 Regulations and any guidelines that have relevance to the proposed activity;
- I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information in my possession that
 reasonably has or may have the potential of influencing any decision to be taken with respect to the application by
 the competent authority; and the objectivity of any report, plan or document to be prepared by myself for
 submission to the competent authority;
- all the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of regulation 48 and is punishable in terms of section 24F of the Act.



Signature of the Specialist

GEOSS SOUTH AFRICA (PTY) LTD

Name of Company:

07 July 2023

Details of Specialist, Declaration and Undertaking Under Oath

Page 2 of 3

Date
3. UNDERTAKING UNDER OATH/ AFFIRMATION
I, Hardy Luttig, swear under oath / affirm that all the information submitted or to be submitted for the purposes of this application is true and correct. Signature of the Specialist
GEOSS SOUTH AFRICA (PTY) LTD
Name of Company
07 July 2023 Date
Signature of the Commissioner of Oaths
07 July 2023
Date

Ex offició COMMISSIONER OF OATHS (RSA)
Samantha Scheeman ACMA – 1-7FUWGN
The Boulevard Office Park, Block B
Ground'Floor, Searle Street, Woodstock, 7925

Details of Specialist, Declaration and Undertaking Under Oath

Page 3 of 3



DETAILS OF THE SPECIALIST, DECLARATION OF INTEREST AND UNDERTAKING UNDER OATH

File Reference Number: NEAS Reference Number: Date Received:

(For official use only)	45
DEA/EIA/	,
DEWEIN	

Application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

PROJECT TITLE

Scoping and Environmental Impact Assessment Processes for the Proposed Development of 12 Solar Photovoltaic (PV) Facilities and associated infrastructure (i.e. Kudu Solar Facility 1 - 12), near De Aar, Northern Cape

Kindly note the following:

- This form must always be used for applications that must be subjected to Basic Assessment or Scoping & Environmental Impact Reporting where this Department is the Competent Authority.
- This form is current as of 01 September 2018. It is the responsibility of the Applicant / Environmental Assessment
 Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the
 Competent Authority. The latest available Departmental templates are available at
 https://www.environment.gov.za/documents/forms.
- A copy of this form containing original signatures must be appended to all Draft and Final Reports submitted to the department for consideration.
- All documentation delivered to the physical address contained in this form must be delivered during the official Departmental Officer Hours which is visible on the Departmental gate.
- All EIA related documents (includes application forms, reports or any EIA related submissions) that are faxed; emailed; delivered to Security or placed in the Departmental Tender Box will not be accepted, only hardcopy submissions are accepted.

Departmental Details

Postal address:

Department of Environmental Affairs
Attention: Chief Director: Integrated Environmental Authorisations
Private Bag X447

Pretoria 0001

Physical address:

Department of Environmental Affairs
Attention: Chief Director: Integrated Environmental Authorisations
Environment House
473 Steve Biko Road
Arcadia

Queries must be directed to the Directorate: Coordination, Strategic Planning and Support at: Email: EIAAdmin@environment.gov.za

Details of Specialist, Declaration and Undertaking Under Oath

Page 1 of 3

SPECIALIST INFORMATION

Specialist Company Name:	GEOSS SOUTH AFRICA (PT	Y) LTD				
B-BBEE	Contribution level (Indicate 1 to 8 or non-compliant)		Percenta Procuren recognition	nent	110%	
Specialist name:	SHANE TEEK					
Specialist Qualifications:	MEng - Civil Engineering					
Professional						
affiliation/registration:						
Physical address:	Unit 12, Techno Stell Bldg, 09	Quantum St	treet, Techno	Park, Stelle	nbosch	
Postal address:	PO Bo12412, Die Boord, Stell	lenbosch				
Postal code:	7613	Cel	N:	079 183 77	782	
Telephone:	021 880 1079	Fax	C:	n/a		
E-mail:						

2. DECLARATION BY THE SPECIALIST

I, SHANE TEEK, declare that -

- I act as the independent specialist in this application;
- I will perform the work relating to the application in an objective manner, even if this results in views and findings
 that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act,
 Regulations and any guidelines that have relevance to the proposed activity;
- I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information. In my possession that
 reasonably has or may have the potential of influencing any decision to be taken with respect to the application by
 the competent authority; and the objectivity of any report, plan or document to be prepared by myself for
 submission to the competent authority;
- all the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of regulation 48 and is punishable in terms of section 24F of the Act.

Stuk			
Signature of the Specialist	3.7.7000000		
GEOSS SOUTH AFRICA (PTY) LTD			
Name of Company:			
28 November 2022			
Date			

Details of Specialist, Declaration and Undertaking Under Cath

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DETAILS OF THE SPECIALIST, DECLARATION OF INTEREST AND UNDERTAKING UNDER OATH

×	(For official use only)
File Reference Number:	
NEAS Reference Number:	DEA/EIA/
Date Received:	

Application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

PROJECT TITLE

Scoping and Environmental Impact Assessment Processes for the Proposed Development of 12 Solar Photovoltaic (PV) Facilities and associated infrastructure (i.e. Kudu Solar Facility 1 - 12), near De Aar, Northern Cape

Kindly note the following:

- This form must always be used for applications that must be subjected to Basic Assessment or Scoping & Environmental Impact Reporting where this Department is the Competent Authority.
- This form is current as of 01 September 2018. It is the responsibility of the Applicant / Environmental Assessment
 Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the
 Competent Authority. The latest available Departmental templates are available at
 https://www.environment.gov.za/documents/forms.
- A copy of this form containing original signatures must be appended to all Draft and Final Reports submitted to the department for consideration.
- All documentation delivered to the physical address contained in this form must be delivered during the official Departmental Officer Hours which is visible on the Departmental gate.
- All EIA related documents (includes application forms, reports or any EIA related submissions) that are faxed; emailed; delivered to Security or placed in the Departmental Tender Box will not be accepted, only hardcopy submissions are accepted.

Departmental Details

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Arcadia

Queries must be directed to the Directorate: Coordination, Strategic Planning and Support at: Email: EIAAdmin@environment.gov.za

Details of Specialist, Declaration and Undertaking Under Oath

Page 1 of 3

1. SPECIALIST INFORMATION

Specialist Company Name:	GEOSS SOUTH AFRICA (PTY) LTD						
B-BBEE	Contribution level (indicate 1 to 8 or non-compliant)	3	Percenta Procurer recogniti	nent	110%		
Specialist name:	DALE BARROW						
Specialist Qualifications:	MSc in Hydrogeology						
Professional	SACNASP: 400289/13						
affiliation/registration:							
Physical address:	Unit 12, Techno Stell Bldg, 09 Quantum Street, Techno Park, Stellenbosch						
Postal address:	PO Box 12412, Die Boord, Stellenbosch						
Postal code:	7613	Ce	ell;	074 172 2862			
Telephone:	021 880 1079	Fa	X:	n/a			
E-mail:	dbarrow@geoss.co.za		3118	250			

2. DECLARATION BY THE SPECIALIST

I, Dale Barrow, declare that -

- · 1 act as the independent specialist in this application;
- I will perform the work relating to the application in an objective manner, even if this results in views and findings
 that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act,
 Regulations and any guidelines that have relevance to the proposed activity;
- · I will comply with the Act, Regulations and all other applicable legislation;
- · I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information in my possession that
 reasonably has or may have the potential of influencing any decision to be taken with respect to the application by
 the competent authority; and the objectivity of any report, plan or document to be prepared by myself for
 submission to the competent authority;
- · all the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of regulation 48 and is punishable in terms of section 24F of the Act.



Signature of the Specialist

GEOSS SOUTH AFRICA (PTY) LTD

Name of Company:

07 July 2023

Date

Details of Specialist, Declaration and Undertaking Under Oath

Page 2 of 3

3.	UNDERTAKING UNDER OATH/ AFFIRMATION	
I, <u>Dale I</u> purpose	Barrow, swear under oath / affirm that all the information submitted or to be submitted for the softhis application is true and correct.	he
Ø		
Signatu	re of the Specialist	
GEOSS	S SOUTH AFRICA (PTY) LTD	
Name o	of Company	
07 July	2023	
Date	Le .	
Signatu	re of the Commissioner of Oaths	
07 July	7 2023	
Date	•	_

Ex officio COMMISSIONER OF OATHS (RSA)
Samantha Schoaman ACMA = 1-7FUWGN
The Boulevard Office Park, Block B
Ground'Floor, Searle Street, Woodstock, 7925

Details of Specialist, Declaration and Undertaking Under Oath

APPENDIX C - SITE SENSITIVITY VERIFICATION

Geotechnical themes do not exist on the National Web-based Environmental Screening Tool (Screening Tool) (as of May 2023); therefore, the environmental sensitivity of the proposed project area as identified by the Screening Tool is not applicable. For this reason, no site sensitivity verification report is required. Furthermore, there is no dedicated assessment protocol prescribed for conducting a Desktop Geotechnical Assessment. Therefore, this specialist assessment has been undertaken in compliance with Appendix 6 of the National Environmental Management Act (Act 107 of 1998, as amended) (NEMA) Environmental Impact Assessment (EIA) Regulations of 2014. However, GEOSS had previously undertaken a site visit during the undertaking of the separate groundwater specialist assessment (Chapter 16 of this EIA Report), the details of which are indicated below:

Date of Site Visit	23-24 March 2022
Specialist Name	Christel van Staden and Dale Barrow
Professional Registration Number	Cand.Sci.Nat: 122591 and Pr.Sci.Nat: 400289/13
Specialist Affiliation / Company	GEOSS

The relevant data collected during the hydrogeological site visit have been considered in this report. For example, no additional/unmapped rock types or sedimentary deposits were identified. Therefore, the desktop analysis of the geotechnical conditions is considered to be appropriate for the scope of the present investigation.

All relevant desktop information, consultation with landowners, and previous assessments undertaken by the author in the study area have been taken into consideration during the undertaking of this specialist desktop geotechnical assessment.

The hydrogeological site visit was undertaken using the following means:

- (a) desk top analysis, using satellite imagery; geological maps and hydrogeological and geotechnical reports and databases where possible and applicable.
- (b) preliminary on-site inspection; and drive over.
- (c) collected water samples, field chemistry and water levels where possible and relevant; assessed site conditions to determine whether literature information is generally confirmed.

APPENDIX D - IMPACT ASSESSMENT METHODOLOGY

The impact assessment includes:

- the nature, status, significance and consequences of the impact and risk;
- the extent and duration of the impact and risk;
- the probability of the impact and risk occurring;
- the degree to which impacts and risks can be mitigated;
- the degree to which the impacts and risks can be reversed; and
- the degree to which the impacts and risks can cause loss of irreplaceable resources.

Terminology used in impact assessment can overlap. To avoid ambiguity, please note the following clarifications (that are based on NEMA and the EIA Regulations):

- The term environment is understood to have a broad interpretation that includes both the natural (biophysical) environment and the socio-economic environment. The term socio-ecological system is also used to describe the natural and socio-economic environment and the interactions amongst these components.
- Significance = Consequence x Probability, which means that significance is equivalent to risk.
- The impact can have a positive or negative status. The significance of a negative impact may be called a risk, and the significance of a positive impact may be called an opportunity.

The following principles are to underpin the application of this methodology:

- Transparent and repeatable process specialists are to describe the thresholds and limits they apply in their assessment, wherever possible.
- Adapt parameters to context (where justified) the methodology proposes some thresholds (e.g. for spatial extent, in Step 3 below), however, if the nature of the impact requires a different definition of the categories of spatial extent, then this can be provided and described.
- Combination of a quantitative and qualitative assessment where possible, specialists are to
 provide quantitative assessments (e.g. areas of habitat affected, decibels of noise, number of
 jobs), however, it is recognised that not all impacts can be quantified, and then qualitative
 assessments are to be provided.

As per the DFFE Guideline 5: Assessment of Alternatives and Impacts, the following methodology is applied to the prediction and assessment of impacts and risks. Potential impacts and risks have been rated in terms of the direct, indirect and cumulative:

- Direct impacts are impacts that are caused directly by the activity and generally occur at the same time and at the place of the activity. These impacts are usually associated with the construction, operation or maintenance of an activity and are generally obvious and quantifiable.
- Indirect impacts of an activity are indirect or induced changes that may occur as a result of
 the activity. These types of impacts include all the potential impacts that do not manifest
 immediately when the activity is undertaken or which occur at a different place as a result of
 the activity.
- Cumulative impacts are impacts that result from the incremental impact of the proposed activity on a common resource when added to the impacts of other past, present or reasonably foreseeable future activities. Cumulative impacts can occur from the collective

impacts of individual minor actions over a period of time and can include both direct and indirect impacts.

The impact assessment methodology includes the aspects described below.

- <u>Step 1</u>: Nature of impact/risk The type of effect that a proposed activity will have on the environment.
- Step 2: Status Whether the impact/risk on the overall environment will be:
 - Positive environment overall will benefit from the impact/risk;
 - o Negative environment overall will be adversely affected by the impact/risk; or
 - Neutral environment overall not be affected.
- <u>Step 3</u>: Qualitatively determine the consequence of the impact/risk by identifying the a) SPATIAL EXTENT; b) DURATION; c) REVERSIBILITY; AND d) IRREPLACEABILITY.
 - o A) Spatial extent The size of the area that will be affected by the impact/risk:
 - Site specific;
 - Local (<10 km from site);
 - Regional (<100 km of site);
 - National; or
 - International (e.g., Greenhouse Gas emissions or migrant birds).
 - B) Duration The timeframe during which the impact/risk will be experienced:
 - Very short term (instantaneous);
 - Short term (less than 1 year);
 - Medium term (1 to 10 years);
 - Long term (the impact will cease after the operational life of the activity (i.e., the impact or risk will occur for the project duration)); or
 - Permanent (mitigation will not occur in such a way or in such a time span that the impact can be considered transient (i.e., the impact will occur beyond the project decommissioning)).
 - C) Reversibility of the Impacts the extent to which the impacts/risks are reversible assuming that the project has reached the end of its life cycle (decommissioning phase):
 - High reversibility of impacts (impact is highly reversible at end of project life i.e., this is the most favourable assessment for the environment);
 - Moderate reversibility of impacts;
 - Low reversibility of impacts; or
 - Impacts are non-reversible (impact is permanent, i.e., this is the least favourable assessment for the environment).
 - D) Irreplaceability of Receiving Environment/Resource Loss caused by impacts/risks –
 the degree to which the impact causes irreplaceable loss of resources assuming that the
 project has reached the end of its life cycle (decommissioning phase):

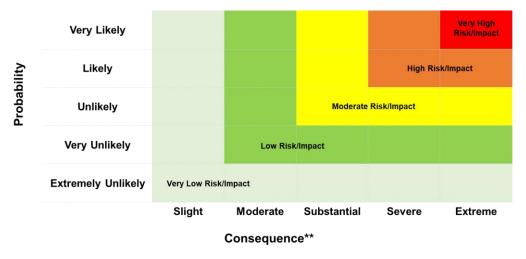
- High irreplaceability of resources (project will destroy unique resources that cannot be replaced, i.e., this is the least favourable assessment for the environment);
- Moderate irreplaceability of resources;
- Low irreplaceability of resources; or
- Resources are replaceable (the affected resource is easy to replace/rehabilitate, i.e., this is the most favourable assessment for the environment).

Some of the criteria are quantitative (e.g., spatial extent and duration) and some may be described in a quantitative or qualitative manner (e.g., reversibility and irreplaceability). The specialist then combines these criteria in a qualitative manner to determine the **consequence**.

The consequence terms ranging from slight to extreme must be calibrated per Specialist Study so that there is transparency and consistency in the way a risk/impact is measured. For example, from a biodiversity and ecology perspective, the consequence ratings could be defined according to a reduction in population or occupied area in relation to Species of Conservation Concern (SCC) status, ranging from slight consequence for defined areas of Least Concern, to extreme consequence for defined areas that are Critically Endangered. For example, from a social perspective, a slight consequence could refer to small and manageable impacts, or impacts on small sections of the community; a moderate consequence could refer to impacts which affect the bulk of the local population negatively or may produce a net negative impact on the community; and an extreme consequence could refer to impacts which could result in social or political violence or institutional collapse.

- Consequence The anticipated consequence of the risk/impact is generally defined as follows:
 - Extreme (extreme alteration of natural or socio-economic systems, patterns or processes, i.e., where environmental or socio-economic functions and processes are altered such that they permanently cease);
 - Severe (severe alteration of natural or socio-economic systems, patterns or processes, i.e., where environmental or socio-economic functions and processes are altered such that they temporarily or permanently cease);
 - Substantial (substantial alteration of natural or socio-economic systems, patterns or processes, i.e., where environmental or socio-economic functions and processes are altered such that they temporarily or permanently cease;
 - Moderate (notable alteration of natural or socio-economic systems, patterns or processes, i.e., where the natural or socio-economic environment continues to function but in a modified manner; or
 - Slight (negligible and transient alteration of natural or socio-economic systems, patterns or processes, i.e., where natural systems/environmental or socio-economic functions, patterns, or processes are not affected in a measurable manner, or if affected, that effect is transient and the system recovers).
- **Step 4**: Rate the **probability** of the impact/risk using the criteria below:
 - o **Probability** The probability of the impact/risk occurring:
 - Extremely unlikely (little to no chance of occurring);
 - Very unlikely (<30% chance of occurring);

- Unlikely (30-50% chance of occurring)
- Likely (51 90% chance of occurring); or
- Very Likely (>90% chance of occurring regardless of prevention measures).
- <u>Step 5</u>: Use both the **consequence** and **probability** to determine the **significance** of the identified impact/risk (qualitatively as shown in Figure 17-6). Significance definitions and rankings are provided below:



**[Qualitatively determined based on Spatial Extent, Duration, Reversibility and Irreplaceability]

Figure 17-6: Guide to assessing risk/impact significance as a result of consequence and probability.

- **Significance** Will the impact cause a notable alteration of the environment?
 - Very low (the risk/impact may result in very minor alterations of the environment and can be easily avoided by implementing appropriate mitigation measures, and will not have an influence on decision-making);
 - Low (the risk/impact may result in minor alterations of the environment and can be easily avoided by implementing appropriate mitigation measures, and will not have an influence on decision-making);
 - Moderate (the risk/impact will result in moderate alteration of the environment and can be reduced or avoided by implementing the appropriate mitigation measures, and will only have an influence on the decision-making if not mitigated);
 - High (the risk/impact will result in major alteration to the environment even with the implementation on the appropriate mitigation measures and will have an influence on decision-making); and
 - Very high (the risk/impact will result in very major alteration to the environment even with the implementation on the appropriate mitigation measures and will have an influence on decision-making (i.e., the project cannot be authorised unless major changes to the engineering design are carried out to reduce the significance rating)).

ENVIRONMENTAL IMPACT ASSESSMENT REPORT: Scoping and Environmental Impact Assessment (EIA)
Process for the Proposed Development of a Solar Photovoltaic (PV) Facility (Kudu Solar Facility 2) and
associated infrastructure, near De Aar, Northern Cape Province

With the implementation of mitigation measures, the residual impacts/risks are ranked as follows in terms of significance:

- *Very low* = 5;
- Low = 4;
- Moderate = 3:
- High = 2; and
- Very high = 1.

The specialists must provide a written supporting motivation of the assessment ratings provided.

- <u>Step 6</u>: Determine the **Confidence Level** The degree of confidence in predictions based on available information and specialist knowledge:
 - o Low;
 - o Medium; or
 - o High.

APPENDIX E - COMPLIANCE WITH THE APPENDIX 6 OF THE 2014 EIA REGULATIONS (AS AMENDED)

Requirements of Appendix 6 (Specialist Reports) of Government Notice R326 (Environmental Impact Assessment (EIA) Regulations of 2014, as amended)	Section where this has been addressed in the Specialist Report
(1) A specialist report prepared in terms of these Regulations must contain - a) details of -	Section 17.1.2 Appendix A
i. the specialist who prepared the report; and	Аррения А
ii. the expertise of that specialist to compile a specialist report including a curriculum vitae;	
b) a declaration that the specialist is independent in a form as may be specified by the competent authority;	
 c) an indication of the scope of, and the purpose for which, the report was prepared; 	17.1.3
(car) an indication of the quality and age of base data used for the specialist report	
(cB) a description of existing impacts on the site, cumulative impacts of the proposed development and levels of acceptable change;	
 d) the duration, date and season of the site investigation and the relevance of the season to the outcome of the assessment; 	and Appendix C
 e) a description of the methodology adopted in preparing the report of carrying out the specialised process inclusive of equipment and modelling used; 	1
f) details of an assessment of the specific identified sensitivity of the site related to the proposed activity or activities and its associated structures and infrastructure, inclusive of a site plan identifying site alternatives;	
g) an identification of any areas to be avoided, including buffers;	Sections 17.4 & 17.6
 a map superimposing the activity including the associated structures and infrastructure on the environmental sensitivities of the site including areas to be avoided, including buffers; 	
 i) a description of any assumptions made and any uncertainties or gaps in knowledge; 	Section 17.2
j) a description of the findings and potential implications of such findings or the impact of the proposed activity or activities;	Section 17.6
k) any mitigation measures for inclusion in the EMPr;	Section 17.6 and Section 17.9
 any conditions for inclusion in the environmental authorisation; 	Sections 17.6 and 17.10
 m) any monitoring requirements for inclusion in the EMPr or environmenta authorisation; 	and 17.10
n) a reasoned opinion- i. whether the proposed activity, activities or portions thereof should be authorised;	Section 17.10
(iA) regarding the acceptability of the proposed activity or activities; and ii. if the opinion is that the proposed activity, activities or portions thereof should be authorised, any avoidance, management and mitigation measures that should be included in the EMPr, and where applicable, the closure plan;	
 a description of any consultation process that was undertaken during the course of preparing the specialist report; 	
 p) a summary and copies of any comments received during any consultation process and where applicable all responses thereto; and 	Section 17.2 and Section 17.5
q) any other information requested by the competent authority.	n/a
(2) Where a government notice by the Minister provides for any protocol of minimum information requirement to be applied to a specialist report, the requirements as indicated in such notice will apply.	

Requirements of Appendix 6 (Specialist Reports) of Government Notice R326 (Environmental Impact Assessment (EIA) Regulations of 2014, as	Section where this has been addressed in the
amended)	Specialist Report
	A of the March 2020
	Assessment Protocol (GN
	320) applies, which refers to
	Appendix 6 of the 2014
	NEMA EIA Regulations (as
	amended).

APPENDIX F - APPROVED RENEWABLE ENERGY PROJECTS

Table 17-10: Approved renewable energy projects, located within 30 km of the proposed Kudu Solar Facility.

