

**REPORT ON ENGINEERING GEOLOGICAL  
INVESTIGATIONS UNDERTAKEN FOR TOWNSHIP  
PROCLAMATION PURPOSES: SIYATHUTHUKA  
EXTENSIONS 5, 6, 7 AND 8 MPUMALANGA**

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**Undertaken for Messrs Sisonke Development Planners**

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# 1. CONCLUSIONS AND RECOMMENDATIONS

## 1.1. General

Based on the results of the investigation, Siyathuthuka Extension 5 has been divided into four geotechnical/soil zones, while Extensions 6, 7 and 8 have each been divided into two zones. The zones identified have similar soil profiles and related geotechnical constraints.

**With the exception of those areas designated D<sub>1</sub> (Figures 2, 3 and 4), the proposed extensions are suitable for residential/township development providing the precautionary measures recommended are implemented.**

## 1.2. Geotechnical considerations and founding recommendations

The Zones identified are delineated on **Figures 2 to 4 (Appendix A)**, while each zone's geotechnical characteristics are summarized in **Table 1**. The zonal prefix is based on the severity of the geotechnical or development constraint, or a combination of both, for a specific soil unit and applied as a worst case scenario. Postscript numerals are used to differentiate between zones with a similar prefix, and do not suggest an increase in severity.

An explanation of the various constraint categories is as follows:

PREFIX	CONSTRAINTS - geotechnical and development		COMMENTS
	Geotechnical - primarily construction costs	Development - installation of services and roads	
A	Typically confined to C, S, H Site Classes <sup>7</sup> .	Nominal <i>hardrock</i> (<10%) <i>excavation</i> <sup>4</sup> , and/or no evidence of a shallow (<1.5m) perched water table, and/or gentle slopes (<6%).	No restrictions on development.
B	Typically confined to Site Classes <sup>7</sup> C≤2, S≤2, H≤2 or S / R.	10-50% <i>hardrock excavation</i> <sup>4</sup> , and/or moderately steep (6 -15%) slopes, and/or seasonal perched water table at shallow (<1.5m) depth.	Developable, but with minor geotechnical and/or development constraints.
C	Typically confined to Site Classes <sup>7</sup> H <sub>3</sub> , R and/or P.	Greater than 50% <i>hardrock excavation</i> <sup>4</sup> , and/or steep slopes (>15%), and/or perennial perched water table at shallow (<1.5m) depth, and/or possible slope instability.	Developable but with more costly geotechnical and/or development constraints. More detailed geotechnical investigations may be required.
D	Areas typically classifying as Site Class <sup>7</sup> P, eg. areas of instability in soluble rock, uncontrolled fill, settlement due to dewatering, undermined ground etc.	Below the 1:100 year floodline, and/or swamps/marshes, and/or dispersive soils, and/or high risk of slope instability.	No development recommended, or more detailed geotechnical investigations required.

**Table 1: Summary of geotechnical and development constraints for township development: Siyathuthuka Extensions 5, 6, 7 and 8** - to be read in conjunction with the report

Zone	Abbreviated soil profile to 2m	Interpolated Geotechnical Constraints							Lightly loaded residential structures: typically <50kPa							Potentially suitable for on-site sanitation		Possible uses for surficial horizons, i.e. <1m				
		Class of problem envisaged based on soil movement: 0 - most favourable; II/III - least favourable							Code of Practice <sup>7</sup>			Founding Considerations										
		<b>Compressible soils:</b> Class 0: <10mm; Class I: 10-20mm; Class II: >20mm <b>Expansive soils:</b> Class 0: <7.5mm; Class I: 7.5 - 15mm; Class II: 15 - 30mm; Class III: >30mm <b>Collapsible soils:</b> Class 0: <5mm; Class I: 5 - 10mm; Class II: >10mm							Predicted range in soil movements <sup>++</sup>	Site Class	Typical founding solutions - see <b>Notes</b>	Recommended founding horizon for conventional or deep foundations	Estimated bearing capacity <sup>**</sup> at conventional founding depth	Estimated range in founding depth	Distress noted in existing structures	Dry	Wet*	base	subbase	selected	general fill	pipe bedding
		Excavatability to 1.5m in terms of SABS 1200D	Depth to perched ground water table	Expansive	Collapsible	Compressible	Other geotechnical constraints	+ ≈ heave - ≈ consolid														
Classification	Trench instability?	[%]	[yes/no]	[m]	[Class]	[Class]	[Class]															
<b>B<sub>1</sub></b>	TSMO becoming weakly ferruginous cemented with depth / pebble marker / completely weathered sandstone with intercalated shale and tillite locally	<i>soft</i> >80 <i>hardrock</i> <20	yes	<1.5	0	II	II	slopes typically 2 to 4%	<50 (-)	C <sub>2</sub>	3 and 4	weakly ferruginous cemented TSMO or stiff residua	<15	0.8 - 1.4	N/A	yes	no	X	X	✓	✓	✓
<b>C<sub>1</sub></b>	sandstone outcrops with thin surficial regolith locally	<i>hardrock</i> >50 <i>soft</i> <50	no	<0.5	0	0	0	slopes <3%	<10 (-)	R	1	very soft rock sandstone, shale or tillite	>200	0.0 - 0.6	N/A	yes	no	X	X	✓	✓	X
<b>C<sub>2</sub></b>	thin surficial regolith / nodular and hardpan ferricrete	<i>soft</i> >60 <i>hardrock</i> <40	no	<0.3 (perennial)	0	0	0	susceptible to surface seepage and marshy ground conditions locally; slopes <4%	<10 (-)	R - S	1	hardpan ferricrete or ferruginous cemented residua	>200	0.0 - 0.6	N/A	yes	no	X	✓	✓	✓	X
<b>D<sub>1</sub></b>	alluvium / sandstone or shale	<i>soft</i> >90 <i>hardrock</i> <10	yes	0.0	0	0	II	drainage line / surface flow; mostly below 1:100 year floodline; or marshy ground conditions	<i>highly variable</i>	P <sub>marsh</sub>		no development recommended			N/A	no	no	X	X	X	X	X

**Notes:**

- 1 Conventional founding methods as per SABS 0161-1980 (as amended 1984, 1985 and 1986) Foundations placed on unfavourably dipping bedrock must be dowelled at regular intervals
- 2 Modified normal construction techniques - reinforced strip footings, wide strip footings, articulation joints, light reinforcing in masonry, site drainage and plumbing precautions<sup>7</sup> Construct walls independent of the floors
- 3 Compaction of *in situ* soils below individual footings - remove *in situ* soils to 1.5B (single storey) and 2B (double storey) - B = maximum footing width - and over a width of 1.5B before backfilling the excavation with suitable inert material in controlled layers; controlled layers must be a maximum of 150mm thick and compacted to a minimum of 93% Modified AASHTO density at -1 to +2% of optimum moisture content<sup>7</sup> Backfill material must comprise a minimum of a G7 material; alternatively, it may be possible to stabilize the *in situ* soils, e.g. for PI's greater than 15, but less than 25, the soils could be stabilized with 3 to 5% lime
- 4 Deep strip footings - found on competent horizon below the potentially problematical horizon Construct walls independent of the floors
- 5 Soil raft - remove *in situ* soils to 1.0m beyond the perimeter of the structure and to a depth of 1.5B (single storey) and 2B (double storey), or to competent material, before backfilling the excavation with suitable imported inert material - minimum of a G7 in terms of TRH 14 - in controlled layers as per Note 3; normal construction with site drainage requirements<sup>7</sup>
- 6 Split construction - combination of reinforced brickwork, blockwork and full movement joints with suspended floors or reinforced slabs acting independently from the structure Good site drainage and plumbing precautions<sup>7</sup>
- 7 Stiffened or cellular raft - stiffened or cellular raft with articulation joints or solid light reinforced masonry; good site drainage and plumbing precautions<sup>7</sup>
- 8 Dynamic compaction - directly engineer *in situ* material
- 9 Piled foundations using end-bearing or displacement type piles; floors to be suspended  
(*FOUNDING COSTS GENERALLY INCREASE FROM 1 - 9*)

**Comments:** \* = subject to confirmatory percolation tests; + = subject to confirmatory laboratory tests; b/l = beyond limit of present investigation; n/a = not applicable; N/A = not available; \*\* = for less than 10mm of settlement for a typical soil profile; ++ = for conventional strip footings founded at 0.6m and underlain by a typical soil profile

**Additional comments on abbreviated soil profile:** / = overlying; = horizon may contain potentially expansive clays; ( ) = horizons in brackets may be present locally; TSMO = transported soils of mixed origin

**Zones** designated **B<sub>1</sub>** comprise those areas characterised by mostly thick transported soils of mixed origin (TSMO), which often become weakly ferruginous cemented with depth, overlying completely weathered sandstone with intercalated shale horizons and tillite locally. The geotechnical characteristics of these zones are summarized as follows:

- Greater than 80% of the zone will classify as *soft excavation*<sup>4</sup> to 1.5m, with up to 20% *hardrock excavation*<sup>4</sup>.
- Owing to the prevalence of pedocrete development with depth, these areas are susceptible to the development of a perched groundwater table after periods of prolonged precipitation, and mostly within 1.5m of ground level. It is therefore recommended that damp proofing measures be included throughout all structures, with subsoil drains behind all retaining structures.
- The topography is gently undulating with slopes typically less than 4%, which is ideal for residential development, but will require that stormwater control is adequately addressed.
- No expansive soils are envisaged in this zone. However, the TSMO is compressible and potentially collapsible, while the underlying residuum is *moderately* compressible. Taking cognisance of the maximum predicted settlement of approximately 50mm, with up to 20mm of collapse settlement possible under the present moisture regime, these areas have been classified as *C<sub>2</sub>* in terms of the Code of Practice<sup>7</sup>. To counteract the settlements envisaged, it is recommended that the substrate beneath the foundations be engineered in controlled layers; to this end, foundation excavations must be taken down to a depth and breadth of at least 1.5B (where B equals the maximum footing width), or down to competent material, e.g. weakly ferruginous cemented TSMO, before returning the excavated material in controlled layers to the desired founding level; controlled layers must be a maximum of 150mm thick and compacted to a minimum of 93% Modified AASHTO density at -1 to +2% of optimum moisture content. The backfill must comprise a minimum of a G7<sup>4</sup> quality material, and the TSMO should mostly suffice. The subgrade beneath all lightly loaded floors must also be engineered in controlled to a depth of at least 0.3m, and floor slabs must be cast independent of the walls.

**Zones** designated  $C_1$  comprise those areas characterised by sub-outcropping and outcropping sandstone with sporadic, intercalated shale horizons. The geotechnical characteristics of these zones are summarized as follows:

- In view of the sub-outcropping and/or outcropping sandstone and/or shale, *hardrock excavation*<sup>4</sup> is envisaged throughout greater than 50% of these areas to 1.5m, with less than 50% *soft excavation*<sup>4</sup>.
- Owing to the prevalence of competent bedrock at shallow depth, these areas are susceptible to the development of a perched groundwater table after periods of prolonged precipitation, and probably within 0.5m of ground level. It is therefore recommended that damp proofing measures be included throughout all structures, with subsoil drains behind all retaining structures.
- The topography is gently undulating with slopes typically less than 3%, which is ideal for residential development, but will require that stormwater control is adequately addressed.
- No expansive soils are envisaged in these areas. Furthermore, the prevalence of competent bedrock at shallow depths will provide an ideal founding substrate for the residential structures. These areas have therefore been classified as *R* in terms of the Code of Practice<sup>7</sup> and conventional foundations will suffice. However, foundations must be placed on the bedrock sandstone or shale throughout, failing which the structures could be susceptible to increased differential settlement.

**Zones** designated  $C_2$  are geotechnically similar to those areas designated  $C_1$ , although with competent pedocrete present at shallow depth as opposed to sandstone or shale. The geotechnical characteristics of these zones are summarized as follows:

- Owing to the prevalence of competent pedocrete at shallow depth, *intermediate excavation*<sup>4</sup> is envisaged throughout greater than 50% of these areas to 1.5m, with less than 50% *soft excavation*<sup>4</sup>, i.e. the pedocrete could not be penetrated with a backhoe, but a 20-ton excavator or similar should penetrate the material.
- The prevalence of competent pedocrete at shallow depths makes these areas susceptible to the development of a perennial perched groundwater table, mostly within 0.3m of ground level. Furthermore, marshy ground conditions and surface seepage may occur after periods of prolonged precipitation. To ensure these areas are habitable, it is paramount that subsoil drains are incorporated with the bulk services to lower the perched groundwater table and prevent water-logged ground conditions. Despite the installation of “regional” drains, subsoil drains are also

recommended around individual structures, with damp proofing measures throughout all-structures.

- As is typical of the areas earmarked for new extensions to Siyathuthuka, the topography is gently undulating with slopes mostly less than 4%, which are deemed ideal for township development. However, owing to the susceptibility of these areas to marshy ground conditions, with surface seepage after periods of prolonged precipitation, stormwater control is deemed paramount.
- No expansive soils are envisaged in these areas. Furthermore, the prevalence of competent pedocrete at shallow depths, will provide an ideal founding substrate for residential structures. These areas have therefore been classified as *R - S* in terms of the Code of Practice<sup>7</sup> and conventional foundations will suffice, providing these are placed on competent pedocrete throughout.

**Zones** designated **D<sub>1</sub>** comprises those areas falling below the 1:100 year floodline and adjoining areas characterised by marshy ground conditions. The soil profiles in these areas are similar to those of Zone B<sub>1</sub>, i.e. transported soils overlying residua derived from the in situ weathering of sandstone, shale and tillite. The geotechnical characteristics of this zone are summarized as follows:

- Greater than 90% of the zone will classify as *soft excavation*<sup>4</sup> to a depth of 1.5m, with less than 10% *hardrock excavation*<sup>4</sup>.
- These areas mostly fall below the 1:100 year floodline and/or are susceptible to perennial, marshy ground conditions.
- The marshy ground conditions and/or constraint of the 1:100 year flood line, makes these areas unsuitable for residential development. As such, they have been classified as *P<sub>marsh</sub>* in terms of the Code of Practice<sup>7</sup>. No development is recommended, and these areas should ideally be zoned as private open space (POS).

## General

Notwithstanding the mostly virgin grassveld characteristic of the areas earmarked for the proposed extensions, these areas border existing residential development with evidence mounds and pockets of fill locally (**Figure 3**). The possibility of areas of buried fill should therefore not be discounted, e.g. ash/waste/compost pits etc. Should fill of any nature be encountered in the foundation excavations, this material must be removed to spoil and be

replaced with suitable inert material in controlled layers - see not 3 (**Table 1**). Backfill must comprise a minimum of a G7<sup>6</sup> quality material.

Throughout the proposed township, it is recommended that the ground surface around individual structures be suitably landscaped to ensure that ponding of surface water does not occur near foundations. Furthermore, all downpipes should discharge well away from individual structures, and all water bearing services should be fitted with flexible joints at points of ingress and egress to structures or soil rafts.

While the susceptibility of the area to a perched groundwater table has been discussed in the various zones identified, it is imperative that measures are incorporated during the installation of bulk services to intercept and divert percolating groundwater. (This should provide a cost-effective means of removing the percolating groundwater). Failure to address this constraint adequately, could result in failure of surfaced roads, excessive damp in residential structures and marshy ground conditions in gardens, especially in Zones designated C<sub>2</sub>.

### **1.3. Roads**

The design of all roads must be undertaken by a Professional Engineer taking cognisance of the potentially collapsible TSMO prevalent in Zone B<sub>1</sub>, shallow (<1.5m), perched, groundwater throughout most of the various extensions, shallow bedrock in Zone C<sub>1</sub> and hardpan ferricrete in Zone C<sub>2</sub>.

The surficial TSMO prevalent throughout the townships is likely to classify as G7 in terms of TRH14 - see interpolated soil parameters in the summary table of results in **Appendix C** - making these soils potentially suitable for use in the selected layers of paved areas and roadways. The hardpan ferricrete in Zone C<sub>2</sub> has been extensively exploited as a source or road building material, and it is envisaged that this material will classify as G5 in terms of TRH14, making it suitable for use as a subbase. Material for use in the base layers will have to be imported. Alternatively, the pedocrete can be stabilized with cement, of which 4% should suffice in yielding a C3/C4 material in terms of TRH14.



## 2. INTRODUCTION

### 2.1. Terms of reference

In terms of an appointment dated 11 November 2011 from Mr E van Veenhuysen of Messrs Sisonke Development Planners, Geo3cc has undertaken an engineering geological investigation for township proclamation purposes. Our appointment follows the submission of a proposal and costing dated 26 October 2011 (Our Reference: GQ/1297/a/hjs).

The investigation has been carried out according to the requirements for township proclamation purposes as laid down by the Council for Geosciences and Provincial Administrations in terms of the Town Planning and Ordinance Act of 1986. The investigation has also taken cognisance of the published *Guidelines for Urban Engineering Geological Investigations*<sup>5b</sup> and the *Code of Practice*<sup>7</sup>.

This report, together with the accompanying Engineering Geological Maps (**Figure 2 to 4, Appendix A**), summarizes the findings of the investigation.

### 2.2. Site details and physical characteristics

The proposed townships - Extensions 5, 6, 7 and 8 - with a combined area of approximately 110-hectares, are situated on the outskirts of Siyathuthuka, northwest of Belfast in Mpumalanga (**Figure 1**). The proposed townships are mostly undeveloped:

- Extensions 5, situated on the northwestern corner of Siyathuthuka, is characterized by gently sloping topography with grassveld throughout and a new cemetery at the southern end of the proposed township
- Extension 7, situated on the southeastern corner of Siyathuthuka, slopes gently to the east, with remnants of a farmstead at the southern end of the proposed township, while vegetation comprises grassveld and bluegum plantations
- Extensions 6 and 8, at the southern end of Siyathuthuka, slope gently to the south and are characterised by grassveld and the remnants of a bluegum plantation

### 2.3. Reference sources

The following maps and aerial photographs were consulted during our investigation:

- 1:250,000 Scale published Geographical Series Map of the area, Barberton 2530 and Pretoria 2528
- 3x Enlargements of 1:60,000 Scale published aerial photographs 858, 859 and 860, strip 1, job 996, date 1997. Chief Directorate of Survey and Mapping

### 3. SITE INVESTIGATION

#### 3.1. Fieldwork

The fieldwork phase of the investigation was undertaken at the beginning of February 2012, and comprised the excavation of thirty-three pits with a Bell 315S backhoe. Each pit was excavated to refusal or to a depth of at least 2m. In addition, a further three typical sandstone exposures were profiled, although the positions of many more were recorded using a hand-held GPS and have been included in our evaluation. The positions of the pits, as indicated on **Figures 2 to 4**, were selected to probe the soil zones identified using the stereoscopic analysis of aerial photographs.

All pits and representative exposures were profiled according to standard procedures<sup>5a</sup> by a professionally registered engineering geologist and the resultant profiles are included in **Appendix B**.

#### 3.2. Sampling and laboratory testing

During inspection of the *in situ* soils, seven *undisturbed*, six lump and twenty-eight indicator samples, representative of the soils present beneath the proposed township, were extracted from the sidewalls of the pits for laboratory testing purposes. The samples were submitted to the laboratories of Messrs EngeoLab in Nelspruit for testing according to our instructions.

The test results, in the format they were received from the laboratory, are included in **Appendix C**.

### 4. GEOLOGY AND SUBSOILS

#### 4.1. Site geology

Based on information gleaned the fieldwork phase of the investigation, the bedrock beneath the extensions comprises mostly shale and sandstone. In terms of the published 1:250,000 scale geological series maps of the area, Pretoria 2528 and Barberton 2530, these sedimentary rocks belong to the Vryheid Formation (Pv) of the Ecca Group, Karoo Supergroup. Typically, this Formation is characterised by quartzitic cross-bedded sandstone, which is pebbly near its base, with gritty sandstone and shale, i.e. consistent with the rocks encountered. Anomalous to the area however, is the gravelly and bouldery residuum with a fine-grained matrix, noted in Extensions 6, 7 and 8. This sedimentary rock have been classified as tillite, suggesting it belongs to the slightly older Dwyka Formation

(Pd) of the Karoo Supergroup, i.e. underlies the sandstones and shale. However, the published geological series map only indicate tillite much further to the southwest.

Dolerite and diabase dykes are also prevalent in the area, although no such intrusions were documented during the fieldwork. Of concern with these intrusive bodies, is that the soils derived from the *in situ* weathering of these rock can vary from fine-grained, potentially expansive soils to very hard rock boulders in a fine-grained matrix. Since these intrusions can vary from a few metres to several hundred metres wide and may form expansive soils on weathering, their possible presence must be borne in mind during development of the townships.

#### **4.2. Site soils**

The basic soil parameters obtained from grading and Atterberg Limits tests are summarized in **Table 2**, while generalized soil profiles for the various zones encountered are discussed below.

Zone B<sub>1</sub> comprises those areas characterised by mostly thick transported soils of mixed origin (TSMO), comprising silty or clayey fine sand that often becomes weakly ferruginous cemented with depth, overlying deeply weathered sedimentary rocks comprising mostly sandstone with intercalated shale horizons that have yielded clayey sand and sandy clay residua respectively. Residual tillite encountered locally in Extensions 6, 7 and 8, comprises scattered gravels, cobbles and boulders, in a floury fine-grained matrix.

Zone C<sub>1</sub> comprises those areas characterised by sub-outcropping and outcropping sandstone, with intercalated sub-outcropping shale locally, and pockets of surficial regolith comprising silty sand (TSMO) or abundant gravels and cobbles (coarse colluvium).

Zone C<sub>2</sub> comprises those areas characterised by sub-outcropping and outcropping hardpan ferricrete with thin surficial regolith of mostly silty fine sand (TSMO).

Zone D<sub>1</sub> comprises the drainage lines traversing the proposed townships and incorporate the adjoining marshy areas that are deemed unsuitable for development. These areas are

**Table 2: Laboratory determined soil properties**

Test Pit No.	Soil Origin	Horizon Depth [m]		Soil Constituents [%]				Atterberg Limits			GM	LS [%]	Activity 0,4 = kaolinite; 0,9 = illite; 1,5-6,0 = montmorillonite	Natural Moisture Content [%]	Classification		
		From	To	clay [<0,002mm]	silt [0,002-0,06mm]	sand [0,06-2,0mm]	gravel [2,0-60mm]	LL	PI	PI*					UNIFIED	PRA	
TP 8	TSMO	0.30	1.25	7	24	69		26	4	3	0.78	2.0	0.4	LOW		SM	A.4 (1)
TP 10	TSMO	0.30	0.65	8	24	60	8	27	5	4	0.92	2.0	0.5	LOW		SM	A.4 (1)
TP 13	TSMO	0.25	1.20	12	34	54		33	11	10	0.51	5.4	0.8	LOW		CL	A.6 (5)
TP 16	TSMO	0.20	0.60	9	29	59	3	24	3	3	0.66	1.3	0.3	LOW		SM	A.4 (3)
TP 18	TSMO	0.80	1.60	5	17	54	24	0	0		1.40	0.0		LOW	10.30	SM	A.2.4 (0)
TP 21	TSMO	0.30	0.60	2	16	63	19	0	0		1.35	0.0		LOW		SM	A.2.4 (0)
TP 22	TSMO	0.30	0.90	5	24	59	12	23	3	2	0.98	1.7	0.4	LOW		SM	A.4 (1)
TP 25	TSMO	0.20	1.60	9	34	54	3	30	4	4	0.63	2.0	0.4	LOW		SM	A.4 (4)
TP 28	TSMO	0.30	0.75	9	27	62	2	24	5	4	0.73	2.0	0.4	LOW		SM/SC	A.4 (2)
TP 33	TSMO	0.30	1.20	7	23	69	1	20	4	3	0.81	2.0	0.4	LOW	15.50	SM/SC	A.4 (1)
TP 8	f/c TSMO	1.25	1.70	3	15	38	44	0	0		1.77	0.0		LOW		SM	A.1.b (0)
TP 13	w/f/c TSMO	1.20	1.90	11	33	49	7	34	5	4	0.67	5.4	0.4	LOW	27.60	ML	A.4 (5)
TP 2	hardpan ferricrete	0.30	1.30	2	7	23	68	0	0		2.27	0.0		LOW		GM	A.1.a (0)
TP 21	residual sandstone / ti	0.85	1.50	3	16	46	35	0	0		1.69	0.0		LOW	12.50	SM	A.1.b (0)
TP 21	nodular ferricrete / pebble marker	0.60	0.85	1	3	19	77	0	0		2.57	0.0		LOW		GP	A.1.a (0)
TP 34	residual sandstone	0.50	2.10	17	41	38	4	44	12	10	0.52	5.4	0.6	LOW	17.10	ML	A.7.5 (8)
TP 4	residual sandstone	0.60	1.10	2	6	26	66	0	0		2.30	0.0		LOW		GP	A.1.a (0)
TP 12	r/ residual sandstone	0.65	1.60	8	21	31	40	28	6	3	1.56	2.7	0.4	LOW		SM/SC	A.2.4 (0)
TP 16	residual sandstone	0.70	1.30	4	20	33	43	26	2	1	1.64	1.0	0.3	LOW		SM	A.2.4 (0)
TP 29	r/residual sandstone	0.70	1.00	9	27	41	23	30	4	3	1.20	2.0	0.3	LOW		SM	A.4 (2)
TP 9	w/f/c r/ residual sands	1.30	2.30	4	18	44	34	26	6	3	1.53	2.7	0.8	LOW		SM/SC	A.2.4 (0)
TP 28	w/f/c r/ residual sands	0.75	1.60	9	29	47	15	32	6	4	1.04	3.0	0.4	LOW		SM	A.4 (2)
TP 29	residual tillite	1.00	2.10	11	30	46	13	28	7	5	0.92	3.4	0.5	LOW		SM/SC	A.4 (3)
TP 31	residual tillite	0.50	1.00	4	11	33	52	27	4	2	1.96	2.0	0.5	LOW		SM	A.1.b (0)
TP 31	residual tillite	1.00	2.20	5	18	38	39	28	8	4	1.65	3.4	0.8	LOW	13.70	SC	A.2.4 (0)
TP 6	residual shale	1.60	2.10	15	43	31	11	36	8	7	0.63	3.4	0.5	LOW		ML	A.4 (7)
TP 6	residual shale	0.40	1.60	20	38	40	2	35	13	12	0.43	5.4	0.6	MEDIUM		CL	A.6 (8)
TP 14	residual shale	1.00	1.60	19	34	38	9	34	9	8	0.61	34.0	0.4	LOW		ML	A.4 (7)

Notes: PI = plasticity index (\*) = on whole sample  
 LL = liquid limit; LS = linear shrinkage;  
 GM = grading modulus; n/t = not tested;  
 w/ = weakly; f/c = ferruginous cemented  
 r/ = residual; r/r = reworked residual;  
 TSMO = transported soils of mixed origin.

characterised by transported and residual soils similar to those encountered in Zone B<sub>1</sub>, albeit with the residuum usually more deeply weathered.

## 5. GEOTECHNICAL EVALUATION

### 5.1. Excavatability and material usage

The pits excavated beyond those areas of outcropping and sub-outcropping bedrock (**Zone C<sub>1</sub>**, **Figures 2 and 4**), were mostly excavated without refusal to depths in excess of 1.5m, although the presence of more competent ferruginous cemented regolith locally in Zones B<sub>1</sub> and prevalence of it in Zone C<sub>2</sub>, often resulted in refusal of the backhoe at depths varying from 0.5 to 1.5m. It is therefore recommended that in Zone B<sub>1</sub>, allowance be made for up to 20% *hardrock excavation*<sup>4</sup> in the Bill of Quantities (BoQ) for excavations to 1.5m. In Zone C<sub>1</sub>, characterised by sub-outcropping and outcropping sandstone and shale, the BoQ must make allowance for greater than 50% *hardrock excavation*<sup>4</sup>, while Zone C<sub>2</sub>, characterised by shallow ferricrete, it is recommended that the BoQ make allowance for greater than 50% *intermediate excavation*, since the pedocrete should be penetrated by larger plant, although it could not be penetrated using a backhoe. In Zone D<sub>1</sub>, characterised by thick transported soils overlying unconsolidated residua, it is envisaged that greater than 90% of these areas are characterised by *soft excavation*<sup>4</sup>.

After clearing and grubbing the road reserves in Zone B<sub>1</sub>, the surficial regolith will comprise mostly TSMO. These soils typically classify as A.4 (1-4) in terms of the PRA Classification with a grading moduli mostly less than 1 (**Table 2**). Based on our experience with similar material, and taking cognisance of the interpolated TRH14 classification for these soils - see the summary table in **Appendix C** - the surficial regolith should mostly classify as G7<sup>6</sup>, making them potentially suitable for use in the selected layers of paved areas and roadways and in high quality engineered fills. The ferruginous cemented TSMO prevalent at depth in Zone B<sub>1</sub> and pedocrete in Zone C<sub>1</sub>, are likely to classify as A.1.a/b (0) in terms of the PRA classification with grading moduli mostly greater than 1.5 and an interpolated TRH14 classification of G5; these soils are therefore potentially suitable for use in the subbase layers of paved areas and roadways. (The hardpan ferricrete prevalent in the area has been extensively exploited for road building material, e.g. large borrow pit downslope from TP01 (**Figure 2**), with numerous similar borrow pits around the outskirts of Belfast). If sufficiently weathered, the sandstone outcrops in Zone C<sub>1</sub> should also provide a viable source of construction materials for roads if necessary. However, irregular weathering of

the shallow bedrock usually only makes for thin surficial deposits of potentially suitable regolith.