CSIR NUMBER	DFFE REFERENCE	TECHNOLOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
1	12/12/20/2258 12/12/20/2258/1	Solar PV	75	Approved and Preferred Bidder (Operational)	The Proposed Establishment of Photovoltaic (Solar Power) Farms in the Northern Cape Province - Kalkbult	2010	Scoping and EIA	Scatec Solar SA Pty Ltd	Sustainable Development Projects cc
2	12/12/20/2463/1 12/12/20/2463/1/2 12/12/20/2463/1/A2 12/12/20/2463/1/AM3 12/12/20/2463/1/AM4 12/12/20/2463/1/AM5	Onshore Wind	140	Approved and Preferred Bidder (Operational)	Longyuan Mulilo De Aar 2 North Wind Energy Facility Longyuan Mulilo De Aar Maanhaarberg Wind Energy Facility The Wind Energy Facility (North and South) situated on the Plateau Near De Aar, Northern Cape Province	2010 and 2014	Scoping and EIA and Amendment	Longyuan Mulilo De Aar 2 South (Pty)	Aurecon South Africa (Pty) Ltd and Holland and Associates Environmental Consultants
3	12/12/20/2463/2 12/12/20/2463/2/AM2	Onshore Wind	100	Approved and Preferred Bidder (Operational)	Longyuan Mulilo De Aar Maanhaarberg Wind Energy Facility The Wind Energy Facility (North and South) Situated On The Plateau Near De Aar, Northern Cape Province	2010 and 2014	Scoping and EIA and Amendment	Mulilo Renewable Energy (Pty) Ltd	Aurecon South Africa (Pty) Ltd
4	14/12/16/3/3/1/1166 14/12/16/3/3/1/1166/A M3 14/12/16/3/3/1/1166/A M4	Transmission line	132	Approved	Basic Assessment for the proposed construction of a 132 kV transmission line corridor adjacent to the existing Eskom transmission line from	2010 and 2014	Basic Assessment	Longyuan Mulilo De Aar 2 North (Pty) Ltd	Aurecon South Africa (Pty) Ltd

CSIR NUMBER	DFFE REFERENCE	TECHNOLOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
					Longyuan Mulilo De Aar 2 North Wind Energy Facility (WEF) to the Hydra Substation in De Aar, Northern Cape				
5	14/12/16/3/3/1/785	Transmission line	132	Approved	Proposed construction of two 132kV transmission lines from the South & North Wind Energy Facilities on the Eastern Plateau (De Aar 2) near De Aar, Northern Cape.	2010	Basic Assessment	Mulilo Renewable Energy (Pty) Ltd	Aurecon South Africa (Pty) Ltd
6	14/12/16/3/3/2/278 14/12/16/3/3/2/278/1 14/12/16/3/3/2/278/2	Onshore Wind	118	Approved	Proposed Castle Wind Energy Facility Project, located near De Aar, Northern Cape	2010 and 2014	Scoping and EIA	Castle Wind Farm (Pty) Ltd	Aurecon South Africa (Pty) Ltd; and Savannah Environmental Consultants (Pty) Ltd
7	14/12/16/3/3/2/564 14/12/16/3/3/2/564/A M1 14/12/16/3/3/2/564/A M2	Solar PV	75	To be confirmed	Proposed Swartwater 75MW solar PV power facility in Petrusville within Renosterburg Local Municipality, Northern Cape	2010 and 2014	Scoping and EIA and Amendment	AE-AMD Renewable Energy (Pty) Ltd	USK Environmental and Waste Engineering (Pty) Ltd
8	14/12/16/3/3/2/740	Solar PV	300	Approved	Proposed 300MW Solar Power Plant in Phillipstown area in Renosterberg Local Municipality	2010	Scoping and EIA	To be confirmed	Tshikovha Environmental and Communication Consultants
9	14/12/16/3/3/2/744	Solar PV	0	Approved	Proposed PV facility on farm Jakhalsfontein near De Aar	2010	Scoping and EIA	Solar Capital (Pty) Ltd	Eco Compliance (Pty) Ltd
10	14/12/16/3/3/2/739	Solar PV	70 - 100	To be confirmed	Proposed 70 - 100 MW Solar Power Plant in Petrusville	2010	Scoping and EIA	To be confirmed	Tshikovha Environmental and Communication Consultants

CSIR NUMBER	DFFE REFERENCE	TECHNOLOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
11	Not issued yet (it is understood that the project is still within the pre-application stage)	Solar PV	800 (Max imu m)	Pre-Application	The Proposed Keren Energy Odyssey Solar PV Facilities (Odyssey Solar 1, Odyssey Solar 2, Odyssey Solar 3, Odyssey Solar 4, Odyssey Solar 5, Odyssey Solar 6, Odyssey Solar 7 And Odyssey Solar 8)	2014	Scoping and EIA	Keren Energy Group Holdings	EnviroAfrica cc
12	To be confirmed	Solar PV	3050	Scoping	The Proposed Development of the Crossroads (formally referred to as the Hydra B) Green Energy Cluster of Renewable Energy Facilities and Grid Connection Infrastructure, Pixley Ka Seme District Municipality, Northern Cape Province. The Cluster entails the development of up to 21 solar energy facilities, with the Scoping and EIA Processes consisting of three phases. Phases 1, 2 and 3 consist of 9, 6 and 6 solar facilities, respectively. The Phase 1 Scoping and EIA Processes were launched in January 2023.	2014	Scoping and EIA	Akuo Energy Afrique	Savannah Environmental Consultants (Pty) Ltd
Study area shown on map	14/12/16/3/3/2/2244 14/12/16/3/3/2/2245 14/12/16/3/3/2/2246 14/12/16/3/3/2/2247 14/12/16/3/3/2/2248 14/12/16/3/3/2/2249	Solar PV	2180	Scoping and EIA Process underway	Proposed Development of 12 Solar Photovoltaic (PV) Facilities (Kudu Solar Facility 1 to 12) and associated infrastructure, near De Aar, Northern Cape Province	2014	Scoping and EIA	Kudu Solar Facility 1 (Pty) Ltd to Kudu Solar Facility 12 (Pty) Ltd	CSIR

CSIR NUMBER	DFFE REFERENCE	TECHNOLOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
	14/12/16/3/3/2/2250 14/12/16/3/3/2/2251 14/12/16/3/3/2/2252 14/12/16/3/3/2/2253 14/12/16/3/3/2/2254 14/12/16/3/3/2/2255								
Shown on map as Existing HV Lines	N/A	Transmission Line	220	Existing Power Line	HYDRA ROODEKUIL 2	-	-	-	-
Shown on map as Existing HV Lines	N/A	Transmission Line	132	Existing Power Line	HYDRA ROODEKUIL 1	-	-	-	-
Shown on map as Existing HV Lines	N/A	Transmission Line	765	Existing Power Line	BETA HYDRA 2	-	-	-	-
Shown on map as Existing HV Lines	N/A	Transmission Line	400	Existing Power Line	HYDRA PERSEUS 3	-	-	-	-
Shown on map as Existing HV Lines	N/A	Transmission Line	220	Existing Power Line	VAN DER KLOOF ROODEKUIL 2	-	-	-	-
Shown on map as Existing HV Lines	N/A	Transmission Line	220	Existing Power Line	VAN DER KLOOF ROODEKUIL 1	-	-	-	-
Shown on map as	N/A	Transmission Line	400	Existing Power Line	BETA HYDRA 1	-	-	-	-

CSIR NUMBER	DFFE REFERENCE	TECHNOLOGY	MW/ KV	STATUS	PROJECT TITLE	EIA REGULATIONS	ASSESSMENT PROCESS	APPLICANT	EAP
Existing HV Lines									
Shown on map as Existing HV Lines	N/A	Transmission Line	400	Existing Power Line	HYDRA PERSEUS 2	-	-	-	-
Shown on map as Existing HV Lines	N/A	Transmission Line	132	Existing Power Line	KALKBULT/KAREEBOSCHPA N 1	-	-	-	-
Shown on map as Existing HV Lines	N/A	Transmission Line	132	Existing Power Line	ROODEKUIL/ORANIA 1	-	-	-	-
Shown on map as Planned HV Lines	N/A	Transmission Line	765	Planned Power Line	Perseus to Gamma 2nd 765 kV line Cape Corridor Phase 4: 2nd Zeus-Per-Gam-Ome 765kV Line	-	-	-	-
Shown on map as Planned HV Lines	N/A	Transmission Line	765	Planned Power Line	Relocate Beta-Hydra 765kV line to form Perseus-Hydra 1st 765kV line Cape Corridor Phase 2: Zeus - Hydra 765kV Integration	-	-	-	-
Shown on map as Planned HV Lines	N/A	Transmission Line	765	Planned Power Line	Perseus to Gamma 2nd 765 kV line Cape Corridor Phase 4: 2nd Zeus-Per-Gam-Ome 765kV Line	-	-	-	-

APPENDIX G - RELEVANT GEOTECHNICAL LITERATURE & INFORMATION

G.1 Sandstones and mudstones (Zone A)

Karoo sandstone is often not desirable in construction, e.g. as an aggregate, as it may cause concrete to deteriorate over time (Brink, 1977). In this regard, the following has been observed when making use of Karoo sandstones in construction (after Brink, 1983):

- 1. Deflection and shrinkage of reinforced members.
- 2. Corrosion of reinforcing steel.
- 3. Coincident cracking of concrete and reinforcement.
- 4. Surface crazing or pattern cracking.
- 5. Premature distress of roads constructed using aggregates derived from Karoo sandstones.

Control of material properties is required when making use of Karoo sandstones in construction.

Table 17-11: Strength and deformation characteristics of some Karoo Sandstones (Brink, 1983).

		V	ryheid Form	Estcourt Formation				
b _i ,		UCS (MPa)	E: (GPa)	Bulk density (kg/m³)	UCS (MPa)	E ₁₍₅₀₎ (GPa)	Poisson's ratio v	Bulk density (kg/m³)
Maximum	Χm	44,7	11,364	2 493	271	13,4	0,28	2 660
Minimum	Хπ	8,6	0,621	2 356	57	5,9	0,06	2 350
Mean Number of	X	27,0	2,426	2 421	116	9,9	0,14	2 473
ests Standard	n	17	17	17	20	9	9	. 3
deviation Coefficient	S	12,3	2,9	43,6	56,5	2,43	0,08	164
of variation	S/x̄	0,45	1,18	0,02	0,49	0,25	0,57	0,07

UCS = Unconfined compressive strength

E_t = Tangent modulus

 $E_{t(50)}$ = Tangent modulus at 50 per cent ultimate strength

*Data provided by W. J. Neely.

Table 17-12: Geotechnical properties of Ecca Group sandstone at Matimba Power Station (Brink, 1983).

		Density (kg/m³)	UCS (MPa)	Secant modulus (GPa)	Poisson's ratio v	Point load index (MPa)
Maximum	ΧM	2 452,0	83,2	49,7	0,21	7,2
Minimum	χ_{m}	2 332,8	46,6	19,6	0,11	0,1
Mean	Χ̈́	2 394,6	69,1	36,1	0,16	2,9
Number of tests	n	19	19	19	19	20
Standard deviation	S	31,7	8,9	10	0,04	1,9
Coefficient of variation	S/x̄	0,01	0,13	0,28	0,25	0,66

Table 17-13: Drying and shrinkage determinations on some sandstones of the Beaufort Group (Brink, 1983).

			Dootho	Linear shrinkage per cent		
Subgroup	Locality	Reference	Depths - below surface	Specimen cut parallel to bedding	Specimen cut 90° to bedding	
Adelaide	Graaff-Reinet municipal quarry	Stutterheim (1954)	Quarry face near surface	0,038	0,058	
Adelaide	Adendorp quarry (near Graaff-Reinet)	Stutterheim (1954)	Quarry face near surface	0,23	0,84	
Tarkastad	Cores from borehole situated at: x = 324,300 y = 1 235,350 approx. lat. 31° 15′ S approx. long. 25° 30′ E (cores supplied by Orange—Fish Tunnel Consultants; tests by NBRI—CSIR	Pienaar (1966)	7 m 48 m 116 m 156 m 222 m 311 m		0,12 0,12 0,07 0,16 0,095 0,11	
Adelaide	Aberdeen	Roper (1959)	Near surface	0,024		
Tarkastad	Queenstown	Roper (1959)	Near surface	0,12	_	
Adelaide	Beaufort West	Roper (1959)	Near surface	0,04*		

^{*} Quartzitic sandstone.

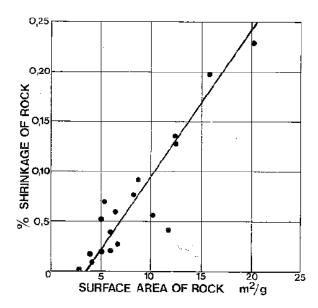


Figure 17-7: Relation between shrinkage and surface area for a variety of rocks including Karoo sandstone (Brink, 1983).

Table 17-14: Road construction characteristics of some Karoo sandstones (Brink, 1983).

		Molteno, E	Elliot and Claren	Laingsburg Formation**			
		CBR (%)	CBR +3% cement (%)	10% FACT (kN)	ACV (%)	10% FACT (kN)	Treton (%)
Maximum	ΧM	125	417	136	46	410	72,9
Minimum	Xm	24	157	7	9,7	160	16,4
Mean	X	68	234	46	17,3	282	31,4
No. of tests Standard	n	10	. 7	10	21	10	21
deviation Coefficient of	S	38	86	35,4	7,7	84,4	13,7
variation	S/x̄	0,56	0,37	0,77	0,45	0,23	0,44

^{*} Partly after Holleman (1975)

^{**}Data provided by Ninham Shand Inc

Table 17-15: Changes in engineering properties of Adelaide Subgroup sandstone aggregates under traffic (Brink, 1983).

			Pl	coarse s	Percentage coarse sand (cs) 0,425mm <cs<2mm< th=""><th colspan="2">Percentage smaller than 75μm</th></cs<2mm<>		Percentage smaller than 75 μ m	
		(a)*	(b)†	(a)	(b)	(a)	(b)	(b)
Road in vicin of East Lond			•				,	
Maximum	X_{M}	6	8	50	39	12	13	
Minimum	Xm	2	4	24	26	2	7	
Mean	x	4.3	6.0	33.2	31.0	7.9	9.3	
Number of tests Standard	n	156	32	158	32	158	32	
deviation Coefficient of	S	0,94	1,20	4,14	3,0	1,30	2,53	
variation	S/x	0,22	0,20	0,12	0,10	0,16	0,27	
2. Road in vicing of Richmond								(115/215)
Maximum	Xы	6	9	42	35	11	-13	(53%)
Minimum	X_{III}	3	7	26	25	6	7	
Mean	×	5.2	7,6	31.9	30,8	8.3	9.2	·
Number of tests Standard	'n	10	5	10	5	10	5	
deviation Coefficient of	\$	1,0	1,3	4,4	4,5	1,5	2,4	
variation	S/x̄	0,19	0,17	0,14	0,15	0,18	0,26	
3. Road in vicin of Colesberg								(75/185) (40%)
Maximum	XM	7	10	47	39	14	19	, ,
Minimum	xm	5	7	24	18	5	9	
Mean	x	6,0	9,0	3 5,5	29,9	8,6	14,0	
Number of tests Standard	n	28	7	28	14	28	7	
deviation Coefficient of	S	0,79	1,15	5,98	5,07	1,93	3,65	
variation	S/x	0,13	0,13	0,17	0,17	0,22	0,26	
4. Road in vicin of Noupcort	ity							
Maximum	XM	6	13	48	56	9	13	
Minimum	Xm	3	6.	33	30	5	6	
vlean	X	4,2	9,8	40.5	38,6	6.6	10,2	
Number of tests Standard		13	12	13	12	13	12	
deviation Coefficient of	S	1,07	1,76	3,86	7,3	1,12	2,25	
ariation	S/x	0,25	0,18	0,10	0,19	0,17	0,22	

^{* (}a) Construction control data

^{†(}b) Data obtained during later investigations after distress occurred

G.2 Dolerite (Zone B)

Dolerite has been used extensively in road construction; however, material from chill zones (surrounding metamorphosed rocks) are usually undesirable due to low adhesion properties (Brink, 1983). Dolerite has also been used successfully as a concrete aggregate (Brink, 1983).

Table 17-16: Engineering properties of very hard rock dolerite from various locations (Brink, 1983).

Locality	Percussion drill-bit penetration rate (minutes/ 200 mm)	Loss of drill-bit length (mm/10 minutes)	Loss of drill-bit gauge (mm/10 minutes)	Abrasive- ness (mass loss) (g)	Energy consumed during rod-milling (kWh/kg)	Proto- dyakonov strength (MPa)
1. Hilton,				EQ 47	4,87 × 10⁻³	-
Pietermaritzburg 2. Mountain Rise,	_	_	_	53,47	4,87 × 10 °	_
Pietermaritzburg	· —	_	. —	67,59	$3,33 \times 10^{-3}$	31,66
3. Kinross		_	_	74,71	$2,45 \times 10^{-3}$	34,53
4. Standerton	15,4	0,15	0,22	69,32	$4,87 \times 10^{-3}$	30,95
5. Cradock	_	-	. —	64,87	$2,20 \times 10^{-3}$	23,39
Beaufort West	12,2	0,26	0,15	61,25	$3,40 \times 10^{-3}$	35,88
7. Bloemfontein	16,2	0,22	0,17	71,20	$3,28 \times 10^{-3}$	32,92
8. Hendrik Ver-						
woerd dam site	13,7	0,19	0,20	61,26	$3,75 \times 10^{-3}$	33,51
9. P.K. le Roux dam site	12,1	0,10	0,13	65,94	$3,10 \times 10^{-3}$	29,92

Table 17-17: Strength properties of fresh dolerite from various locations (Brink, 1983).

Coefficient of variation				Site 1 Hilton quarry, Pietermaritz burg	Site 2 Mountain Rise - quany, Pletermaritz- burg	Site 3 Kinross road cutting	Site 4 Borchards Crushers quarry, Standerton	Site 5 South African Railways quarry, Cradock	Site 6 South African Railways National Roads quarry, Beaufort West
Strongth (MPa)	Linconfined	Movimum	V.,	540	268	265	400	260	407
Strength (MPa) Mean X 472 336 297 370 293 495 576 581	a real miner								
Number of tests n 6 9 8 6 15 27									
Standard deviation S	•								
Part									57,66
Minimum Xm 34,9 16,3 22,7 23,2 16,3 22,5			S/R	0,090	0,100	0,080	0,322	0,183	0,142
Mean X 37,6 26,3 23,8 30,4 24,4 31,4 1,4	Tensile`								
Number of tests Standard deviation Strength (MPa) Strength (MPa) Maximum Xu 34,2 39,1 32,2 37,9 36,0 47,2 37,9 47,2 47,									
Standard deviation S									
Variation S/R 0,039 0,166 0,059 0,136 0,169 0,134	1	Standard deviation							
Strength Minimum			S/\$	0,039	0,166	0,059	0,136	0,169	0,134
Strength Minimum	Shear box	Maximum	XM	34,2	33,1	32.2	37.9	36.0	47,2
Mean	Strength		Xm	14,5					
Standard deviation S 8,02 2,59 6,24 4,80 4,50 7,13	(MPa)	Mean	x	28,1	29,8	25,0		28,5	30,3
Coefficient of variation S/x 0,285 0,087 0,260 0,148 0,157 0,255				7	9		€	15	27
Site 7 Olive Hill Quarry P.K. le Roux dam			S	8,02	2,59	6,24	4,80	4,50	.7,13
P.K. te Roux dame		variation	S/x	0,285	0,087	0,250	0,148	0,157	0,235
Bloemfontein Excavations for wall and abutments A B County Eleft Gramman Gramm				Olive		ik Verwoerd		P.K. le Ro	ux dam
Tensile						В	c	Α .	В.
Strength Maximum XM 386 561 527 486 360 479					for wall	00000	Cuami	Louise	1.66
Minimum Xm 254 133 164 285 238 328 328 3391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 321 392 393 388 382 391 391 393 333 383 382 393 333			•						
Strength (MPa) Mean x 303 388 382 391 321 392	Unconfined								
Number of tests n 15 82 49 28 15 18 Standard deviation S 42,50 66,56 67,68 45,28 29,10 56,80 Coefficient of variation S/X 0,140 0,172 0,177 0,116 0,091 0,145 Tensile Maximum x _M 31,6 46,3 43,5 39,1 31,9 32,7 Strength Minimum x _m 23,1 9,5 19,5 26,9 11,9 26,3 (MPa) Mean X 27,0 30,5 31,7 31,9 25,9 29,9 Number of tests n 15 81 50 28 15 18 Standard deviation S 2,24 5,67 4,29 2,60 5,12 1,83 Coefficient of variation S/X 0,083 0,186 0,135 0,081 0,198 0,061 Shear box Maximum x _M 30,5 66,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 16,5 14,3 16,6 16,8 18,8 (MPa) Mean X 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of 1,76 1,76 Coefficient of 1,76 1,76 Coefficient of 1,76 Coefficient of 1,76 Coefficient of 1,76 Coefficient of 1,76 Coefficie									
Standard deviation S 42,50 66,56 67,68 45,28 29,10 56,80	Strength (MPa)		8	303	388	382			
variation S/x 0,140 0,172 0,177 0,116 0,091 0,145 Tensile Maximum x _M 31,6 46,3 43,5 39,1 31,9 32,7 Strength Minimum x _m 23,1 9,5 19,5 26,9 11,9 26,3 (MPa) Mean x 27,0 30,5 31,7 31,9 25,9 29,9 Number of tests n 15 81 50 28 15 18 Standard deviation S 2,24 5,67 4,29 2,60 5,12 1,83 Coefficient of variation S/x 0,083 0,186 0,135 0,061 0,198 0,061 Shear box Maximum x _M 30,5 68,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 16,5 14,3 16,6 16,8 18,8 Strength Minimum x _m 18,0	each Bar (mir a)								
Strength (MPa) Minimum ken x _n 23,1 9,5 19,5 26,9 11,9 26,3 (MPa) Mean x 27,0 30,5 31,7 31,9 25,9 29,9 Number of tests n 15 81 50 28 15 18 Standard deviation S 2,24 5,67 4,29 2,60 5,12 1,83 Coefficient of variation S/x 0,083 0,186 0,135 0,081 0,198 0,061 Shear box Maximum x _M 30,5 66,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 15,5 14,3 16,6 16,8 18,8 (MPa) Mean x 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95		Number of tests Standard deviation	n	15	82				
Strength (MPa) Minimum ken x _n 23,1 9,5 19,5 26,9 11,9 26,3 (MPa) Mean x 27,0 30,5 31,7 31,9 25,9 29,9 Number of tests n 15 81 50 28 15 18 Standard deviation S 2,24 5,67 4,29 2,60 5,12 1,83 Coefficient of variation S/x 0,083 0,186 0,135 0,081 0,198 0,061 Shear box Maximum x _M 30,5 66,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 15,5 14,3 16,6 16,8 18,8 (MPa) Mean x 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95		Number of tests Standard deviation Coefficient of	n S	15 42,50	82 66,56	67,68	45,28	29,10	56,80
Mean X 27,0 30,5 31,7 31,9 25,9 29,9 Number of tests n 15 81 50 28 15 18 Standard deviation S 2,24 5,67 4,29 2,60 5,12 1,83 Coefficient of variation S/x 0,083 0,186 0,135 0,081 0,198 0,061 Shear box Maximum x _M 30,5 66,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 16,5 14,3 16,6 16,8 18,8 (MPa) Mean X 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of 15 16 17,6 Coefficient of 15 17,6 Coefficient of 15 18 Coefficient of 15 18 Coefficient of 17,6 Coefficient of 17,7		Number of tests Standard deviation Coefficient of variation	n S S/x̄	15 42,50 0,140 31,6	82 66,56 0,172 46,3	67,68 0,177 43,5	45,28 0,116 39,1	29,10 0,091 31,9	56,80 0,145 32,7
Number of tests n 15 81 50 28 15 18 Standard deviation S 2,24 5,67 4,29 2,60 5,12 1,83 Coefficient of variation S/x 0,083 0,186 0,135 0,081 0,198 0,061 Shear box Maximum x _M 30,5 66,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 16,5 14,3 16,6 16,8 18,8 (MPa) Mean x 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of 15 18 1,76 Coefficient of 15 18 1,76 Coefficient of 15 18 Coefficient of 15 Coeff	Strength	Number of tests Standard deviation Coefficient of variation Maximum	n S S/x̄	15 42,50 0,140 31,6	82 66,56 0,172 46,3	67,68 0,177 43,5	45,28 0,116 39,1	29,10 0,091 31,9	56,80 0,145 32,7
Coefficient of variation S/x 0,083 0,186 0,135 0,081 0,198 0,061 Shear box Maximum x _M 30,5 68,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 16,5 14,3 16,6 16,8 18,8 (MPa) Mean x 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of Coefficient of 1,76	Strength	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean	n S S/x̄ XM Xm	15 42,50 0,140 31,6 23,1 27,0	82 66,56 0,172 46,3 9,5 30,5	67,68 0,177 43,5 19,5 31,7	45,28 0,116 39,1 26,9 31,9	29,10 0,091 31,9 11,9 25,9	56,80 0,145 32,7 26,3 29,9
Shear box Maximum x _M 30,5 68,3 49,7 59,2 34,8 24,3 Strength Minimum x _m 18,0 16,5 14,3 16,6 16,8 18,8 (MPe) Mean x 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of Coefficient of 15 15 18 15 18	Strength	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean Number of tests	N S/X XM Xm X n	15 42,50 0,140 31,6 23,1 27,0 15	82 66,56 0,172 46,3 9,5 30,5 81	67,68 0,177 43,5 19,5 31,7 50	45,28 0,116 39,1 26,9 31,9 28	29,10 0,091 31,9 11,9 25,9 15	56,80 0,145 32,7 26,3 29,9 18
Strength Minimum xm 18,0 16,5 14,3 16,6 16,8 18,8 (MPa) Mean x 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of Coefficient of 1,76 1,7	Tensile Strength (MPa)	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of	S/X S/X XM Xm R D S	15 42,50 0,140 31,6 23,1 27,0 15 2,24	82 66,56 0,172 46,3 9,5 30,5 81 5,67	67,68 0,177 43,5 19,5 31,7 50 4,29	45,28 0,116 39,1 26,9 31,9 28 2,60	29,10 0,091 31,9 11,9 25,9 15 5,12	56,80 0,145 32,7 26,3 29,9 18 1,83
(MPa) Mean x 22,7 32,1 32,1 35,9 24,2 21,4 Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of Coefficient of 1,76<	Strength	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of	S/X S/X XM Xm R D S	15 42,50 0,140 31,6 23,1 27,0 15 2,24	82 66,56 0,172 46,3 9,5 30,5 81 5,67	67,68 0,177 43,5 19,5 31,7 50 4,29	45,28 0,116 39,1 26,9 31,9 28 2,60	29,10 0,091 31,9 11,9 25,9 15 5,12	56,80 0,145 32,7 26,3 29,9 18 1,83
Number of tests n 15 81 49 28 15 18 Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of	Strength (MPa)	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum Maximum	n S S/X XM Xn R R S S/X	15 42,50 0,140 31,6 23,1 27,0 15 2,24 0,083	82 66,56 0,172 46,3 9,5 30,5 81 5,67 0,186	67,68 0,177 43,5 19,5 31,7 50 4,29 0,135	45,28 0,116 39,1 26,9 31,9 28 2,60 0,061 59,2	29,10 0,091 31,9 11,9 25,9 15 5,12 0,198	56,80 0,145 32,7 26,3 29,9 18 1,83 0,061 24,3
Standard deviation S 3,26 9,39 7,95 9,71 4,60 1,76 Coefficient of	Strength (MPa) Shear box Strength	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum Minimum Minimum	n S S/X XM Xn X D S S/X	15 42,50 0,140 31,6 23,1 27,0 15 2,24 0,083	82 66,56 0,172 46,3 9,5 30,5 81 5,67 0,186 66,3 16,5	67,68 0,177 43,5 19,5 31,7 50 4,29 0,135 49,7 14,3	45,28 0,116 39,1 26,9 31,9 28 2,60 0,061 59,2 16,6	29,10 0,091 31,9 11,9 25,9 15 5,12 0,198 34,8 16,8	56,80 0,145 32,7 26,3 29,9 18 1,83 0,061 24,3 18,8
	Strength (MPa)	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum Minimum Minimum Mean	n S S/x XM Xm x D S S/x XM	15 42,50 0,140 31,6 23,1 27,0 15 2,24 0,083 30,5 18,0 22,7	82 66,56 0,172 46,3 9,5 30,5 81 5,67 0,186 66,3 16,5 32,1	67,68 0,177 43,5 19,5 31,7 50 4,29 0,135 49,7 14,3 32,1	45,28 0,116 39,1 26,9 31,9 28 2,60 0,081 59,2 16,6 35,9	29,10 0,091 31,9 11,9 25,9 15 5,12 0,198 34,8 16,8 24,2	56,80 0,145 32,7 26,3 29,9 18 1,83 0,061 24,3 18,8 21,4
	Strength (MPa) Shear box Strength	Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum Minimum Minimum Mean Number of tests Standard deviation	N S S/X XM Xm S S/X XM Xm X	15 42,50 0,140 31,6 23,1 27,0 15 2,24 0,083 30,5 18,0 22,7 15	82 66,56 0,172 46,3 9,5 30,5 81 5,67 0,186 66,3 15,5 32,1 81	67,68 0,177 43,5 19,5 31,7 50 4,29 0,135 49,7 14,3 32,1 49	45,28 0,116 39,1 26,9 31,9 28 2,60 0,061 59,2 16,6 35,9 28	29,10 0,091 31,9 11,9 25,9 15 5,12 0,198 34,8 16,8 24,2 15	56,80 0,145 32,7 26,3 29,9 18 1,83 0,061 24,3 18,8 21,4 18