## 5.2. Groundwater

In general, the extensions are all susceptible to the development of a perched groundwater table to a greater or lesser degree. In Zone B<sub>1</sub> characterised by thicker unconsolidated regolith, a perched groundwater table is still envisaged on the pedocrete development prevalent with 1.5m of ground level. In Zone C<sub>1</sub> with outcropping and sub-outcropping bedrock, a perched groundwater table is envisaged within 0.5m of ground level. Zone C<sub>2</sub> is characterised by shallow pedocrete, which in itself is indicative of a perched groundwater table. These areas are therefore susceptible to the development of a perennial, perched groundwater table within 0.3m of ground level; marshy ground conditions with surface seepage locally, may also occur after periods of prolonged precipitation.

Zones designated D<sub>1</sub> comprise those areas mostly falling below the 1:100 year floodline. However, the outer boundaries of these areas (1:100 year floodline) have been extended, where necessary, to incorporate those areas characterised by marshy and water-logged ground conditions.

## 5.3. Potentially expansive soils

Plotting the Plasticity Index (whole sample) against the clay percentage on a Standard Activity diagram<sup>8</sup>, for the soils tested (**Table 2**), revealed that an isolated sample of the residual shale classified as *medium*. However, this material has a linear shrinkage of only 5.4%, suggesting that it is unlikely to prove expansive. The remainder of the soils tested all classify as *low*.

## 5.4. Potentially collapsible and compressible soils

The open texture noted in the TSMO make these soils susceptible to consolidation and/or collapse settlement. To assess these properties, representative samples of the material were subjected to double oedometer tests and/or moisture, density and specific gravity determinations. Representative samples of the residual shale and sandstone, were also subjected to similar tests to assess their consolidation properties. The results from tests undertaken on the undisturbed samples are all summarized in **Table 3**.

Table 3: Summary of soil parameters from tests on undisturbed samples											
Material	Pit position	Depth [m]	Profiled consistency	Dry density [kg/m <sup>3</sup> ]	e <sub>0</sub>	OCR	Mois- ture [%]	Sr [%]	m <sub>v</sub> x10 <sup>-4</sup> [m <sup>2</sup> /kN]	cc	Collapse potential {est} <sup>2</sup> [%]
TSMO	TP 8	0.70	loose	1,390	0.882	2.5	12.7	37.7	8.76	0.289	8.8 {10.6}
TSMO	TP 13	0.80	soft	1,210	1.164	3.4	29.3	66.0	7.23	0.369	3.7 {20.1}
TSMO*	TP 13	1.50	medium dense	1,473	0.779	nd	27.6	92.8	nd	nd	nd
TSMO*	TP 18	1.00	dense	1,949	0.339	nd	10.3	79.3	nd	nd	nd
TSMO	TP 22	0.60	loose	1,370	0.899	4.1	23.3	67.4	7.18	0.321	2.1 {11.6}
TSMO	TP 25	0.70	soft - firm	1,380	0.890	3.8	17.1	50.1	5.95	0.283	3.3 {11.1}
TSMO	TP 33	0.70	loose	1,560	0.673	nd	15.5	60.1	nd	nd	nd
residual shale	TP 6	0.70	firm	1,480	0.767	12.5	21.8	74.5	2.44	0.233	1.0
residual sandstone	TP 21	1.00	dense	1,890	0.392	nd	12.5	83.9	nd	nd	nd
residual sandstone*	TP 28	1.00	medium dense	1,400	0.867	11.8	22.6	68.3	2.04	0.279	0.6
reworked residual sandstone	TP 31	0.70	loose	1,450	0.802	1.7	11.3	36.8	10.20	0.249	nd
residual sandstone	TP 31	1.20	stiff	1,845	0.420	nd	13.7	85.5	nd	nd	nd
residual sandstone	TP 34	0.70	firm	1,586	0.652	nd	17.1	68.7	nd	nd	nd

**Notes:** E' - estimated deformation modulus; e<sub>0</sub> - initial void ratio; S<sub>r</sub> - initial degree of saturation; nt - not tested; n/a - not applicable; OCR - over consolidation ratio; nt - not tested; n/a - not applicable; \* - weakly ferruginous cemented.

<b>Table 4: Coefficient of volume compressibility (<math>m_v</math>)</b>		
Consistency	Compressibility Class	Coefficient $\times 10^{-4} \text{ m}^2/\text{kN}$
very soft/loose	very high	> 15
soft/loose	high	3 - 15
medium dense/firm	moderate	1 - 3
dense/stiff	low	0.5 - 1
very dense/stiff	very low	< 0.5

The test results indicate that the TSMO are potentially collapsible, with the maximum recorded collapse of 8.8%. (The estimated collapse<sup>2</sup> for these soils varied from approximately 11% to 20%, and the discrepancy between the measured and estimated collapse is attributed to the elevated in situ moisture contents). In addition to these soils being collapsible, the calculated coefficient of volume compressibility ( $m_v$ ) over the stress range of 100kPa greater than the overburden pressure (**Table 3**), classifies as *high* (**Table 4**).

With reference to double oedometer tests undertaken on undisturbed samples of the residua, only nominal collapse was recorded. However, the calculated coefficient of volume compressibility ( $m_v$ ) over the stress range of 100kPa greater than the overburden pressure mostly classifies as *moderate*, with an isolated sample of the reworked residual sandstone classifying as *high* (**Table 4**).

### 5.5. Slope angles

Slopes throughout the areas earmarked for residential development - Extensions 5 to 8 - are less than 6%, which is deemed ideal for townships. However, the prevalence of a shallow perched groundwater table, with the possibility of surface seepage locally after periods of prolonged precipitation, dictates that storm water control will be paramount.

### 5.6. Settlement calculations and zonal (NHBRC) classification

The predicted settlement for light foundation pressures, i.e. less than 50kPa, based on our visual assessment of the soils and/or laboratory results suggests that:

- Foundations in Zone B<sub>1</sub> will typically be underlain by *highly* compressible and potentially collapsible TSMO, which in turn overlie residuum that is typically *moderately* (**Table 4**) compressible, grading into more competent residua with depth.



As such, conventionally dimensioned strip footings imposing 50kPa will be susceptible to a maximum of 50mm of settlement, of which approximately 20mm can be attributed to collapse at the current moisture contents. This zone has therefore been classified as  $C_2$  in terms of the Code of Practice<sup>7</sup>.

- Zone  $C_1$  comprises those areas of sub-outcropping and outcropping sandstone with intercalated shale. Throughout most of these zones therefore, foundations for the lightly loaded structures can be placed directly on the bedrock present at shallow depth. As such, these areas classify as  $R$  in terms of the Code of Practice<sup>7</sup>.
- Zone  $C_2$  comprises those areas of sub-outcropping and outcropping hardpan ferricrete, or with pedocrete development at shallow depths. As in the case of Zone  $C_1$ , a competent founding substrate is envisaged at shallow depth and these areas have been classified as  $R - S$  in terms of the Code of Practice<sup>7</sup>.
- Zones designated  $D_1$  comprises those areas falling below the 1:100 year floodline and/or areas adjoining the drainage lines that are susceptible to marshy ground conditions. As such, these areas are deemed unsuitable for residential development and have been classified as  $P_{marsh}$  in terms of the Code of Practice<sup>7</sup>.

## 6. REPORT PROVISIONS

While every effort was made during the fieldwork to identify the different soil and rock horizons and determine their distribution, guaranteeing that isolated zones of either poorer foundation material or hard rock excavation has not been identified is impossible under the constraints of an investigation of this nature. The investigation has therefore sought to highlight potential foundation and excavation problems and provide early warning to the municipal engineers and developers. Detailed geotechnical investigations must be undertaken for all new structures to confirm the constraints identified.

We trust that the above observations meet with your requirements of us in this project, and will make ourselves available to discuss our findings should there be any queries.



H.J. Schurink, Pr.Sci.Nat., GDE.  
for Geo3cc.

## 7. REFERENCES

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**APPENDIX A**  
**FIGURES 1 TO 4**







**Table 1: Summary of geotechnical and development constraints for township development: Siyathuthuka Extensions 5, 6, 7 and 8 - to be read in conjunction with the report.**

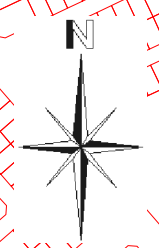
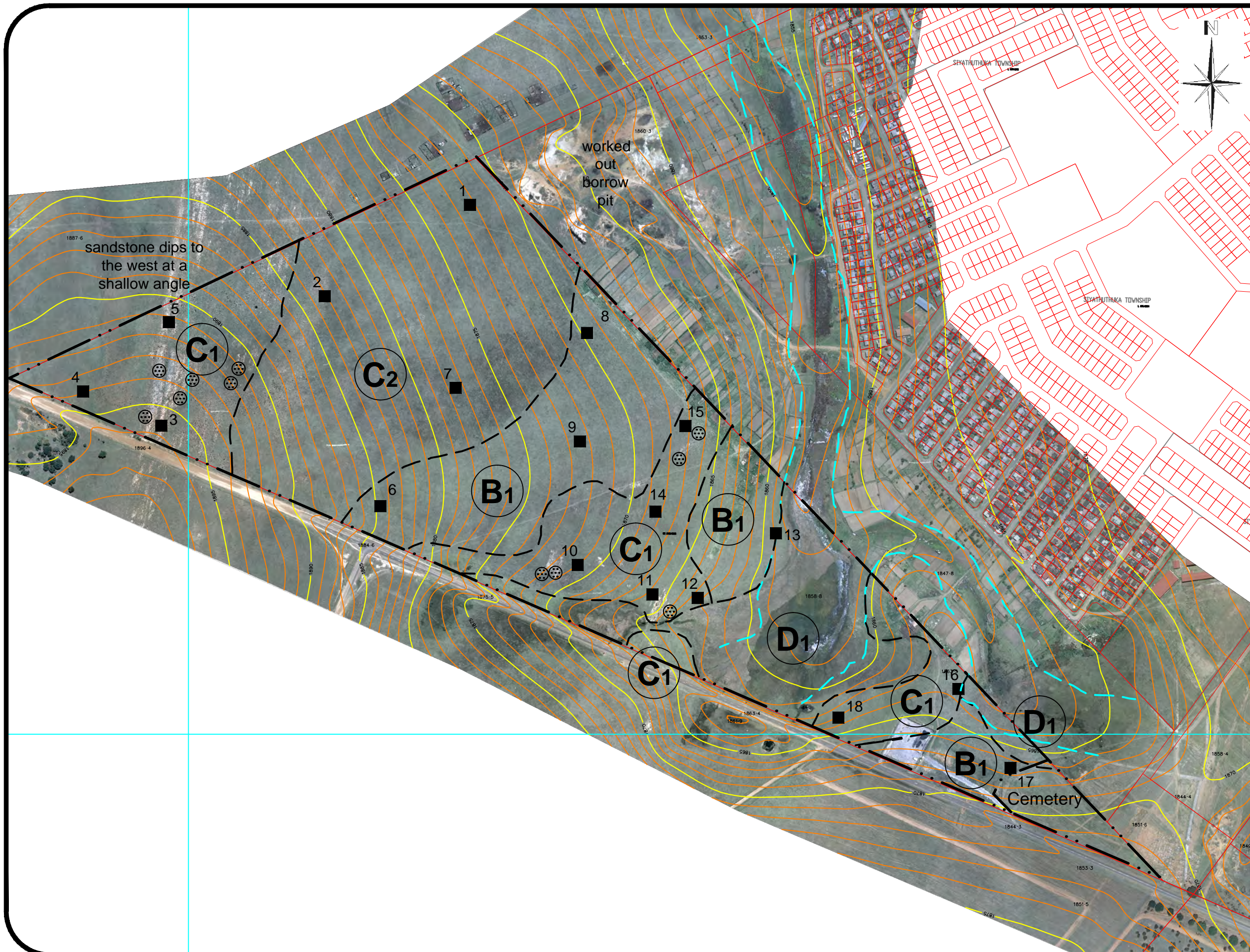
Zone	Abbreviated soil profile to 2m	Interpolated Geotechnical Constraints							Lightly loaded residential structures: typically <50kPa							Potentially suitable for on-site sanitation		Possible uses for surficial horizons, i.e. <1m							
		Class of problem envisaged based on soil movement: 0 - most favourable; II/III - least favourable.							Code of Practice <sup>7</sup>			Founding Considerations													
		<b>Compressible soils:</b> Class 0: <10mm; Class I: 10-20mm; Class II: >20mm. <b>Expansive soils:</b> Class 0: <7.5mm; Class I: 7.5 - 15mm; Class II: 15 - 30mm; Class III: >30mm. <b>Collapsible soils:</b> Class 0: <5mm; Class I: 5 - 10mm; Class II: >10mm.							Predicted range in soil movements++  + ≈ heave - ≈ consolid.	Site Class	Typical founding solutions - see <b>Notes</b>	Recommended founding horizon for conventional or deep foundations.	Estimated bearing capacity** at conventional founding depth	Estimated range in founding depth	Distress noted in existing structures	Dry	Wet*	base	subbase	selected	general fill	pipe bedding			
		Excavatability to 1.5m in terms of SABS 1200D	Depth to perched ground water table	Expansive	Collapsible	Compressible	Other geotechnical constraints																		
Classification	Trench instability ?																								
[%]	[yes/no]	[m]	[Class]	[Class]	[Class]		[mm]					[kPa]	[m]	[y/n ; N/A]											
<b>B<sub>1</sub></b>	TSMO becoming weakly ferruginous cemented with depth / pebble marker / completely weathered sandstone with intercalated shale and tillite locally	<i>soft</i> >80 <i>hardrock</i> <20	yes	<1.5	0	II	II	slopes typically 2 to 4%	<50 (-)	C <sub>2</sub>	3 and 4	weakly ferruginous cemented TSMO or stiff residua	<15	0.8 - 1.4	N/A	yes	no	X	X	✓	✓	✓			
<b>C<sub>1</sub></b>	sandstone outcrops with thin surficial regolith locally	<i>hardrock</i> >50 <i>soft</i> <50	no	<0.5	0	0	0	slopes <3%	<10 (-)	R	1	very soft rock sandstone, shale or tillite	>200	0.0 - 0.6	N/A	yes	no	X	X	✓	✓	X			
<b>C<sub>2</sub></b>	thin surficial regolith / nodular and hardpan ferricrete	<i>soft</i> >60 <i>hardrock</i> <40	no	<0.3 (perennial)	0	0	0	susceptible to surface seepage and marshy ground conditions locally; slopes <4%	<10 (-)	R - S	1	hardpan ferricrete or ferruginous cemented residua	>200	0.0 - 0.6	N/A	yes	no	X	✓	✓	✓	X			
<b>D<sub>1</sub></b>	alluvium / sandstone or shale	<i>soft</i> >90 <i>hardrock</i> <10	yes	0.0	0	0	II	drainage line / surface flow; mostly below 1:100 year floodline; or marshy ground conditions	highly variable	P <sub>marsh</sub>		no development recommended			N/A	no	no	X	X	X	X	X			

**Notes:**

1. Conventional founding methods as per SABS 0161-1980 (as amended 1984, 1985 and 1986). Foundations placed on unfavourably dipping bedrock must be dowelled at regular intervals.
2. Modified normal construction techniques - reinforced strip footings, wide strip footings, articulation joints, light reinforcing in masonry, site drainage and plumbing precautions<sup>7</sup>. Construct walls independent of the floors.
3. Compaction of *insitu* soils below individual footings - remove *in situ* soils to 1.5B (single storey) and 2B (double storey) - B = maximum footing width - and over a width of 1.5B before backfilling the excavation with suitable inert material in controlled layers; controlled layers must be a maximum of 150mm thick and compacted to a minimum of 93% Modified AASHTO density at -1 to +2% of optimum moisture content<sup>7</sup>. Backfill material must comprise a minimum of a G7 material; alternatively, it may be possible to stabilize the *in situ* soils, e.g. for PI's greater than 15, but less than 25, the soils could be stabilized with 3 to 5% lime.
4. Deep strip footings - found on competent horizon below the potentially problematical horizon. Construct walls independent of the floors.
5. Soil raft - remove *in situ* soils to 1.0m beyond the perimeter of the structure and to a depth of 1.5B (single storey) and 2B (double storey), or to competent material, before backfilling the excavation with suitable imported inert material - minimum of a G7 in terms of TRH 14 - in controlled layers as per Note 3; normal construction with site drainage requirements<sup>7</sup>.
6. Split construction - combination of reinforced brickwork, blockwork and full movement joints with suspended floors or reinforced slabs acting independently from the structure. Good site drainage and plumbing precautions<sup>7</sup>.
7. Stiffened or cellular raft - stiffened or cellular raft with articulation joints or solid light reinforced masonry; good site drainage and plumbing precautions<sup>7</sup>.
8. Dynamic compaction - directly engineer *insitu* material.
9. Piled foundations using end-bearing or displacement type piles; floors to be suspended.  
(*FOUNDING COSTS GENERALLY INCREASE FROM 1 - 9*).

**Comments:** \* = subject to confirmatory percolation tests; + = subject to confirmatory laboratory tests; b/l = beyond limit of present investigation; n/a = not applicable; N/A = not available; \*\* = for less than 10mm of settlement for a typical soil profile; ++ = for conventional strip footings founded at 0.6m and underlain by a typical soil profile.  
**Additional comments on abbreviated soil profile:** / = overlying; \_ = horizon may contain potentially expansive clays; ( ) = horizons in brackets may be present locally; TSMO = transported soils of mixed origin.





General Notes

- LEGEND**
- 2 ■ Profile position and number
  - Township boundary
  - - - Geotechnical /soil boundary
  - 1:100 Year floodline
  - (B1) Zone designation
  - (••••) Position of sandstone (...) outcrops recorded during the fieldwork

**Zone Classification**  
 A - Ideal.  
 B - Minor constraints.  
 C - More serious constraints.  
 D - No development recommended.

**Notes:**  
 1 Detailed investigations required for all new structures.  
 2.Pit/Profile positions have not been surveyed.  
 3.Soil boundaries to be confirmed in the field.  
 4.Layout and basemap provided by Messrs Sisonke Development Planners.  
 5.1:100 Year flood-line provided by Messrs Consolv Consulting Engineers.  
 6.Areas of buried fill should not be discounted.

No.	Revision/Issue	Date

Firm Name and Address

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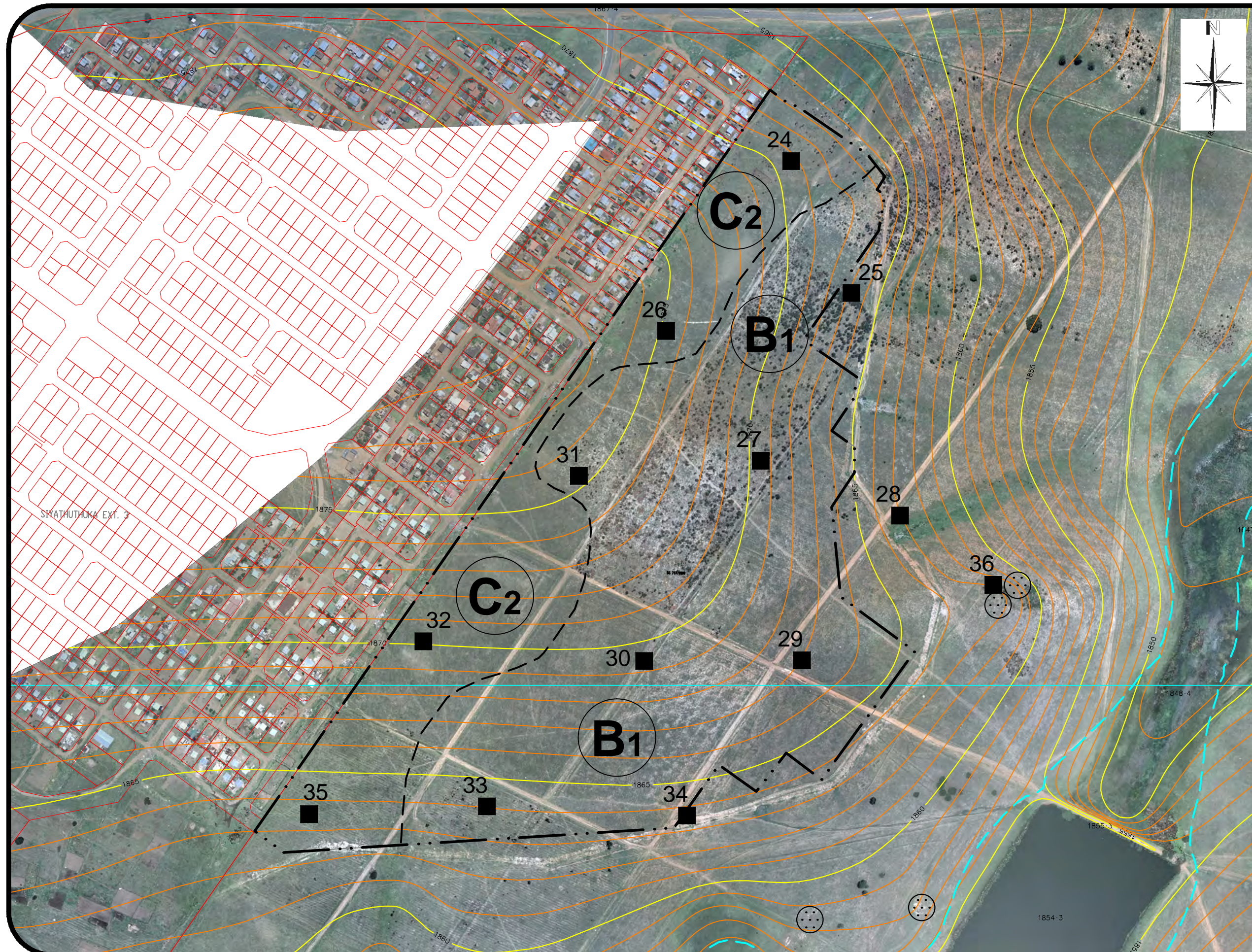
Project Name and Address

**Siyathuthuka Extension 5**

Sisonke Development Planners

Project <b>999</b>	Sheet
Date <b>March 2012</b>	<b>FIGURE 2</b>
Scale <b>1:6 000 (A3)</b>	





General Notes

- LEGEND**
- 2 ■ Profile position and number
  - !- Township boundary
  - - - Geotechnical /soil boundary
  - 1:100 Year floodline
  - (B<sub>1</sub>) Zone designation
  - (••••) Position of sandstone (...) outcrops recorded during the fieldwork

**Zone Classification**  
 A - Ideal.  
 B - Minor constraints.  
 C - More serious constraints.  
 D - No development recommended.

**Notes:**  
 1. Detailed investigations required for all new structures.  
 2. Pit/Profile positions have not been surveyed.  
 3. Soil boundaries to be confirmed in the field.  
 4. Layout and basemap provided by Messrs Sisonke Development Planners.  
 5. 1:100 Year flood-line provided by Messrs Consolv Consulting Engineers.  
 6. Areas of buried fill should not be discounted.

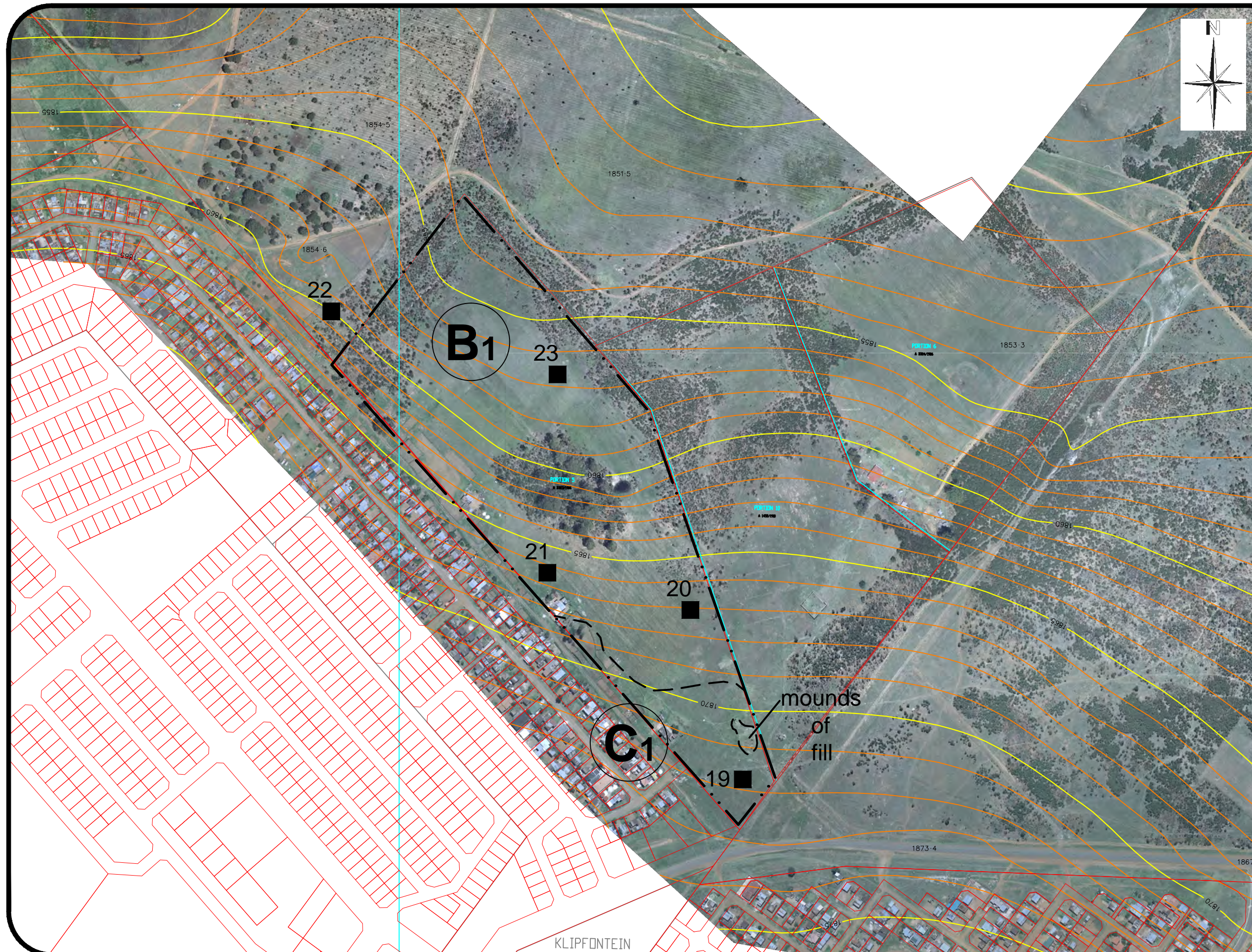
No.	Revision/Issue	Date

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**Siyathuthuka Extensions 6 and 8**  
 Sisonke Development Planners

Project <b>999</b>	Sheet
Date <b>March 2012</b>	<b>FIGURE 3</b>
Scale <b>1 : 4 000 (A3)</b>	





General Notes

**LEGEND**

- 2 ■ Profile position and number
- Township boundary
- - - Geotechnical /soil boundary
- 1:100 Year floodline
- (B1) Zone designation
- ⊙ Position of sandstone (...) outcrops recorded during the fieldwork

**Zone Classification**  
 A - Ideal.  
 B - Minor constraints.  
 C - More serious constraints.  
 D - No development recommended.

**Notes:**  
 1. Detailed investigations required for all new structures.  
 2. Pit/Profile positions have not been surveyed.  
 3. Soil boundaries to be confirmed in the field.  
 4. Layout and basemap provided by Messrs Sisonke Development Planners.  
 5. 1:100 Year flood-line provided by Messrs Consolv Consulting Engineers.  
 6. Areas of buried fill should not be discounted.

No.	Revision/Issue	Date

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**Siyathuthuka Extensions 7**

Sisonke Development Planners

Project <b>999</b>	Sheet
Date <b>March 2012</b>	<b>FIGURE 4</b>
Scale <b>1 : 4 000 (A3)</b>	



**APPENDIX B**  
**SOIL PROFILES**

## SOIL DESCRIPTIVE TERMS

**Descriptive Order** - 1 Moisture 2 Colour 3 Consistency 4 Soil Structure 5 Soil Type 6 Origin

1. MOISTURE CONDITION - assessment of insitu conditions	
Dry	No water detectable; sample cannot be moulded
Slightly Moist	Water just discernable; sample can be moulded
Moist	Water easily discernable
Very Moist	Water can be squeezed out
Wet	Generally below the water table

2. COLOUR - described in profile, at natural moisture content unless otherwise specified	
Speckled	Very small patches of colour < 2mm
Mottled	Irregular patches of colour 2 - 6mm
Blotched	Large irregular patches 6-20mm
Banded	Approximately parallel bands of varying colour
Streaked	Randomly orientated streaks of colour
Stained	Local colour variations; associated with discontinuity surfaces

3(a) CONSISTENCY: GRANULAR SOILS - measure of the hardness or denseness of a soil			
SPT "N"	GRAVELS & clean SANDS Generally free draining soils		Typical Dry Density(kg/m <sup>3</sup> )
< 4	Very Loose	Crumbles very easily when scraped with geological pick	< 1450
4 - 10	Loose	Small resistance to penetration by sharp geological pick	1451 - 1600
>10 - 30	Medium dense	Considerable resistance to penetration by sharp end of geological point	1601 - 1750
>30 - 50	Dense	Very high resistance to penetration by sharp end of geological pick; requires many blows of pick for excavation	1751 - 1925
> 50	Very Dense	High resistance to repeated blows of geological pick; requires power tools for excavation	> 1925

3(b) CONSISTENCY: COHESIVE SOILS - measure of the hardness or denseness of a soil			
SPT "N"	SILTS and CLAYS and combinations thereof with SANDS Generally slow draining soils (N = 0 material)		UCS (kPa)
<2	Very soft	Pick point can easily be pushed in to shaft of handle; easily moulded by fingers	< 50
2 - 4	Soft	Pick point can easily be pushed in 30 - 40 mm; moulded by fingers with some pressure; easily penetrated by thumb	50 - 125
5 - 8	Firm	Pick point penetrates up to 10mm; very difficult to mould with fingers; indented by thumb with effort; can just be penetrated with an ordinary hand spade	126 - 250
9 - 15	Stiff	Slight indentation produced by pushing pick point into soil; cannot be moulded by fingers; penetrated by thumb nail; requires hand pick for excavation	251 - 500
16 - 20	Very Stiff	Slight indentation produced by blow of pick point; requires power tools for excavation; indented by thumb nail with difficulty	501 - 1000

4 SOIL STRUCTURE - presence or absence of fissures or other planes of weakness	
Intact	Structureless, no discontinuities identified
Fissured	Soil contains discontinuities which may be open or closed, stained or unstained and of variable origin
Slickensided	Contains highly polished shear surfaces, glossy and often striated
Shattered	Very closely to extremely closely spaced continuities resulting in gravel size soil fragments which are usually stiff to very stiff and difficult to break down
Micro-shattered	As above, but sand-sized fragments
Controlled / uncontrolled	Descriptive term for fill material; relates to whether the material has been engineered, i e controlled, or not, i e uncontrolled
Open textured	Contains small voids between individual grains-visible to the naked eye Alt pinholed
Stratified	Parallel bedding planes Laminated if layers are less than 20mm thick
Varved	Alternating silty and clayey layers
Foliated	Residual metamorphic texture

5. SOIL TYPE - soil texture described on the basis of the grain size of particles			
SOIL TYPE	PARTICLE SIZE [mm]	REMARKS	
CLAY	< 0 002	Feels sticky; soils hands; shiny when wet	
SILT	0 002 - 0 06	Dilatant; dusts off once dry; chalky feel on teeth	
SAND	fine medium coarse	0 06 -0 02 0 2 - 0 6 0 6 - 2 0	Gritty on teeth Visible to naked eye Visible to naked eye
GRAVEL	fine medium coarse	2 - 6 6 - 20 20 - 60	Observed with the naked eye <b>Matrix-supported</b> - clasts supported by matrix <b>Clast-supported</b> - clasts touching (matrix may or may not be present)
COBBLES	60 - 200		
BOULDERS	>200		

**Fine grained soils:** slightly <5%; clayey/silty 5-15%; very silty/clayey 15-35%  
**Gravels / cobbles and boulders:** occasional <5%, scattered 5-20%, numerous 20-45%; abundant >45%

6. ORIGIN - origination of particular soil horizon	
Transported	Alluvium, hillwash, talus, colluvium etc
Residual	Weathered from parent rock
Pedocretes	Ferricrete, calcrete, laterite, silcrete, dorbank etc

DEGREE OF CEMENTATION OF PEDOCRETES			UCS (MPa)
Very weakly cemented	Some material can be crumbled between finger and thumb; disintegrates under knife blade to friable state		0 1 - 0 5
Weakly cemented	Cannot be crumbled with fingers; some material can be crumbled by strong pressure between thumb and hard surface; under light hammer blows disintegrates to a friable state		0 5 - 2 0
Cemented	Material crumbles under firm blows of sharp pick point; grains can be dislodged with some difficulty by a knife blade		2 - 5
Strongly cemented	Firm blows of sharp pick point on hand held specimen show 1 - 3 mm indentations; grains cannot be dislodged by knife blade		5 - 10
Hardpan	Hand held specimen can be broken by single firm blow of hammer head; similar appearance to concrete		10 - 25

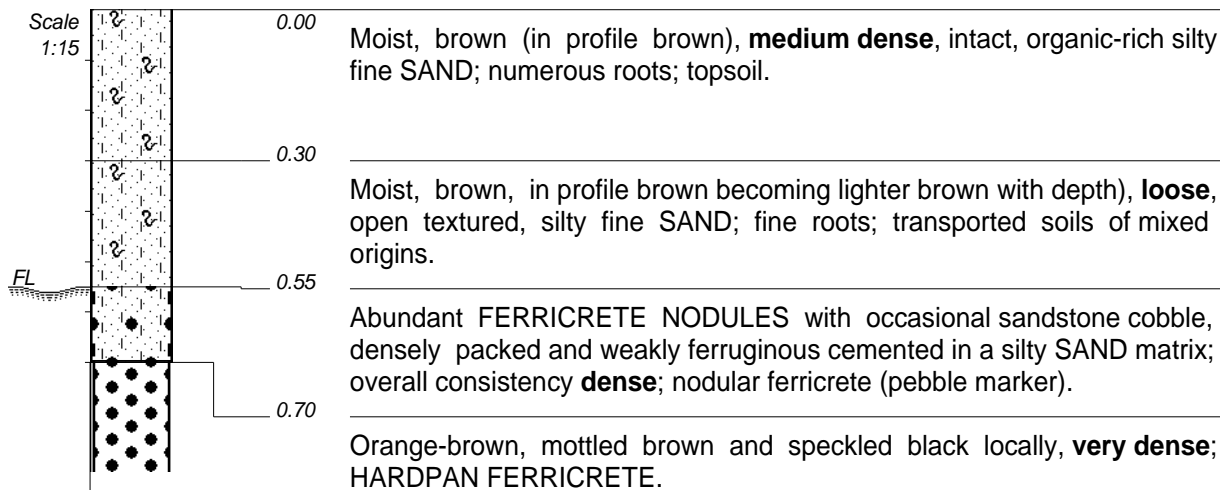
**Reference:** Guide to soil profiling for Civil Engineering Purposes - Geoterminology Workshop (1990) SAIEG - AEG - SAICE (Geotechnical Division)

## ROCK DESCRIPTIVE TERMS

Description for rocks masses: A - description of rock B - description of discontinuities C - description of fracture filling

A. ROCK DESCRIPTION		Descriptive Order for rock description: 1 Colour 2 Weathering 3 Texture 4 Fracture and microtexture 5 Rock hardness 6 Rock type					
1. Colour	Described wet						
<b>2. Weathering</b>							
Degree of Weathering	Extent of Discolouration	Fracture Condition	Surface Characteristics	Original Fabric	Grain Boundary Condition		
Unweathered	No visible alteration	Closed or stained	Unchanged	Preserved	Tight		
Slightly weathered	Fractures stained or discoloured < 20% of fracture spacing on both sides of fracture	Discoloured, may contain thin filling	Partial discolouration Often unweathered rock colour	Preserved	Tight		
Moderately weathered	Staining or discolouration extends >20% of fracture spacing on both sides of fracture	Discoloured, may contain thick filling	Partial to complete discolouration Not friable except poorly cemented rocks	Preserved	Partial opening		
Highly weathered	Extends throughout the rock	-----	Friable and usually pitted	Mainly preserved	Partial separated		
Completely weathered	Totally discoloured	-----	Resembles a soil	Partially preserved	Complete separation of grains		
<b>3. Texture</b>			<b>4. Microstructure and fracture spacing</b>				
Classification	Size	Recognition	Separation	Spacing (foliation, cleavage, bedding, etc.)	Spacing (fractures, joints, etc.)	Fracture spacings/metre	
Very fine grained	< 0,2	Individual grains cannot be seen with a hand lens	< 6	very intensely	Very highly	> 50	
Fine grained	0,2 - 0,6	Just visible as individual grains under hand lens	6 - 20	intensely			
Medium grained	0,6 - 2,0	Grains clearly visible under hand lens, just visible to the naked eye	20 - 60	very thinly	Highly	5 - 50	
Coarse grained	2 - 6	Grains clearly visible to the naked eye	60 - 200	thinly			
Very coarse grained	> 6	Grains measurable	200 - 600	medium	Moderately	~1 - 5	
			600 - 2 000	thickly	Slightly	~ 1	
			> 2 000	very thickly	Very Slightly	< 1	
<b>5. Rock Hardness</b>							
Hardness	Description	UCS (MPa)	Hardness	Description	UCS (MPa)		
Very soft rock	Material crumbles under firm blow with geological pick point; can be peeled with a knife; too hard to cut undisturbed sample by hand	1 - 3	Hard rock	Breaks with difficulty, rings when struck Point load or laboratory test results necessary to distinguish between categories	25 - 70		
Soft rock	Can just be scraped and peeled with a knife; 1-3mm indents with firm blow of geological pick	3 - 10	Very hard rock		70 - 200		
Medium hard rock	Firm blows of pick head will break hand held specimen Cannot be scraped or peeled with a knife	10 - 25	Extremely hard rock		> 200		
6. Rock Type	According to accepted lithographic terminology						
<b>B. DISCONTINUITY SURFACE DESCRIPTION:</b>			Descriptive Order for joint description: 1 Type 2 Separation 3 Fill material 4 Roughness 5 Orientation				
1. Type	Bedding planes, flow banding, foliation, joints, shears, faults, fractures						
<b>2. Separation</b>		<b>3. Fracture filling</b>		<b>4. Roughness of discontinuity planes</b>			
Description	Separation	Description	Definition	Classification	Description		
Closed	0	Clean	No fracture filling material	Smooth	Appears smooth and is essentially smooth to the touch May be slickensided		
Very narrow	0 - 0,6	Stained	Colouration of rock only No recognisable filling	Slightly rough	Asperities on the fracture surface are visible and can be distinctly felt		
Narrow	0,6 - 2,0	Filled	Recognisable filling material	Medium rough	Asperities are clearly visible and fracture surface feels abrasive		
Wide	2,0 - 6,0			Rough	Large angular asperities can be seen Some ridge and high side angle steps are evident		
Very wide	6,0 - 20			Very rough	Near vertical steps and ridges occur on the fracture surface		
<b>5. Discontinuity orientation</b>		Discontinuity inclinations (i.e. of joints, bedding, faults, etc.) are measured with respect to the horizontal i.e. a vertical joint dips at 90° in orientated core the fracture inclinations are w.r.t. the core axis					
<b>C. FRACTURE FILLING DESCRIPTION</b>		Fracture filling should be described in terms of the MCCSSO Soil Classification					

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

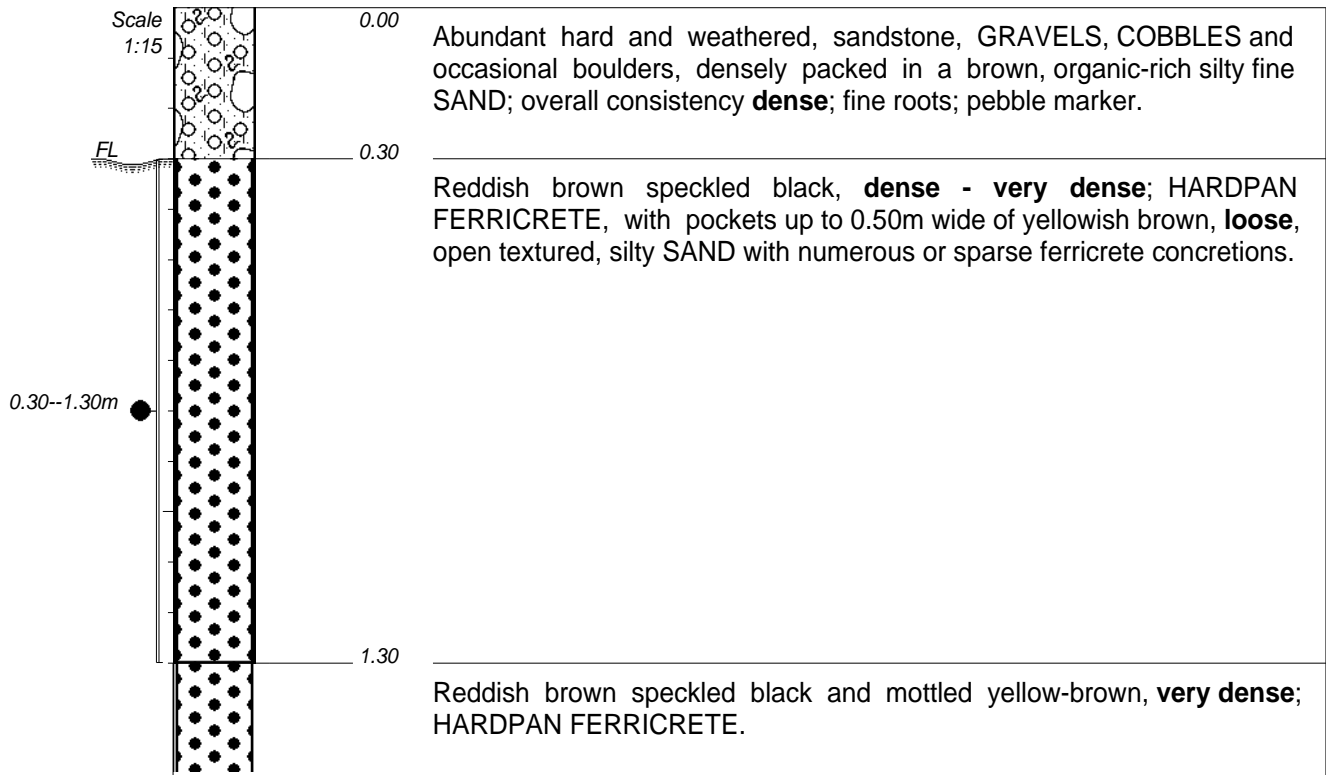
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) No samples taken.
- 4) Worked out borrow pit downslope suggests the ferricrete was exploited previously for road building material.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

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 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
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ELEVATION :  
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 COORD-E/y : -098 452

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

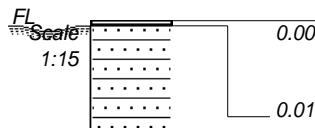
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 0.30--1.30m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
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 COORD-E/y : -098 219

**SIYATHUTHUKA EXTENSIONS  
5, 6, 7 AND 8, MPUMALANGA**



White, slightly weathered, medium grained, highly fractured, **very hard rock**; SANDSTONE - ripple-marked with a low dip to the west.

NOTES

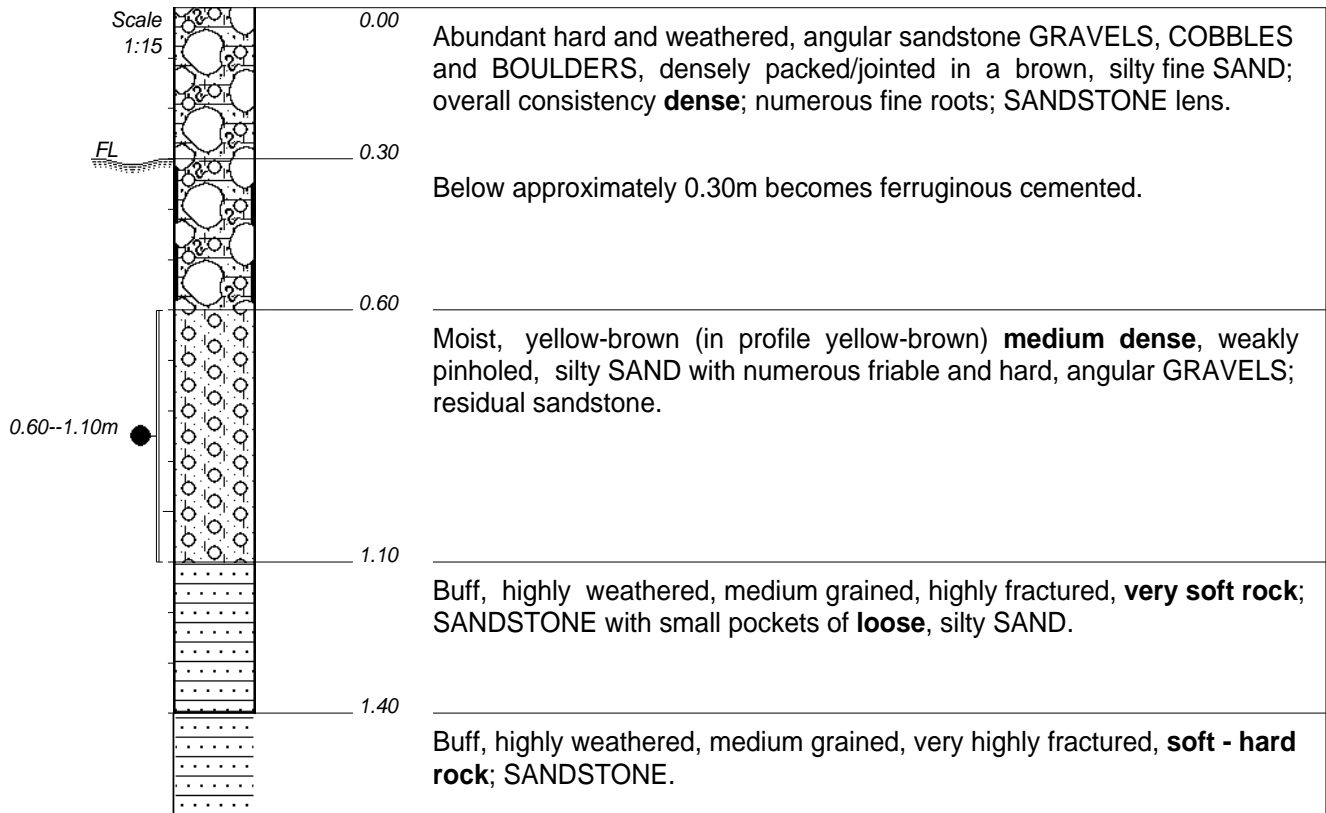
- 1) Profile recorded on sub-outcropping SANDSTONE, with pockets of surficial coarse colluvium - typical of the area.
- 2) No evidence of groundwater seepage.
- 3) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
MACHINE : Bell 315S  
DRILLED BY :  
PROFILED BY : H. Schurink, Pr.Sci.Nat.  
TYPE SET BY :  
SETUP FILE : STANDARD.SET

INCLINATION :  
DIAM :  
DATE :  
DATE : 7 February 2012  
DATE : 22/03/2012 14:46  
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ELEVATION :  
COORD-S/x : 2 841 503  
COORD-E/y : -097 957

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

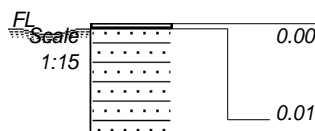
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 0.60--1.10m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 449  
 COORD-E/y : -097 831

**SIYATHUTHUKA EXTENSIONS  
5, 6, 7 AND 8, MPUMALANGA**



White, slightly weathered, medium grained, highly fractured, **very hard rock**; SANDSTONE. (Dips at low angle to the west).

NOTES

- 1) Profile recorded on sub-outcropping SANDSTONE, with pockets of surficial coarse colluvium - typical of the area.
- 2) No evidence of groundwater seepage.
- 3) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

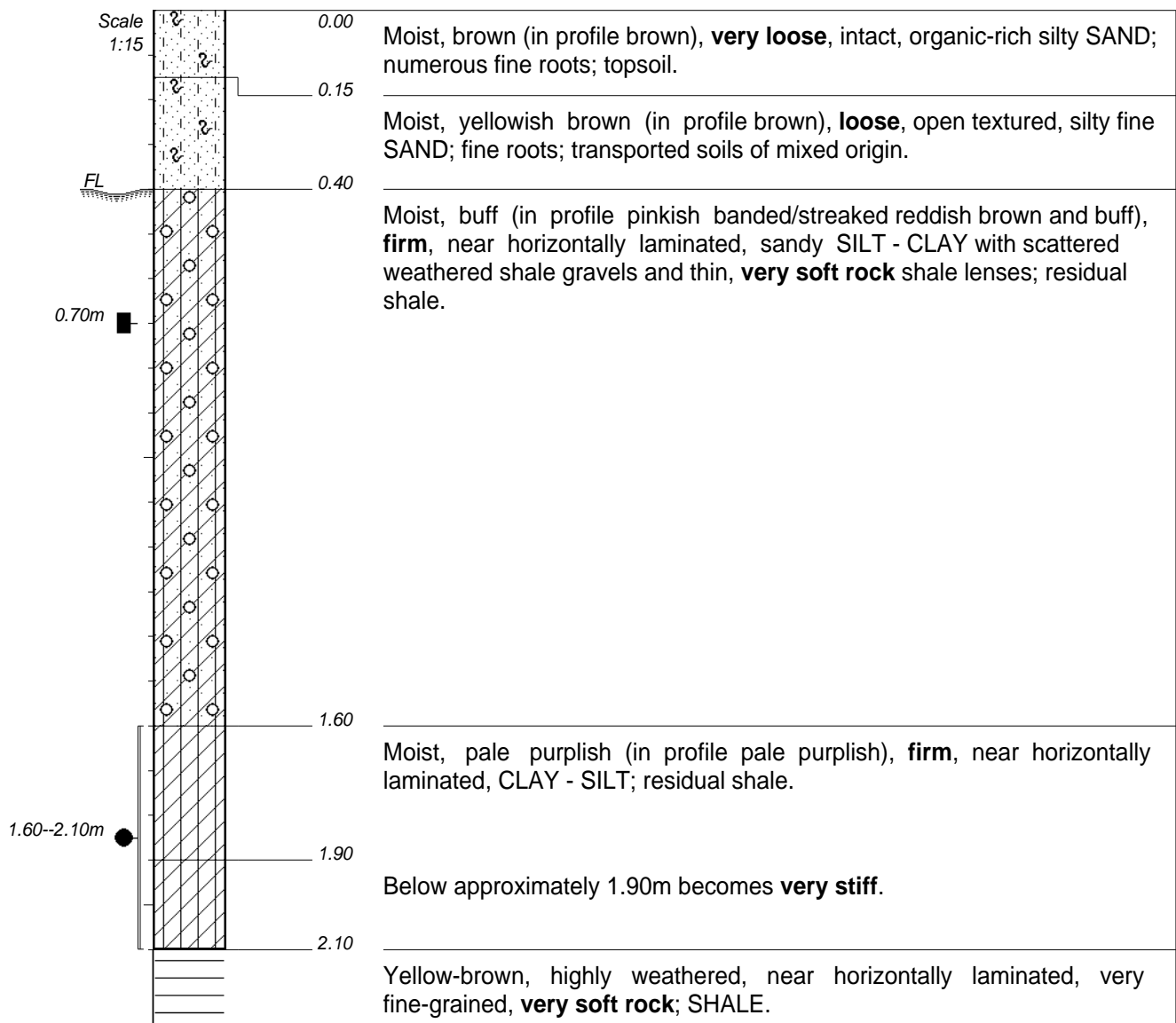
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DRILLED BY :  
PROFILED BY : H. Schurink, Pr.Sci.Nat.  
TYPE SET BY :  
SETUP FILE : STANDARD.SET

INCLINATION :  
DIAM :  
DATE :  
DATE : 7 February 2012  
DATE : 22/03/2012 14:46  
TEXT : ..000\network\testpits.txt

ELEVATION :  
COORD-S/x : 2 841 335  
COORD-E/y : -097 968



**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

- 1) Pit excavated without refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 1.60--2.10m.
- 4) Undisturbed sample taken at 0.70m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

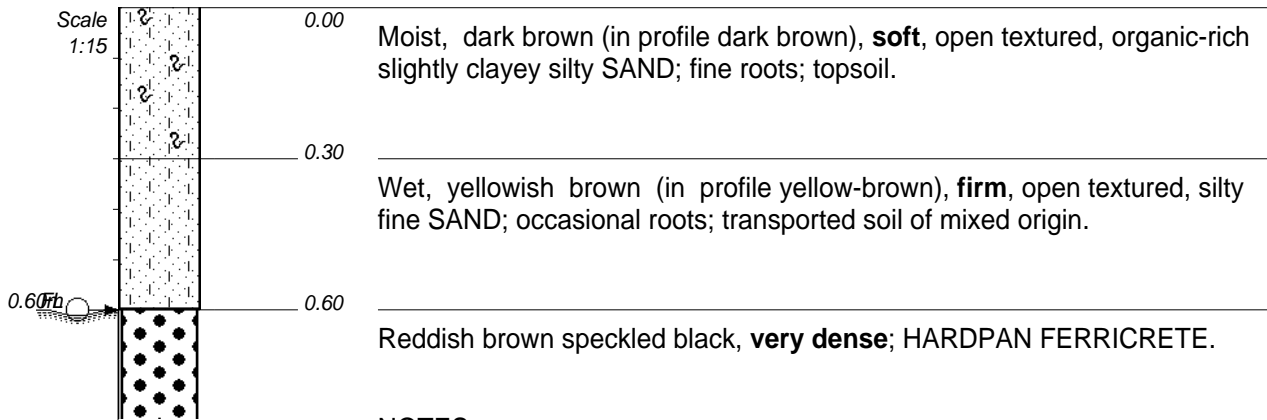
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 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 631  
 COORD-E/y : -098 310

**SIYATHUTHUKA EXTENSIONS  
5, 6, 7 AND 8, MPUMALANGA**

JOB NUMBER: 999



NOTES

- 1) Pit excavated to refusal.
- 2) Slow groundwater seepage at 0.60m.
- 3) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

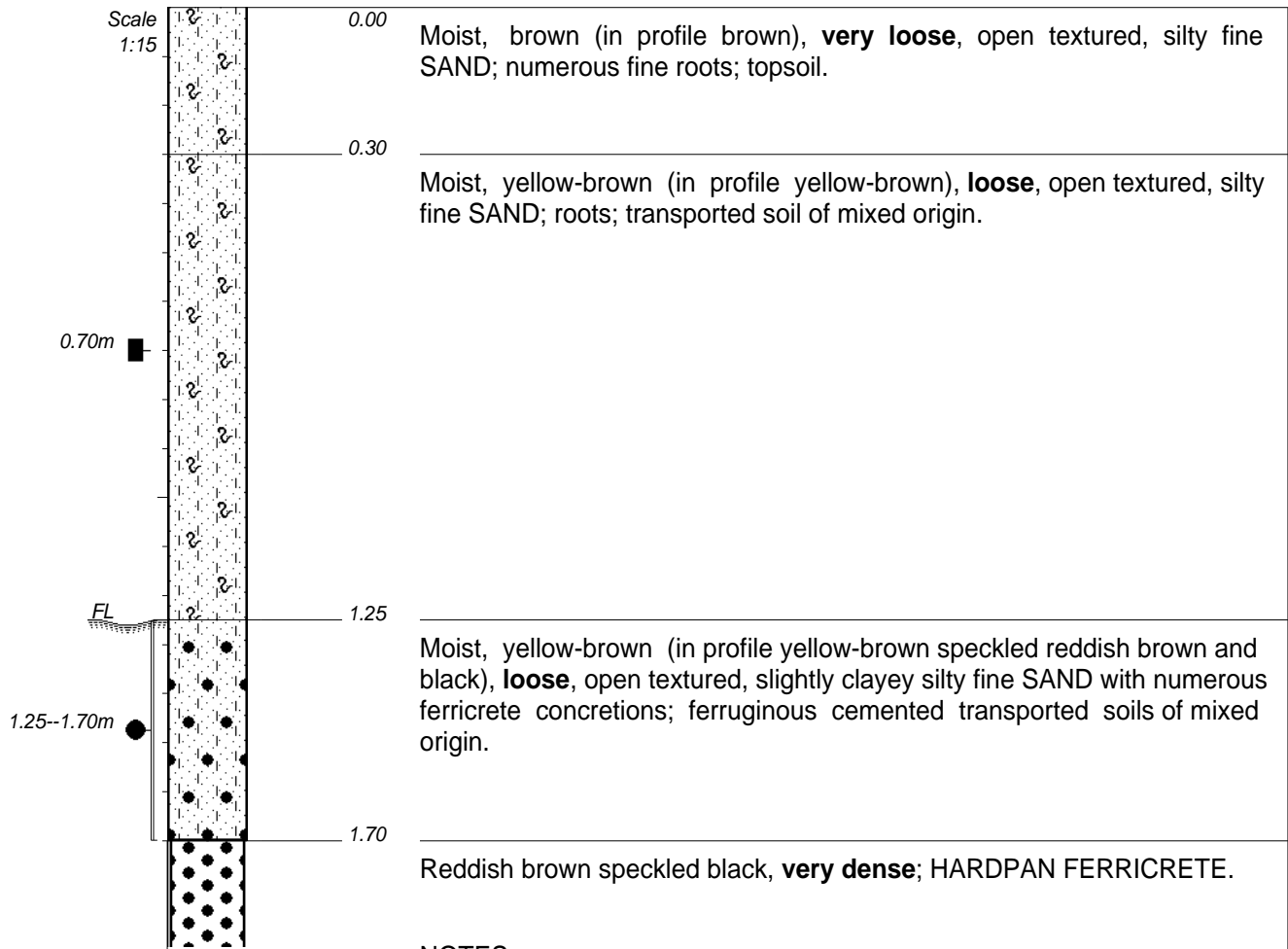
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DRILLED BY :  
PROFILED BY : H. Schurink, Pr.Sci.Nat.  
TYPE SET BY :  
SETUP FILE : STANDARD.SET