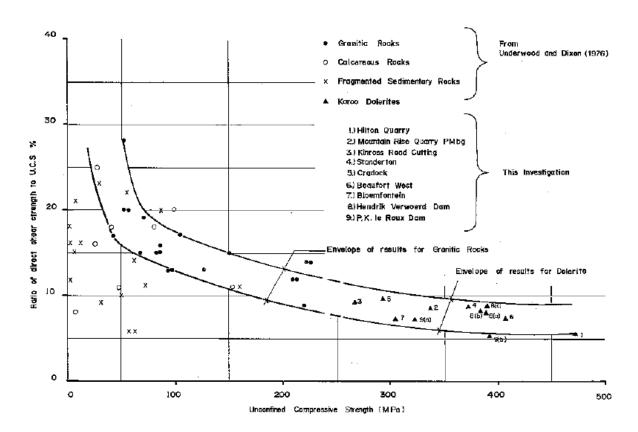


Figure 17-8: Variations of the shear strength to unconfined compressive strength ratio with the Unconfined Compressive Strength (UCS) for dolerite compared with other rock types (Brink, 1983).

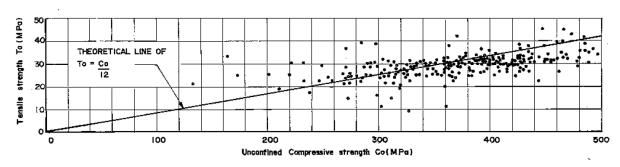


Figure 17-9: Relation between tensile strength and Unconfined Compressive Strength (UCS) of fresh dolerite specimen from South Africa (Brink, 1983).

Table 17-18: Weathering classes and characteristics of dolerite in South Africa (Brink, 1983).

Proposed class	Characteristics	Excavation	Grade of wea AEG (1978)	thering according to Weinert (1964, 1980)		
Solid dolerite	Fresh rock: hard to extremely hard, variably jointed; <15% weathered material in whole rock mass	Blasting	W1 or W2	Fresh		
Fractured dolerite	Fresh angular boulders of <0,5 m diameter, moderately thick zones of weathered material in joint spaces	Blasting or very heavy ripping depending on mass and type of joint fillings	W1 or W2 for boulders, otherwise W3 or W4	Boulders fresh, joint fillings weathered or highly weathered		
Boulder dolerite	Boulders with rounded edges and corners and >0,5 m diameter are fresh and strong; up to 1 m thick zones of intensely weathered material between boulders. 'Stacks' of loose boulders to be included in this class	Blasting for boulders, otherwise rippable; bulidozing for 'stacks' of loose boulders	Boulders W1, otherwise W4 or W5	Boulders fresh, otherwise highly weathered (mostly highly decomposed)		
Gravel dolerite	Gravelly with solid particles <75 mm diameter. Particles vary from fresh to very weathered material	Can usually be ripped or even picked; blasting rarely required	W4	Highly weathered (mostly highly disintegrated)		
Granular (sugar) dolerite	Fine gravelly to occasionally clayey; remnants of boulders with weathered 'onion' shells. May include calcrete where N>5 and ferricrete where N<5	Normally picking, bulldozing or shovelling, occasionally ripping	W4 or W5	Highly weathered (highly disintegrated where N>5, highly decomposed where N<5)		
Residual dolerite soil	Soft, homogeneous sandy to clayey soil	Shovelling, buildozing or picking	W5	Residual soil (sand where N>5, clay where N<5), ccasionally highly weathered		

Table 17-19: Influence of climate on selected physical properties of weathering classes of dolerites (Brink, 1983).

	alue			N = <2			N = 2-5			N = ~5	
,			%<0,075 mm	Pl	Mod AASHO Max. dens. (kg/m ³)	%<0,075 mm	PI	Mod AASHO Max. dens. (kg/m³)	%<0,075 mm	Pl	Mod AASHO Max. dens. (kg/m ³)
Gravel	Maximum	ХМ	32	28	_	15	19	_	23	17	2 220
dolerite	Minimum	Χm	6	8	_	5	1	_	9	6	1 719
`	^-≟:Mean	Χ̈	25	15	_	9	13	_	16	12	2098
	Number of tests	n	6	6	_	3	12	_	15	15	7
	Standard deviation	5	13,4	6,3	_	4,3	8,3	_	3,6	1,8	176
	Coefficient of variation	s/x	0,53	0,42	_	0,48	0,64	_	0,23	0,15	0,08
Granular	Maximum	ХM	85	42	2 008	60	21	2 098	49	22	2 254
dolerite	Minimum	Xm	10	8	1 573	10	3	1 970	14	3	1 767
	Mean	x	37	18	1790	27	13	1 986	31	9	2 026
	Number of tests	n	23	21	6	15	21	5	54	53	22
	Standard deviation	S	16.9	8,2	159	10,9	4,5	140	11,4	4,2	131
	Coefficient of variation	s/x̄	0,46	0,45	0,09	0,40	0,34	0,07	0,37	0,47	0,06
Residual	Maximum	Хм	95	50		94	33	1 914	74	33	1 978
dolerite	Minimum	Χm	50	11	_	48	3	1 514	44	8	1 621
soil	Mean	χ	64	23	1 620	71	18	1 673	59	18	1 831
	Number of tests	П	59	23	1	33	33	7	37	37	11
	Standard deviation	S	12,1	10,36	_	17,5	4,4	136	7,7	7,2	105
	Coefficient of variation	s/x	0,19	0,46	_	0,25	0,25	0,08	0,13	0,40	0,06
OF 11 11											
Climatic N-va	aue			N = 5 10			N = ~10			N = >10	
			%<0,075 mm	PI	Mod AASHO Max. dens. (kg/m ³)	%<0,075 mm	Pl	Mod AASHO Max. dens. (kg/m ³)	%<0,075 mm	PJ	Mod AASHO Max. dens. (kg/m ³)
Gravel	Maximum	ХМ	16	32	2 275	21	18	2 323			
dolerite	Minimum	Χm	1	2	2 034	3	0	2 066			
	Mean	X	7	12	2 146	6	8	2 211		No Results	
	Number of tests	п	35	35	5	33	33	12			
	Standard deviation		3,1	6,2	88			. 91			
		5				3,51	4,21				
	Coefficient of variation	s/x̄	0,44	0,52	0,04	0,55	0,51	0,04			
Granular	Coefficient of variation Maximum	s/x̄	0,44 51	0,52 29	2 227	0,55 24	0,51	2 195	15	14	2370
Granular dolerite	Coefficient of variation Maximum Minimum	S/X XM Xm	0,44 51 2	0,52 29 1	0,04 2 227 1 810	0,55 24 2	0,51 10 0	2 195 1 970	1	1	1 842
	Coefficient of variation Maximum Minimum Mean	S/X XM Xm X	0,44 51 2 13	0,52 29 1 9	0,04 2 227 1 810 2 082	0,55 24 2 9	0,51 10 0 4	2 195 1 970 2 082	1 4	1 4	1 842 2 163
	Coefficient of variation Maximum Minimum Mean Number of tests	S/X XM Xm X X	0,44 51 2 13 80	0,52 29 1 9 80	0,04 2 227 1 810 2 082 13	0,55 24 2 9 61	0,51 10 0 4 61	2 195 1 970 2 082 16	1 4 218	1 4 216	1 842 2 163 80
	Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation	S/X XM Xm X n s	0,44 51 2 13 80 12,8	0,52 29 1 9 80 6,7	0,04 2 227 1 810 2 082 13 142	0,55 24 2 9 61 5,48	0,51 10 0 4 61 2,82	2 195 1 970 2 082 16 57	1 4 218 1,59	1 4 216 3,06	1 842 2 163 80 114
	Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation	S/X XM Xm X X	0,44 51 2 13 80	0,52 29 1 9 80	0,04 2 227 1 810 2 082 13	0,55 24 2 9 61	0,51 10 0 4 61	2 195 1 970 2 082 16	1 4 218	1 4 216	1 842 2 163 80
dolerite Residual	Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum	S/X XM Xm X n s s/x X X X X X X X X X X X X X	0,44 51 2 13 80 12,8 0,98	0,52 29 1 9 80 6,7 0,74	0,04 2 227 1 810 2 082 13 142 0,07	0,55 24 2 9 61 5,48 0,08	0,51 10 0 4 61 2,82 0,07	2 195 1 970 2 082 16 57 0,03	1 4 218 1,59 0,40	1 4 216 3,06 0,77	1 842 2 163 80 114 0,05
dolerite Residual dolerite	Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum Minimum	S/X XM Xm X R S S S/X XM XM XM XM XM	0,44 51 2 13 80 12,8 0,98	0,52 29 1 9 80 6,7 0,74	0,04 2 227 1 810 2 082 13 142 0,07	0,55 24 2 9 61 5,48 0,08	0,51 10 0 4 61 2,82 0,07 26 1	2 195 1 970 2 082 16 57 0,03 2 370 1 810	1 4 218 1,59 0,40	1 4 216 3,06 0,77	1 842 2 163 80 114 0,05 2 355 1 954
dolerite Residual	Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum Minimum Mean	S/X XM Xm X n s s/X XM Xm X x XM	0,44 51 2 13 80 12,8 0,98 56 5 25	0,52 29 1 9 80 6,7 0,74 29 1 12	0,04 2 227 1 810 2 082 13 142 0,07 2 291 1 826 2 066	0,55 24 2 9 61 5,48 0,08	0,51 10 0 4 61 2,82 0,07 26 1 11	2 195 1 970 2 082 16 57 0,03 2 370 1 810 2 082	1 4 218 1,59 0,40 35 2	1 4 216 3,06 0,77	1 842 2 163 80 114 0,05 2 355 1 954 2 243
dolerite Residual dolerite	Coefficient of variation Maximum Minimum Mean Number of tests Standard deviation Coefficient of variation Maximum Minimum	S/X XM Xm X R S S S/X XM XM XM XM XM	0,44 51 2 13 80 12,8 0,98	0,52 29 1 9 80 6,7 0,74	0,04 2 227 1 810 2 082 13 142 0,07	0,55 24 2 9 61 5,48 0,08	0,51 10 0 4 61 2,82 0,07 26 1	2 195 1 970 2 082 16 57 0,03 2 370 1 810	1 4 218 1,59 0,40	1 4 216 3,06 0,77	1 842 2 163 80 114 0,05 2 355 1 954

Table 17-20: Concrete making properties of dolerite (Brink, 1983).

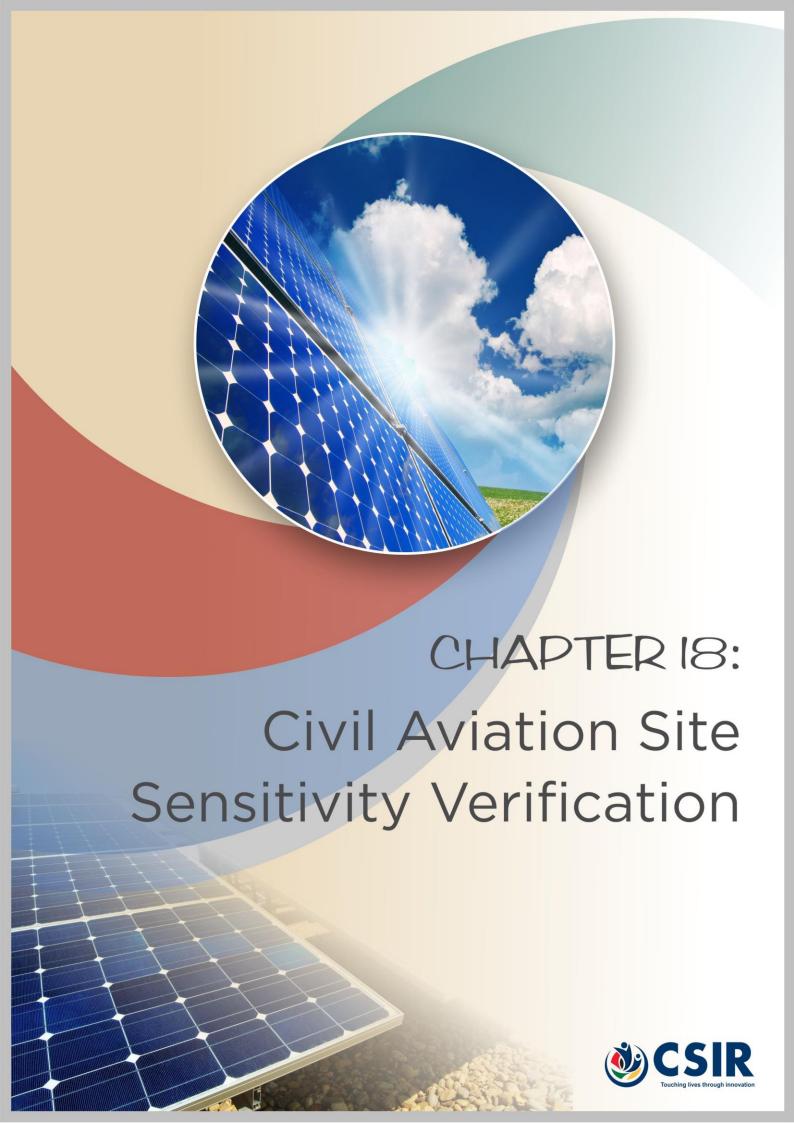
		Specific gravity (or relative density)	Loose bulk density (coarse) (kg/m³)	Loose bulk density (fine) (kg/m³)	Mortar shrinkage (%)	10% FACT (kN)
Maximum	ΧM	3,05	1 500	1 700	0,070	340
Minimum	Χm	2,85	1 350	1 350	0,037	180
Mean	Χ̈́	2,94	1 420	1 520	0,053	300
Number of tests	n	210	120	46	31	37
Standard deviation	S	0,037	29,24	79,19	0,008	37,65
Coefficient of variation	S/x̄	0,013	0,021	0,052	0,152	0,125

Table 17-21: Deformation characteristics (expressed in MPa) for different weathering classes of dolerite from South Africa as determined by a GB Menard pressure meter and jacking tests (Brink, 1983).

		Residual dolerite	Granular dolerite	Gravel	Boulder	Fractured dolerite	Fresh dolerite	
)	soil	dotente	dolerite	dolerite		From H.F. Verwoerd dam	From P.K. le Roux dam
Degree of weathe	ring	W5	W4/W5	W4	WЗ	W2	W 1	W1
Maximum	Χ _M	11,7	200,7	923,3	1 302,0	3 215,5	9 076	19 760
Minimum	Χm	7,3	89,4	404,7	1 071,6	2 034,9	5 615	9 062
Mean	X	9,2	158,3	593,2	1 156,5	2 625,2	7 692	12 587
Number of tests	n	3	4	3	3	2	18	15

G.3 Quaternary Sediments (Zone C)

Quaternary sediments overlying the Karoo Supergroup are variable in nature based on various case studies presented by Brink (1985). Potential geotechnical problems arising from such sediments include expansive and collapsible soils. Based on investigations previously undertaken in the region, some 30 km south of the site, such soils may be encountered. Transported materials are often thin to non-existent, and where present in natural drainage depressions often become more clayey and often exhibit desiccation cracks (Van Rooyen, 2012). Laboratory test results revealed that transported sediments (sheetwash and alluvium/gulleywash in this case) in the region have been described as "worse than G10" and the materials have 'low' to 'high' potential.





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Abbreviations					
ATNS	ATNS Air Traffic and Navigation Services SOC Limited				
EA	Environmental Authorisation				
EIA	Environmental Impact Assessment				
DEA	Department of Environmental Affairs				
DFFE	Department of Forestry, Fisheries and the Environment				
DSR	Draft Scoping Report				
ICAO	International Civil Aviation Organisation Code				
NEMA	National Environmental Management Act				
PV	Photovoltaic				
REDZ	Renewable Energy Development Zones				
SACAA	South African Civil Aviation Authority				
SEA	Strategic Environmental Assessment				

18. CIVIL AVIATION SITE SENSITIVITY VERIFICATION

18.1 Introduction

This report serves as the Site Sensitivity Verification for Civil Aviation for the Scoping and Environmental Impact Assessment (EIA) Process for the proposed development of the Kudu Solar Facility 2 and associated infrastructure near De Aar in the Northern Cape. The proposed project forms part of a cluster of 12 Solar Photovoltaic (PV) facilities and associated infrastructure. This report deals with Kudu Solar Facility 2 (hereafter referred to as the "Kudu Solar Facility" or "proposed project").

18.2 Need for the Site Sensitivity Verification

On 20 March 2020, in Government Gazette 43110, Government Notice (GN) R320, the Department of Environment, Forestry and Fisheries (DEFF) [now operating as the Department of Forestry, Fisheries and the Environment (DFFE)] published procedures for the assessment and minimum criteria for reporting on identified environmental themes in terms of Sections 24(5)(a) and (h) and 44 of the National Environmental Management Act (Act 107 of 1998, as amended) (NEMA) when applying for an Environmental Authorisation (EA). GN R320 prescribes general requirements for undertaking Site Sensitivity Verification, as well as protocols for assessment and minimum report content requirements of environmental impacts associated with specified environmental themes for relevant activities requiring EA. GN R320 was enforced within 50 days of publication of the notice i.e. on 9 May 2020.

GN R320 specifically includes a protocol that provides the criteria for the specialist assessment and minimum report content requirements for impacts on civil aviation installations for relevant activities requiring EA. This protocol replaces the requirements of Appendix 6 of the 2014 NEMA EIA Regulations (as amended).

This specific protocol states that proposed developments (where relevant) that occur on sites identified as Very High, High or Medium sensitivity, as depicted on the National Web-Based Environmental Screening Tool (Screening Tool), must include a Civil Aviation Compliance Statement. It further states that there are no requirements if the proposed developments occur on sites identified as Low sensitivity on the Screening Tool. However, a Site Sensitivity Verification is required for the Civil Aviation Protocol for all sensitivity levels.