INCLINATION :  
DIAM :  
DATE :  
DATE : 7 February 2012  
DATE : 22/03/2012 14:46  
TEXT : ..000\network\testpits.txt

ELEVATION :  
COORD-S/x : 2 841 441  
COORD-E/y : -098 429

HOLE No: TP07  
Extension 5

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

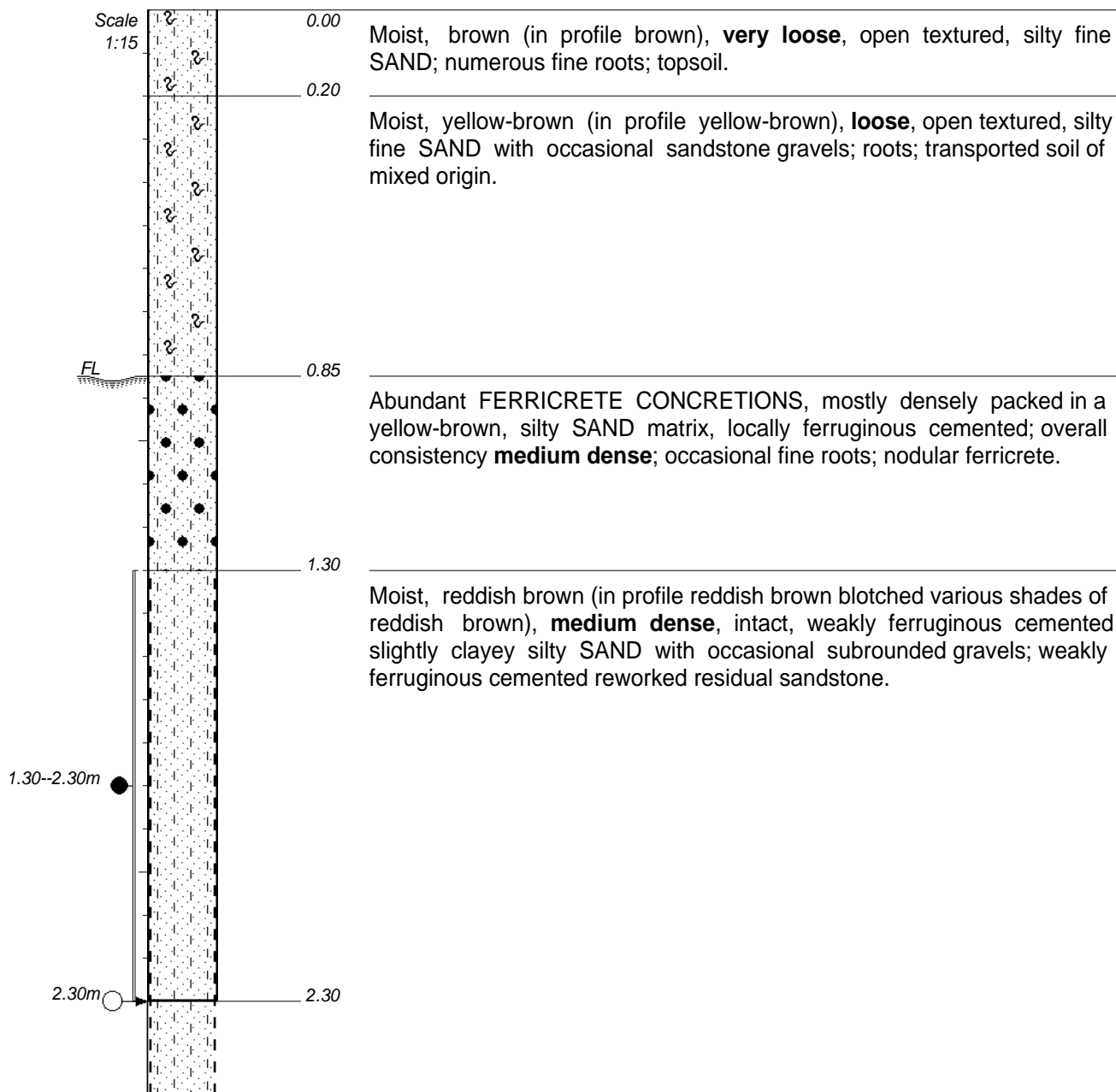
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 1.25--1.70m.
- 4) Undisturbed sample taken at 0.70m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
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 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
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ELEVATION :  
 COORD-S/x : 2 841 352  
 COORD-E/y : -098 639

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

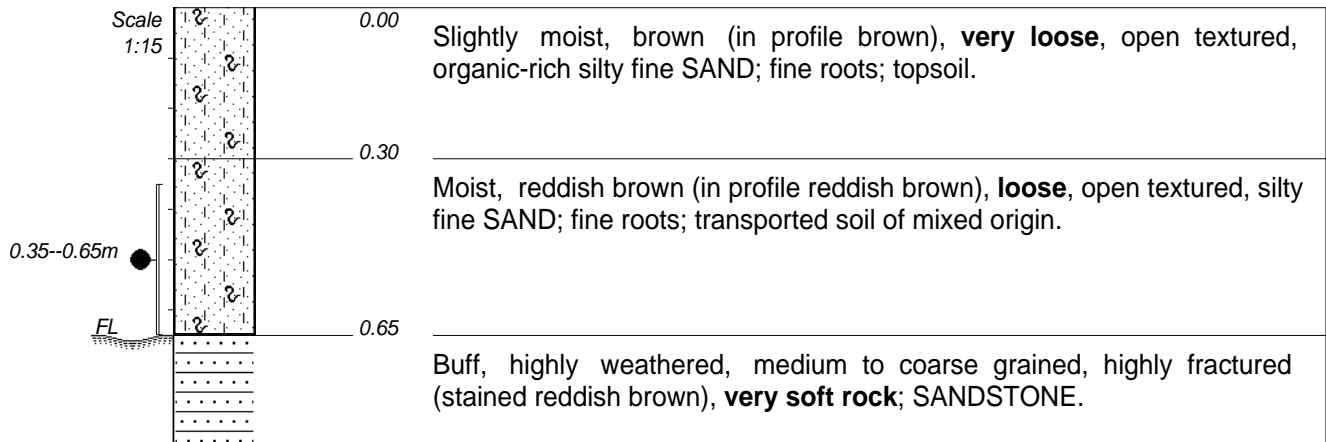
- 1) Pit excavated without refusal.
- 2) Slow groundwater seepage through the base of the pit.
- 3) Indicator sample taken at 1.30--2.30m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
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 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
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ELEVATION :  
 COORD-S/x : 2 841 524  
 COORD-E/y : -098 631

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

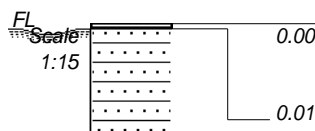
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 0.35--0.65m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
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 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
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ELEVATION :  
 COORD-S/x : 2 841 724  
 COORD-E/y : -098 627

**SIYATHUTHUKA EXTENSIONS  
5, 6, 7 AND 8, MPUMALANGA**



Pinkish, slightly weathered, medium to very coarse-grained, highly fractured, **hard rock**; SANDSTONE - (290/12).

**NOTES**

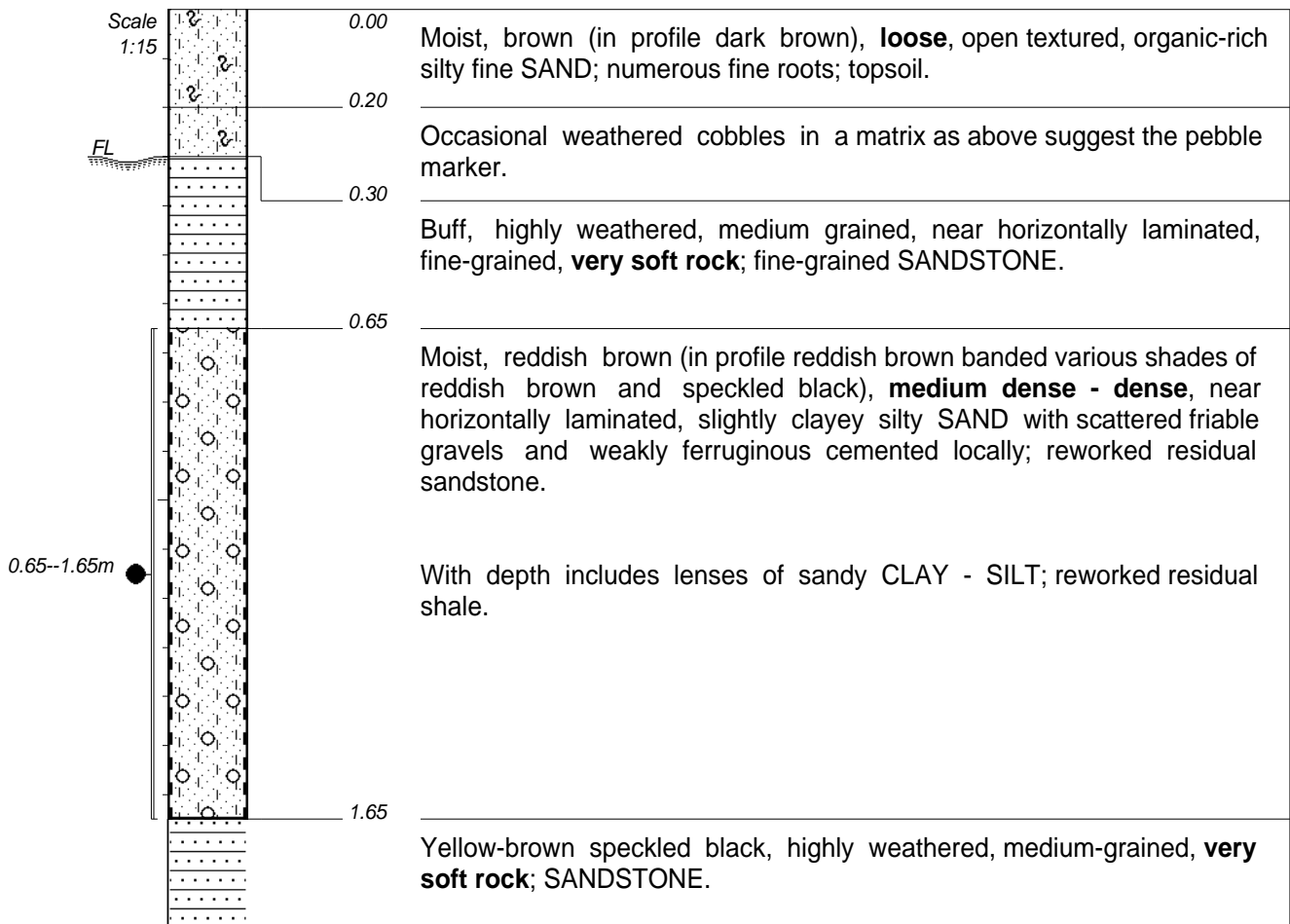
- 1) Profile recorded on sub-outcropping sandstone.
- 2) No evidence of groundwater seepage.
- 3) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
MACHINE : Bell 315S  
DRILLED BY :  
PROFILED BY : H. Schurink, Pr.Sci.Nat.  
TYPE SET BY :  
SETUP FILE : STANDARD.SET

INCLINATION :  
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DATE : 22/03/2012 14:46  
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ELEVATION :  
COORD-S/x : 2 841 773  
COORD-E/y : -098 749

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

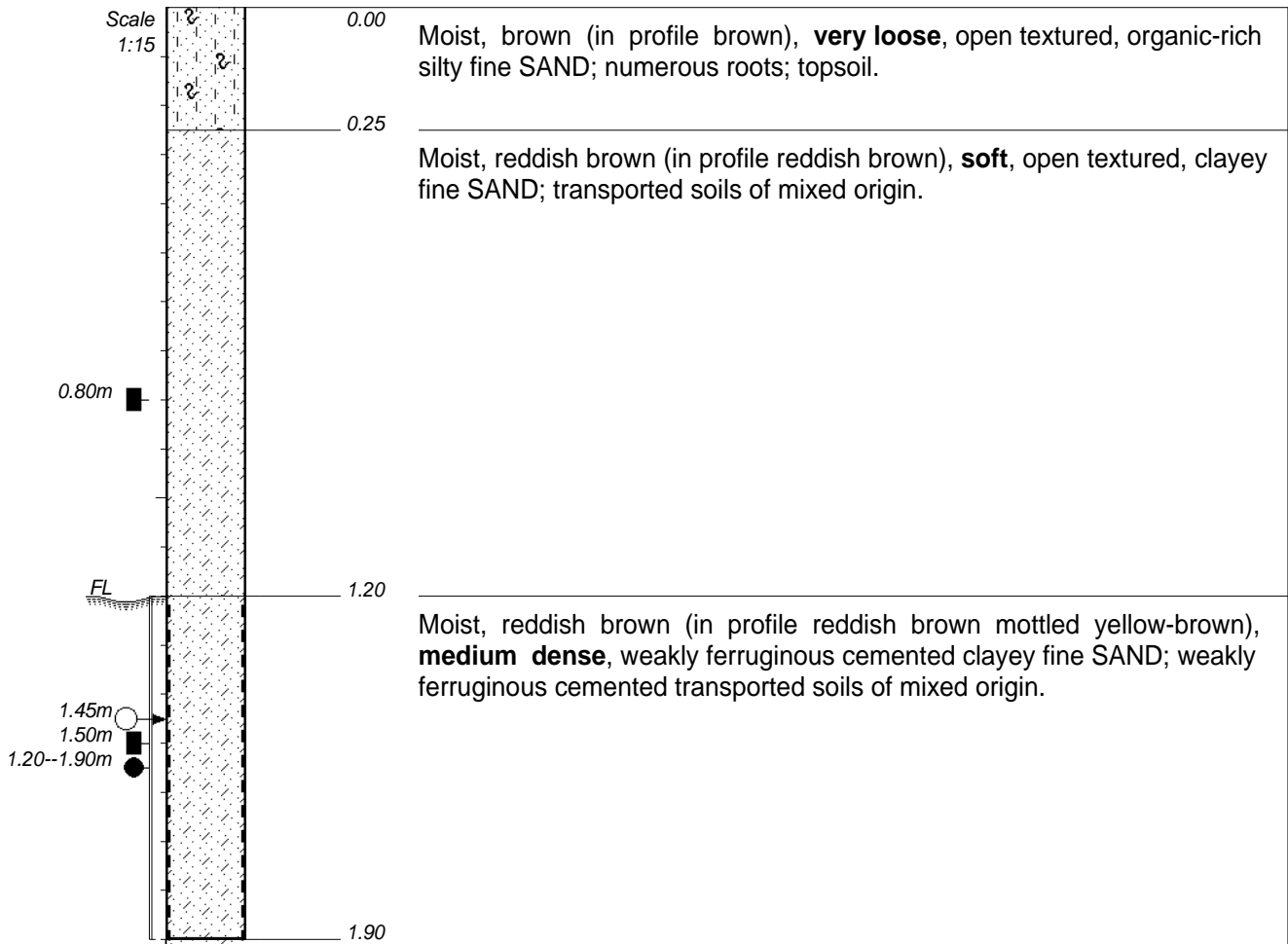
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 0.65--1.65m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
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 DATE : 22/03/2012 14:46  
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ELEVATION :  
 COORD-S/x : 2 841 778  
 COORD-E/y : -098 822

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

- 1) Pit excavated without refusal.
- 2) Strong groundwater seepage - piping - at 1.45m.
- 3) Indicator sample taken at 1.20--1.90m.
- 4) Undisturbed sample taken at 0.80m.
- 5) Lump sample taken at 1.50m.
- 6) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

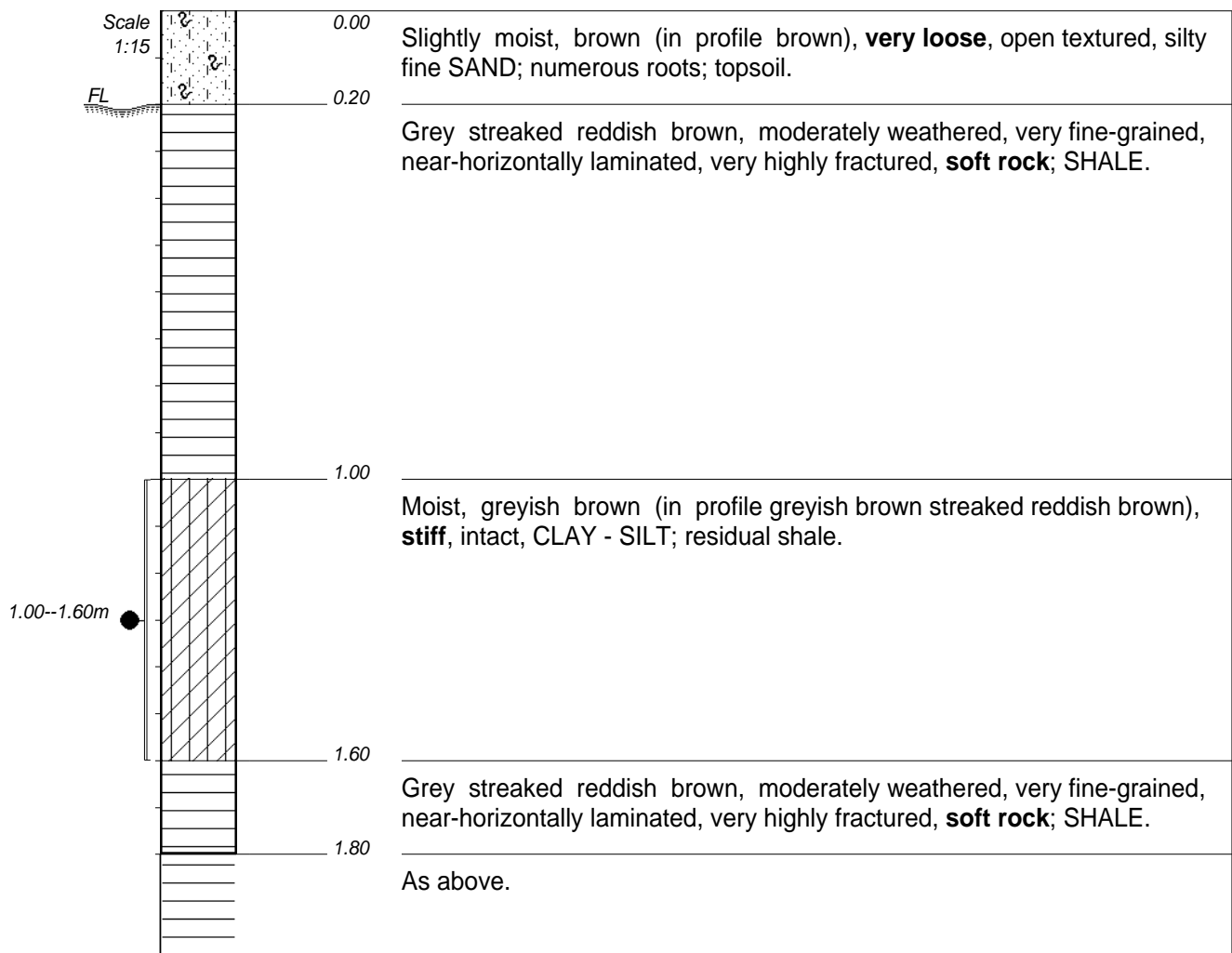
CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
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 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 675  
 COORD-E/y : -098 947



**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

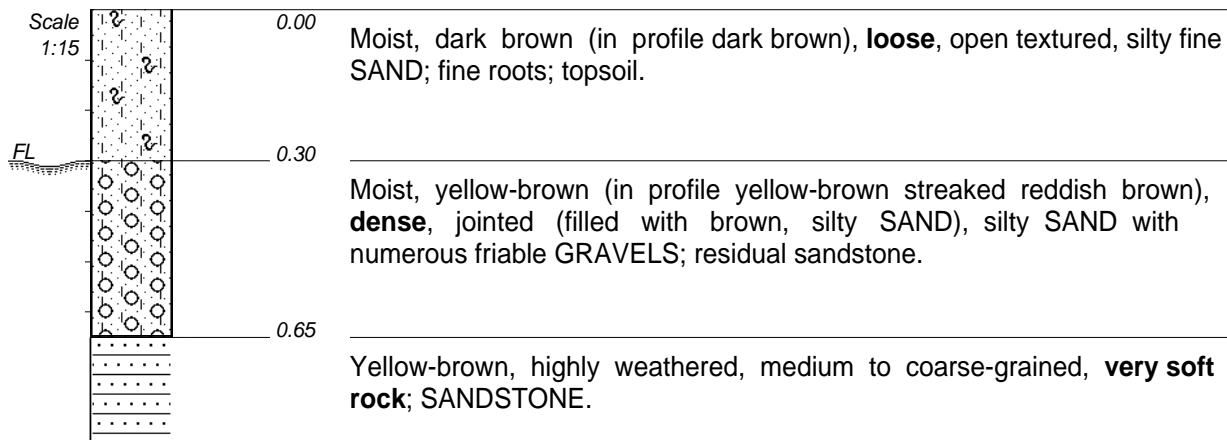
- 1) Pit excavated to refusal.
- 2) Slow groundwater seepage through the base of the pit.
- 3) Indicator sample taken at 1.00--1.60m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 643  
 COORD-E/y : -098 752

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

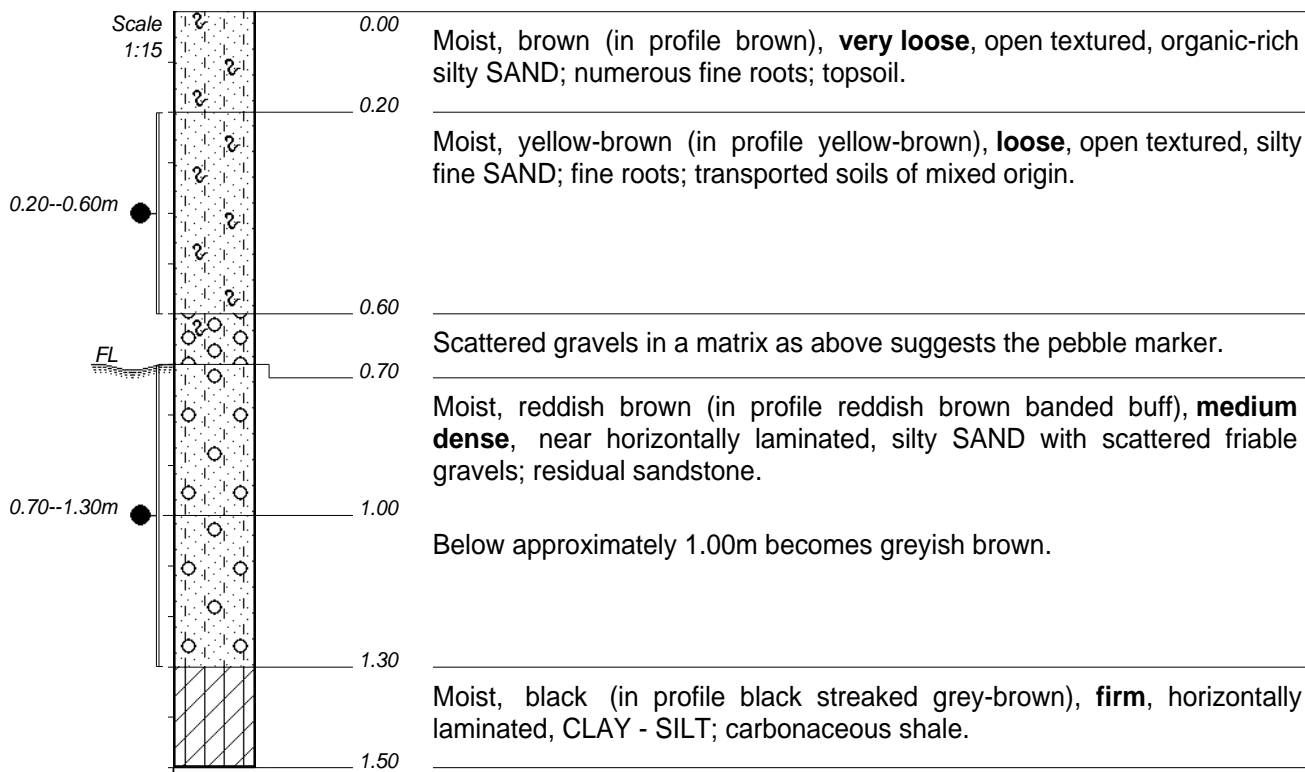
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 502  
 COORD-E/y : -098 00

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

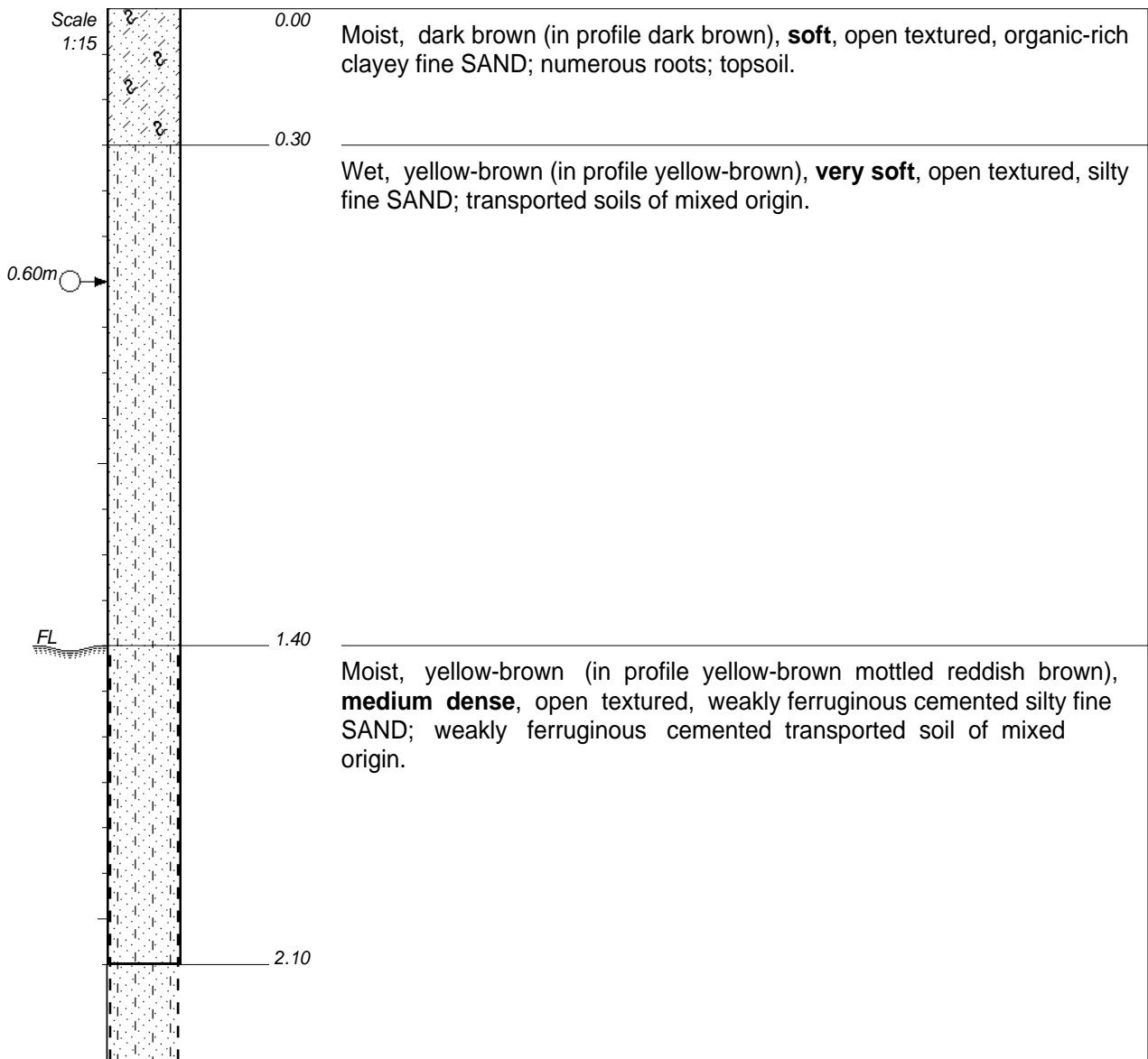
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator samples taken at 0.20--0.60m and 0.70--1.30m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
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 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 926  
 COORD-E/y : -099 241

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

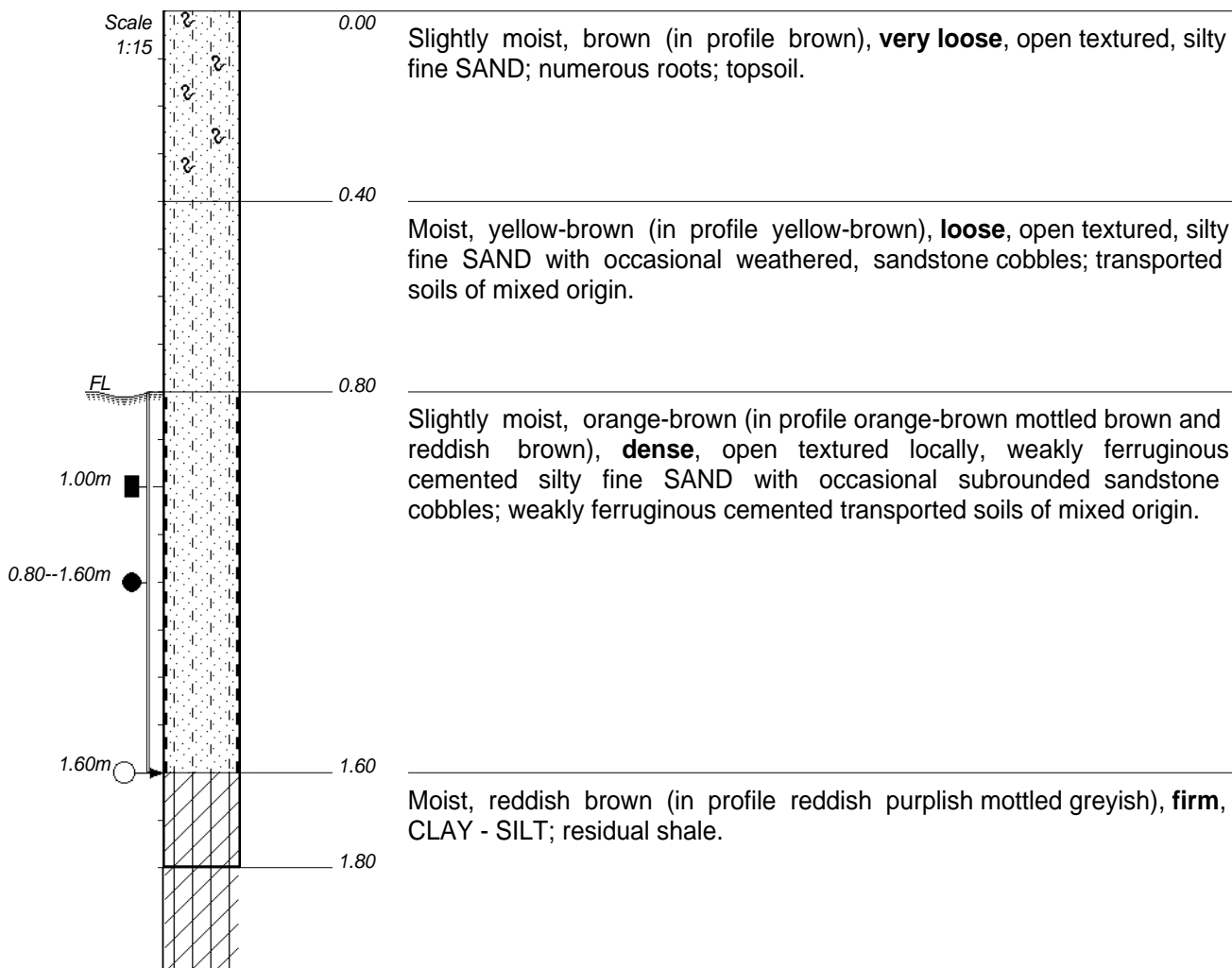
- 1) Pit excavated without refusal.
- 2) Slow groundwater seepage at 0.60m.
- 3) No samples taken.
- 4) Profiled from spoils owing to collapsing sidewalls, which made the pit unsafe.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 842 057  
 COORD-E/y : -099 327

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

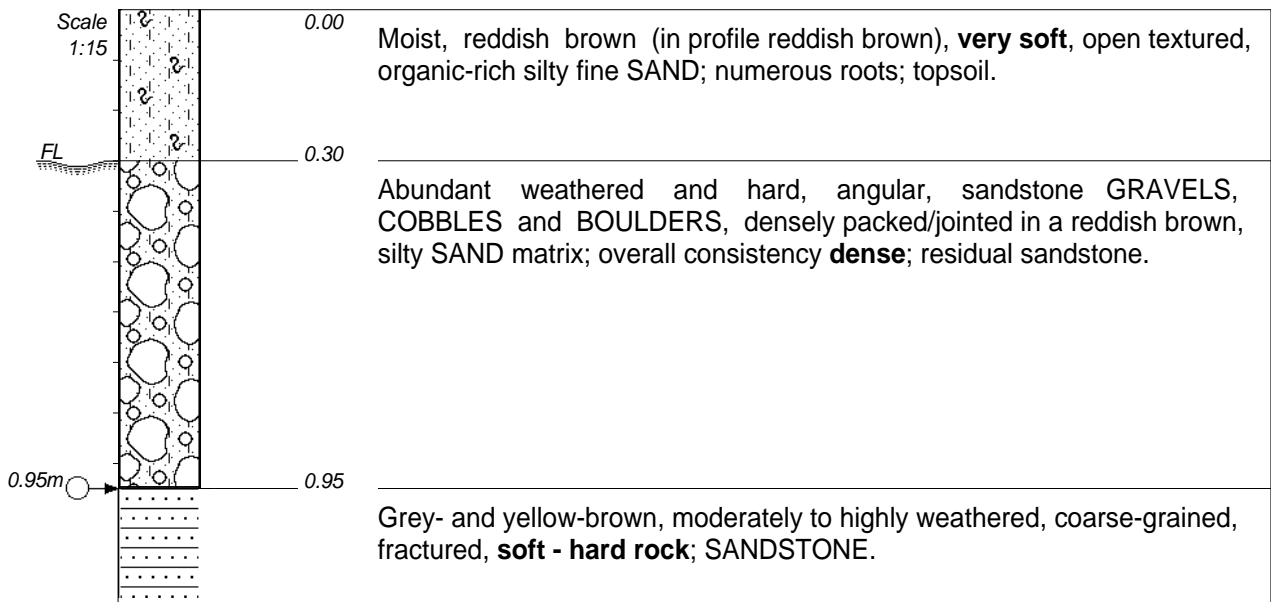
- 1) Pit excavated without refusal.
- 2) Slow groundwater seepage at 1.60m.
- 3) Indicator sample taken at 0.80--1.60m.
- 4) Undisturbed sample taken at 1.00m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
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ELEVATION :  
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 COORD-E/y : -099 048

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

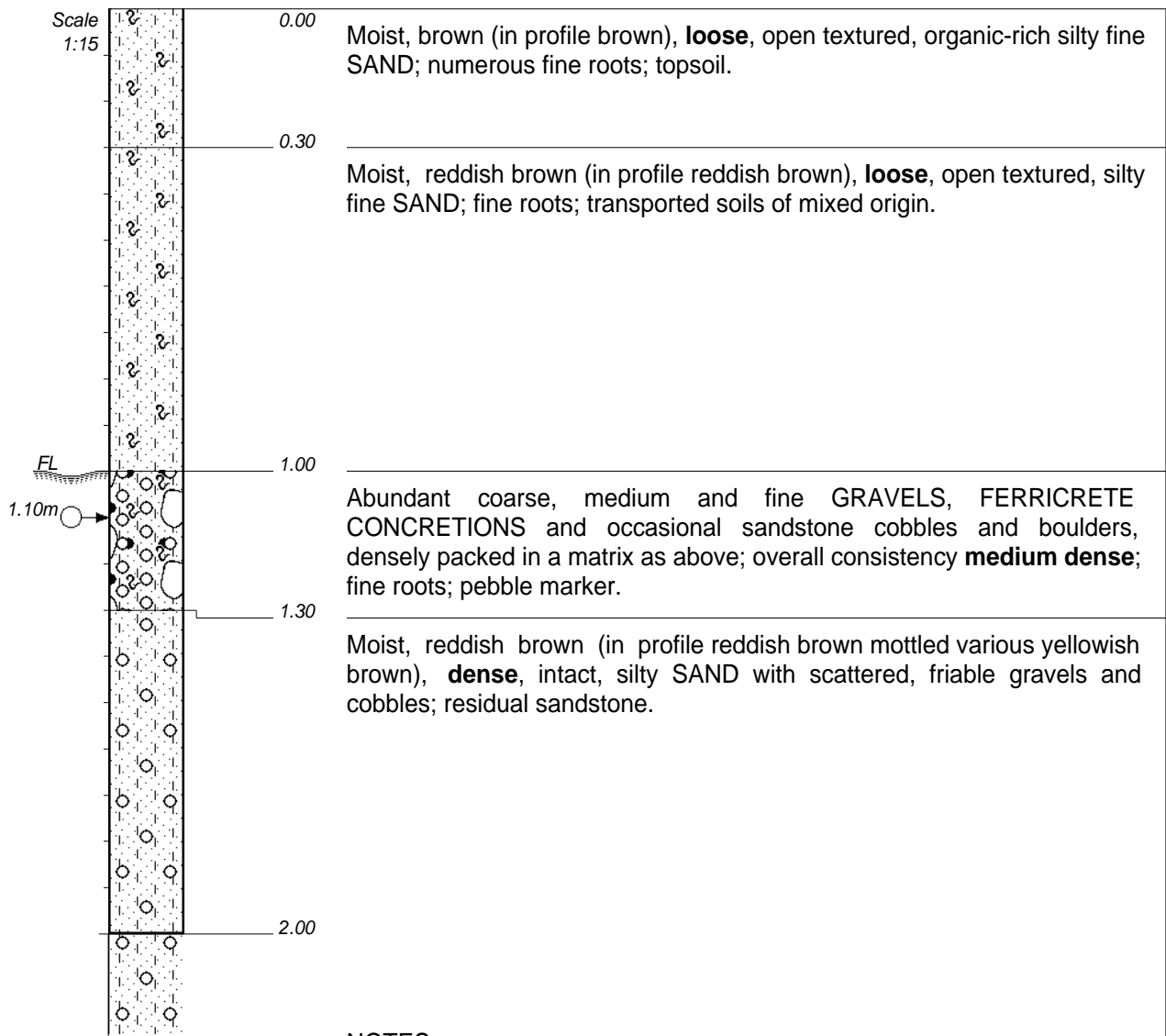
- 1) Pit excavated to refusal.
- 2) Depth to sandstone bedrock varies from 0.50 to 0.95m.
- 3) Slow groundwater seepage through the base of the pit.
- 4) No samples taken.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
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 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 178  
 COORD-E/y : -100 367

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

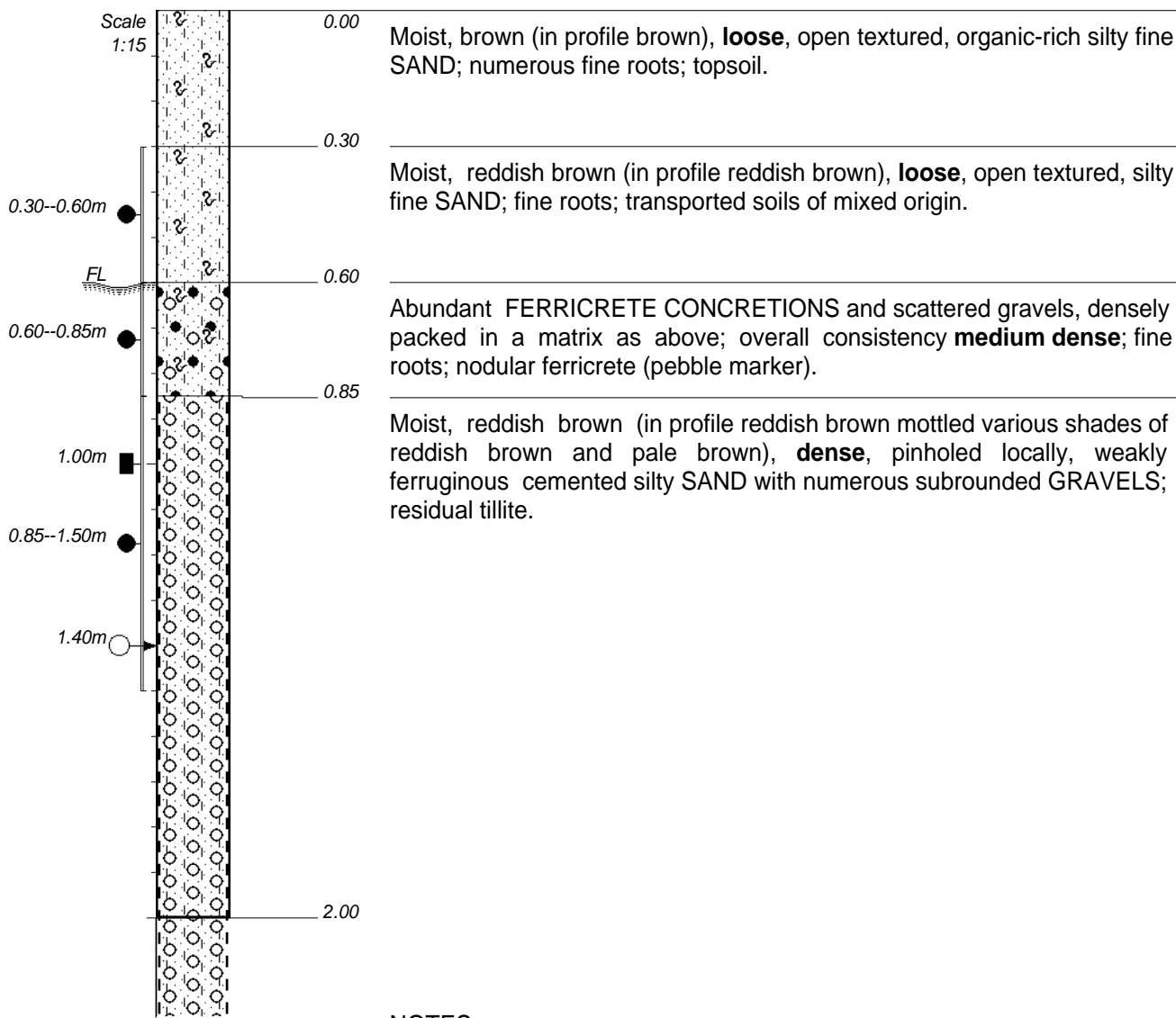
- 1) Pit excavated without refusal.
- 2) Slow groundwater seepage at 1.10m.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 840 960  
 COORD-E/y : -100 159

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

- 1) Pit excavated without refusal.
- 2) Slow groundwater seepage at 1.40m.
- 3) Indicator samples taken at 0.30--0.60m, 0.60--0.85m and 0.85--1.50m.
- 4) Undisturbed sample taken at 1.00m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

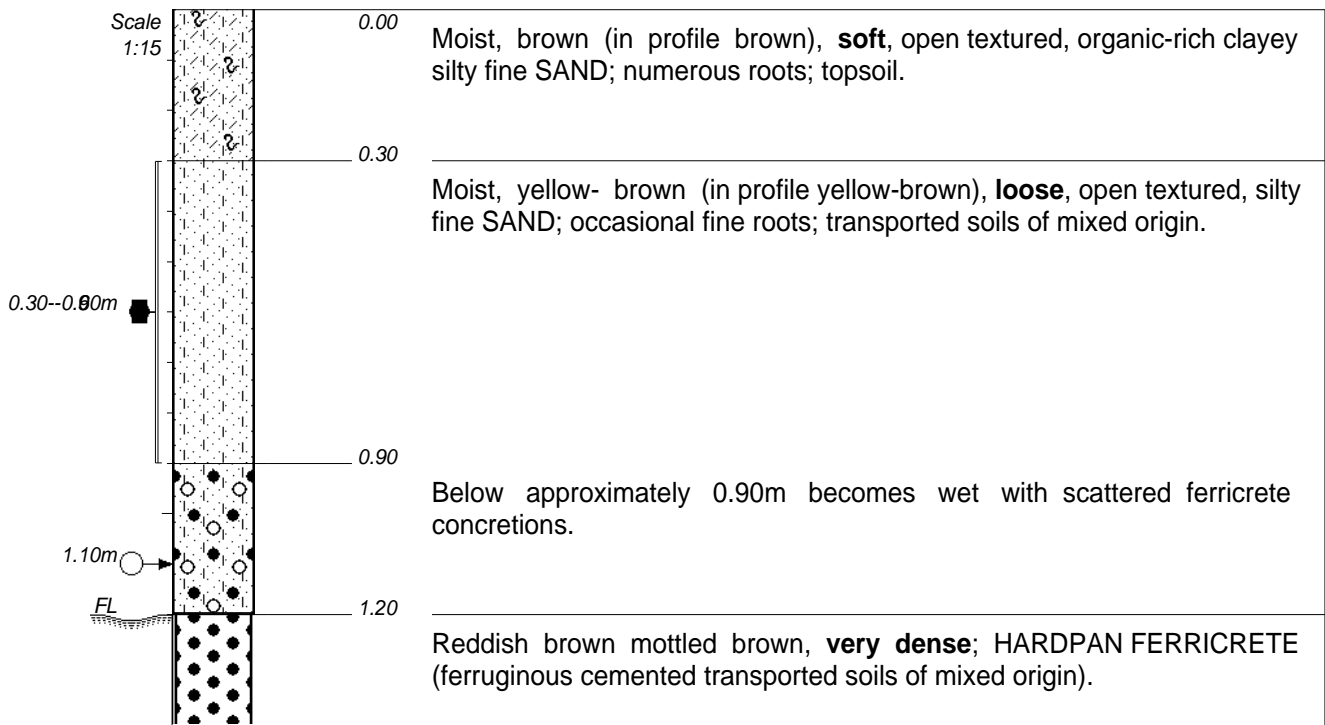
CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 7 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 000  
 COORD-E/y : -100 313



**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

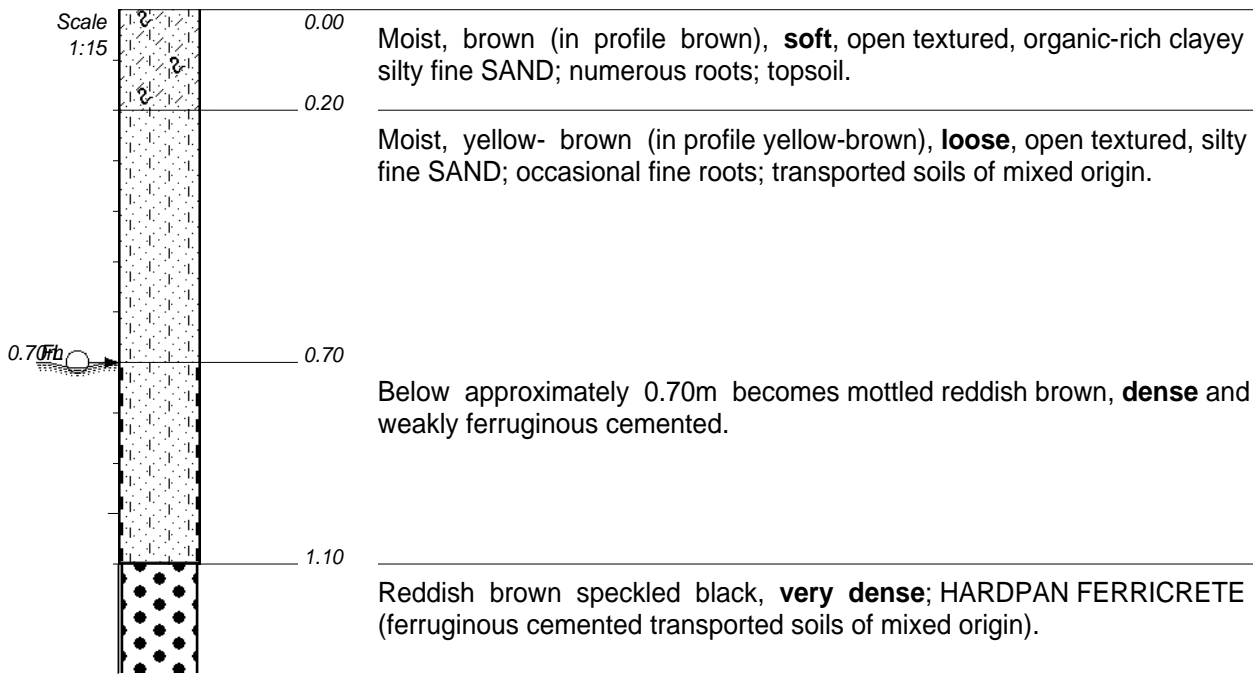
- 1) Pit excavated to refusal.
- 2) Slow groundwater seepage at 1.10m.
- 3) Indicator sample taken at 0.30--0.90m.
- 4) Lump sample taken at 0.60m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 840 680  
 COORD-E/y : -099 926

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

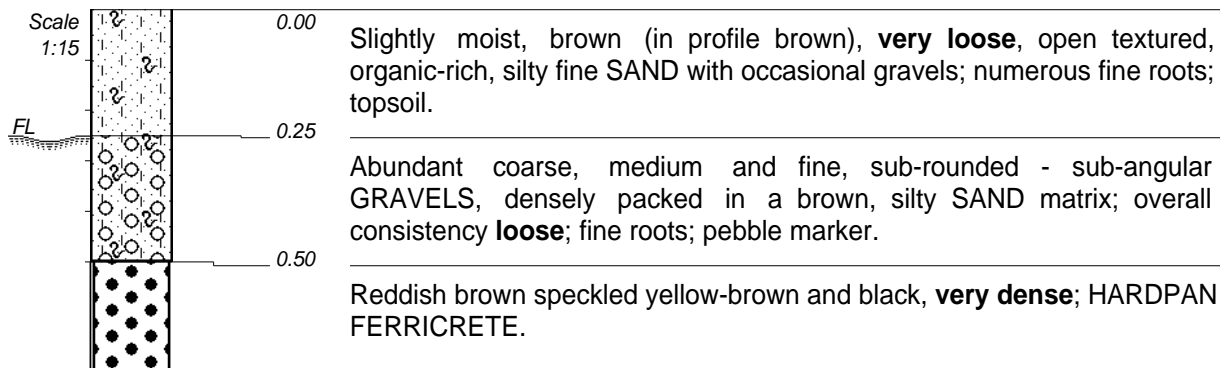
- 1) Pit excavated to refusal.
- 2) Slow groundwater seepage at 0.70m.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 840 747  
 COORD-E/y : -100 169

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

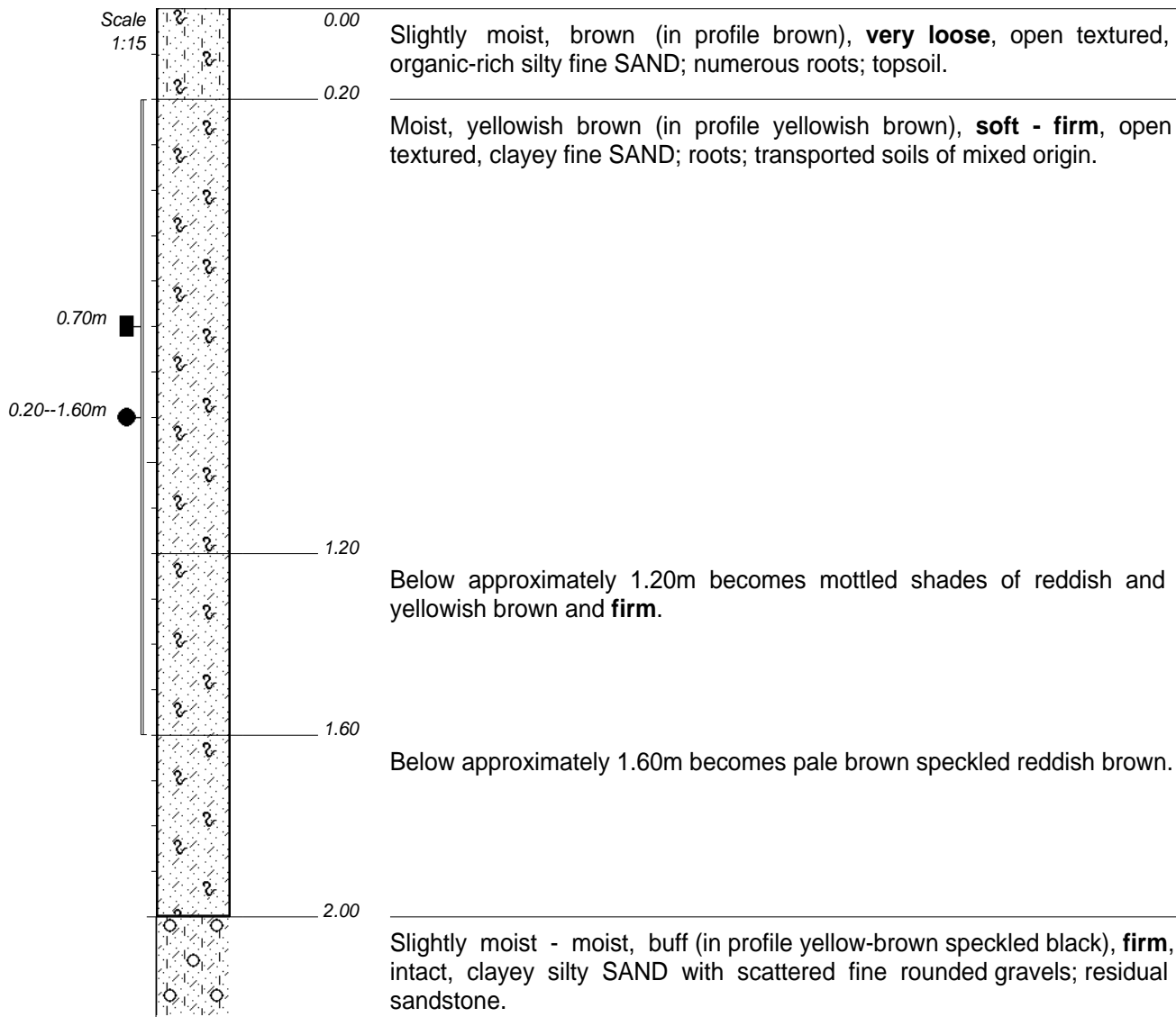
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.
- 5) Extensive sub-outcropping hardpan ferricrete downslope.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 429  
 COORD-E/y : 0 099 674

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

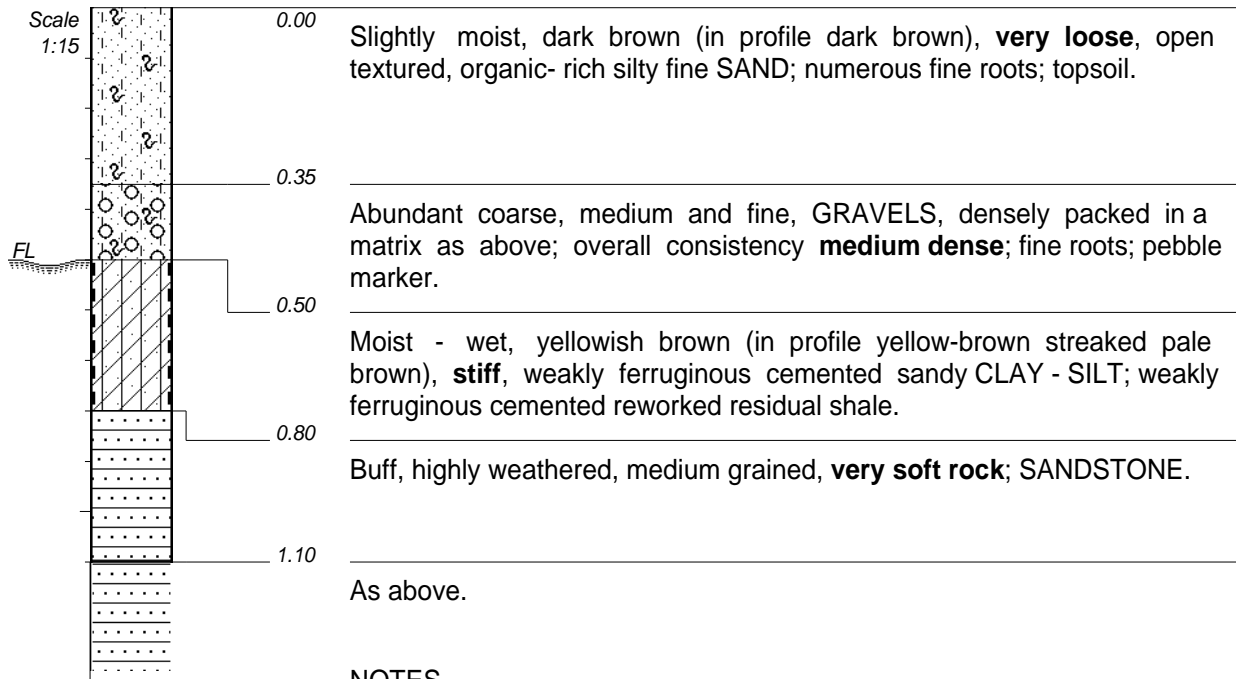
- 1) Pit excavated without refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 0.20--1.60m.
- 4) Undisturbed sample taken at 0.70m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 566  
 COORD-E/y : 0 099 606