Therefore, since the proposed projects require an EA in terms of the 2014 NEMA EIA Regulations (as amended), and Civil Aviation was identified as a relevant theme in the Screening Tool Report, GN R320 must be complied with.

18.3 Methodology

The Site Sensitivity Verification Process and Report has been compiled based on the following methodology:

- Existing spatial databases were used to determine the location of civil aviation installations in relation to the proposed project study area, and to identify preliminary areas of concern in terms of impacts to civil aviation installations;
- The proposed project study area was plotted on the Screening Tool to identify the sensitivity allocated;
- A site visit was undertaken to confirm the current land use and the environmental sensitivity as it relates to Civil Aviation;
- Additional research was undertaken to substantiate the Site Sensitivity Verification process;
 and
- A Site Sensitivity Verification Report was compiled (i.e. this report).

The information sources listed in Table 18-1 were used in the Site Sensitivity Verification process.

Table 18-1: Information Sources used for the Site Sensitivity Verification process

Data / Information	Source	Date	Туре	Description
National Web-Based Environmental Screening Tool (Screening Tool)	Department of Forestry, Fisheries, and the Environment (DFFE)	2022- 2023	Spatial / Online Assessment	The Screening Tool is a geographically based web-enabled application which allows a proponent intending to submit an Application for EA in terms of the 2014 NEMA EIA Regulations (as amended) to screen the proposed site for any environmental sensitivity ¹ .
RSA Airspaces in 3D	Air Traffic and Navigation Services SOC Limited (ATNS)	2022	Google Earth KMZ File	The RSA Airspaces in 3D data KMZ file is an initiative undertaken by the ATNS to illustrate the definitions and complexities of airspace, routes, aerodromes and navigational facilities within South Africa to the public in the interest of safety ² .
Wind and Solar PV Phase 1 Strategic Environmental Assessment (SEA)	Department of Environmental Affairs (DEA) [now operating as the DFFE]	2015	Report	SEA commissioned by the DEA (now operating as the DFFE) in 2013 for an assessment of wind and solar PV energy in South Africa, with an aim of identifying eight Renewable Energy Development Zones (REDZs) to focus and incentivize such development (i.e. Phase 1 REDZs SEA: CSIR Report Number: CSIR/CAS/EMS/ER/2015/0001/B).
Wind and Solar PV Phase 2 SEA	Department of Environment, Forestry, and Fisheries (DEFF) [now operating as the DFFE]	2019	Report	SEA commissioned by the DEFF (now operating as the DFFE) in 2016 for an assessment of wind and solar PV energy in South Africa, with an aim of identifying three additional REDZs to focus and incentivize such development (i.e. Phase 2 REDZ SEA. CSIR Report Number: CSIR/SPLA/SECO/ER/2019/0085).
Scoping Level and EIA Phase Visual Impact Assessments for the proposed project	Quinton Lawson and Bernard Oberholzer, QARC and BOLA	2022, 2023	Report	This Visual Impact Assessment was commissioned for the proposed project.

Therefore, the Site Sensitivity Verification was undertaken using desktop analysis, satellite imagery, on-site inspection, and other available and relevant information.

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¹ https://screening.environment.gov.za/screeningtool/index.html#/pages/welcome

² https://www.atns.co.za/rsakmz.php

18.4 Proposed Project Location

The proposed Kudu Solar Facility is located within the Renosterberg Local Municipality, which falls within the Pixley Ka Seme District Municipality. The proposed project is not located within any of the gazetted Renewable Energy Development Zones (REDZs); however is located within the Central Strategic Transmission Corridor that was gazetted in GN 113 on 16 February 2018. The proposed solar facility and its associated infrastructure will be constructed on a selection of the farm portions indicated in the table below, which also served as the study area for this EIA.

Table 18-2: Farm portions associated with the Kudu Solar Facilities

Farm Portion	SG code
Remaining Extent of the Farm Bas Berg No. 88	C05700000000008800000
Remaining Extent of Portion 3 of the Farm Bas Berg No. 88	C05700000000008800003
Portion 4 (Portion of Portion 3) of the Farm Bas Berg No. 88	C05700000000008800004
Remaining Extent of Portion 2 (Middel Plaats) (a Portion of Portion 1) of the Farm Grasspan No. 40	C05700000000004000002
Remaining Extent of the Farm Annex Wolve Kuil No. 41	C05700000000004100000
Portion 1 (Wolve Kuil West) of the Farm Annex Wolve Kuil No. 41	C05700000000004100001
Portion 2 of the Farm Wolve Kuil No. 43	C05700000000004300002
Remaining Extent of the Farm Wolve Kuilen No. 42	C05700000000004200000

Refer to Chapter 2 of the EIA Report for a list of affected farm properties for each proposed solar facility.

18.5 Details of the EIA Team

GN R320 states that prior to commencing with a specialist assessment, the current use of the land and the potential environmental sensitivity of the site under consideration as identified by the Screening Tool must be confirmed by undertaking a Site Sensitivity Verification.

This Site Sensitivity Verification was undertaken by Lizande Kellerman and Helen Antonopoulos. Lizande Kellerman is registered with the South African Council for Natural and Scientific Professions (SACNASP), with Registration Number 400076/10 in the field of Botanical Sciences. Helen Antonopoulos is an intern Environmental Scientist in the Environmental Management Services (EMS) group of the CSIR and holds BSc, BSc Honours, and MSc degrees in Environmental and Geographical Science from the University of Cape Town.

Inputs to the Site Sensitivity Verification Report were provided by Lizande Kellerman, Helen Antonopoulos, Rohaida Abed and Luanita Snyman-Van der Walt of the CSIR. Refer to Appendix A of the EIA Report for Curriculum Vitae of the project team.

18.6 Findings of the Screening Tool

Screening Tool Reports and/or maps were generated for the proposed projects using the following classifications:

- Solar PV: Utilities Infrastructure → Electricity → Generation → Renewable → Solar → PV → Solar PV: and
- Substations: Utilities Infrastructure → Electricity → Distribution and Transmission →
 Substation.

The Solar PV classification results in the use of the Solar PV methodology, whilst the substations classification results in the use of the general methodology on the Screening Tool.

The civil aviation theme (for Solar PV developments) on the Screening Tool depicted that the entire study area is located in a low sensitivity area from a civil aviation perspective i.e. there are no major or other types of civil aviation aerodromes or buffers that intersect with the study area or the Original and Revised Scoping Buildable Areas. Figure 18-1 illustrates the civil aviation sensitivity in relation to the entire study area and the development footprints. The development footprints were identified following the analysis of the Original and Revised Scoping Buildable Areas in the Scoping Phase.

In line with the above, the civil aviation theme (for substation developments) on the Screening Tool depicted that the entire study area is located in a low sensitivity area from a civil aviation perspective (Figure 18-2). However, the civil aviation theme for substation developments also depicted the following features, which are outside of the study area, and a significant distance away:

- De Aar Aerodrome (classified as "Other Civil Aviation Aerodrome") located approximately 54 km south-west of the study area. High and medium sensitivity are respectively allocated to the area that extends 8 km from the De Aar Aerodrome; and between 8 and 15 km of the aerodrome;
- Petrusville Aerodrome (classified as "Other Civil Aviation Aerodrome") located approximately 25 km north-east of the study area. High and medium sensitivity are respectively allocated to the area that extends 8 km from the Petrusville Aerodrome; and between 8 and 15 km of the aerodrome;
- Dangerous and restricted airspace demarcated as high sensitivity, which is located more than 50 km to the south-west of the study area;
- Civil Aviation Radar, which is located at point 30° 27' 51.4" S and 23° 59' 19.1" E; approximately 37 km south-west of the study area. The area within 15 km of the civil aviation radar is demarcated with a high sensitivity; and the area between 15 and 35 km of the civil aviation radar is rated with a medium sensitivity. This same facility is highlighted under the RFI theme as a Sentech High Power Terrestrial Broadcasting Facility and a Telecommunication Facility; and
- The same area above overlaps with a medium sensitivity area allocated to 5 km from an air traffic control or navigation site.

In terms of GN R320, this means that no further requirements are applicable i.e. a Compliance Statement is not required, if the site is indeed found to be of low sensitivity during the site visit.

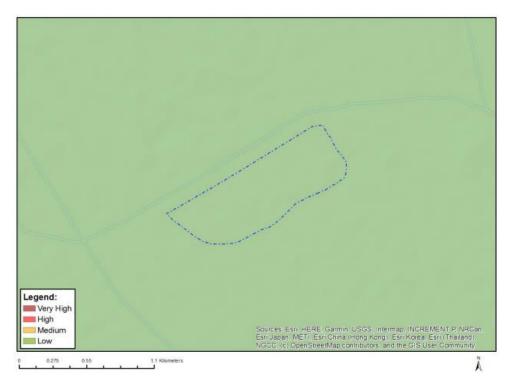


Figure 18-1: Screening Tool Map showing the buildable area for the proposed Kudu Solar Facility in terms of Civil Aviation Sensitivity (Source: DFFE Screening Tool, 2023).



Figure 18-2: Screening Tool Map showing the buildable area for the proposed Solar Facility, as well as the on-site substation complex, in terms of Civil Aviation Sensitivity (Source: DFFE Screening Tool, 2023).

18.7 Details of the Site Visit

The details of the site visit are noted below:

Date of Site Visit 29 – 31 August 2022		
Specialist Name Lizande Kellerman		
Professional Registration Number	SACNASP Registration Number 400076/10	
Specialist Affiliation / Company	CSIR	

18.8 Findings

The site visit confirmed that the land within the study area is used for livestock grazing, and that there are structures such as farm steads, livestock pens, waterpoints, farm roads and fences, and existing high voltage power lines within the area. This is corroborated by the Agricultural Compliance Statement (Chapter 6 of the EIA Report) which states that moisture availability is insufficient for crop production without irrigation and the potential agricultural land use of the study area is therefore limited to grazing. As noted in the Terrestrial Biodiversity and Species Assessment (Chapter 7 of the EIA Report), the study area is located in the Northern Upper Karoo (NKu3), Eastern Upper Karoo (NKu4) and the Besemkaree Koppies Shrubland vegetation types. The habitat is homogenous and consists of extensive plains with low shrubs and grasses. **No civil aviation installations were found within the proposed project study area.** Refer to Figure 18-3 and Figure 18-4 for views of the farm portion on which the proposed project will take place.



Figure 18-3: Panoramic (180°) view from an internal gravel road towards Remaining Extent of Portion 3 of the Farm Bas Berg No. 88 (SW to NE direction). This photo pertains to PV2 (*Photo*: L. Kellerman)



Figure 18-4: View from an internal gravel road towards Remaining Extent of Portion 3 of the Farm Bas Berg No. 88 (SE direction). This photo pertains to PV2 (Photo: L. Kellerman)

The Air Traffic and Navigation Services SOC Limited (ATNS) data has confirmed that there is an unlicensed aerodrome outside of the 30 km radius of the proposed project site. The Petrusville Airfield (International Civil Aviation Organisation Code (ICAO): FAPV) (30° 5′ 0.69" S; 24° 40′ 48.16" E) is located approximately 26 km north-east of the entire study area. During the site visit it was concluded that the airfield is out of use, as indicated by the dilapidated condition of the runway and lack of civil aviation infrastructure, such as windsocks. Figure 18-5 and Figure 18-6 show the airfield and its lack of maintenance. The location of the Petrusville Airfield, which is approximately 1.4 km long and is oriented SE to NW, is indicated on the Screening Tool as medium sensitivity for solar PV developments; and high sensitivity within 8 km of the aerodrome for substation developments (based on the general methodology); however, the actual aerodrome will not be impacted on by the proposed solar facility and associated infrastructure due to its distance from the study area.



Figure 18-5: Petrusville Airfield (FAPV) (view in NW direction) (Photo: L. Kellerman)



Figure 18-6: Petrusville Airfield (FAPV) (view in SE direction). Note the lack of aviation infrastructure, such as a windsock (*Photo*: L. Kellerman)

Research indicates that the Department of Defence Ammunition Depot and School of Ammunition is located approximately 5 km north-west of De Aar (ArchaeoMaps Archaeological Consultancy, 2009)³. The ATNS data classifies this facility as restricted airspace, which is located more than 50 km to the south-west of the study area. The Screening Tool shows this area as dangerous and restricted airspace (high sensitivity) based on the general methodology for substations; however, it is not identified for the Solar PV methodology. The De Aar Airport (International Civil Aviation Organisation Code: FADA) (30°41'29.51"S; and 24°1'27.13" E) lies roughly 4 km east of the Department of Defence Ammunition Depot and School of Ammunition; and approximately 55 km south-west of the study area (at its closest point), thus falling outside of the 30 km radius around the study area. Based on their locations, neither the restricted airspace nor the De Aar Airport will be impacted on by the proposed project.

The ATNS data also notes that both Conventional (Upper and Lower ATS) and Area Navigation Routes associated with the Johannesburg Area Central Airspace fall within the 30 km radius of the study area. However, the proposed solar panels will range to a maximum height of 3.5 m, and the substation complex is estimated to extend up to 10 m from ground level and are thus not likely to impact negatively on civil aviation installations or air traffic associated with the Johannesburg Area Central Airspace. Most of the features noted above are in line with the findings of the Phase 1 and Phase 2 Wind and Solar SEA Reports.

Figure 18-7 indicates the location of the civil aviation features noted above, which informed this Site Sensitivity Verification.

³ ArchaeoMaps Archaeological Consultancy (2009). Archaeological Impact Assessment: Establishment of an Ammunition Disposal Plant, Sinclair's Dam 133, De Aar, Northern Cape, South Africa. Date: 2009-03-23. Available online: https://sahris.sahra.org.za/sites/default/files/heritagereports/AIA%20-%20ADP,%20Sinclairs%20Dam,%20De%20Aar,%20NC.pdf, Accessed October 2022.

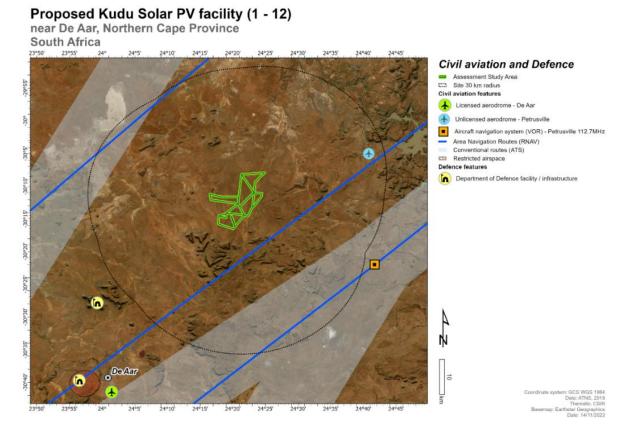


Figure 18-7: Civil Aviation features relative to the proposed project study area based on the site visit and existing databases.

18.9 Review of the Scoping and EIA Reports

The Draft EIA Reports were made available to all registered Interested and/or Affected Parties (I&APs), Organs of State and other relevant key stakeholders for a 30-day comment period which extended from 2 June to 3 July 2023, excluding public holidays, whereas the Draft Scoping Reports (DSRs) were made available to all registered I&APs Organs of State and other relevant key stakeholders for a 30-day comment period which extended from 09 December 2022 to 30 January 2023, excluding public holidays and the regulated shutdown period.

The South African Civil Aviation Authority (SACAA) and the ATNS are included as key stakeholders on the project stakeholder database and were afforded the opportunity to comment on the DSRs and Draft EIA Reports, including this Site Sensitivity Verification Report for the Civil Aviation (Solar) Theme applicable to the proposed project.

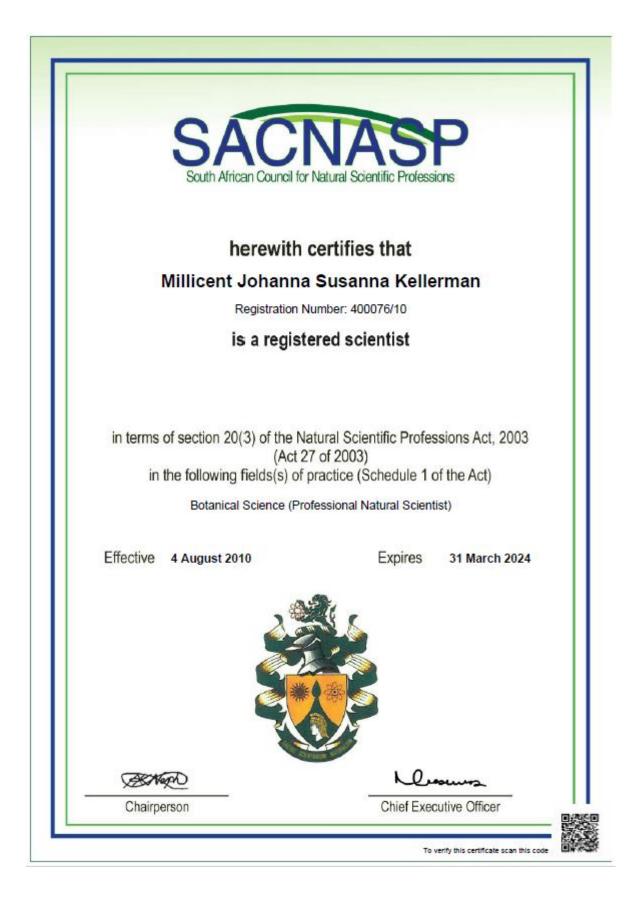
The SACAA provided written comment during the Background Information Document phase, acknowledging the acceptance of the Final Scoping Report, and EIA Phase, in which it was noted that ATNS is responsible for Solar Obstacle Applications, as published on the SACAA website⁴. The

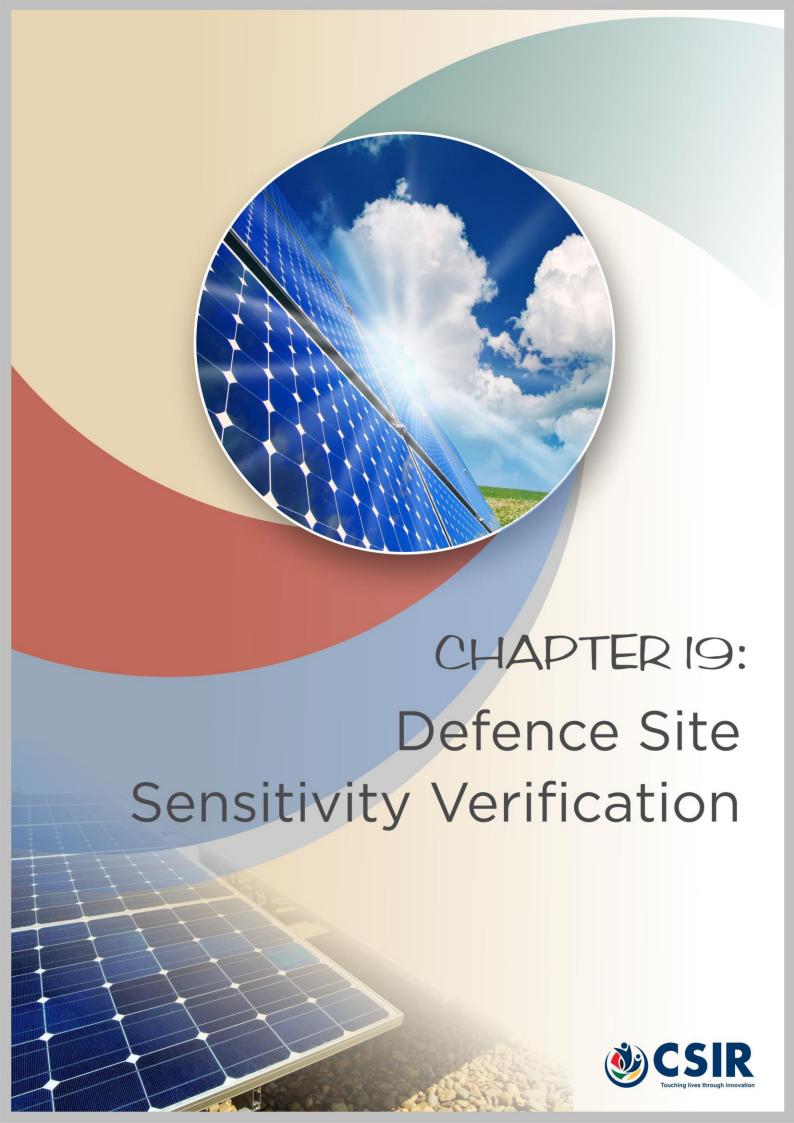
⁴ https://www.caa.co.za/

Project Applicant has lodged the necessary documents for the Obstacle Application and approval in May 2023 (outside of the NEMA process). Moreover, during the EIA Phase, the SACAA confirmed that they have no objection against the proposed development. Refer to Appendix H.6 of this EIA Report for a copy of this correspondence.

18.10Concluding Statement

The proposed project study area was determined and verified to be of low sensitivity (as it relates to civil aviation). This was determined through a site visit and based on existing databases, and confirms the sensitivity allocated on the Screening Tool. Based on the above, in terms of GN R320, no further requirements are applicable i.e. a Compliance Statement is not required.







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Abbreviations					
ATNS	Air Traffic and Navigation Services SOC Limited				
EA	Environmental Authorisation				
EIA	Environmental Impact Assessment				
DEA	Department of Environmental Affairs				
DFFE	Department of Forestry, Fisheries and the Environment				
DoD	Department of Defence				
DSR	Draft Scoping Report				
NEMA	National Environmental Management Act				
PV	Photovoltaic				
REDZ	Renewable Energy Development Zone				
SANDF	South African National Defence Force				
SEA	Strategic Environmental Assessment				

19. DEFENCE SITE SENSITIVITY VERIFICATION

19.1 Introduction

This report serves as the Site Sensitivity Verification for Defence for the Scoping and Environmental Impact Assessment (EIA) Process for the proposed development of the Kudu Solar Facility 2 and associated infrastructure near De Aar in the Northern Cape. The proposed project forms part of a cluster of 12 Solar Photovoltaic (PV) facilities and associated infrastructure. This report deals with Kudu Solar Facility 2 (hereafter referred to as the "Kudu Solar Facility" or "proposed project").

19.2 Need for the Site Sensitivity Verification

On 20 March 2020, in Government Gazette 43110, Government Notice (GN) R320, the Department of Environment, Forestry and Fisheries (DEFF) [now operating as the Department of Forestry, Fisheries and the Environment (DFFE)] published procedures for the assessment and minimum criteria for reporting on identified environmental themes in terms of Sections 24(5)(a) and (h) and 44 of the National Environmental Management Act (Act 107 of 1998, as amended) (NEMA) when applying for an Environmental Authorisation (EA). GN R320 prescribes general requirements for undertaking Site Sensitivity Verification, as well as protocols for assessment and minimum report content requirements of environmental impacts associated with specified environmental themes for relevant activities requiring EA. GN R320 was enforced within 50 days of publication of the notice i.e. on 9 May 2020.

GN R320 specifically includes a protocol that provides the criteria for the specialist assessment and minimum report content requirements for impacts on defence installations for relevant activities requiring EA. This protocol replaces the requirements of Appendix 6 of the 2014 NEMA EIA Regulations (as amended).

This specific protocol states that proposed developments (where relevant) that occur on sites identified as Very High, High or Medium sensitivity, as depicted on the National Web-Based Environmental Screening Tool (Screening Tool), must include a Defence Compliance Statement. It further states that there are no requirements if the proposed developments occur on sites identified as Low sensitivity on the Screening Tool. However, a Site Sensitivity Verification is required for the Defence Protocol for all sensitivity levels.