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

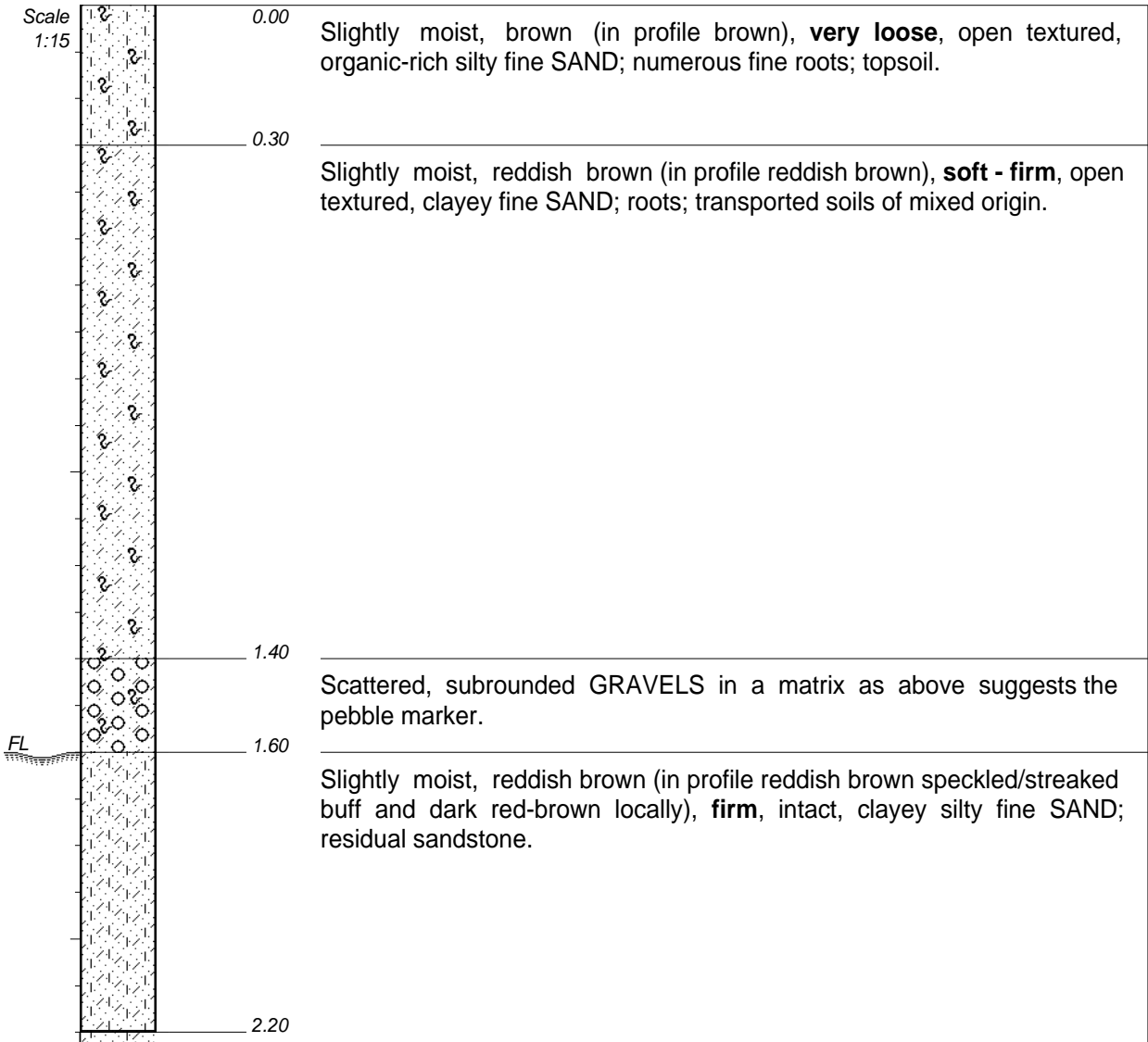
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 613  
 COORD-E/y : 0 099 805

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

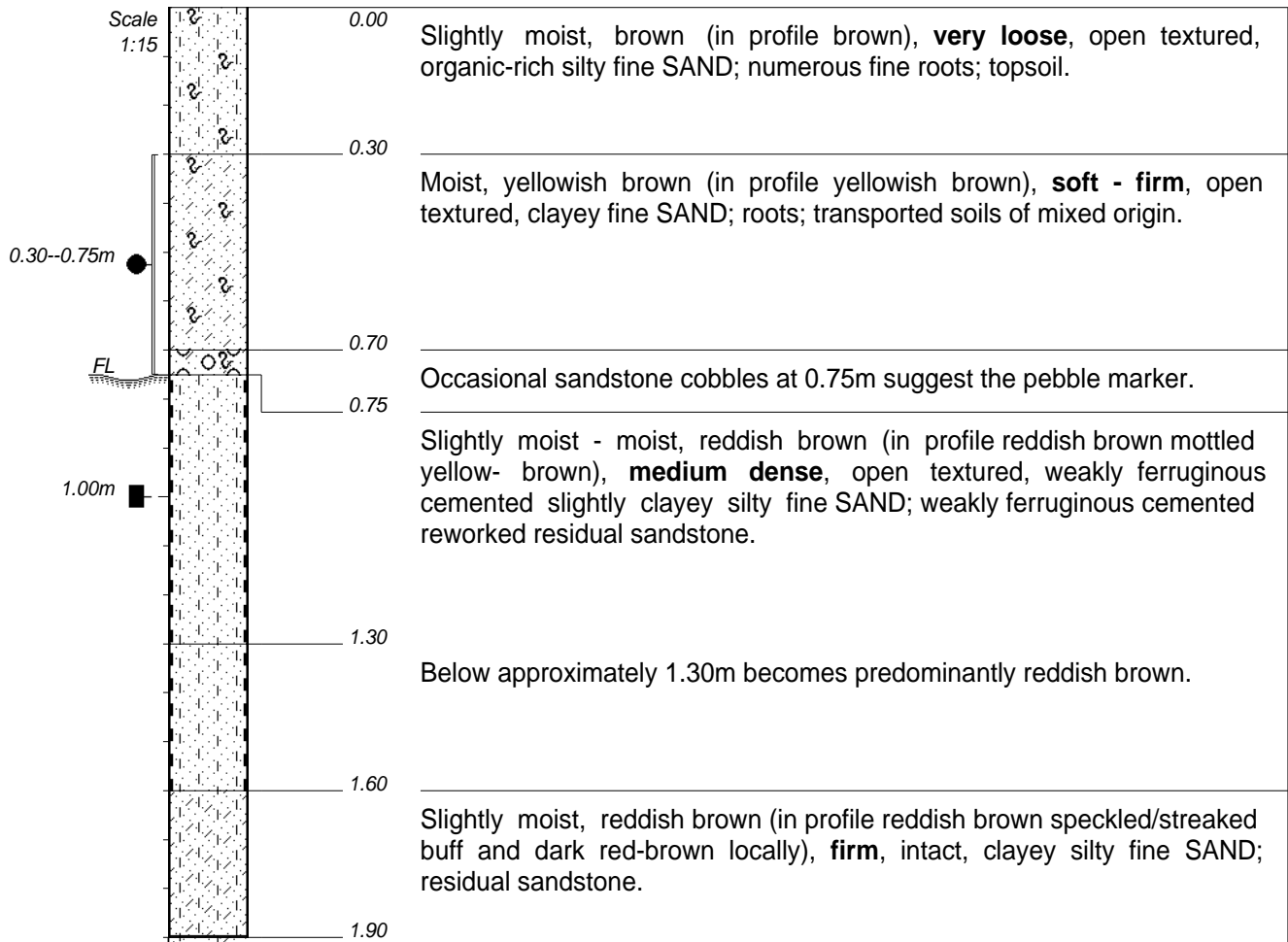
- 1) Pit excavated without refusal.
- 2) No groundwater seepage encountered.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 749  
 COORD-E/y : 0 099 699

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

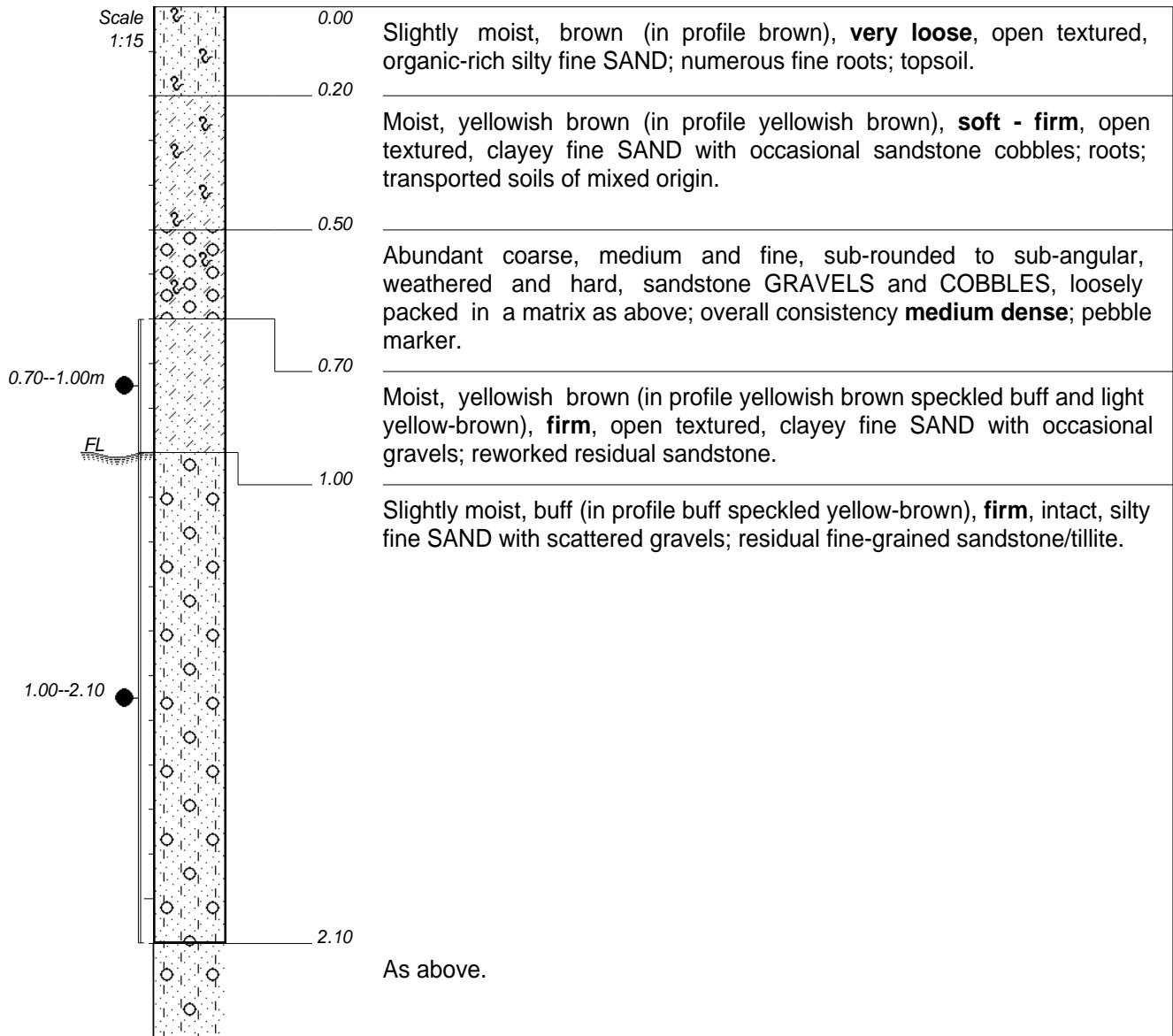
- 1) Pit excavated without refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 0.30--0.75m.
- 4) Undisturbed sample taken at 1.00m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 805  
 COORD-E/y : 0 099 552

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

- 1) Pit excavated without refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator samples taken at 0.70--1.00m and 1.00--2.10.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

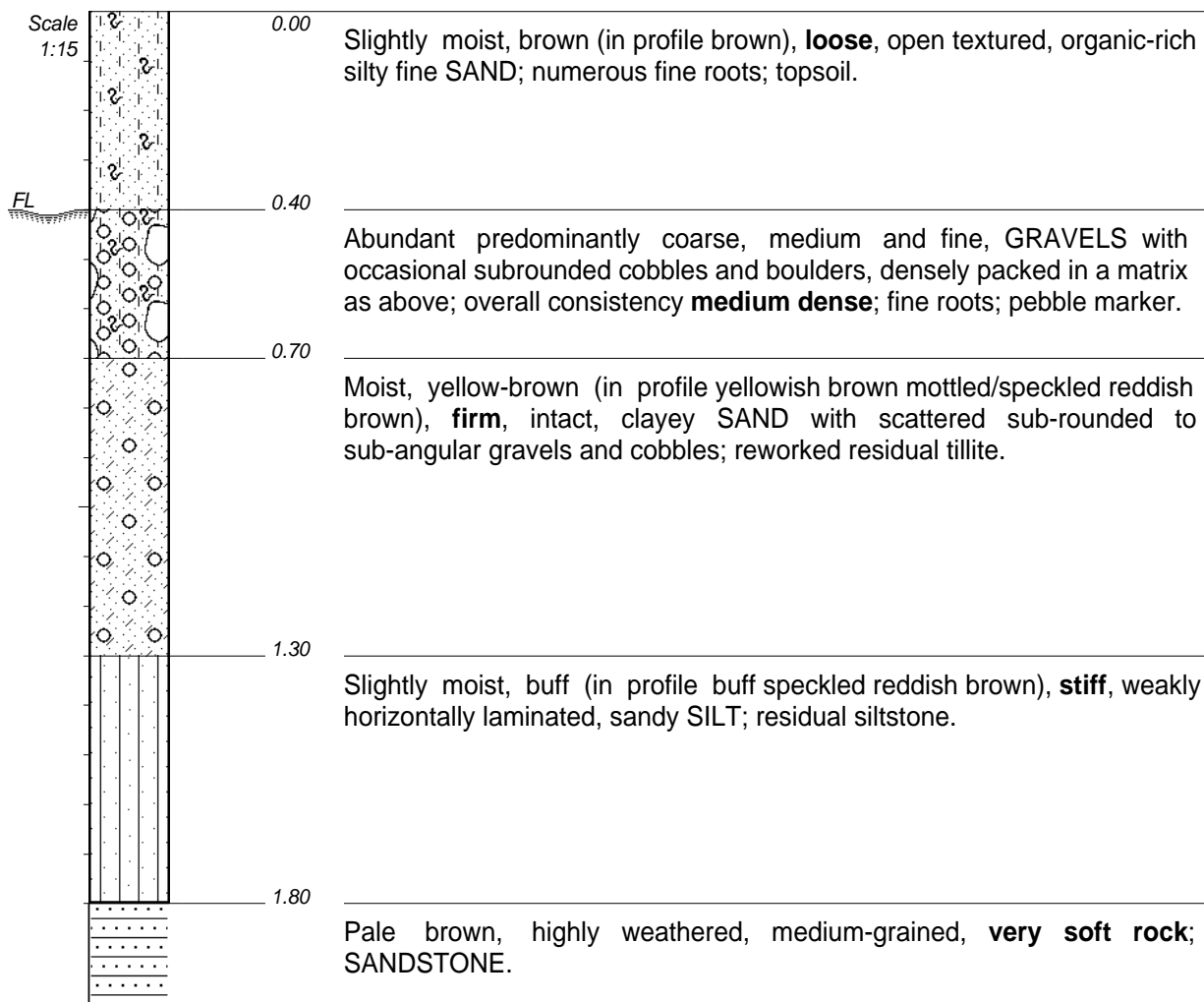
CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 964  
 COORD-E/y : 0 099 653



**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

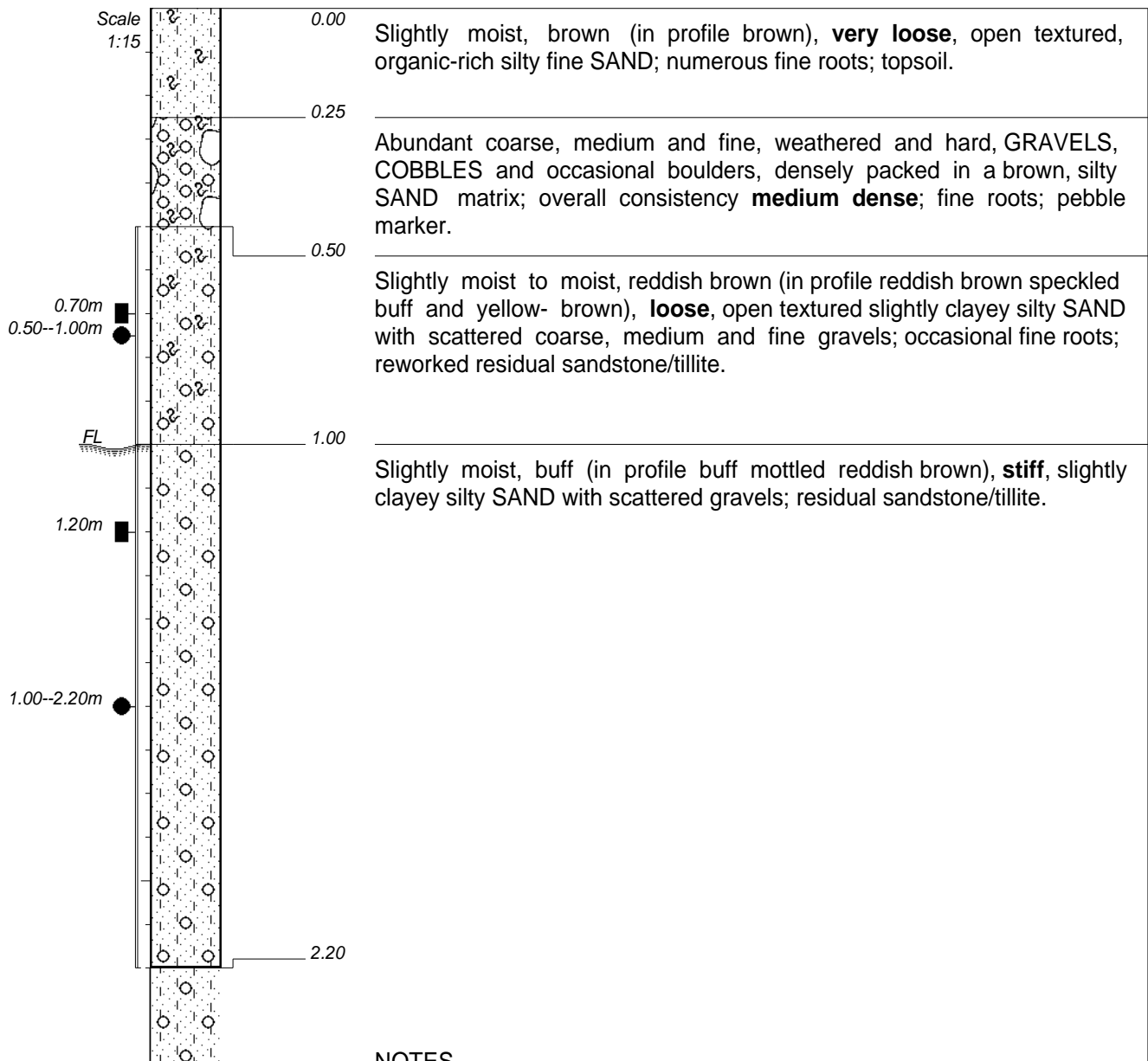
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 965  
 COORD-E/y : 0 099 822

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

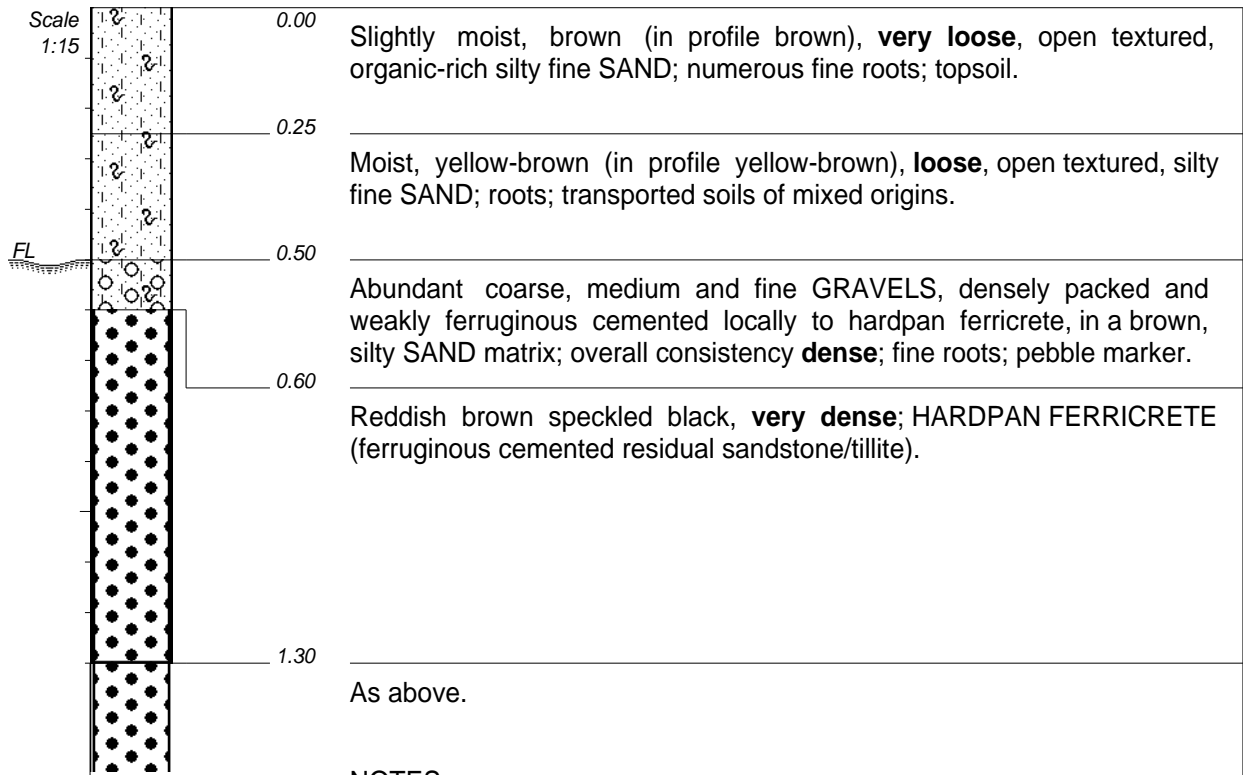
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator samples taken at 0.50--1.00m and 1.00--2.20m.
- 4) Undisturbed sample taken at 0.70m.
- 5) Lump sample taken at 1.20m.
- 6) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 768  
 COORD-E/y : 0 099 900

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



NOTES

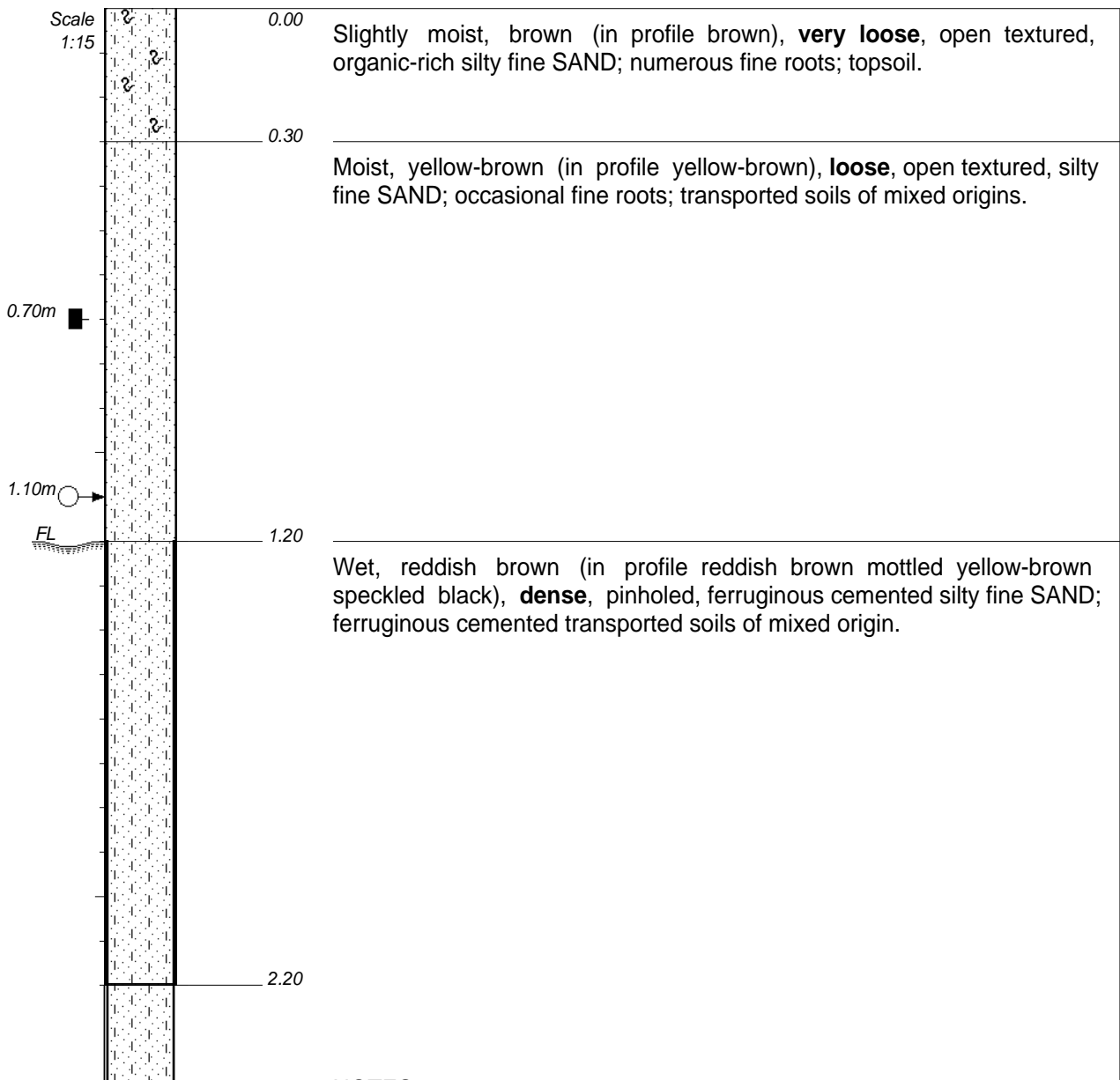
- 1) Pit excavated to refusal.
- 2) No groundwater seepage encountered.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 949  
 COORD-E/y : 0 100 059

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

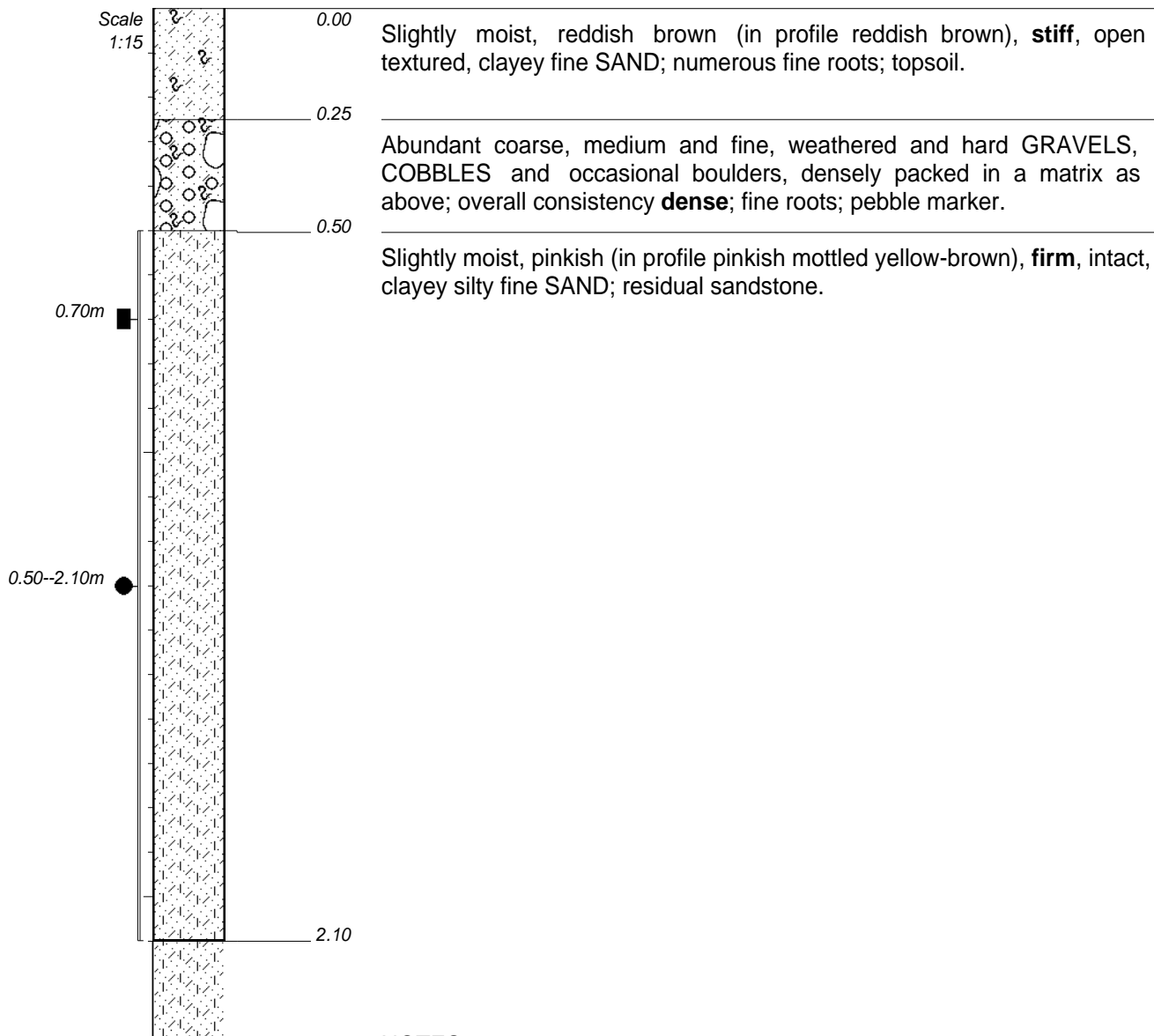
- 1) Pit excavated without refusal, but slow excavation.
- 2) Slow groundwater seepage at 1.10m.
- 3) Undisturbed sample taken at 0.70m.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 842 127  
 COORD-E/y : 0 099 991