Therefore, since the proposed projects require an EA in terms of the 2014 NEMA EIA Regulations (as amended), and Defence was identified as a relevant theme in the Screening Tool Report, GN R320 must be complied with.

19.3 Methodology

The Site Sensitivity Verification Process and Report has been compiled based on the following methodology:

- Existing spatial databases were used to determine the location of defence installations in relation to the proposed project study area, and to identify preliminary areas of concern in terms of potential impacts to defence installations;
- The proposed project study area was plotted on the Screening Tool to identify the sensitivity allocated;
- A site visit was undertaken to confirm the current land use and the environmental sensitivity as it relates to Defence;
- Additional research was undertaken to substantiate the Site Sensitivity Verification process;
 and
- A Site Sensitivity Verification Report was compiled (i.e. this report).

The information sources listed in Table 19-1 were used in the Site Sensitivity Verification process.

Table 19-1: Information Sources used for the Site Sensitivity Verification process

Data /	0	Data	T	Description
Information	Source	Date	Туре	Description
National Web-Based	Department of	2022	Spatial /	The Screening Tool is a geographically
Environmental	Forestry, Fisheries	-	Online	based web-enabled application which allows
Screening Tool	and the	2023	Assessment	a proponent intending to submit an
(Screening Tool)	Environment			Application for EA in terms of the 2014
	(DFFE)			NEMA EIA Regulations (as amended) to
				screen the proposed site for any
				environmental sensitivity ¹ .
Republic of South	Air Traffic and	2022	Google Earth	The RSA Airspaces in 3D data KMZ file is
Africa (RSA)	Navigation Services		KMZ File	an initiative undertaken by the ATNS to
Airspaces in 3D	SOC Limited			illustrate the definitions and complexities of
	(ATNS)			airspace, routes, aerodromes and
				navigational facilities within South Africa to
				the public in the interest of safety ² .
Wind and Solar PV	Department of	2015	Report	SEA commissioned by the DEA [now
Phase 1 Strategic	Environmental			operating as the DFFE) in 2013 for an
Environmental	Affairs (DEA)			assessment of wind and solar PV energy in
Assessment (SEA)				South Africa, with an aim of identifying eight
				Renewable Energy Development Zones
				(REDZs) to focus and incentivize such
				development (i.e. Phase 1 REDZs SEA:
				CSIR Report Number:
				CSIR/CAS/EMS/ER/2015/0001/B).
Wind and Solar PV	Department of	2019	Report	SEA commissioned by the DEFF in 2016 for
Phase 2 SEA	Environment,			an assessment of wind and solar PV energy
	Forestry and			in South Africa, with an aim of identifying
	Fisheries (DEFF)			three additional REDZs to focus and
				incentivize such development (i.e. Phase 2
				REDZ SEA. CSIR Report Number:
				CSIR/SPLA/SECO/ER/2019/0085).

Therefore, the Site Sensitivity Verification was undertaken using desktop analysis, satellite imagery, on-site inspection, and other available and relevant information.

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¹ https://screening.environment.gov.za/screeningtool/index.html#/pages/welcome

² https://www.atns.co.za/rsakmz.php

19.4 Proposed Project Location

The proposed Kudu Solar Facility is located within the Renosterberg Local Municipality, which falls within the Pixley Ka Seme District Municipality. The proposed project is not located within any of the gazetted Renewable Energy Development Zones (REDZs); however is located within the Central Strategic Transmission Corridor that was gazetted in GN 113 on 16 February 2018. The proposed solar facility and its associated infrastructure will be constructed on a selection of the farm portions indicated in the table below, which also served as the study area for this EIA:

Table 19-2: Farm portions associated with the Kudu Solar Facilities

Farm Portion	SG Code
Remaining Extent of the Farm Bas Berg No. 88	C05700000000008800000
Remaining Extent of Portion 3 of the Farm Bas Berg No. 88	C05700000000008800003
Portion 4 (Portion of Portion 3) of the Farm Bas Berg No. 88	C05700000000008800004
Remaining Extent of Portion 2 (Middel Plaats) (a Portion of Portion 1) of the Farm Grasspan No. 40	C05700000000004000002
Remaining Extent of the Farm Annex Wolve Kuil No. 41	C05700000000004100000
Portion 1 (Wolve Kuil West) of the Farm Annex Wolve Kuil No. 41	C05700000000004100001
Portion 2 of the Farm Wolve Kuil No. 43	C05700000000004300002
Remaining Extent of the Farm Wolve Kuilen No. 42	C05700000000004200000

Refer to Chapter 2 of the EIA Report for a list of affected farm properties for each proposed solar facility.

19.5 Details of the EIA Team

GN R320 states that prior to commencing with a specialist assessment, the current use of the land and the potential environmental sensitivity of the site under consideration as identified by the Screening Tool must be confirmed by undertaking a Site Sensitivity Verification.

This Site Sensitivity Verification was undertaken by Lizande Kellerman and Helen Antonopoulos. Lizande Kellerman is registered with the South African Council for Natural and Scientific Professions (SACNASP), with Registration Number 400076/10 in the field of Botanical Sciences. Helen Antonopoulos is an intern Environmental Scientist in the Environmental Management Services (EMS) group of the CSIR and holds BSc, BSc Honours, and MSc degrees in Environmental and Geographical Science from the University of Cape Town.

Inputs to the Site Sensitivity Verification Report were provided by Lizande Kellerman, Helen Antonopoulos, Rohaida Abed and Luanita Snyman-Van der Walt of the CSIR. Refer to Appendix A of the EIA Report for Curriculum Vitae of the project team.

19.6 Findings of the Screening Tool

Screening Tool Reports and/or maps were generated for the proposed projects using the following classifications:

- Solar PV: Utilities Infrastructure → Electricity → Generation → Renewable → Solar → PV;
 and
- **Substations:** Utilities Infrastructure → Electricity → Distribution and Transmission → Substation.

The Solar PV classification results in the use of the Solar PV methodology, whilst the substations classification results in the use of the general methodology on the Screening Tool.

The defence theme (for Solar PV developments) on the Screening Tool depicted that the entire study area is located in a low sensitivity area from a defence perspective i.e. there are no major or other types of defence installations or buffers that intersect with the study area or the Original and Revised Scoping Buildable Areas. Figure 19-1 illustrates the defence sensitivity in relation to the entire study area and the development footprints. The development footprints were identified following the analysis of the Original and Revised Scoping Buildable Areas in the Scoping Phase.

In line with the above, the defence theme (for substation developments) on the Screening Tool depicted that the entire study area is located in a low sensitivity area from a defence perspective (Figure 19-2).

In terms of GN R320, this means that no further requirements are applicable i.e. a Compliance Statement is not required, if the site is indeed found to be of low sensitivity during the site visit.



Figure 19-1: Screening Tool Map showing the buildable area for the proposed Kudu Solar Facility in terms of Defence Sensitivity (Source: DFFE Screening Tool, 2023).



Figure 19-2: Screening Tool Map showing the buildable area for the proposed Solar Facility, as well as the on-site substation complex, in terms of Defence Sensitivity (Source: DFFE Screening Tool, 2023).

19.7 Details of the Site Visit

The details of the site visit are noted below:

Date of Site Visit	29 – 31 August 2022
Specialist Name	Lizande Kellerman
Professional Registration Number	SACNASP Registration Number 400076/10
Specialist Affiliation / Company	CSIR

19.8 Findings

The site visit confirmed that the land within the study area is used for livestock grazing, and that there are structures such as farm steads, livestock pens, waterpoints, farm roads and fences, and existing high voltage power lines within the area. This is corroborated by the Agricultural Compliance Statement (Chapter 6 of the EIA Report) which states that moisture availability is insufficient for crop production without irrigation and the potential agricultural land use of the study area is therefore limited to grazing. As noted in the Terrestrial Biodiversity and Species Assessment (Chapter 7 of the EIA Report), the study area is located in the Northern Upper Karoo (NKu3), Eastern Upper Karoo (NKu4) and the Besemkaree Koppies Shrubland vegetation types. The habitat is homogenous and consists

of extensive plains with low shrubs and grasses. **No defence installations were found within the study area.** Refer to Figure 19-3 and Figure 19-4 for views of the farm portion on which the proposed project will take place.



Figure 19-3: Panoramic (180°) view from an internal gravel road towards Remaining Extent of Portion 3 of the Farm Bas Berg No. 88 (SW to NE direction). This photo pertains to PV2 (*Photo*: L. Kellerman)



Figure 19-4: View from an internal gravel road towards Remaining Extent of Portion 3 of the Farm Bas Berg No. 88 (SE direction). This photo pertains to PV2 (*Photo*: L. Kellerman)

Research indicates that the Department of Defence Ammunition Depot and School of Ammunition is located approximately 5 km north-west of De Aar (ArchaeoMaps Archaeological Consultancy, 2009)³. The Air Traffic and Navigation Services SOC Limited (ATNS) data classifies this facility as restricted airspace, which is located more than 50 km to the south-west of the study area. The Screening Tool shows this area as low sensitivity in relation to the solar methodology; however based on the general methodology for substations, this area is indicated as medium and very high sensitivity (for a military and defence site). The Screening Tool also shows another military and defence site as very high sensitivity located approximately 25 km north-west of De Aar and 37 km south-west of the study area. This same facility is highlighted under the RFI theme as a Sentech High Power Terrestrial Broadcasting Facility and a Telecommunication Facility. However, based on its location and vast distance from the study area, it will not be impacted on by the proposed project.

The features noted above are in line with the findings of the Phase 1 and Phase 2 Wind and Solar Strategic Environmental Assessment (SEA) Reports.

Figure 19-5 indicates the location of the defence features noted above, which informed this Site Sensitivity Verification.

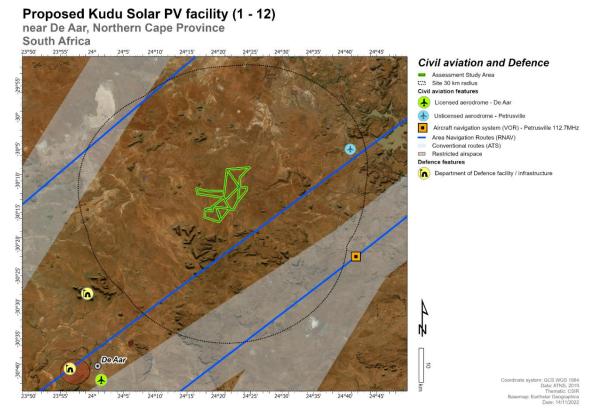


Figure 19-5: Defence features relative to the proposed project study area based on the site visit and existing databases.

³ ArchaeoMaps Archaeological Consultancy (2009). Archaeological Impact Assessment: Establishment of an Ammunition Disposal Plant, Sinclair's Dam 133, De Aar, Northern Cape, South Africa. Date: 2009-03-23. Available online: https://sahris.sahra.org.za/sites/default/files/heritagereports/AIA%20-%20ADP,%20Sinclairs%20Dam,%20De%20Aar,%20NC.pdf, Accessed October 2022.

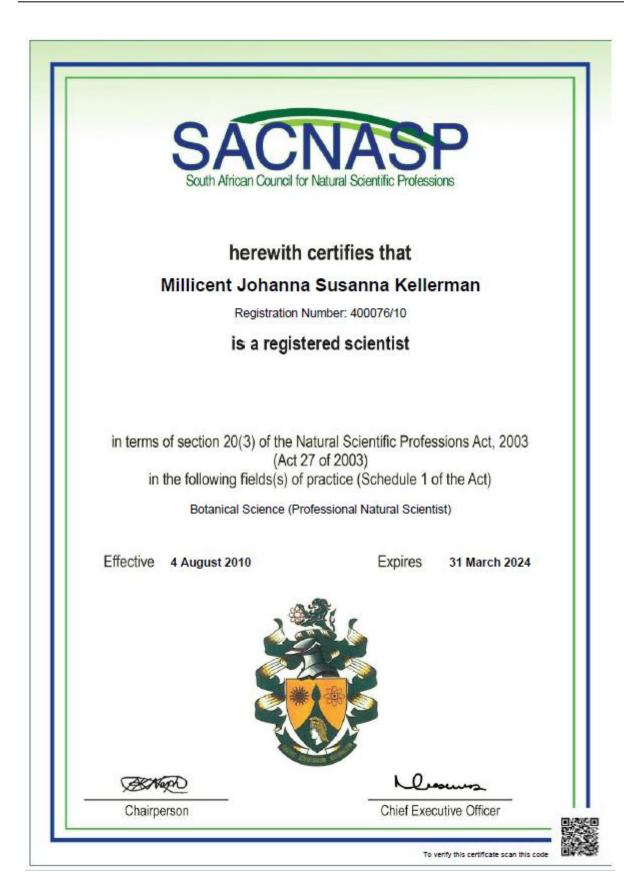
19.9 Review of the Scoping and EIA Reports

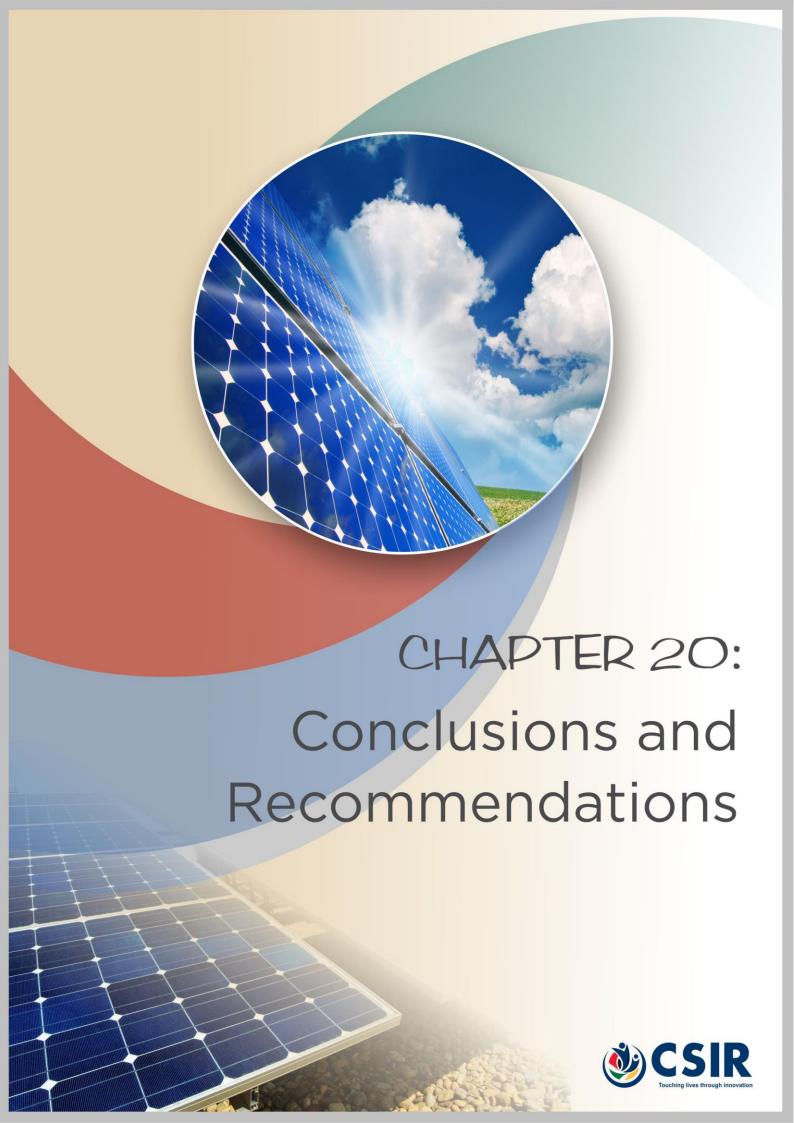
The Draft EIA Reports were made available to all registered Interested and/or Affected Parties (I&APs), Organs of State and other relevant key stakeholders for a 30-day comment period which extended from 2 June to 3 July 2023, excluding public holidays, whereas the DSRs were made available to all registered I&APs Organs of State and other relevant key stakeholders for a 30-day comment period which extended from 09 December 2022 to 30 January 2023, excluding public holidays and the regulated shutdown period.

The Department of Defence (DoD) is included as a key stakeholder on the project stakeholder database and was afforded the opportunity to comment on the DSRs and Draft EIA Reports, including this Site Sensitivity Verification Report for the Defence (Solar) Theme applicable to the proposed project. Note that no comments were received from the SANDF or the DoD on the DSRs or Draft EIA Reports, apart from a request for a KMZ file of the proposed project. Refer to Appendix H.6 of this EIA Report for a copy of this email request.

19.10 Concluding Statement

The proposed project study area was determined and verified to be of low sensitivity (as it relates to defence installations). This was determined through a site visit and based on existing databases, and confirms the sensitivity allocated on the Screening Tool. Based on the above, in terms of GN R320, no further requirements are applicable i.e. a Compliance Statement is not required.







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20. CONCLUSIONS AND RECOMMENDATIONS

This chapter contains the main conclusions and recommendations from the Environmental Impact Assessment (EIA) Process, provides the key findings of the specialist assessments (i.e., outlines the most significant impacts identified, together with the key mitigation and management actions required to avoid or mitigate the negative impacts or enhance positive benefits), and an integrated summary of factors that will inform decision-making by the Competent Authority (i.e., the Department of Forestry, Fisheries and the Environment (DFFE)). In addition, the chapter also includes the recommendation of the Environmental Assessment Practitioner (EAP) on the environmental suitability of the project and whether the project should receive Environmental Authorisation (EA).

This EIA Report has investigated and assessed the significance of potential positive and negative direct, indirect and cumulative impacts associated with the proposed Kudu Solar Facility 2 project (hereafter referred to as the "proposed project" or "Kudu Solar Facility"). Detailed assessments of the potential impacts identified and assessed by the specialists during the EIA Phase are included in Chapter 6 to 17 of this EIA Report. Following the exclusion of all "no-go" areas as shown in Figure 20.2, no negative residual impacts have been identified within this EIA that, in the opinion of the EAP who has conducted this Scoping and EIA Process, should be considered "fatal flaws" from an environmental perspective, and thereby necessitate substantial redesign or termination of the project.

This chapter constitutes an **Environmental Impact Statement**, as required in terms of Appendix 3 of the 2014 NEMA EIA Regulations (as amended), which includes the following:

- a map at an appropriate scale which superimposes the proposed activity and its associated structures and infrastructure on the environmental sensitivities of the preferred development footprint on the approved site as contemplated in the accepted Scoping Report indicating any areas that should be avoided, including buffers (Section 20.1);
- a summary of the identified project alternatives (Sections 20.2);
- a summary of the key findings of the environmental impact assessment (Section 20.4 and Section 20.5); and
- a summary of the positive and negative impacts and risks of the proposed activity and identified alternatives (Section 20.4 and Section 20.5).

20.1 Environmental Sensitivity Mapping and Development Footprint for Approval

During the Scoping Phase, detailed specialist assessments were conducted for the 8150 ha study area, including further desktop analysis and field surveys, where relevant. The farm portions forming part of the study area are listed in the previous chapters of this EIA Report. The assessment of the study area led to the identification of environmental features, which were assigned relevant sensitivities by the specialists, as described in Table 20.1 below. The sensitivities identified were taken into consideration and the Revised Scoping Buildable Areas were formulated, which avoid all no-go areas. During the EIA Phase, the development footprint and layout plan were developed based on the acceptable buildable areas.

Table 20-1: Key Environmental Features and Sensitivities identified by the Specialists

Specialist Assessment / Technical Study	Environmental Features and Sensitivities Identified
Chapter 6: Agriculture Compliance Statement	 The Site Sensitivity Verification (SSV) verified that the entire study area is of less than high agricultural sensitivity with a land capability value of 5 to 6. There are no areas that need to be avoided from an agricultural perspective. The layout has no relevance to agricultural impact in this case. Project specific description: The development footprint for the
	PV Facility is predominantly low sensitivity with minor portions encroaching on medium sensitivity.
	 High Sensitivity: The Koppies habitat is considered highly sensitive which must be avoided. No buffers are allocated. Note that this is applicable to Kudu Solar Facility 6, but it is important to mention from a contextual perspective for the study area. Linear infrastructure such as roads and overhead powerlines should not cross the Koppies, and pylons should not be constructed in this habitat. Linear infrastructure such as roads and overhead powerlines can cross the Watercourse, but it is advised to construct pylons outside the buffer areas.
Chapter 7: Terrestrial Biodiversity, Terrestrial Plant Species, and Terrestrial Animal Species Assessment	 Medium Sensitivity: The White and Shrubby Grasslands are considered of medium sensitivity owing to its pristine nature with limited major impacts. The Watercourse sensitivity is medium as per the findings of the Aquatic Specialist. Refer to the feedback below.
	Very Low Sensitivity: Existing transformed areas.
	Project specific description: The development footprint for the PV Facility is entirely medium sensitivity due to Shrubby Grassland. The medium and low sensitivity watercourse features are avoided and do not intersect with the layout for the development footprint of the PV Facility. Existing access roads leading to the site traverse the medium sensitivity watercourse features, however this is acceptable as explained above and below.
Chapter 8: Aquatic Biodiversity	 The recommended buffer area between the aquatic features and the project components to ensure these aquatic ecosystems are not impacted by the proposed activities is as follows: The larger tributary: The delineated edge of the surrounding floodplain wetland features (medium sensitivity). No buffer area is deemed to be required. Smaller streams and drainage features that are indicated to be of medium sensitivity: At least 35 m for

Specialist Assessment / Technical Study	Environmental Features and Sensitivities Identified
	the watercourse or the delineated edge of wetland features. The Battery Energy Storage System (BESS) should be preferably not be placed within 100 m of major rivers, watercourses and wetlands. Pans: One pan was found within the study area on Remaining Extent of the farm Wolve Kuilen No. 42. A 50 m buffer around this pan has been recommended. It does not intersect with the development footprint. Features that have been allocated a low sensitivity (smaller feeder streams, dams and minor drainage features) do not need to be avoided by the proposed development. Some access roads do cross water courses, which would be acceptable provided the recommended mitigation is implemented. For road crossings, the sensitivities are not regarded as no-go. Project specific description: The development footprint for the PV Facility is entirely low sensitivity. The nearby medium sensitivity
	watercourse features are avoided and do not intersect with the layout for the development footprint of the PV Facility. Existing access roads leading to the site traverse the medium sensitivity watercourse features, however this is acceptable as explained above. • All infrastructure exclusion zones: Verreaux's Eagle nest: A
Chapter 9: Avifauna Assessment	 All Immastructure exclusion zone is recommended to prevent the displacement of the breeding pair during the construction phase due to disturbance. Solar panel exclusion zones (other infrastructure allowed): Water points (e.g. water troughs, dams, boreholes): Surface water in this semi-arid habitat is important for priority avifauna and many non-priority species. The surrounding area contains several boreholes which are sources of surface water. It is preferable to leave some open space where possible with no solar panels, for birds to access and leave the surface water area unhindered. Some water points have been buffered by a minimum of 50 m, and some may be removed. High sensitivity areas: The entire Study Area is a high sensitivity zone due to the potential presence of several SCC including Ludwig's Bustard, Secretarybird, Martial Eagle, Cape Vulture and White-backed Vulture which could utilise the whole Study Area for foraging. However, these species do not require specific avoidance because there is still adequate habitat available outside the Study Area. Therefore, the high sensitivity is not a no-go and does not need to be avoided. Project specific description: The entire development footprint is High Sensitivity (not a no-go and does not need to be avoided, as described above). The development footprint does not overlap

Specialist Assessment / Technical Study	Environmental Features and Sensitivities Identified
Chapter 10: Visual Impact Assessment	with any waterpoint solar panel exclusion zones; however it is located adjacent to two of these features. Existing access roads leading to the site traverse the waterpoint solar panel exclusion zones, however this is acceptable as the exclusion only applies to solar panels (other infrastructure is allowed). Verreaux's Eagle nest is more than 2 km away from the development footprint. The following features are assigned Very High sensitivity (i.e. no-go) and need to be avoided for the proposed solar PV Facility itself (i.e. not for associated infrastructure such as substations, BESS, internal power lines and access roads; which would have minor buffers): Scenic Resources: Topographic features: Feature. Steep slopes: Slopes > 1:4. Drainage courses: Feature. Cultural landscapes within 250 m. Protected Landscapes / Sensitive Receptors: Nature reserves / game farms within 500 m. Farmsteads outside study area within 500 m. Farmsteads inside study area within 250 m. Arterial routes within 250 m (not applicable). District roads within 50 m. Note that the area of high sensitivity to the southern end of the development footprint / buildable area is due to a 50 m buffer from a drainage course as per the Visual Impact Assessment, however this is not a no-go area, as confirmed by the specialist and explained in the
	study, and the layout as currently proposed succeeds in avoiding visually sensitive areas. Note that all aquatic no-go areas have also been considered in the layout planning (discussed above). • Project specific description: The proposed solar PV borders on a drainage feature and local farm road but it is outside the no-go buffer areas. The nearest surrounding farmstead, Vrede, is 3,03 km away, and well outside the buffer area. The development footprint is low sensitivity from a visual perspective.
Chapter 11: Heritage Impact Assessment (Archaeology and Cultural Landscape)	Most resources located within the study area are cultural landscape components and are of low cultural significance and hence sensitivity. The site visit confirmed that the study area is of low sensitivity but with several pockets of higher sensitivity being present in the surrounding landscape (where archaeological and other heritage resources were found). Some of these areas outside of the project development footprint are considered to be archaeologically sensitive (i.e. of high sensitivity), but those sites marked as low cultural significance can be seen as medium sensitivity. The remaining land in between is of low sensitivity. A minimum 50 m buffer has been placed around relevant features.

Specialist Assessment /	Environmental Features and Sensitivities Identified	
Technical Study	■ There are no significant concerns for the proposed project. The facility layout has been designed to avoid all known culturally significant heritage resources with the exception of the cultural landscape which will not be significantly impacted. There are no areas requiring avoidance and no further protective buffers are needed.	
	 Project specific description: The development footprint is low sensitivity from a heritage perspective. There are no areas that need to be avoided from a palaeontology 	
Chapter 12: Palaeontology Site Sensitivity Verification Report	perspective. The site visit undertaken by the specialist found very low bedrock exposure and concluded that the site is of low to very low palaeo-sensitivity.	
	 Project specific description: The development footprint has a low desktop and field-based palaeo-sensitivity. No fossils were recorded within the footprint. 	
Chapter 13: Socio- Economic Assessment	 Not applicable. There are no sensitivities of this nature that can be mapped and that would influence the layout of the proposed project. 	
Chapter 14: Traffic Impact Assessment	 Project specific description: Not applicable. Not applicable. There are no sensitivities of this nature that can be mapped and that would influence the layout of the proposed project. 	
	Project specific description: Not applicable.	
Chapter 15: Battery Energy Storage System High Level Safety, Health and Environment Risk Assessment	 The BESS should be placed at least 50 m away from known boreholes and water points, and 100 m away from major surface water features, such as major rivers and wetlands. Due to the possibility of noxious smoke from potential fires, any lithium-ion BESS should be located over 500 m from residential areas, in this case isolated farm houses that are occupied. If this is not possible, it is noted that the risks are low and advice of mitigative measures should be provided to the farm occupants, e.g. shelter in place indoors. 	
	■ Project specific description: The BESS is located 50 m away from known water points and boreholes; 100 m away from major surface water features identified by the Aquatic Biodiversity Specialist; and more than 500 m away from the nearest farmstead.	
Chapter 16: Geohydrology Assessment	 It is recommended that all BESS are placed a minimum of 50 m from any borehole. Project specific description: The BESS is located 50 m away from known boreholes. 	

Specialist Assessment / Technical Study	Environmental Features and Sensitivities Identified	
Chapter 17: Geotechnical Assessment	There are no areas within the study area that should be avoided from a geotechnical sensitivity perspective. However, areas of moderate to steep topography would likely render development financially unfeasible.	
	 Project specific description: No areas identified for avoidance in the development footprint. 	
Chapter 18: Civil Aviation	 No sensitive civil aviation features have been identified within the study area. 	
	 Project specific description: The development footprint is low sensitivity from a civil aviation perspective. 	
Chapter 19: Defence	No sensitive defence features have been identified within the study area.	
	Project specific description: The development footprint is low sensitivity from a defence perspective.	

Based on the environmental sensitivities identified and verified by the specialists on site, an overall combined environmental feature map and environmental sensitivity map have been compiled for the study area. The comments received from the DFFE on the requirements for the sensitivity maps have been considered and incorporated as best as possible.

Figure 20.1 shows the identified and assessed environmental features present within the study area and allocated buffers; whereas Figure 20.2 shows the environmental sensitivity that has been allocated to these features. These maps indicate that the inherent environmental sensitivity of the proposed project study area is generally medium to low, with some very high and high sensitivity areas. The study area is suited for the development of the proposed project based on the understanding that measures have been taken to firstly avoid the sensitive features as best as possible, and all aspects to manage or mitigate potential impacts have been taken into consideration and detailed during the EIA Phase.

The buildable areas and development footprints are overlain onto these maps to show how they relate to the environmental features and sensitivities, and how the no-go areas have been avoided. Figure 20.3 shows a detailed layout map indicating the development footprint and buildable area; and Figure 20.4 indicates a combined layout and sensitivity map. Figure 20.5 is a combined cumulative impacts and environmental sensitivity map (based on the sensitivities identified by the specialists). Key maps are also included in Appendix C of this EIA Report.

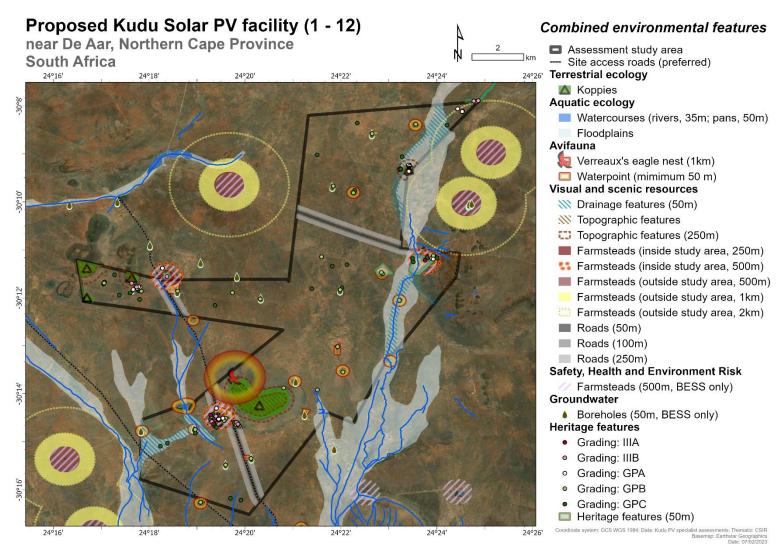


Figure 20-1: Combined environmental feature map for the proposed project study area based on specialist inputs.

Proposed Kudu Solar PV facility (1 - 12) near De Aar, Northern Cape Province

South Africa 24°16' 24°22' 24°18' 24°20' 24°24' Combined sensitivity Assessment Study Area (farm portions) Very high High Medium Potentially sensitive features (BESS only) 「」 No-go buffer (PV only) Coordinate system; GCS WGS 1984 Data: Kudu PV specialist assessi 24°18' 24°20' 24°22' Basemap: Earthstar Geographics Date: 11/05/2023

Figure 20-2: Combined environmental sensitivity map for the proposed project study area based on specialist inputs

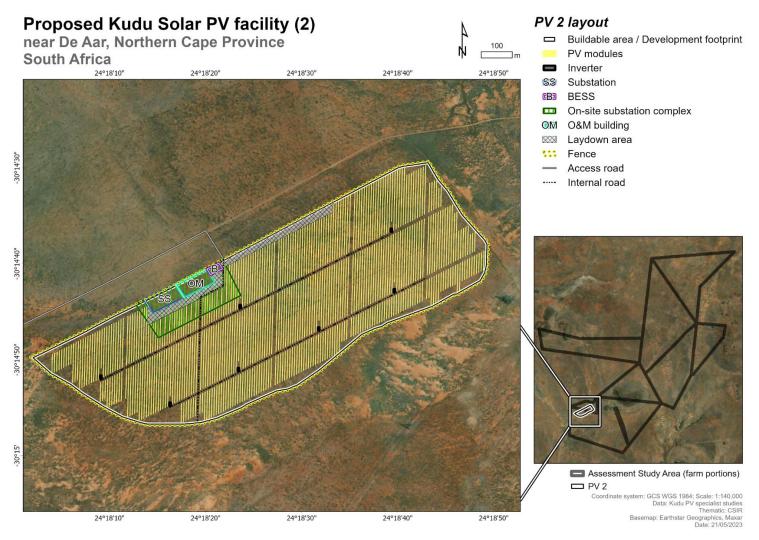


Figure 20-3: Project Layout Map showing the detailed infrastructure, buildable area and development footprints.

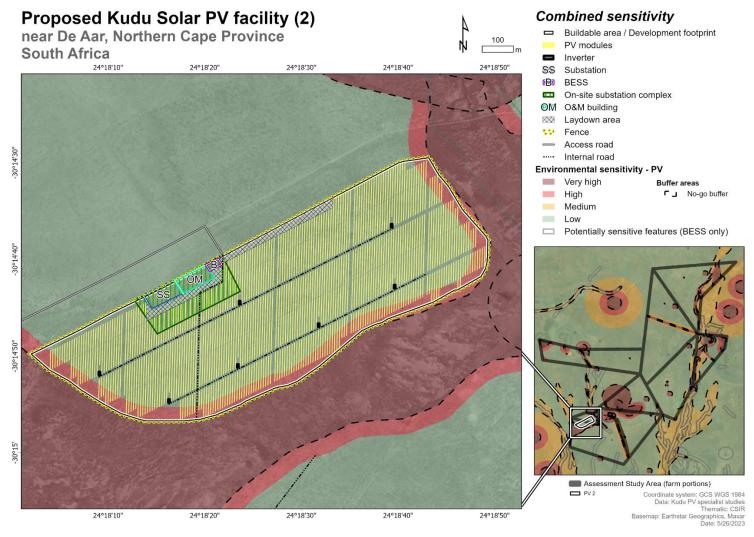


Figure 20-4: Combined Project Layout and Sensitivity Map.

Proposed Kudu Solar PV facility (1 - 12)

near De Aar, Northern Cape Province South Africa

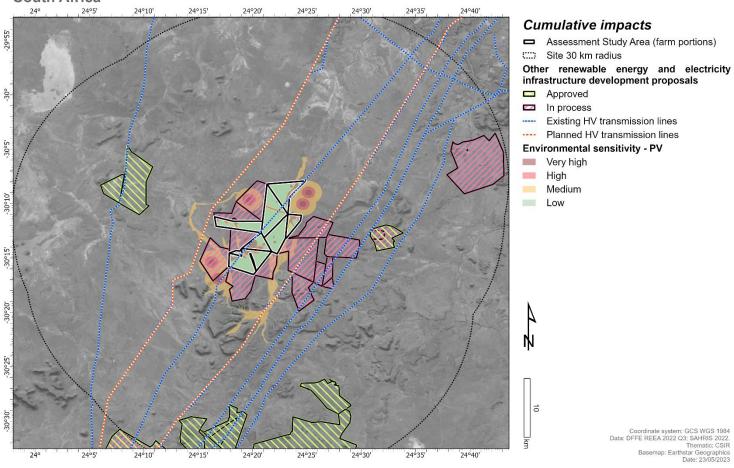


Figure 20-5: Combined Environmental Sensitivity and Cumulative Impact Map.

20.2 Summary of Project Alternatives

As discussed in Chapter 5 of this EIA Report, various alternatives have been considered and assessed as part of the EIA Phase.

Land-Use Alternative:

The current land-use is agriculture, specifically low density small stock grazing. There
is no cultivation in the area. The study area has low to medium agricultural sensitivity.
The Solar PV facility is regarded as the preferred land-use.

• Type of Activity Alternative:

This relates to the generation of electricity from a renewable energy source, and in this particular case, from solar resources. The generation of electricity from a renewable energy source was the only activity considered, and thus considered in this Scoping and EIA Process. No other activity types were considered or deemed appropriate based on the expertise of the Project Developer.

Renewable Energy Alternatives:

Given the above, the development of Solar PV is the preferred and only renewable energy technology to be developed on site because the site has a very good solar resource availability (i.e. GHI of 2 000 to 2 200 kWh/m² in terms of the long-term yearly total) and the local conditions are favourable.

• Preferred Site and Development Footprint within the site:

- The preferred site for all the proposed Kudu Solar Facilities comprises eight farm portions which cover a combined footprint of 8 150 ha, which serves as the study area for this Scoping and EIA Process. This is the approved site as per the accepted Final Scoping Report.
- This led to the identification of the buildable areas and development footprints within the preferred site that avoids no-go environmental sensitivities identified by the specialists. The combined layout and environmental sensitivity map is shown in Figure 20.4.
- The approach followed was to use environmental and social constraints to avoid sensitive features, thus applying mitigation hierarchy thinking. This approach replaces the need to rank alternative sites and locations, as it leads to the selection of the least sensitive development footprint.

No-Go Alternative:

The no-go alternative assumes that the proposed project will not go ahead i.e. it is the option of not constructing the proposed Kudu Solar Facility. This alternative would result in no environmental impacts (positive and negative) on the preferred site or surrounding local area, as a result of the proposed project. The no-go alternative has been assessed by all relevant specialists during the EIA Phase. Table 20.2 is a summary of the findings of the no-go alternative consideration.

Table 20-2: Summary of the No-Go Alternative based on Specialist Assessments

Specialist Assessment	No-Go Alternative		
Chapter 6: Agriculture Compliance Statement	 The no-go alternative considers impacts that will occur to the agricultural environment in the absence of the proposed development. There are no agricultural impacts of the no-go alternative. The development offers an alternative income source to agriculture, but it excludes agriculture from a proportion of the land. Therefore, even though the excluded land has no crop production potential, the negative agricultural impact of the development is more significant than that of the no-go alternative, and so, purely from an agricultural impact perspective, the no-go alternative is the preferred alternative between the development and the no-go. However, the no-go option would prevent the proposed development from contributing to the environmental, social and economic benefits associated with the development of renewable energy in South Africa. 		
Chapter 7: Terrestrial Biodiversity, Terrestrial Plant Species, and Terrestrial Animal Species Assessment	 The no-go alternative means the project does not get developed and no transformation or disturbance of topsoil and vegetation takes place, and no removal of provincially protected species are required. The baseline conditions signify the two grasslands, the Northern Upper Karoo and the Eastern Upper Karoo, remain as is with all current impacts still present, including livestock pens, waterpoints, windpumps, alien invasive species, fences and existing overhead powerlines. Furthermore, impacts on ecosystem functions including biodiversity protection, water regulation, quantity and quality, protection of medicinal plants, and climate refugia habitats will not be impacted on, and will continue as normal. Should the development not proceed, the landowners will continue to utilise the grassland (baseline - dominant land use) for grazing purposes and creates an opportunity for the land to be used for other means, should the landowner, for example, wish to do other developments on site. Any development considered for this site, should result in a net benefit to society and should avoid undesirable negative impacts. It must be noted however, that not approving this project does not exclude other renewable energy projects from being developed in this area. Accordingly, since this area is not considered an exclusion zone for development, multiple applications for renewable energy has and is being submitted to the competent authority for approval. Therefore, the no-go alternative cannot be looked in isolation and must take into account the regional land use and other developments to determine the 'sense of place' and whether this development will significantly impact on the 		
Chapter 8: Aquatic Biodiversity	 baseline conditions in a regional context. The watercourses and associated wetlands and floodplains are in a largely natural to moderate condition due to the low level of impact in the area. The no-go option will thus result in no additional impacts on aquatic biodiversity and will result in the ecological status quo being maintained, which will be to the advantage of aquatic systems and biodiversity. However, with that being said, no fatal flaws were discovered in the course of the investigations for the proposed Kudu Solar Facility. The potential aquatic ecosystem impact significance for the proposed activities, with mitigation, is rated as very low. 		
Chapter 9: Avifauna Assessment	The no-go option will result in no additional impacts on avifauna and will result in the ecological status quo being maintained, which will be to the advantage of the avifauna. However, with that being said, no fatal flaws were discovered in the course of the investigations for the proposed Kudu Solar Facilities, and with mitigation the potential impact significance is rated as mainly low.		
Chapter 10: Visual Impact Assessment	The 'no-go' alternative is the option of not constructing the project in which case the status quo of the current landscape character would prevail, the disadvantage being that no solar energy would be produced for export to the national grid. The potential visual impact would be neutral where the status quo is maintained, with neither impacts or benefits occurring.		

Specialist Assessment	No-Go Alternative	
Chapter 11: Heritage Impact Assessment (Archaeology and Cultural Landscape)	 If the project were not implemented, then the site would stay as it currently (impact significance of negligible for archaeology and graves and very low negative for the landscape). Although the heritage impacts with implementation would be greater than the existing impacts, the loss of socio-economic benefits is more significant an suggests that the No-Go option is less desirable in heritage terms. 	
Chapter 12: Palaeontology Site	Not applicable as the study did not require an impact assessment due to the	
Sensitivity Verification Report Chapter 13: Socio-Economic Assessment	low to very low palaeo-sensitivity. The no development option would represent a lost opportunity for South Africa to improve energy security and supplement its current energy needs with clean, renewable energy. Given South Africa's current energy security challenges and its position as one of the highest per capita producers of carbon emissions in the world, this would represent a significant negative social cost. The no development option is not supported by the findings of the Socio-Economic	
Chapter 14: Traffic Impact Assessment	Assessment. The no-go option will result in no additional impacts on traffic and will result in the road and traffic status quo being maintained. However, with that being said, no fatal flaws were discovered in the course of the investigations for the proposed project, and with mitigation the potential impact significance is rated as mainly low to very low.	
Chapter 15: Battery Energy Storage System High Level Safety, Health and Environment Risk Assessment	 No-go alternative is not required to be assessed based on technical nature of the study. 	
Chapter 16: Geohydrology Assessment The farm portions where the project is proposed does not cu significant volumes of groundwater and small-scale ab predominantly for domestic purposes. As such the No-go alternate represent a risk to groundwater or aquifer depletion. However, the water demand in the study area and a large spatial extent; and relating to the use of ground water are not considered to be verification.		
Chapter 17: Geotechnical Assessment	 In terms of the no-go alternative, if the proposed development does not go ahead, there will be no need for displacement and/or loss of topsoil in the area. However, to date, apart from the construction of farmhouses and the erection of boundary and subcamp fences for farming purposes; little disturbance of the subsoils and rocks in the area proposed for development has taken place. For this reason, the no-go alternative is considered of low significance. However, the potential impacts of the proposed project from a geotechnical perspective are not considered to be very significant, especially if the recommended mitigation measures are adopted. 	

- As outlined in Section 20.4 and Section 20.5 of this chapter, the majority of the negative impacts identified as part of this assessment can be reduced to moderate or low significance with the implementation of mitigation measures. None of specialists found that the proposed projects should not go ahead i.e. no fatal flaws were identified. As noted above, the Socio-Economic Impact Assessment identified positive impacts from a social upliftment perspective. These include benefits to the local community via employment opportunities and the development of locally-owned industries to support construction related activities.
- Therefore, while the "no-go" alternative will not result in any negative environmental impacts as a result of the proposed project; it will also not result in any positive community development or socio-economic benefits. It will not assist government in addressing climate change commitments and reaching its set targets for reduced carbon emissions. Furthermore, it will not assist in generating the additional electricity

that is urgently required to address the shortage of generation capacity in the country and the need for new solar PV generation capacity that is specified in the energy planning for the country. Hence the "no-go" alternative is not a preferred alternative, or a reasonable and feasible alternative considered in this Scoping and EIA Process.

Technology Alternatives

- Solid State Lithium Ion Battery Energy Storage System (BESS) and Redox Flow BESS technology types have been assessed and were considered by the specialists as part of the proposed project components.
- None of the specialists have identified any specific concerns relating to the BESS.
- As noted previously, a High-Level High Level Safety, Health and Environment Risk Assessment (Chapter 15 of the EIA Report) was specifically commissioned for the BESS and it provides significant detail and information of the BESS technology alternatives.
- Table 20.3 provides a summary of the specialist findings regarding the BESS technologies.

Table 20-3: Summary of the BESS Technology Alternatives based on Specialist Assessments

Specialist Assessment	Battery Energy Storage System (BESS) Technology Assessment		
Chapter 6:	■ Technology alternatives with respect to the BESS will make absolutely no		
Agriculture Compliance	material difference to the significance of the agricultural impacts.		
Statement	 All BESS technology alternatives are acceptable. 		
	 No BESS is located in a sensitive area, but it is located within the grassland. 		
	• For the Solid State Lithium Ion BESS, the necessary measures need to be put		
	in place to limit potential fires, including considering a fire break (i.e. A natural		
	or constructed barrier used to stop or check fires that may occur), if possible,		
	around each Kudu PV facility (this is a worst-case scenario).		
Chapter 7: Terrestrial	 However, as a containerised approach including the usual good practice of 		
Biodiversity, Terrestrial Plant	separation between containers which will be applied for this project, the impacts		
Species, and Terrestrial Animal	are likely restricted to events to one container at a time.		
Species Assessment	• For Redox Flow BESS, the most significant hazard is the possibility of spills of		
Species Assessment	corrosive and environmentally toxic electrolyte. Several preventative and		
	mitigative measures have been proposed in the EMPr and High-Level BESS		
	Safety, Health and Environment Risk Assessment.		
	 The type of BESS technology will have no influence on terrestrial biodiversity; 		
	therefore, both are considered viable options. There are no fatal flaws		
	associated with the proposed battery installation for either technology types.		
	 Both BESS technologies have been considered. 		
Chapter 8: Aquatic Biodiversity	■ The proposed BESS within the site is not of aquatic ecosystem concern, given		
Chapter of Aquatic Blourversity	that the aquatic ecosystems have been avoided and adequately buffered.		
	 Either BESS technology would thus be suitable. 		
	 Both BESS technologies have been considered in this assessment. 		
	■ The type of technology will have no influence on avifauna; therefore, both are		
Chapter 9: Avifauna Assessment	considered viable from an avifaunal perspective.		
	• The impacts of habitat transformation and disturbance associated with the		
	BESS are covered in the assessment.		
	■ The substation and BESS have been considered as an integral part of the solar		
Chapter 10: Visual Impact	facility and mitigations for these have been included in the Visual Impact		
Assessment	Assessment.		
	 Both BESS technologies are considered viable from a visual perspective. 		
Chapter 11: Heritage Impact	• Two different battery technologies are being considered, but this makes no		
Assessment (Archaeology and	difference to the heritage assessment and, being equally acceptable, they were		
Cultural Landscape)	not assessed separately in the Heritage Impact Assessment report.		