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



**NOTES**

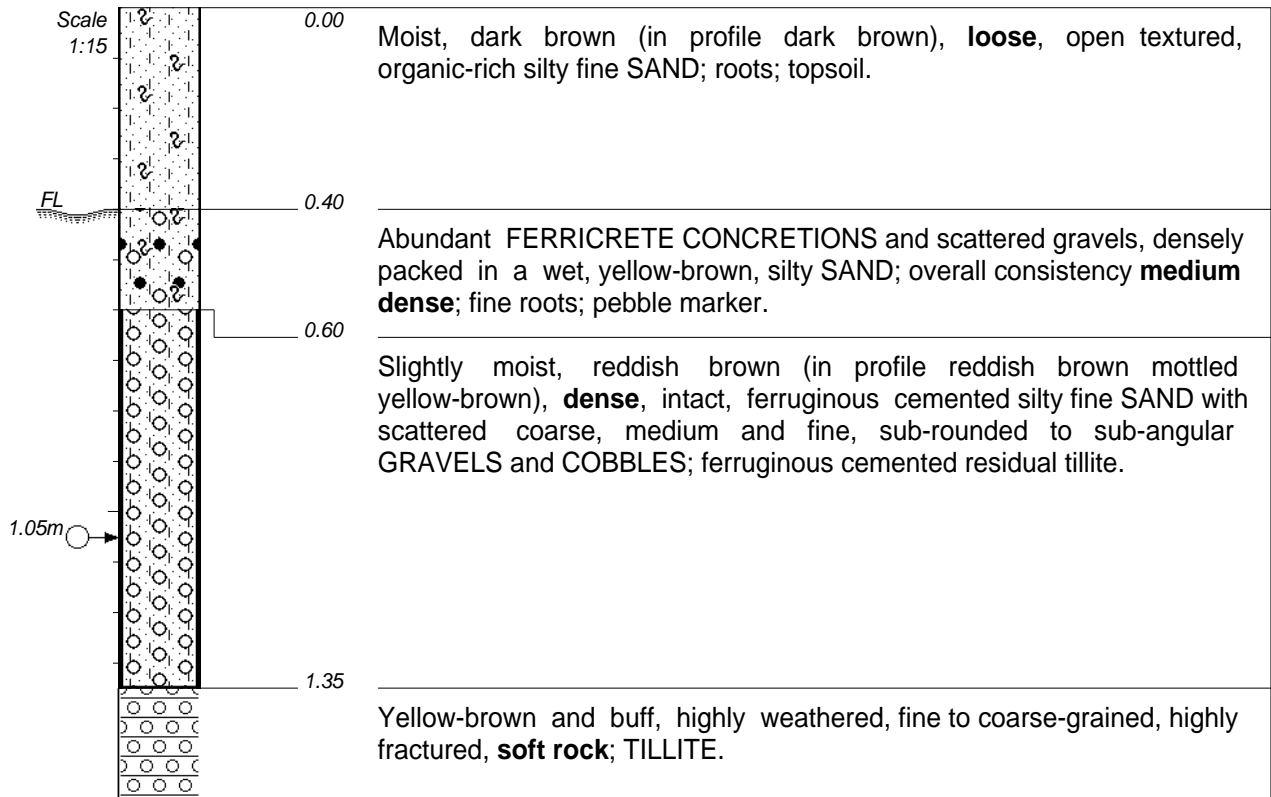
- 1) Pit excavated without refusal.
- 2) No groundwater seepage encountered.
- 3) Indicator sample taken at 0.50--2.10m.
- 4) Lump sample taken at 0.70m.
- 5) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 842 130  
 COORD-E/y : 0 099 776

**SIYATHUTHUKA EXTENSIONS  
 5, 6, 7 AND 8, MPUMALANGA**



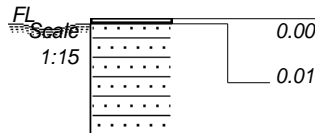
**NOTES**

- 1) Pit excavated to refusal.
- 2) Slow groundwater seepage at 1.05m.
- 3) No samples taken.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 842 136  
 COORD-E/y : 0 100 180



Greenish, highly weathered, medium grained, **soft rock**; SANDSTONE.

**NOTES**

- 1) Profile recorded on a bouldery outcrop extending along the
- 2) contour.
- 3) No evidence of groundwater seepage.
- 4) FL = interpolated minimum founding level for residential structures imposing up to 50kPa.

CONTRACTOR :  
 MACHINE : Bell 315S  
 DRILLED BY :  
 PROFILED BY : H. Schurink, Pr.Sci.Nat.  
 TYPE SET BY :  
 SETUP FILE : STANDARD.SET

INCLINATION :  
 DIAM :  
 DATE :  
 DATE : 8 February 2012  
 DATE : 22/03/2012 14:46  
 TEXT : ..000\network\testpits.txt

ELEVATION :  
 COORD-S/x : 2 841 880  
 COORD-E/y : 0 099 451

**APPENDIX C**  
**LABORATORY TEST RESULTS**



				Interpolated soil parameters based on available literature/experience - to be confirmed through appropriate laboratory tests before being used												
Test Pit No.	Soil Origin	Horizon Depth [m]		Basic					Geotechnical					Road		
		From	To	Relative Density	PI	k		Classification	C	Kenny (1959) Ø effective	Ø	Cc (Skempton - Terzaghi & Peck)	TRH 14	Group index	CBR @ MOD AASHTO	
						[cm/s]	[cm/s]								90 - 93%	100%
TP 8	TSMO	0.30	1.25	0.25	4	3.03E-004	2.50E-005	low	15	43	12	0.112 - 0.144	G8	1	23	121
TP 10	TSMO	0.30	0.65	0.25	4	4.33E-004	3.60E-005	low	14	41	14	0.119 - 0.153	G7	1	24	106
TP 13	TSMO	0.25	1.20	0.25	11	3.58E-005	2.25E-006	low	52	35	8	0.161 - 0.207	G8	5	13	46
TP 16	TSMO	0.20	0.60	0.25	3	2.46E-004	4.00E-006	low	16	45	10	0.098 - 0.126	G8	3	22	121
TP 18	TSMO	0.80	1.60	0.60	0	2.49E-003	2.25E-004	medium	13		33		G6	0	43	
TP 21	TSMO	0.30	0.60	0.25	0	1.04E-002	4.84E-004	medium	6		20		G6	0	42	
TP 22	TSMO	0.30	0.90	0.25	3	8.24E-004	8.10E-005	low	11	45	15	0.091 - 0.117	G7	1	28	139
TP 25	TSMO	0.20	1.60	0.35	4	9.50E-005	4.00E-004	low	26	43	11	0.140 - 0.180	G8	4	21	106
TP 28	TSMO	0.30	0.75	0.35	4	1.07E-004	4.00E-006	low	26	41	13	0.098 - 0.126	G8	2	21	106
TP 33	TSMO	0.30	1.20	0.25	4	3.38E-004	2.50E-005	low	15	43	12	0.070 - 0.090	G7	1	23	121
TP 8	f/c TSMO	1.25	1.70	0.25	0	2.13E-001	5.76E-004	high	4		27		G5	0	56	
TP 13	w/f/c TSMO	1.20	1.90	0.50	11	4.34E-005	2.25E-006	low	40	41	14	0.168 - 0.216	G8	5	20	106
TP 2	hardpan ferricrete	0.30	1.30	0.85	0	1.93E+000	3.97E-003	high	11		63		G5		78	
TP 21	residual sandstone / ti nodular ferricrete / pebble marker	0.85	1.50	0.75	0	1.25E-002	5.29E-004	medium	13		44		G5	0	53	
TP 21	residual sandstone	0.60	0.85	0.50	0	1.58E+002	2.89E-002	high	6		55		G5		95	
TP 34	residual sandstone	0.50	2.10	0.50	11	7.57E-006	1.00E-006	very low	115	34	11	0.238 - 0.306	G8	8	12	46
TP 4	residual sandstone	0.60	1.10	0.50	0	7.65E+000	5.63E-003	high	7		49		G5		79	
TP 12	r/ residual sandstone	0.65	1.60	0.60	5	2.40E-003	9.00E-006	medium	23	39	36	0.126 - 0.162	G6	0	35	121
TP 16	residual sandstone	0.70	1.30	0.50	2	1.34E-002	1.69E-004	medium	12	49	35	0.112 - 0.144	G5	0	46	159
TP 29	r/residual sandstone	0.70	1.00	0.50	4	5.14E-004	4.00E-006	low	20	43	25	0.140 - 0.180	G6	2	30	121
TP 9	w/f/c r/ residual sands	1.30	2.30	0.50	5	2.79E-003	1.69E-004	medium	20	39	32	0.112 - 0.144	G6	0	34	121
TP 28	w/f/c r/ residual sands	0.75	1.60	0.50	6	1.54E-004	9.00E-006	low	29	39	22	0.154 - 0.198	G8	2	24	106
TP 29	residual tillite	1.00	2.10	0.50	7	7.40E-005	3.24E-006	low	37	38	20	0.126 - 0.162	G8	3	21	92
TP 31	residual tillite	0.50	1.00	0.25	4	5.18E-001	5.76E-004	high	6	43	29	0.119 - 0.153	G5	0	51	139
TP 31	residual tillite	1.00	2.20	0.75	7	2.04E-003	1.21E-004	medium	34	37	43	0.126 - 0.162	G6	0	33	106
TP 6	residual shale	1.60	2.10	0.50	7	2.17E-005	1.00E-006	low	60	37	13	0.182 - 0.234	G8	7	17	70
TP 6	residual shale	0.40	1.60	0.50	11	5.14E-006	1.00E-006	very low	156	34	9	0.175 - 0.225	G8	8	11	35
TP 14	residual shale	1.00	1.60	0.75	68	7.53E-006	1.00E-008	very low	104	36	16	0.168 - 0.216	G8	7	15	61

Notes: PI = plasticity index (\*) = on whole sample  
LL = liquid limit; LS = linear shrinkage;  
GM = grading modulus; n/t = not tested;  
w/ = weakly; f/c = ferruginous cemented  
r/ = residual; r/r = reworked residual;  
TSMO = transported soils of mixed origin.



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 2	<b>Depth [m] :</b>	0.300-1.300
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0283

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	86	77	59	51	40	32	29	25	20	12	9	7	4	2	2	2	2

**ATTERBERG LIMITS**

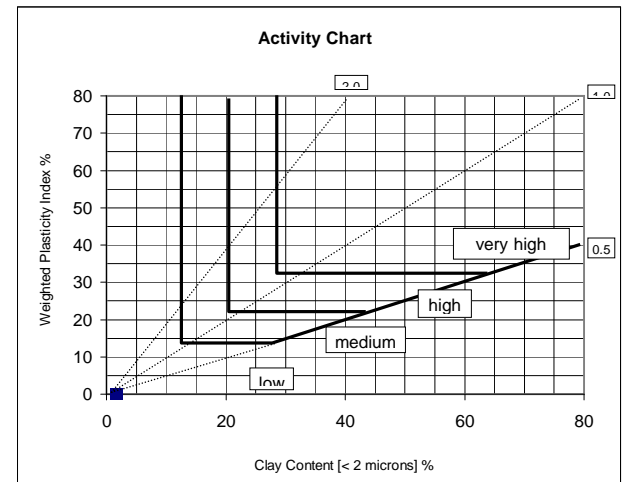
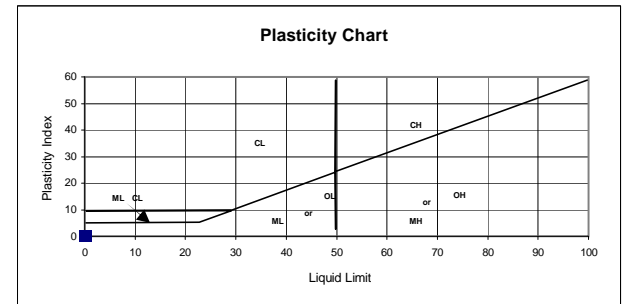
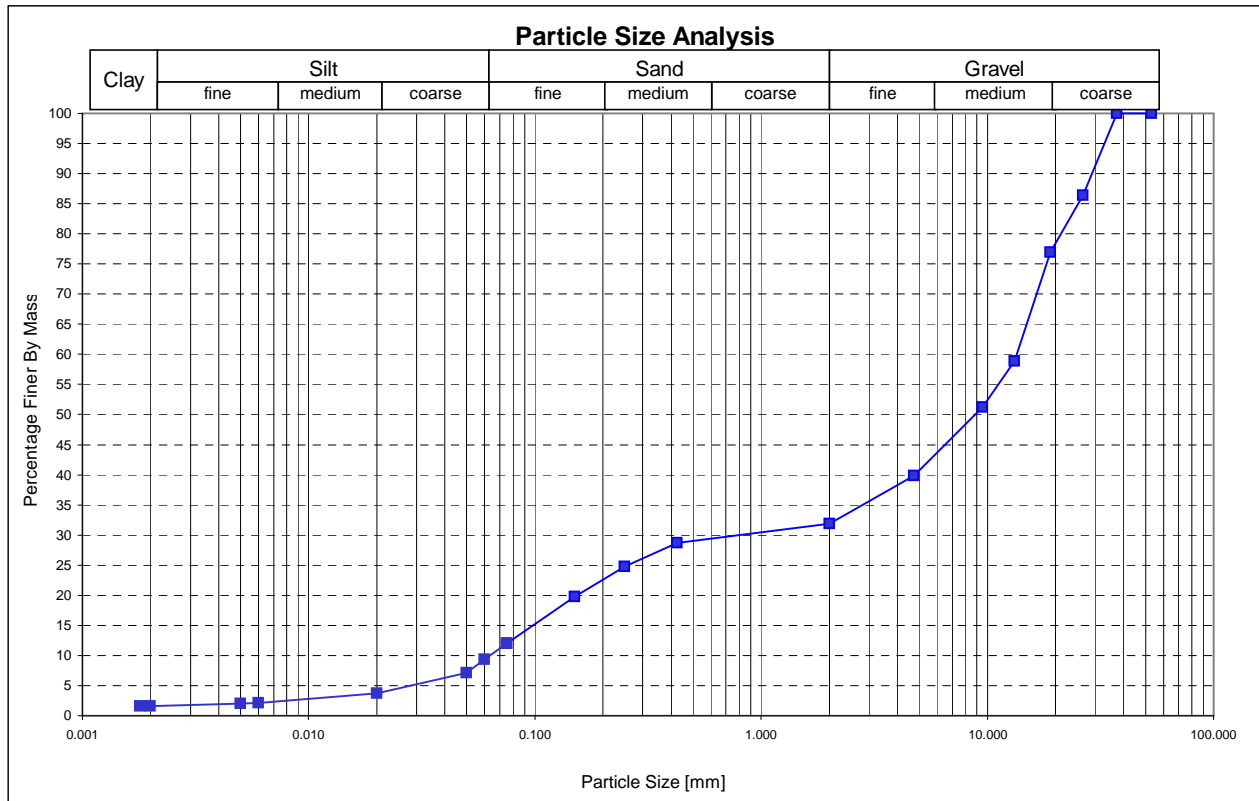
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
0	NP		0.0	2.27

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
GM	A.1.a (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	2	<b>Silt :</b>	8	<b>Sand :</b>	23	<b>Gravel :</b>	68	<b>Fines :</b>	29	<b>Soil description :</b>	Dark Brown Soil
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<b>D<sub>10</sub> :</b>	0.063	<b>D<sub>30</sub> :</b>	0.810	<b>D<sub>60</sub> :</b>	13.495	<b>Uniformity coefficient :</b>	213	<b>Curvature coefficient :</b>	1	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 4	<b>Depth [m] :</b>	0.600-1.000
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0284

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	80	68	59	54	46	34	26	22	16	10	8	7	4	2	2	2	1

**ATTERBERG LIMITS**

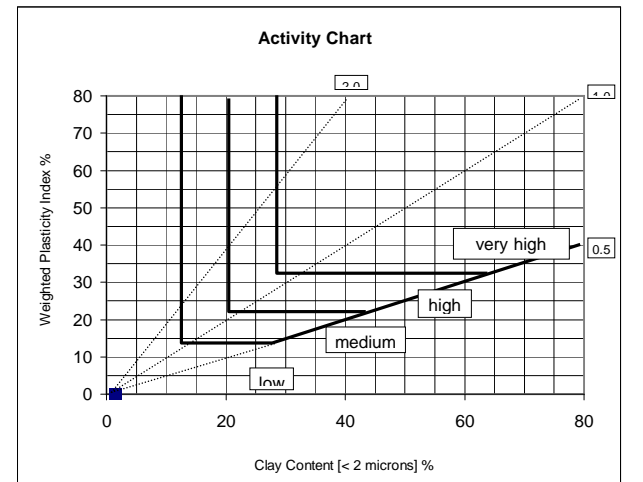
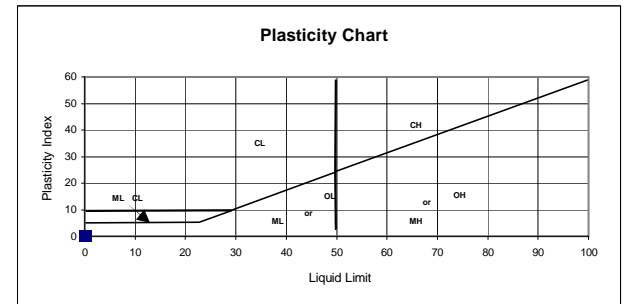
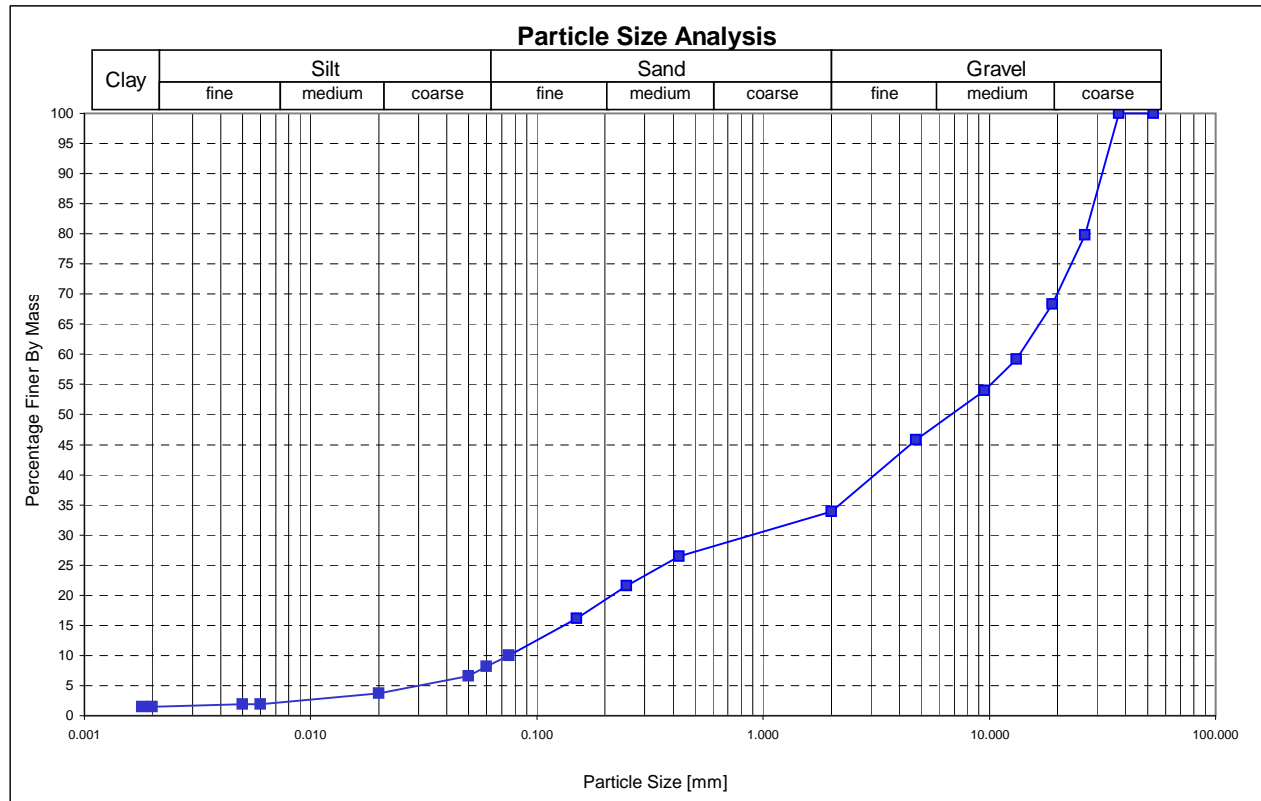
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
0	NP		0.0	2.30

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
GP	A.1.a (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	2	<b>Silt :</b>	7	<b>Sand :</b>	26	<b>Gravel :</b>	66	<b>Fines :</b>	26	<b>Soil description :</b>	Light Reddish Brown Soil
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<b>D<sub>10</sub> :</b>	0.075	<b>D<sub>30</sub> :</b>	0.895	<b>D<sub>60</sub> :</b>	13.654	<b>Uniformity coefficient :</b>	182	<b>Curvature coefficient :</b>	1	<b>Active program :</b>	YES
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**REMARKS:**

none

**CHECKED BY :**

G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 6	<b>Depth [m] :</b>	@ 0.70m
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
21-Feb-12	<b>Sample No.</b>	12/0285

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	100	98	91	87	82	68	59	52	41	30	29	20	19

**ATTERBERG LIMITS**

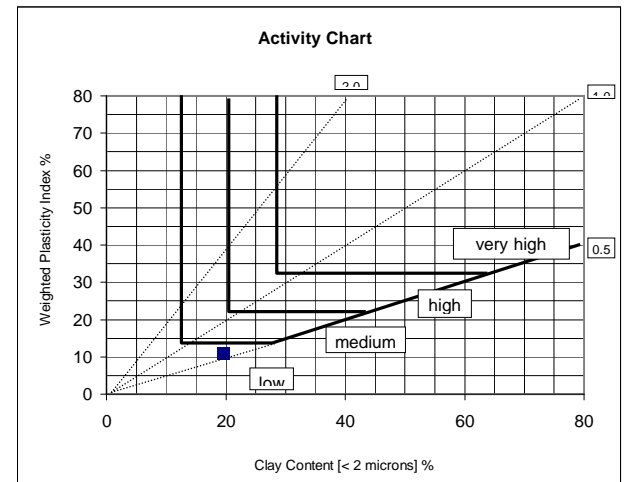
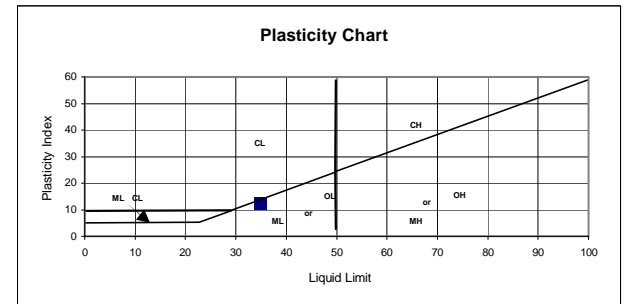
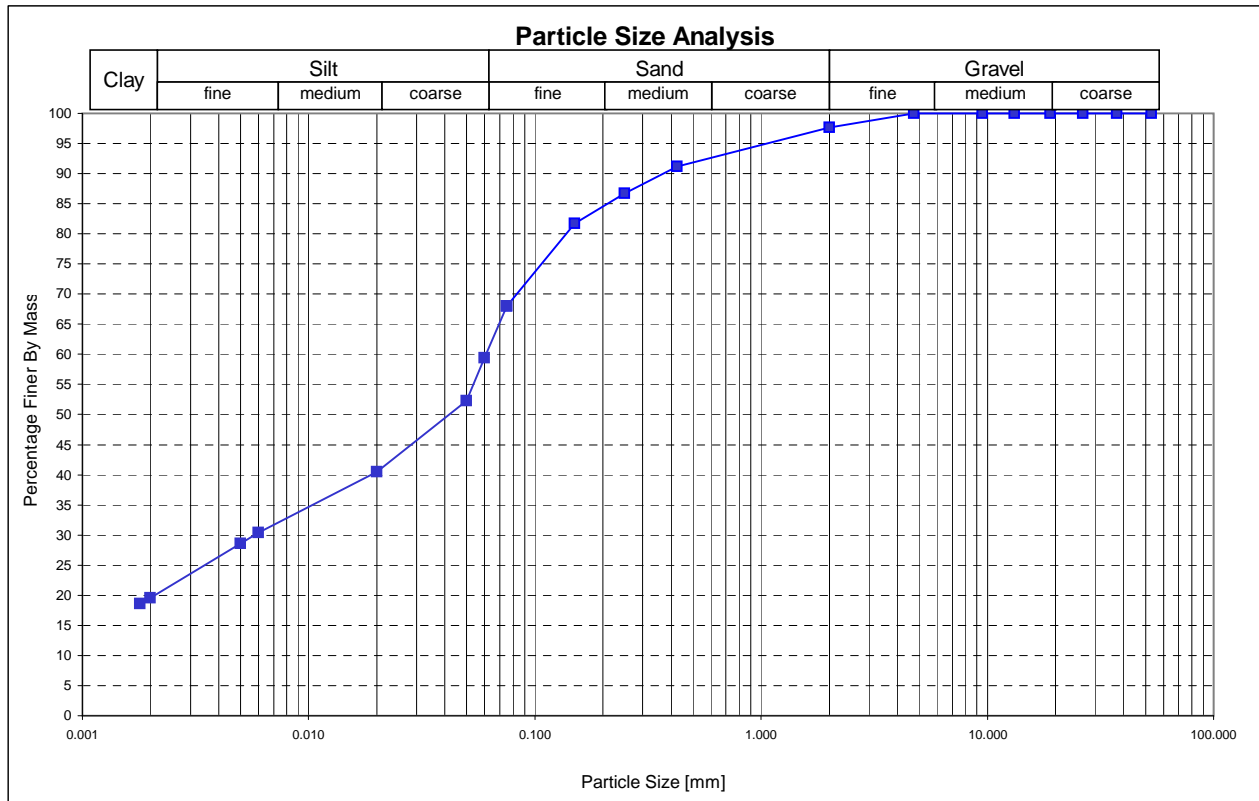
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
35	13	11	5.4	0.43

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
CL	A.6 (7)	

<b>Soil constituents % :</b>	<b>Clay :</b>	20	<b>Silt :</b>	40	<b>Sand :</b>	38	<b>Gravel :</b>	2	<b>Fines :</b>	91	<b>Soil description :</b>	Light Brown Soil
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<b>D<sub>10</sub> :</b>	<b>D<sub>30</sub> :</b>	0.006	<b>D<sub>60</sub> :</b>	0.061	<b>Uniformity coefficient :</b>		<b>Curvature coefficient :</b>		<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder

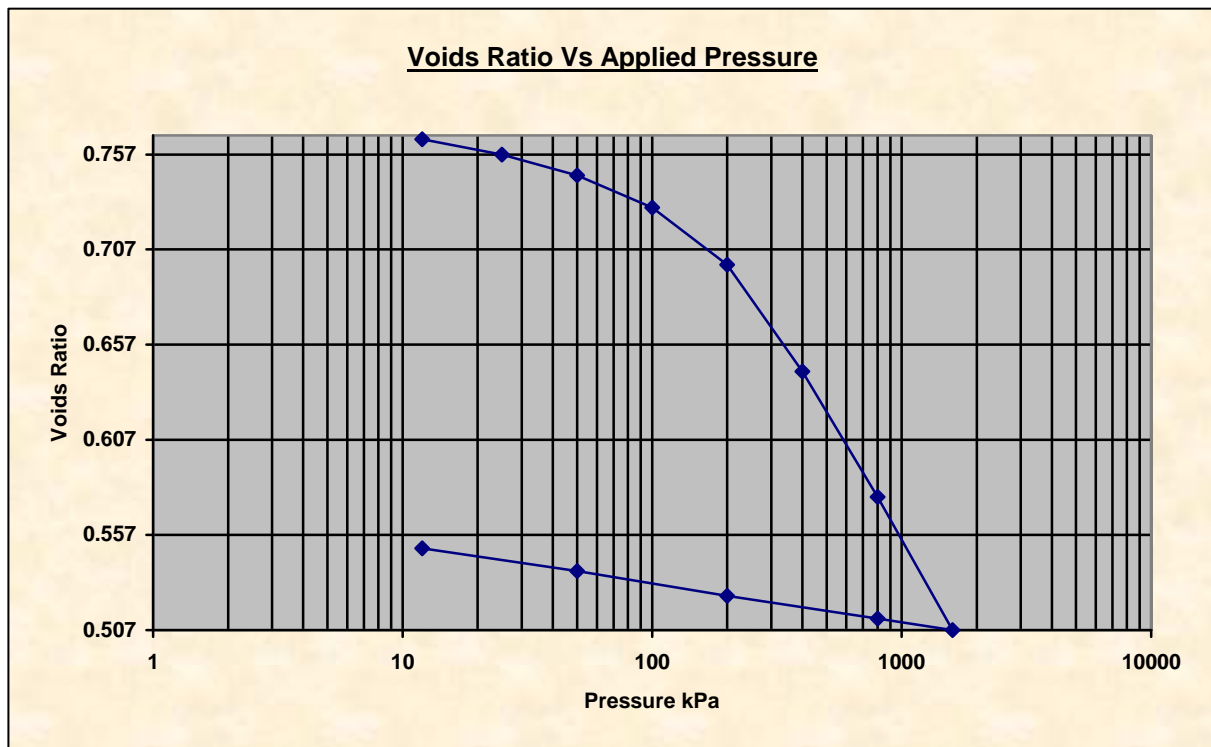
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 06	<b>Sample</b>	12-0285