Specialist Assessment Battery Energy Storage System (BESS) Technology Assessm	
Chapter 12: Palaeontology Site Sensitivity Verification Report	Not applicable as the study did not require an impact assessment due to the low to very low palaeo-sensitivity. However, no concerns were raised for all project components. The BESS was considered as part of the project components.
Chapter 13: Socio-Economic Assessment	 The proposed BESS site is not located within significant proximity to any social receptors. The study area is very sparsely populated. No inhabited dwellings are located within 2 km of the site. The proposed site is therefore suitable from a social impact assessment point of view. Both proposed technology options (Redox flow and Lithium ion) are acceptable from a Social Assessment perspective.
Chapter 14: Traffic Impact Assessment	 Both BESS technologies have been considered in the Traffic Impact Assessment. This type of technology will have no significant influence on traffic; therefore, both are considered viable from a traffic perspective. The traffic impacts discussed in the Traffic Impact Assessment are also associated with the BESS.
Chapter 15: Battery Energy Storage System High Level Safety, Health and Environment Risk Assessment	 A detailed BESS High-Level Safety, Health and Environment Risk Assessment was undertaken as part of the EIA Process. Note that this assessment is a technical study and does not need to comply with the requirements of the 2014 NEMA EIA Regulations (as amended). From a safety and health point of view, the Risk Assessment shows that risks posed by Vanadium Redox Flow BESS may be slightly lower than those of Solid State Lithium Ion BESS, particularly with respect to fire and explosion risks. From an environmental spill and pollution point of view the Vanadium Redox Flow BESS present higher short-term risks than the SSL systems. However, the above conclusions may be due to the fact that the Vanadium Redox Flow BESS technology is not as mature as Solid State Lithium technology and therefore there is not as much operating experience and accident information available for the Redox Flow BESS. Overall, from a Safety, Health and Environment Risk Assessment point of view, there is no specific preference for a type of technology. The assessment confirmed that there are no fatal flaws associated with the proposed battery installation for either technology type.
Chapter 16: Geohydrology Assessment	 Both BESS technologies have been considered in the assessment. T he risks associated with each individual technology is such that, with strict adherence to the appropriate mitigation measures, both technologies will have little risk to the local hydrogeological system. Furthermore, no fatal flaws of either technology with respect to the geohydrological system have been identified. Considering this, both Lithium Ion BESS and Redox Flow BESS are considered suitable, and no preference is given to either one.
Chapter 17: Geotechnical Assessment	 Both Lithium Ion and Redox Flow BESS technologies have been assessed. It is important to note that the choice of technology will not be influenced by geotechnical factors, thus both options are considered suitable from a geotechnical standpoint.

Based on the above, and the High-Level Safety, Health and Environment (SHE) Risk Assessment which has provided significantly detailed inputs, Solid State Lithium Ion BESS has been selected as the preferred BESS technology.

It must be re-iterated that both BESS technologies were assessed during the EIA Phase and found to be acceptable. However, Solid State Lithium Ion is the preferred and if this changes post EA (should such authorisation be granted), the Project Applicant will apply for a separate amendment process with the Competent Authority.

20.3 Need and Desirability

This EIA considered the nature, scale and location of the proposed development as well as the wise use of land (i.e., is this the right time and place for the development of this proposed project). The proposed project is linked to the national planning vision for large-scale wind and solar development in South Africa. The development of solar energy is important for South Africa to reduce its overall environmental footprint from power generation (including externality costs), and thereby to steer the country on a pathway towards sustainability.

The development of renewable energy is strongly supported at a national, provincial, and local level. The Northern Cape region is attractive for renewable energy projects due to the significant solar energy resources. Several renewable energy projects have been approved within a 30 km radius of the proposed project side, with a few facilities already developed and in operation.

The Final Integrated Development Plan (IDP) (2022 – 2027) for the Pixley Ka Seme District Municipality (PKSDM) identifies solar energy as a development opportunity in the RLM. The 2019-2020 IDP notes that the economy in the PKSDM is characterized by high levels of poverty, and low levels of development despite the strategic location in terms of the national transport corridors. The IDP recognises renewable energy projects as potential sustainable economic development opportunities. The development of the proposed project will therefore also be in line with the vision of the PKSDM to diversify the job market by creating and supporting sustainable economic growth and development opportunities.

20.4 Specialist Impact Assessment

Based on the detailed specialist assessments, various potential impacts have been identified. A summary of the main impacts identified is provided in Table 20.4. Note that several mitigation measures have also been provided by the specialists, however only selected key measures are noted in the table below. The specialist assessments included in Chapters 6 to 17 of this EIA Report contain all the detail. The recommended mitigation measures have been included in the Environmental Management Programme (EMPr) in Appendix I and Appendix J of this EIA Report.

Table 20-4: Summary of Key Impacts that were identified and assessed during the EIA Phase as part of the Specialist Assessments, including key recommended mitigation measures

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
Chapter 6 – Agriculture Compliance Statement	Construction Phase: Loss of agricultural potential by occupation of land. Loss of agricultural potential by soil degradation. Soil can be degraded by impacts in three different ways: erosion; topsoil loss; and contamination. Loss of agricultural potential by dust generation. Decommissioning Phase: Loss of agricultural potential by soil degradation. Soil can be degraded by impacts in three different ways: erosion; topsoil loss; and contamination. Loss of agricultural potential by dust generation. Positive Indirect Impacts (mainly during operations): Increased financial security for farming operations. Improved security against stock theft and other crime due to the presence of	 Design Phase: Design an effective system of stormwater run-off control, where it is required - that is at any points where run-off water might accumulate. The system must effectively collect and safely disseminate any run-off water from all accumulation points and it must prevent any potential down slope erosion. This is included in the stormwater management plan. Construction and Decommissioning Phases: Implement an effective system of stormwater run-off control, where it is required (as specified above). Maintain where possible all vegetation cover and facilitate re-vegetation of denuded areas throughout the site, to stabilize disturbed soil against erosion. If an activity will mechanically disturb the soil below surface in any way, then any available topsoil should first be stripped from the entire surface to be disturbed and stockpiled for re-spreading during rehabilitation. During rehabilitation, the stockpiled topsoil must be evenly spread over the entire disturbed surface. Operational Phase:
	security infrastructure and security personnel at the energy facility.	 Maintain the stormwater run-off control system. Monitor erosion and remedy the stormwater control system in the event of any erosion occurring. Facilitate re-vegetation of denuded areas throughout the site.
Chapter 7: Terrestrial Biodiversity, Terrestrial Plant Species, and Terrestrial Animal Species Assessment	Negative Direct Impacts: Construction Phase: Habitat loss and fragmentation Loss of protected species Increased alien invasive species Increased erosion and soil compaction Littering and general pollution Operational Phase: Loss of species composition and diversity Increased alien invasive species Littering and general pollution	 Construction Phase: No development should take place within High sensitivity areas or buffer zones. Accordingly, the Koppies habitat (where relevant) should be avoided. The Watercourse habitats of medium sensitivity should be avoided, as recommended by the Aquatic specialist. No construction related activities, such as the site camp, storage of materials, temporary roads or ablution facilities may be located in the high sensitivity areas. Where the approved layout designs impact on individuals, permit applications are required for either the relocation or destruction of provincially protected species (Northern Cape Nature Conservation Act No.9 of 2009) and for protected trees in terms of the National Forests Act No. 84 of 1998. Alien invasive species establishment and spreading should be monitored on an ongoing basis to ensure that the disturbed areas do not become infested with such plants.

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
	Decommissioning Phase: Loss of habitat Increased alien invasive species Cumulative Impacts – Construction Phase and Negative: Loss of habitat and vegetation	 Utilise existing access routes as far as possible. Confine the movement of vehicles to the access routes to and from the site and to the construction areas. Rehabilitate new vehicle tracks and areas where the soil has been compacted as soon as possible. Monitor the entire site for signs of erosion. General good housekeeping in terms of spills, refuelling and waste management. These
	Loss of Habitat and Vegetation	have been included in the Environmental Management Programme. Operational Phase: The loss of species composition and diversity cannot be mitigated due to a permanent structure which will change microclimatic conditions for the life of the facility operation. Implement appropriate rehabilitation measures to restore each habitat to a natural state that is representative of the respective vegetation type after construction. Follow an alien and invasive species control and monitoring plan. General good housekeeping in terms of spills, refuelling and waste management. These have been included in the Environmental Management Programme. Decommissioning Phase: The loss of vegetation is unavoidable within the approved layout development footprint, but sensitive areas must be avoided. Rehabilitation and alien invasive management as per the construction and operational
Chapter 8: Aquatic Biodiversity	Negative Direct Impacts: Disturbance of aquatic habitat and impact on aquatic biota; Removal of indigenous aquatic vegetation and associated loss of aquatic ecological integrity and functionality; Water supply for construction and stress on available water resources; Road crossing structures may impede flow in the aquatic features; Alien vegetation infestation within the aquatic features due to disturbance; and Increased sedimentation and contamination of surface water runoff may result from construction activities. Operational Phase: Ongoing disturbance of aquatic features and associated vegetation along access roads or adjacent to the infrastructure that needs to be maintained;	Construction Phase: Ensure the final layout of the PV facility and associated infrastructure avoids watercourses and recommended buffers as far as possible; utilisation should be made of existing disturbed areas where possible. The medium sensitivity aquatic habitats should be avoided in the layout design, with only low-sensitivity habitats being disturbed during construction. Note that this has been achieved in the EIA Phase, whereby the recommended development setbacks (i.e. recommended buffer of at least 35 m for the smaller drainage features; and setback from the wider floodplain adjacent to the larger rivers) have been adopted in the identification of the development footprints. The recommended avoidance areas have been avoided. Clearing of indigenous vegetation should not take place within the aquatic features and the recommended buffers. Rehabilitate disturbed aquatic habitats by revegetating them with suitable local indigenous vegetation.

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
	Modified runoff characteristics from hardened surfaces has the potential to result in erosion of adjacent watercourses; and Water supply and water quality impacts (e.g. contamination from sewage) as a result of the operation of the proposed Solar Facility and associated infrastructure. Decommissioning Phase: Increased disturbance of aquatic habitat due to the increased activity; and Increased sedimentation and contamination of surface water runoff. Negative Cumulative Impacts: Construction and Decommissioning Phases: Increased disturbance of aquatic habitat due to the increased activity in the wider area. Operational Phases: Degradation of ecological condition of aquatic ecosystems	 Water use for construction should be minimised as much as possible. The water should be obtained from an existing water allocation or other viable water sources for construction purposes. The road crossing structures should be designed to not impede flow in watercourses - low water crossing is preferred. Use existing crossings, as best as possible and where allowable. The existing road infrastructure, particularly within the floodplain, should be utilised as far as possible to access new infrastructure to minimise the overall disturbance. It is recommended that any new linear type of infrastructure crossings over watercourses be placed where there are existing structures or road crossings within the watercourse corridors, where possible. Undertake monitoring for the growth of alien vegetation. Operational Phase: Implement avoidance setbacks as recommended above the for the construction phase. Develop a stormwater management plan for the proposed development that addresses the stormwater run-off infrastructure must be designed to mitigate both the flow and water quality impacts of any stormwater leaving the developed areas. The runoff should rather be dissipated over a broad area covered by natural vegetation or managed using appropriate shaping of the road with berms or channels and swales adjacent to hardened surfaces where necessary. Should any erosion features develop, they should be stabilised immediately. Sewage generated within the site should be discharged to a conservancy tank that is properly serviced and regularly evacuated to nearby wastewater treatment works. Decommissioning Phase: Minimise works within aquatic ecosystems. If the project layout avoided these areas, the decommissioning works would also be able to avoid aquatic habitats as delineated. Note that all aquatic areas recommended for avoidanc

Specialist		
Assessment	Key Impacts Identified	Recommended Mitigation Measures
undertaken		
Assessment	Negative Direct Impacts: Construction Phase: Displacement due to disturbance associated with the construction of the solar PV plant and associated infrastructure. Operational Phase: Displacement due to habitat transformation associated with the presence of the solar PV plant and associated infrastructure. Collisions with the solar panels. Entrapment in perimeter fences. Electrocutions in the onsite substation complex. Electrocution of priority species on the internal 33kV powerlines. Decommissioning Phase: Displacement due to disturbance associated with the decommissioning of the solar PV plant and associated infrastructure. Negative Cumulative Impacts: Construction and Decommissioning Phases: Displacement due to disturbance associated with the construction and decommissioning of the solar PV plants and associated infrastructure. Operational Phase: Displacement due to habitat transformation associated with the presence of the solar PV plants and associated infrastructure. Collisions with the solar panels. Entrapment in perimeter fences. Electrocutions in the onsite substation complexes. Electrocutions of priority species on the internal 33kV powerlines.	Construction Phase: Activity should as far as possible be restricted to the footprint of the infrastructure. Measures to control noise and dust should be applied according to best practice in the industry at the time. Maximum use should be made of existing access roads and the construction of new roads should be kept to a minimum as far as practical. Access to the rest of the property must be restricted. The recommendations of the ecological and botanical specialist studies must be strictly implemented, especially as far as limitation of the construction footprint is concerned. A 1km all infrastructure exclusion zone around the Verreaux's Eagle nest at -30.227660° 24.329773° must be implemented to provide unhindered access to the nest. The development footprint assessed in this report does not infringe on this buffer. Operational Phase: The recommendations of the botanical specialist must be strictly implemented, especially as far as limiting the vegetation clearance to what is absolutely necessary, and rehabilitation of transformed areas are concerned. Where possible, surface water (pans, dams and water troughs) must be buffered by a minimum of 50m to ensure unhindered access of priority species to the water. No PV panels should be constructed in this zone. Note that some of the waterpoints in the development footprint will be removed, however, since the minimum circular solar panel exclusion zone of 50m will be applied, the removal of some of the waterpoints will therefore not be a significant impact. A single perimeter fence should be used. The hardware within the proposed substation yard is too complex to warrant any mitigation for electrocution at this stage. It is recommended that if on-going impacts are recorded once operational, site-specific mitigation (insulation) be applied reactively. This is an acceptable approach because Red List priority species are unlikely to frequent the substation and be electrocuted. Use underground cabling as far as possible. Where the use overhead lines are unavoidable d
		Decommissioning Phase: Activity should as far as possible be restricted to the footprint of the infrastructure. Measures to control noise and dust should be applied according to best practice in the industry at the time.

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
		 Maximum use should be made of existing access roads during the decommissioning phase and the construction of new roads should be kept to a minimum as far as practical. The recommendations of the ecological and botanical specialist studies must be strictly implemented, especially as far as limitation of the activity footprint is concerned.
Chapter 10: Visual Impact Assessment	Negative Direct Impacts: Construction Phase: Potential effect of dust and noise from trucks and construction machinery during the construction period, and the effect of this on nearby farmsteads and visitors to the area. Potential visual effect of haul roads, access roads, stockpiles and construction camps in the visually exposed landscape. Operational Phase: Potential visual intrusion of solar arrays and related infrastructure on receptors including glint and glare. Potential visual impact of an industrial type activity on the pastoral / rural character and sense of place of the area. Decommissioning Phase: Potential visual effect of any remaining structures, platforms and disused roads on the landscape. Negative Cumulative Impacts: Construction, Operational and Decommissioning Phases: Potential combined visual effect of the proposed 12 solar PV facilities in the study area, seen together with other existing and proposed renewable energy facilities in the area, and could potentially increase the overall cumulative visual impact.	 Construction Phase: Locate construction camps, batching plants and stockpiles in visually unobtrusive areas, away from public roads. Implement EMPr with ECO during construction. Operational Phase: Substation and BESS to be located in an unobtrusive low-lying area, away from public roads. Muted natural colours and non-reflective finishes to be used for structures generally. Internal access roads to be as narrow as possible, and existing roads or tracks used as far as possible. Outdoor/ security lighting to be fitted with reflectors to obscure the light source, and to minimise light spillage. Internal powerlines (i.e. 22 kV or 33 kV) to be located underground where possible. (In some cases, such as stream crossings, internal powerlines may need to be above ground). Outdoor signage to be discrete and commercial / billboard signage avoided. Decommissioning Phase: Solar arrays and infra-structure to be removed and recycled. Access roads no longer required to be ripped and regraded. Exposed or disturbed areas to be revegetated to blend with the surroundings.
Chapter 11: Heritage Impact Assessment (Archaeology and Cultural Landscape)	Negative Direct Impacts: Construction Phase: Potential impacts to archaeology; Potential impacts to graves; and Potential impacts to the cultural landscape.	Construction Phase: Report any chance finds of dense clusters of artefacts to SAHRA and/or an archaeologist. Protect in situ and appoint archaeologist to sample as needed. Report any chance finds of graves to SAHRA and/or an archaeologist. Protect in situ and appoint archaeologist to exhume. Minimise the duration of construction period.

Specialist		
Assessment	Key Impacts Identified	Recommended Mitigation Measures
undertaken		
	Operational Phase:	Ensure effective rehabilitation, at the end of the construction period, of areas not needed
	Potential impacts to the cultural landscape.	during operation.
	Decommissioning Phase:	
	Potential impacts to the cultural landscape.	Operational Phase:
		Ensure that all maintenance vehicles and operational activities stay within designated
	Negative Cumulative Impacts:	areas.
		Paint buildings in earthy colours to reduce contrast.
	Construction, Operational and Decommissioning Phases:	Make use of motion detectors and downlighting to reduce night-time light pollution.
	Potential impacts to the cultural landscape.	Decembrical animar Disease
	Construction Phase:	Decommissioning Phase:
	Potential impacts to archaeology; and	 Minimise duration of decommissioning period Ensure effective rehabilitation of the entire site once the infrastructure has been removed.
	Potential impacts to archaeology, and Potential impacts to graves.	Libute effective reliabilitation of the entire site office the infrastructure has been removed.
	The study area has been confirmed as low to very low palaeo-sensitivity.	The Chance Fossil Finds Protocol has been incorporated into the project EMPrs
Chapter 12:	Provided that the Chance Fossil Finds Protocol is incorporated into the EMPrs	(Appendix I and Appendix J of this EIA Report).
Palaeontology	and fully implemented during the construction phase of the solar PV facility,	() pportain raile / pportain of this En respond
Site Sensitivity	there are no objections on palaeontological heritage grounds to authorisation of	
Verification	the proposed project. Pending the discovery of significant new fossil finds before	
Report	or during construction, no further specialist palaeontological studies, reporting,	
	monitoring or mitigation are recommended for the proposed project.	
	Direct Negative Impacts	Note that several mitigation and enhancement measures have been identified in the
		assessment. The list below is only a summary of some of the recommendations.
	Construction Phase:	
	Impacts associated with the presence of construction workers on local	Positive Impacts – Enhancement Measures:
	communities.	
	Impacts related to the potential influx of job seekers.	Construction Phase:
Chantar 43.	Increased risks to livestock and farming infrastructure associated with the	Where reasonable and practical, the proponent should appoint local contractors and
Chapter 13: Socio-Economic	construction related activities and presence of construction workers on the site. Increased risk of grass fires associated with construction related activities;	implement a 'locals first' policy, especially for semi and low-skilled job categories. However, due to the low skills levels in the area, the majority of skilled posts are likely to
Assessment	Nuisance impacts, such as noise, dust, and safety, associated with construction	be filled by people from outside the area.
Assessineill	related activities and vehicles.	Where feasible, efforts should be made to employ local contactors that are compliant with
	Impact on productive farmland.	Broad Based Black Economic Empowerment (BBBEE) criteria.
		Before the construction phase commences the proponent should meet with
	Operational Phase:	representatives from the Renosterberg Local Municipality (RLM) and the Emthanjeni
	 Visual impacts and associated impacts on sense of place. 	Local Municipality (ELM) to establish the existence of a skills database for the area. If such
	Potential impact on property values.	as database exists, it should be made available to the contractors appointed for the
	Potential impact on tourism.	construction phase.

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
undertaken	Decommissioning Phase: Social Impacts associated with retrenchment, including loss of jobs and source of income. Direct Positive Impacts Construction Phase: Creation of employment and business opportunities, and opportunity for skills development and on-site training. Operational Phase: Establishment of infrastructure to improve energy security and support renewable sector. Creation of employment opportunities. Benefits associated with socio-economic contributions to community development. Benefits for local landowners. Cumulative impacts: Negative: Cumulative impacts on sense of place Negative: Cumulative impact on local services and accommodation Positive: Cumulative impact on local economy.	 The local authorities, community representatives, and organisations on the interested and affected party database should be informed of the final decision regarding the project and the potential job opportunities for locals and the employment procedures that the proponent intends following for the construction phase of the project. Where feasible, training and skills development programmes for locals should be initiated prior to the initiation of the construction phase. The recruitment selection process should seek to promote gender equality and the employment of women wherever possible. The proponent and contractor should develop a Code of Conduct (CoC) for construction workers. The code should identify which types of behaviour and activities are not acceptable. Construction workers in breach of the code should be subject to appropriate disciplinary action and/or dismissed. All dismissals must comply with the South African labour legislation. The CoC should be signed by the proponent and the contractors before the contractors move onto site. The CoC should form part of the CHSSP. Operational Phase: Maximise the number of employment opportunities for local community members. Implement training and skills development programs for members from the local community. Maximise opportunities for local content and procurement. Implement agreements with affected landowners on which the PV facility will be constructed. Negative Impacts – Mitigation Measures: Construction Phase: Preparation and implementation of a Stakeholder Engagement Plan (SEP) prior to and during the construction phase. Preparation and implementation of a Community Health, Safety and Security Plan (CHSSP) prior to and during the construction phase. All f
		farming activities.

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
		 All areas disturbed by construction related activities, such as access roads on the site, construction platforms, workshop area etc., should be rehabilitated at the end of the construction phase. Operational Phase: The recommendations of the Visual Impact Assessment should be implemented. Decommissioning Phase: The proponent should ensure that retrenchment packages are provided for all staff retrenched when the plant is decommissioned. All structures and infrastructure associated with the proposed facility should be dismantled and transported off-site on decommissioning.
Chapter 14: Traffic Impact Assessment	Construction and Decommissioning Phases: Potential congestion and delays on the surrounding road network. Potential impact on traffic safety and increase in accidents with other vehicles or animals. Potential change in the quality of the surface condition of the roads. Potential noise and dust pollution. Operational Phase: The traffic generated during the operational phase are mainly related to the staff that will be transported to and from the sites and are not anticipated to have a significant traffic impact on the surrounding road network. Cumulative Negative Impacts Construction and Decommissioning Phases: Potential congestion and delays on the surrounding road network. Potential impact on traffic safety and increase in accidents with other vehicles or animals. Potential change in the quality of the surface condition of the roads. Potential noise and dust pollution.	 Construction and Decommissioning Phases: Stagger delivery trips and schedule trips, including staff trips outside of peak hours where possible. Implement speed control by means of a stop and go system and speed limit road signage within the construction and decommissioning site. Ensure all vehicles are roadworthy, visible, adequately marked, and operated by an appropriately licenced operator. Regular maintenance of internal farm access roads by the contractor. Ensure private access roads that are impacted on by the proposed development are restored to original pre-construction road condition. Implement dust control on gravel roads within the construction and decommissioning site.
Chapter 15: Battery Energy Storage System	Various risks were identified in terms of safety, health and the environment due to the proposed BESS. The BESS High Level Safety, Health and Environment Risk Assessment identified risks, hazards, and consequences, such as, but not limited to:	There are numerous different battery technologies but using one consistent battery technology system for the BESS installations associated with all the proposed Kudu Solar

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
High Level Safety, Health and Environment Risk Assessment	 Human Health - chronic exposure to toxic chemical or biological agents. Causes - Construction materials such as cement, paints, solvents, welding fumes, truck fumes etc. Consequences - Employee / contractor illness. Human Health - exposure to noise. Causes - Drilling, piling, generators, air compressors. Consequences - Adverse impact on hearing of workers. Possible nuisance factor in near-by areas. Human and Equipment Safety - exposure to fire radiation Causes - Involvement in an external fire. Fire involving fuels used in construction vehicles or vehicles themselves (e.g., tyre fire). Fire due to uncontrolled welding or other hot-work. Consequences - Injuries due to radiation especially amongst first responders and bystanders. Fatalities unlikely from the heat radiation as not highly flammable nor massive fire. Human and Equipment Safety - exposure to explosion over pressures. Transformer shorting / overheating / explosion. Consequences - Potential fatalities, e.g., amongst first responders. Damage to nearby equipment. 	Facilities would allow for ease of training, maintenance, emergency response and could significantly reduce risks. Where reasonably practicable, state-of-the-art battery technology should be used with all the necessary protective features e.g., draining of cells during shutdown and standby-mode, full Battery Management System (BMS) with deviation monitoring and trips, leak detection systems. Ensure that the technical and system suggestions for reducing risks, as specified in the assessment, specifically in terms of preventative and mitigative measures are included in the design. The overall design should be subject to a full Hazard and Operability Study (HAZOP) prior to finalisation of the design. For Redox Flow systems, an end of life (and for possible periodic purging requirements) solution for the large quantities of hazardous electrolyte should be investigated, e.g., can it be returned to the supplier for re-conditioning. Prior to importing any solid-state battery containers into the country, the contractor should ensure that: An Emergency Response Plan is in place that would be applicable for the full route from the ship to the site. This plan needs to include details of the most appropriate emergency response to fires both while the units are in transit and once they are installed and operating. An End-of-Life Plan is in place for the handling, repurposing or disposal of dysfunctional, severely damaged batteries, modules and containers. The site layout and spacing between lithium solid-state containers should be such that it mitigates the risk of a fire or explosion event spreading from one container to another. In order to limit the possibility of domino failures the BESS should be separated from the substation by at least 20 m. Where there is a choice of alternative locations for the BESS, those that are further from water courses would be preferred. Redox Flow BESS hazards are mostly related to possible loss of containment of electrolyte and solid-state systems may experience fires that may r

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
Chapter 16: Geohydrology Assessment	Direct Negative Impacts: Construction Phase: Potential lowering of the groundwater level from construction requirements; Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages. Operational Phase: Potential lowering of the groundwater level from operational requirements. Potential impact of groundwater quality as a result of using cleaning agents for cleaning the solar panels. Groundwater quality deterioration as a result of electrolyte that will be used for the BESS. Decommissioning Phase: Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages. Potential lowering of the groundwater level from decommissioning requirements. Cumulative Negative Impacts: Potential lowering of groundwater level during the construction, operational and decommissioning phase for all 12 of the Kudu PV facilities. Potential impact on groundwater quality as a result of accidental oil spillages or fuel leakages from the construction and the decommissioning phase for all 12 Kudu facilities. Potential of impact on groundwater quality as a result of using cleaning agents for cleaning the solar panels during the operational phase for all the 12 Kudu facilities. Potential impact on groundwater quality as a result of electrolyte that will be used for the BESS. Other wind and solar, and EGI projects within a 30 km radius.	Construction and Decommissioning Phases: Adhere to the borehole's safe yield and to monitor water levels and flow. Boreholes must be correctly yield tested according to the National Standard (SANS 10299-4:2003, Part 4 – Test pumping of water boreholes). This includes a Step Test, Constant Discharge Test and recovery monitoring. Vehicles must be regularly serviced and maintained to check and ensure there are no leakages. Diesel fuel storage tanks, if required, should be above ground on an impermeable surface in a bunded area. Vehicles and equipment should also be refuelled on an impermeable surface. A designated area should be established at the construction site camp for this purpose, if off-site refuelling is not possible. If spillages occur, they should be contained and removed as rapidly as possible, with correct disposal procedures of the spilled material, and reported. Operational Phase: Borehole's safe yield, monitoring and yield testing as per the construction phase. Use environmentally safe cleaning agents that breakdown naturally and do not cause adverse effects. Ensure that all electrolyte or chemicals stored or used on site have secondary containment systems in place with reliable leak detection, annunciation in place. Ensure that all chemicals are handled on concrete bunded surfaces and not on bare soil. Wastewater produced by fire hydrants should not be allowed to runoff into the environment. It is recommended that all BESS's are placed a minimum of 50m from any borehole.
Chapter 17: Geotechnical Assessment	Direct and Cumulative Negative Impacts: Construction Phase: Displacement of geologic materials.	Construction Phase: Favour dolerite as an aggregate (as opposed to Karoo sandstones and mudstones). Subject to investigation. Any road cuttings should be designed by an appropriately qualified professional. Drainage in the region should be designed and managed appropriately.

Specialist Assessment undertaken	Key Impacts Identified	Recommended Mitigation Measures
	 Contamination of geologic materials as a consequence of the construction activities. Operational and Decommissioning Phase: Increased unnatural hard surfaces. Contamination of geologic materials as a consequence of typical maintenance and decommissioning activities. 	 Investigate and confirm the geotechnical suitability of each structure (or other appropriate level of investigation) prior to construction (i.e., determine that soil with an adequate bearing capacity is obtained beneath each footing). Such investigations would not be required to fulfil the requirements of this EIA process. However, it would be necessary prior to construction. Only strip vegetation necessary for the next phase of construction. Install temporary drainage to divert stormwater away from active construction activities, where required. Where impacted through construction-related activities, all sloped areas must be stabilised to ensure proper rehabilitation is affected and erosion is controlled.
		Operational Phase:
		Decommissioning Phase: Land rehabilitation to near natural state, i.e., removal of foundations and backfilling of any resultant voids within the soil, as well as removal of hard surfaced areas. Replacement soil should be sourced locally to ensure homogeneity. Reinstate natural topography where cut-to-fill embankments have been constructed.

20.5 Summary of Key Impact Assessment Findings

Based on the findings of the detailed specialist impact assessments, which are included in Chapter 6 to 17 of this EIA Report, the proposed project is considered to have an <u>overall Moderate to Very Low negative environmental impact</u> and an <u>overall High to Moderate positive socio-economic impact</u> (with the implementation of respective mitigation and enhancement measures). Table 20.5 below provides a summary of the impact assessment for the proposed project post mitigation for direct impacts. Table 20.6 provides the same information for the cumulative impacts.

As indicated in Table 20.5, the direct negative impacts were rated with an overall **Low to Very Low** post-mitigation impact significance for the **construction phase**, with only Terrestrial Biodiversity impacts being rated as Moderate. In terms of the **operational and decommissioning phases**, the majority of the direct negative impacts were rated with a **Low to Very Low** post-mitigation impact significance. In terms of direct positive impacts, the Socio-Economic impacts are rated as having a **Moderate** impact significance post-mitigation for the construction phase; and **Moderate to High** impact significance post-mitigation for the operational phase.

Based on Table 20.6, the majority of the cumulative negative impacts were rated with a <u>Low</u> post-mitigation impact significance for the **construction phase**, with the exception of Terrestrial and Socio-Economic impacts, which were respectively rated with a Moderate and Moderate to Low post-mitigation impact significance. A similar trend is applicable to the **operational phase**, with Visual and Avifauna impacts being rated as **Moderate**; and Socio-Economic impacts being rated as <u>Moderate</u> to <u>Low</u>.

During the **decommissioning phase**, the majority of cumulative impacts were rated with a **Low to Very Low** post-mitigation impact significance, whereas some were not identified, or are considered insignificant, or could not be measured empirically at the time of assessment. In terms of cumulative positive impacts, the Socio-Economic impacts were rated with an overall **Moderate** post-mitigation impact significance.

Table 20-5: Overall Impact Significance with the Implementation of Mitigation Measures for Direct Negative and Positive Impacts

Specialist Assessment	Construction Phase		Operational Phase		Decommissioning Phase	
DIRECT NEGATIVE IMPACTS						
Agriculture and Soils	L	.ow	Low		Low	
Terrestrial Biodiversity, Terrestrial Plant Species, and Terrestrial Animal Species	Moderate		Low		Low	
Aquatic Biodiversity	Ver	y Low	Very Low		Very	Low
Avifauna	Low		Very Low	Low	Low	
Visual	Low		Low		Very Low	
Heritage (Archaeology and Cultural Landscape)	Low		Low		Low	
Palaeontology	Insignificant and/or not identified and/or not applicable		identified	nt and/or not and/or not icable	Insignifican identified appli	and/or not
Socio-Economic	Low		L	ow	Lo)W
Traffic	Low	Very Low	Insigr	nificant	Low	Very Low
Geohydrology	Low	Very Low	Low	Very Low	Very Low	
Geotechnical	Very Low		Very Low		Very Low	
DIRECT POSITIVE IMPACTS						
Socio-Economic	Moderate		Moderate	High	Insignificant and/or not identified and/or not applicable	

Table 20-6: Overall Impact Significance with the Implementation of Mitigation Measures for Cumulative Negative and Positive Impacts

Specialist Assessment	Construction Phase		Operational Phase		Decommissioning Phase	
CUMULATIVE NEGATIVE IMPACTS						
Agriculture and Soils	Lo	ow .	Low		Low	
Terrestrial Biodiversity, Terrestrial Plant Species, and Terrestrial Animal Species	Moderate		Low		Low	
Aquatic Biodiversity	Very	Low	Very Low		Very Low	
Avifauna	Low		Moderate		Low	
Visual	Low		Moderate		Very Low	
Heritage (Archaeology and Cultural Landscape)	Low		Low		Low	
Palaeontology	Insignificant and/or not identified and/or not applicable		Insignificant and/or not identified and/or not applicable		Insignificant and/or not identified and/or not applicable	
Socio-Economic	Low Moderate		Low	Moderate	identified	t and/or not and/or not cable
Traffic	Low		Insignificant		Low	Very Low
Geohydrology	Low	Very Low	Low	Very Low	Very Low	
Geotechnical	Low		Low		Low	
CUMULATIVE POSITIVE IMPACTS						
Socio-Economic	Moderate		Moderate		Moderate	

20.6 Overall Environmental Impact Statement and Reasoned Opinion from the EAP

The information presented above, contributes to this overall environmental impact statement and reasoned opinion from the EAP as to whether the proposed project should or should not be authorised, including any conditions that should be made in respect of the authorisation (should it be granted).

Based on the findings of the detailed specialist assessments and technical studies, which all recommend that the proposed project can proceed and should be authorised by the DFFE, the proposed project is considered to have an <u>overall Moderate to Very Low negative environmental impact</u>, and an <u>overall Moderate to High positive socio-economic impact</u> (with the implementation of respective mitigation and enhancement measures).

The proposed project will take place within the development footprint on the preferred and approved project site, as contemplated in the accepted Final Scoping Report. The development footprint and buildable areas will avoid the "no-go" sensitive features identified and mapped by the respective specialists, where relevant and applicable, as discussed in Section 20.1 of this chapter.

This EIA has considered the nature, scale and location of the development as well as the wise use of land. When considering the timing of this project, the IRP 2019 proposes to secure 17 800 MW of renewable energy capacity by 2030. As discussed in the preceding chapters of this EIA Report, it is the Project Applicant's intention to bid this project in the future bidding rounds of the REIPPPP.

The proposed project will be in line with and will be supportive of the objective of the PKSDM IDP in terms of creating more job opportunities. The proposed Solar PV Facility will assist in local job creation during the construction and operational phases of the project (if approved by the DFFE). It should be noted that employment during the construction phase will be temporary and provided for a period of 12 to 18 months.

Section 24 of the Constitutional Act states that "everyone has the right to an environment that is not harmful to their health or well-being and to have the environment protected, for the benefit of present and future generations, through reasonable legislative and other measures, that prevents pollution and ecological degradation; promotes conservation; and secures ecologically sustainable development and use of natural resources while promoting justifiable economic and social development". Based on this, this EIA was undertaken to ensure that these principles are met through the inclusion of appropriate management and mitigation measures, and monitoring requirements. These measures will be undertaken to promote conservation by avoiding the sensitive environmental features present on site and through appropriate monitoring and management plans (refer to the EMPr in Appendix I and Appendix J of this EIA Report).

The outcomes of this project therefore succeed in meeting the environmental management objectives of protecting the ecologically sensitive areas and supporting sustainable development and the use of natural resources, whilst promoting justifiable socio-economic development in the towns nearest to the project site. The findings of this EIA show that all natural resources will be used in a sustainable manner (i.e., this project is a renewable energy project, and the majority of the negative site specific and cumulative environmental impacts are considered to be of low significance with mitigation measures implemented), while the benefits from the project will promote justifiable economic and social development. Furthermore, additional specialist studies (not recommended by the Screening Tool) have been undertaken as part of the EIA Process to ensure that all potential environmental impacts are addressed and assessed. Refer to Table 20.7 for a summary of reasoned opinions from the specialists.

Table 20-7: Summary of the Reasoned Opinions from the Specialists

Specialist Assessment undertaken	Reasoned Opinion on whether the project should be authorised
Chapter 6: Agriculture Compliance Statement	 The conclusion of the assessment is that the proposed development offers a valuable opportunity for renewable energy development with very little loss of future agricultural production potential. Based on various factors, the impact of the proposed development on the agricultural production capability of the site is assessed as being acceptable. Therefore, from an agricultural impact point of view, it is recommended that the development be approved.
Chapter 7: Terrestrial Biodiversity, Terrestrial Plant Species, and Terrestrial Animal Species Assessment	 The proposed development is not located in a threatened vegetation type or ecosystem and is located in an ESA mainly due to presence of sensitive birds and watercourses. However, in the specialist's opinion, ESA cannot be regarded as Very High sensitivity as it is not irreplaceable areas, and depending on what ecological features it is based on, can be regarded as Medium or High sensitivity. There are no high sensitivity features on site, and no plant SCC were recorded. However, provincially protected species recorded will require permits for relocation from the provincial authority. The proposed project can proceed should all no-go sensitive areas be avoided (which has been achieved in the layout plan), and the recommended mitigation measures are implemented.
Chapter 8: Aquatic Biodiversity	 Based on the findings of the specialist assessment, there is no reason from a freshwater perspective, why the proposed activity (with the implementation of the recommended mentioned mitigation measures) should not be authorised. The proposed development footprint within the preferred development site (i.e. study area) has been amended through the EIA process to ensure that it will be within aquatic ecosystem areas of "low" sensitivity and are thus considered appropriate areas for development.
Chapter 9: Avifauna Assessment	 The proposed project will have a range of potential premitigation impacts on priority avifauna ranging from low to high significance, which is expected to be reduced to medium and low significance with the appropriate mitigation. No fatal flaws were discovered during the investigations. The proposed project is supported, and it is therefore recommended that the activity is authorised, with the understanding that all mitigation measures recommended in this report will be strictly implemented.
Chapter 10: Visual Impact Assessment	 The layout of the proposed facility has been subject to revisions, based on the various specialist findings, including the mapping of scenic resources and sensitive receptors. The currently proposed layout succeeds in avoiding visually sensitive areas as indicated on the visual sensitivity map in the Visual Impact Assessment. It is the opinion of the Visual Specialists that provided the recommended mitigation measures and EMPr are implemented, the proposed project would not present a potential fatal flaw in visual terms and may be authorised.

Specialist Assessment undertaken	Reasoned Opinion on whether the project should be authorised
Chapter 11: Heritage Impact Assessment (Archaeology and Cultural Landscape)	Given the lack of significant heritage resources in the proposed project footprint and generally limited impacts to the cultural landscape, it is the opinion of the heritage consultant that the project may be authorised in full using either battery technology.
Chapter 12: Palaeontology Site Sensitivity Verification Report	Provided that the Chance Fossil Finds Protocol is incorporated into the EMPrs and fully implemented during the construction phase of the solar PV facility, there are no objections on palaeontological heritage grounds to authorisation of the proposed renewable energy developments.
Chapter 13: Socio-Economic Assessment	The establishment of the proposed project and associated infrastructure is supported by the findings of the socio-economic assessment.
Chapter 14: Traffic Impact Assessment	 The proposed project will have a range of potential traffic related impacts ranging from very low to moderate significance before mitigation, which is expected to be reduced to very low to low significance with the appropriate mitigation. No fatal flaws were discovered during the investigations. The proposed project is supported, and it is therefore recommended that the activity is authorised, with the understanding that all mitigation measures recommended in this report will be strictly implemented.
Chapter 15: Battery Energy Storage System High Level Safety, Health and Environment Risk Assessment	The Risk Assessment found that with suitable preventative and mitigative measures in place, none of the identified potential risks are excessively high, i.e., from a Safety, Health and Environment (SHE) perspective no fatal flaws were found with either type of technology for the proposed BESS installation.
Chapter 16: Geohydrology Assessment	Based on various factors, such as the anticipated demands of the facility (individually) being less than the regional yield potential of the underlying aquifer, and the low to very low post-mitigation impact assessment, it is the opinion of the specialist that development of the proposed project may be authorised, provided that the mitigation measures are implemented during each phase of the project to suppress the intensity of identified impacts.
Chapter 17: Geotechnical Assessment	Based on the geotechnical analysis conducted, it is recommended that the proposed project be authorised, as no fatal flaws were found during the desktop assessment. However, it is crucial to implement appropriate mitigation measures at every phase of the project to minimise the intensity of the identified impacts.

Taking into consideration the findings of the Scoping and EIA Process and given the national and provincial strategic requirements for infrastructure development, particularly from an electricity generation perspective, and based on the fact that the environmental sensitivity of the study area is largely medium to low, with a few isolated high and very high sensitivity areas, it is the opinion of the EAP, that the project benefits outweigh the costs and that the project will make a positive contribution to sustainable infrastructure development in the RLM, as well as the towns of Petrusville and Phillipstown.

Provided that the specified mitigation measures and management actions are applied effectively throughout, it is <u>recommended that the proposed project receive EA</u> in terms of the 2014 NEMA EIA Regulations (as amended), promulgated under the NEMA.

It is understood that the information contained in this EIA Report and appendices is sufficient to make a decision in respect of the activity applied for.

It is recommended that the EA (should it be granted) be valid for a period of 10 years.

In addition, it is recommended that the EMPr compiled as part of this EIA Process, included in Appendix I and Appendix J of this EIA Report be approved concurrently in the EA (should it be granted). A detailed layout of the PV Facility has been identified at the EIA Phase. However, as confirmed by the specialists, changes to the detailed layouts are deemed acceptable if the changes remain within the approved buildable areas / development footprints and area assessed during the Scoping and EIA Process with no-go sensitive areas avoided. Any changes can be subjected to an EA amendment process, where warranted.

20.7 Cumulative Environmental Impact Statement

The cumulative impacts have been assessed by all the relevant specialists. The cumulative assessment included other renewable energy and grid connection projects within a 30 km radius of the proposed project.

No cumulative impacts have been identified that were considered to be fatal flaws. The specialists recommended that the project receive EA in terms of the 2014 NEMA EIA Regulations (as amended), including consideration of cumulative impacts, provided the mitigation is applied.

20.8 Conditions to be included in the EA

In order to ensure the effective implementation of the mitigation measures and management actions, EMPrs have been compiled and are included in Appendix I and Appendix J of this EIA Report. Appendix I includes the EMPr for the proposed Solar PV facility and associated infrastructure, and Appendix J includes the EMPr for the proposed Independent Power Producer (IPP) substation. The EMPr for the proposed IPP substation is a Generic EMPr and it is required to comply with the Generic EMPr published for substation development (Government Gazette 42323, GN 435, dated 22 March 2019).

The mitigation measures necessary to ensure that the proposed projects are planned and carried out in an environmentally responsible manner are listed in the EMPr. The EMPr includes the mitigation measures noted in this EIA Report, inclusive of the specialist assessments and technical studies. The EMPr is a dynamic document that should be updated as required and provides clear and implementable measures for the proposed project.

Listed below are the main recommendations applicable to the proposed project that should be considered for inclusion in the EA (should such authorisation be granted by the DFFE). These main recommendations as well as additional recommendations are included in the EMPr and EIA Report.

- Mitigation measures detailed within the EIA Report, specialist assessments and technical studies are to be implemented, where relevant and applicable.
- No-go areas of very high sensitivity identified by the specialists, and mapped accordingly, should be avoided.
- Vegetation clearing must be limited to the development footprint, as much as possible.
- A walk through of the approved site prior to construction activities must be undertaken in the relevant season to record all provincially protected species that will be impacted on by the development.
- Ensure the necessary permit applications are submitted with the provincial authority prior to construction for the relocation of provincially protected species. Copies of the permits must be kept on site by the Environmental Control Officer (ECO).
- Implement appropriate rehabilitation measures to restore each habitat to a natural state that is representative of the respective vegetation type after construction (for temporary use facilities in natural areas) and decommissioning.
- No alien and invasive plant species may be used for rehabilitation purposes; only indigenous species of the area / vegetation type may be used.
- Invasive alien plant growth and signs of erosion should be monitored on an ongoing basis to ensure that the disturbed areas do not become infested with invasive alien plants.
- The recommended buffer area between the aquatic features and the project components should be implemented.
- Visually permeable fences, preferably in a dark colour, should be used.
- Buildings are to be painted in earthy colours to reduce contrast.
- Night-time light spillage should be minimised, possibly through the use of motion detectors so that the area can stay dark until light is needed.
- If any archaeological material or human burials are uncovered during the course of development, then work in the immediate area should be halted. The find would need to be reported to the heritage authorities and may require inspection by an archaeologist. Such heritage is the property of the state and may require excavation and curation in an approved institution.
- Implement the Chance Fossil Finds Protocol during the construction phase of the solar PV facility.
- Undertake regular maintenance of the internal farm access roads by the contractor during the construction and decommissioning phases and by the operator during the operational phase.
- Ensure that the necessary permits or approvals from the relevant road authority are in place for the removal of the island at the TR38/01 and DR3093 intersection to accommodate the turning movements of the abnormal load vehicles.
- The route to the site should be further investigated to ensure that the abnormal loads are not obstructed at any point by geometric, height and width limitations along the route.
- If groundwater is sourced from existing boreholes, in the case that multiple Kudu Solar Facility
 projects are constructed simultaneously, adherence to recommended mitigation measures
 should be strictly followed to prevent over abstraction of groundwater.
- Phase two of the groundwater monitoring plan is to be discussed and evaluated in the event that groundwater is to be used in the project.
- Ensure that the BESS facilities are placed at least 50 m from any boreholes along with appropriate bunding and secondary containment.
- A stormwater management plan should be developed prior to the construction phase by an accredited professional.

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- Rehabilitation of soil and geological material to commence during the construction phase, if possible, alternatively following the construction phase to allow successful re-vegetation.
- Authorised vehicles to only use proposed access points and roads and keep within the footprint
 of the facility.
- Ground protection measures to be implemented during maintenance and refuelling operations.

Paul Lochner	
NAME OF EAP	
flocker	7 July 2023
SIGNATURE OF EAP	DATE