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	A	<b>Description</b>	
<b>Depth within Sample</b>	50.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	159.62 g	<b>Condition</b>	Inundated
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	1	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	116.00 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	11.32 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 06	<b>Sample</b>	12-0285

<b>Initial Moisture Content*</b>	21.8 % (trimmings: 23.5 %)	<b>Final Moisture Content</b>	21.4 %
<b>Initial Bulk Density</b>	1.81 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.05 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.48 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.69 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.7671	<b>Final Void Ratio</b>	0.5495
<b>Initial Degree of Saturation</b>	74.61%	<b>Final Degree of Saturation</b>	101.91 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.09 m <sup>2</sup> /MN	3.22 m <sup>2</sup> /yr
25.0 kPa	0.36 m <sup>2</sup> /MN	33.82 m <sup>2</sup> /yr
50.0 kPa	0.26 m <sup>2</sup> /MN	16.08 m <sup>2</sup> /yr
100.0 kPa	0.19 m <sup>2</sup> /MN	22.96 m <sup>2</sup> /yr
200.0 kPa	0.17 m <sup>2</sup> /MN	28.22 m <sup>2</sup> /yr
400.0 kPa	0.16 m <sup>2</sup> /MN	36.40 m <sup>2</sup> /yr
800.0 kPa	0.10 m <sup>2</sup> /MN	28.28 m <sup>2</sup> /yr
1600.0 kPa	0.06 m <sup>2</sup> /MN	26.74 m <sup>2</sup> /yr
800.0 kPa	0.01 m <sup>2</sup> /MN	-----
200.0 kPa	0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.06 m <sup>2</sup> /MN	-----
12.0 kPa	0.20 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120220
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317

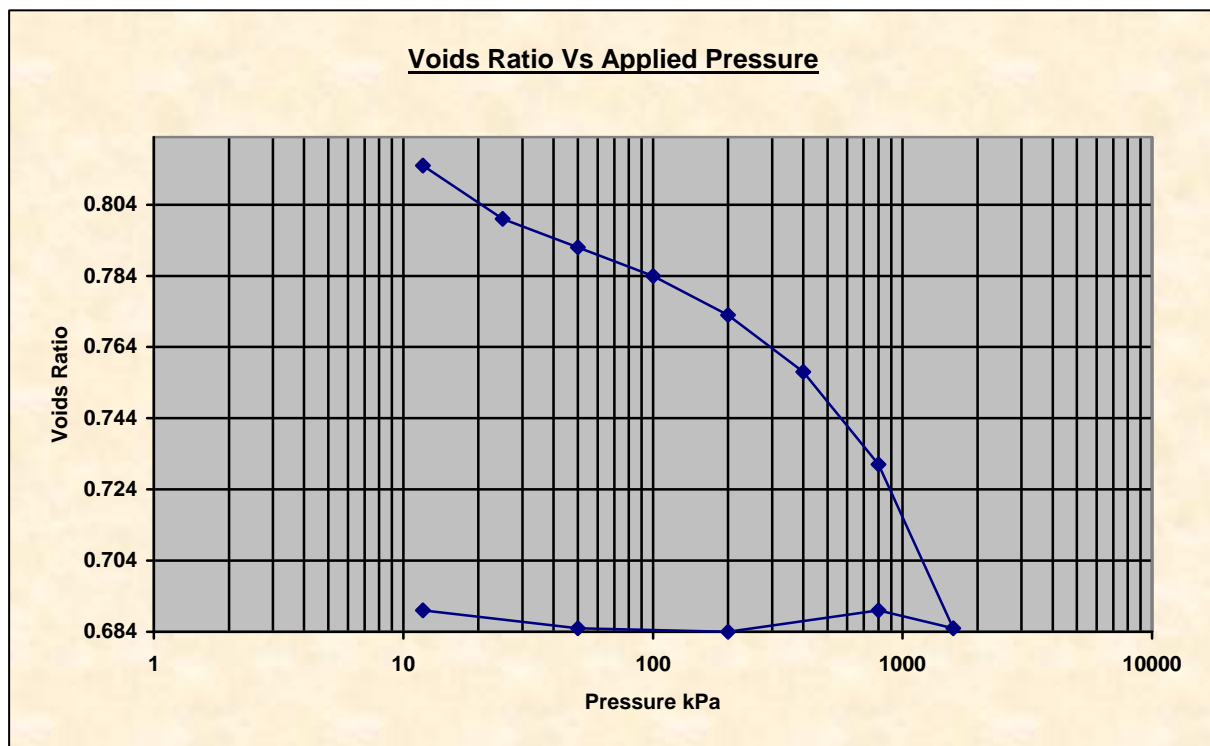
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 06	<b>Sample</b>	12-0285

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	B	<b>Description</b>	
<b>Depth within Sample</b>	75.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	157.14 g	<b>Condition</b>	Natural Moisture
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	2	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	114.20 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.97 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 06	<b>Sample</b>	12-0285

<b>Initial Moisture Content*</b>	23.7 % (trimmings: 23.5 %)	<b>Final Moisture Content</b>	9.4 %
<b>Initial Bulk Density</b>	1.78 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	1.70 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.44 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.55 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8228	<b>Final Void Ratio</b>	0.6898
<b>Initial Degree of Saturation</b>	75.57%	<b>Final Degree of Saturation</b>	35.89 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.38 m <sup>2</sup> /MN	-----
25.0 kPa	0.62 m <sup>2</sup> /MN	-----
50.0 kPa	0.17 m <sup>2</sup> /MN	-----
100.0 kPa	0.10 m <sup>2</sup> /MN	-----
200.0 kPa	0.06 m <sup>2</sup> /MN	-----
400.0 kPa	0.04 m <sup>2</sup> /MN	-----
800.0 kPa	0.04 m <sup>2</sup> /MN	-----
1600.0 kPa	0.03 m <sup>2</sup> /MN	-----
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.00 m <sup>2</sup> /MN	-----
12.0 kPa	0.07 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120220
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317





**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 6	<b>Depth [m] :</b>	1.600-2.100
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0286

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	96	89	83	81	77	65	58	53	37	24	23	15	14

**ATTERBERG LIMITS**

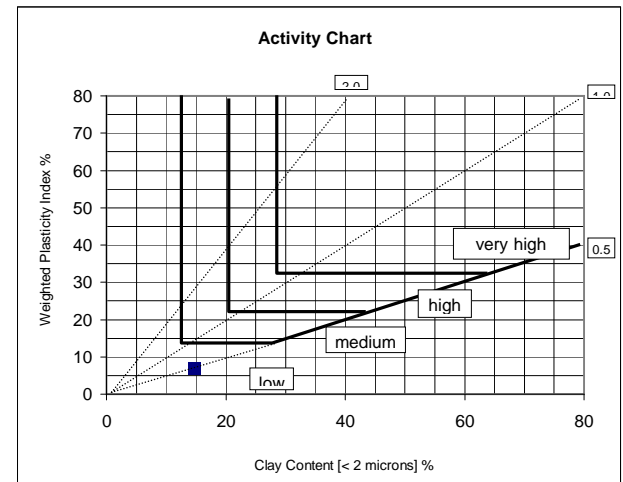
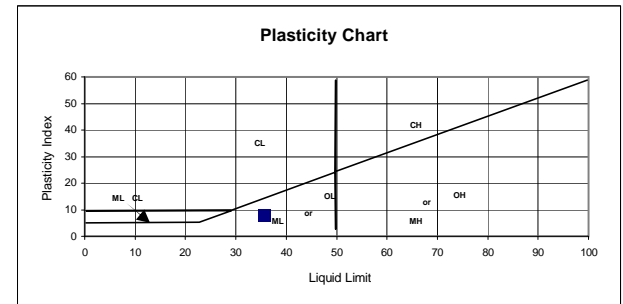
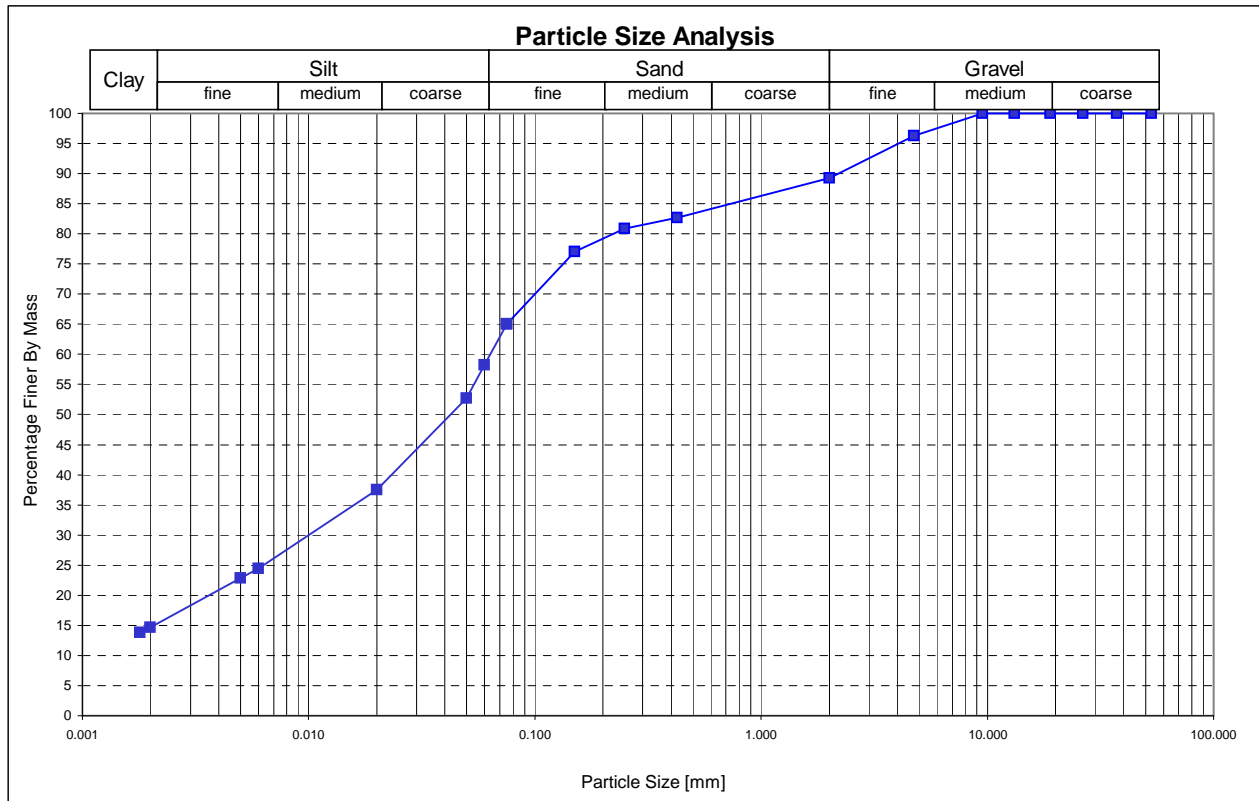
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
36	8	7	3.4	0.63

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
ML	A.4 (6)	

<b>Soil constituents % :</b>	<b>Clay :</b>	15	<b>Silt :</b>	44	<b>Sand :</b>	31	<b>Gravel :</b>	11	<b>Fines :</b>	83	<b>Soil description :</b>	Buff Soil
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<b>D<sub>10</sub> :</b>	<b>D<sub>30</sub> :</b>	0.010	<b>D<sub>60</sub> :</b>	0.064	<b>Uniformity coefficient :</b>		<b>Curvature coefficient :</b>		<b>Active program :</b>	YES
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**REMARKS:**

none

**CHECKED BY :**

G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 8	<b>Depth [m] :</b>	@ 0.70m
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
21-Feb-12	<b>Sample No.</b>	12/0287

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	100	100	84	71	54	38	32	27	18	11	10	7	7

**ATTERBERG LIMITS**

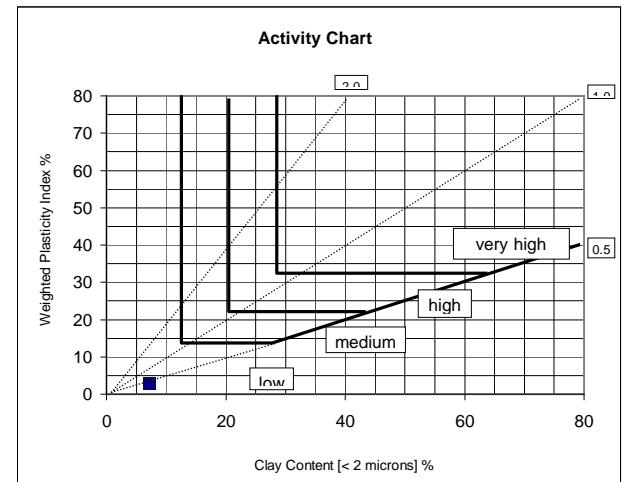
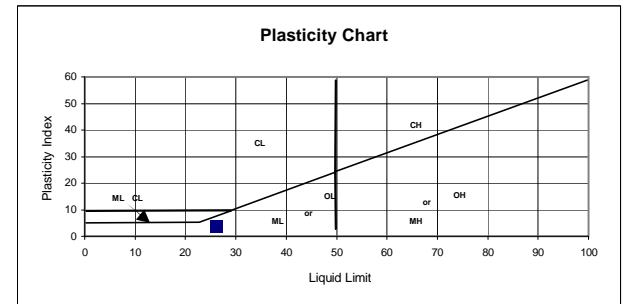
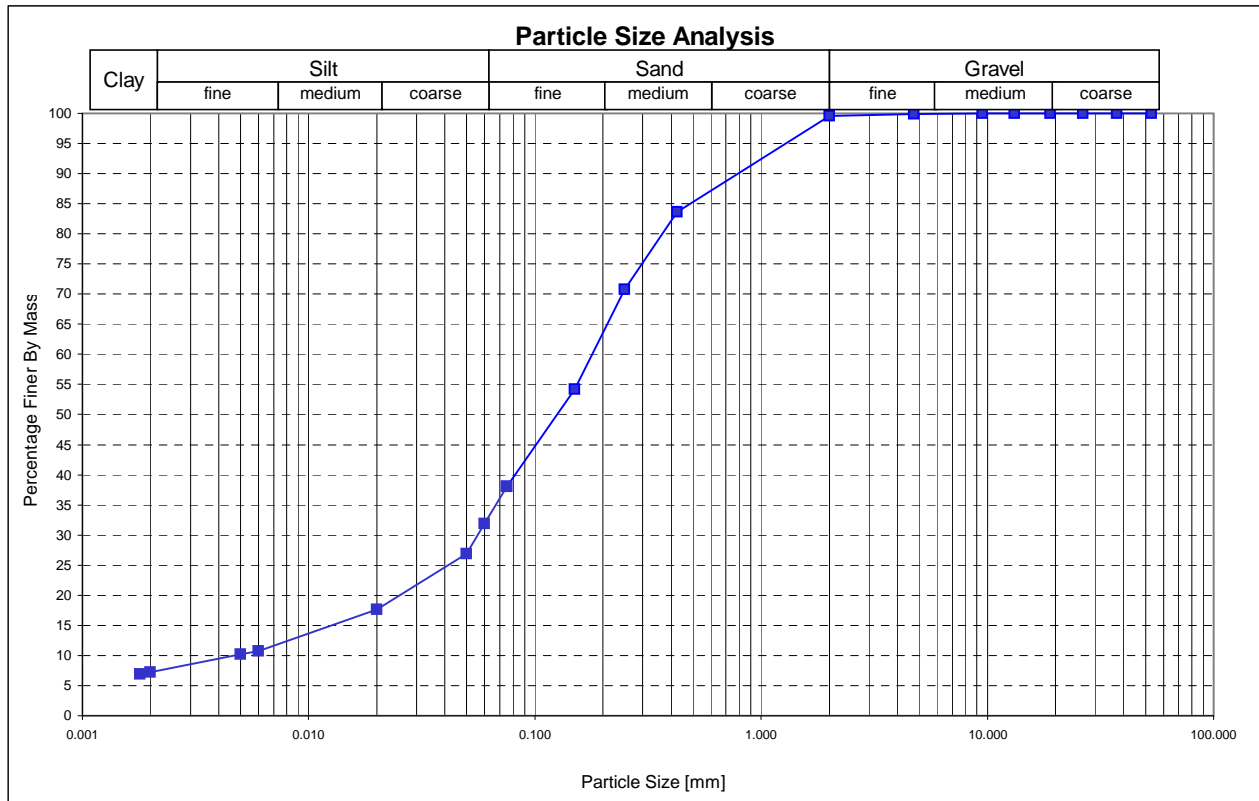
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
26	4	3	2.0	0.79

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.4 (1)	

<b>Soil constituents % :</b>	<b>Clay :</b>	7	<b>Silt :</b>	25	<b>Sand :</b>	68	<b>Gravel :</b>	0	<b>Fines :</b>	84	<b>Soil description :</b>	Dark Yellowish Orange Soil
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<b>D<sub>10</sub> :</b>	0.005	<b>D<sub>30</sub> :</b>	0.056	<b>D<sub>60</sub> :</b>	0.179	<b>Uniformity coefficient :</b>	38	<b>Curvature coefficient :</b>	4	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder

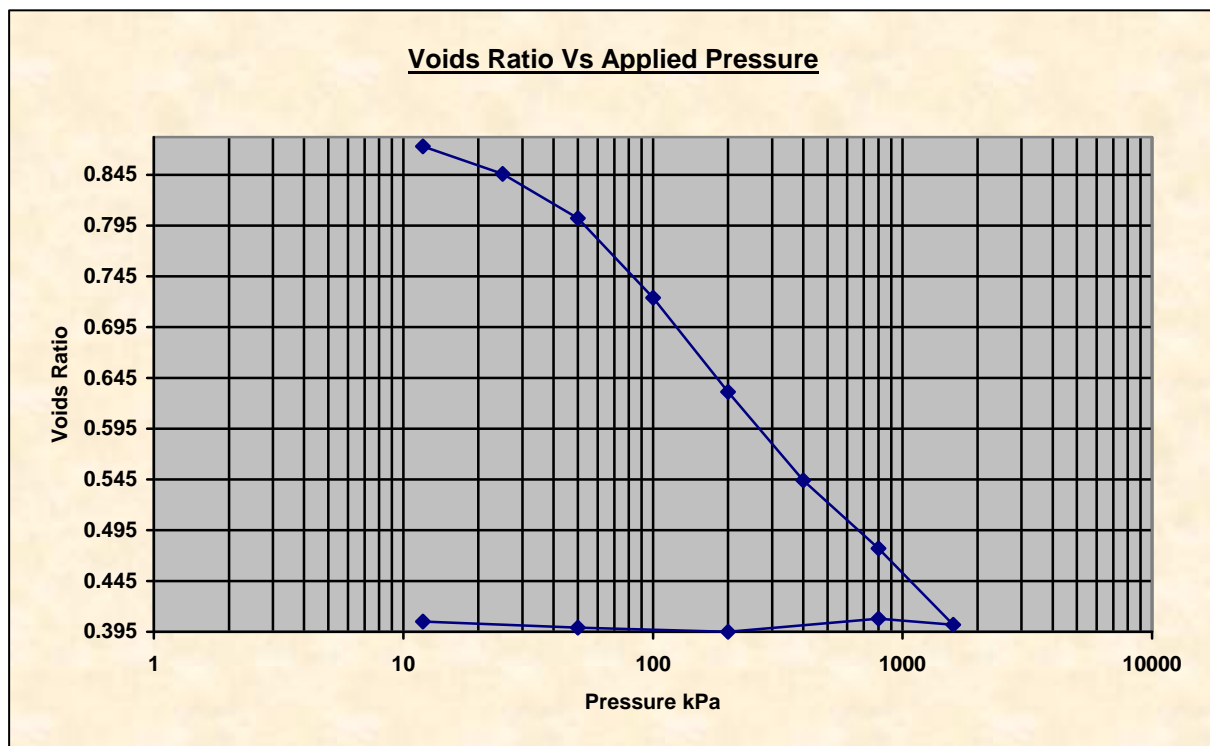
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 08	<b>Sample</b>	12-0287

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	A	<b>Description</b>	
<b>Depth within Sample</b>	60.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	138.62 g	<b>Condition</b>	Inundated
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	3	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	116.74 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.63 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 08	<b>Sample</b>	12-0287

<b>Initial Moisture Content*</b>	12.7 % (trimmings: 12.3 %)	<b>Final Moisture Content</b>	13.8 %
<b>Initial Bulk Density</b>	1.57 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.12 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.39 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.87 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8821	<b>Final Void Ratio</b>	0.4047
<b>Initial Degree of Saturation</b>	37.72%	<b>Final Degree of Saturation</b>	89.48 %

- Calculated from initial and dry weights of whole specimen

<b>Pressure (Loading Stages)</b>	<b>Coefficient of Volume Compressibility (m<sub>v</sub>)</b>	<b>Coefficient of Consolidation (c<sub>v</sub>)</b>
<b>0.00</b>		
12.0 kPa	0.42 m <sup>2</sup> /MN	12.36 m <sup>2</sup> /yr
25.0 kPa	1.08 m <sup>2</sup> /MN	18.21 m <sup>2</sup> /yr
50.0 kPa	0.97 m <sup>2</sup> /MN	30.41 m <sup>2</sup> /yr
100.0 kPa	0.86 m <sup>2</sup> /MN	32.03 m <sup>2</sup> /yr
200.0 kPa	0.54 m <sup>2</sup> /MN	29.96 m <sup>2</sup> /yr
400.0 kPa	0.27 m <sup>2</sup> /MN	37.45 m <sup>2</sup> /yr
800.0 kPa	0.11 m <sup>2</sup> /MN	26.32 m <sup>2</sup> /yr
1600.0 kPa	0.06 m <sup>2</sup> /MN	19.71 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.02 m <sup>2</sup> /MN	-----
50.0 kPa	0.02 m <sup>2</sup> /MN	-----
12.0 kPa	0.12 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120220
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317

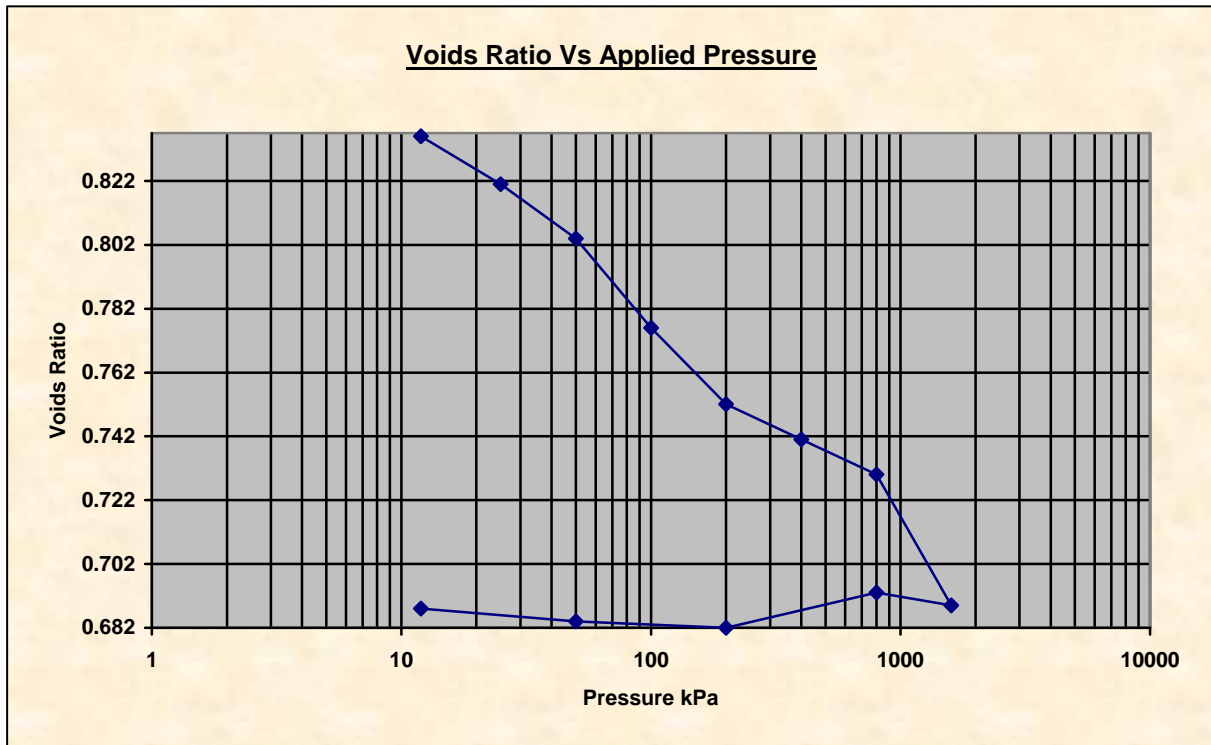
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 08	<b>Sample</b>	12-0287

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	B	<b>Description</b>	
<b>Depth within Sample</b>	75.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	141.84 g	<b>Condition</b>	Natural Moisture
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	4	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	108.80 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.89 mm	<b>Swelling Pressure</b>	0.0 kPa
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# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 08	<b>Sample</b>	12-0287

<b>Initial Moisture Content*</b>	12.6 % (trimmings: 12.3 %)	<b>Final Moisture Content</b>	3.2 %
<b>Initial Bulk Density</b>	1.61 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	1.60 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.43 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.55 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8373	<b>Final Void Ratio</b>	0.6879
<b>Initial Degree of Saturation</b>	39.34%	<b>Final Degree of Saturation</b>	12.09 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.07 m <sup>2</sup> /MN	39.75 m <sup>2</sup> /yr
25.0 kPa	0.62 m <sup>2</sup> /MN	7.74 m <sup>2</sup> /yr
50.0 kPa	0.37 m <sup>2</sup> /MN	16.70 m <sup>2</sup> /yr
100.0 kPa	0.32 m <sup>2</sup> /MN	35.03 m <sup>2</sup> /yr
200.0 kPa	0.13 m <sup>2</sup> /MN	2.08 m <sup>2</sup> /yr
400.0 kPa	0.03 m <sup>2</sup> /MN	3.58 m <sup>2</sup> /yr
800.0 kPa	0.02 m <sup>2</sup> /MN	4.92 m <sup>2</sup> /yr
1600.0 kPa	0.03 m <sup>2</sup> /MN	2.32 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.01 m <sup>2</sup> /MN	-----
12.0 kPa	0.06 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120220
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 8	<b>Depth [m] :</b>	1.250-1.700
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0288

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	93	90	79	70	60	56	47	39	29	20	18	16	9	5	5	3	3

**ATTERBERG LIMITS**

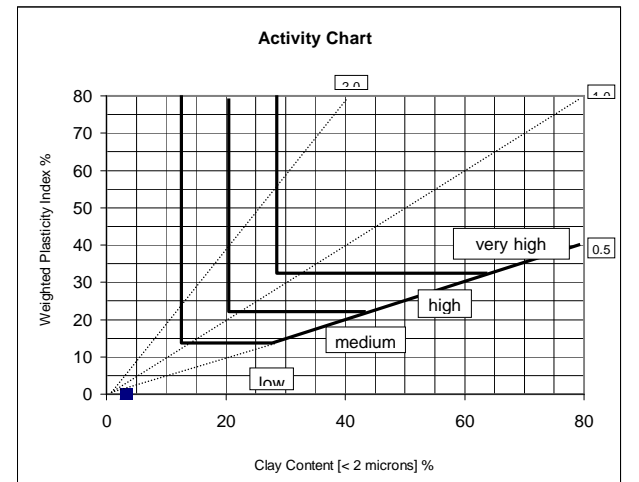
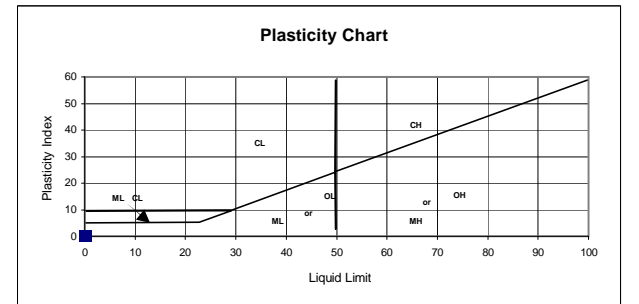
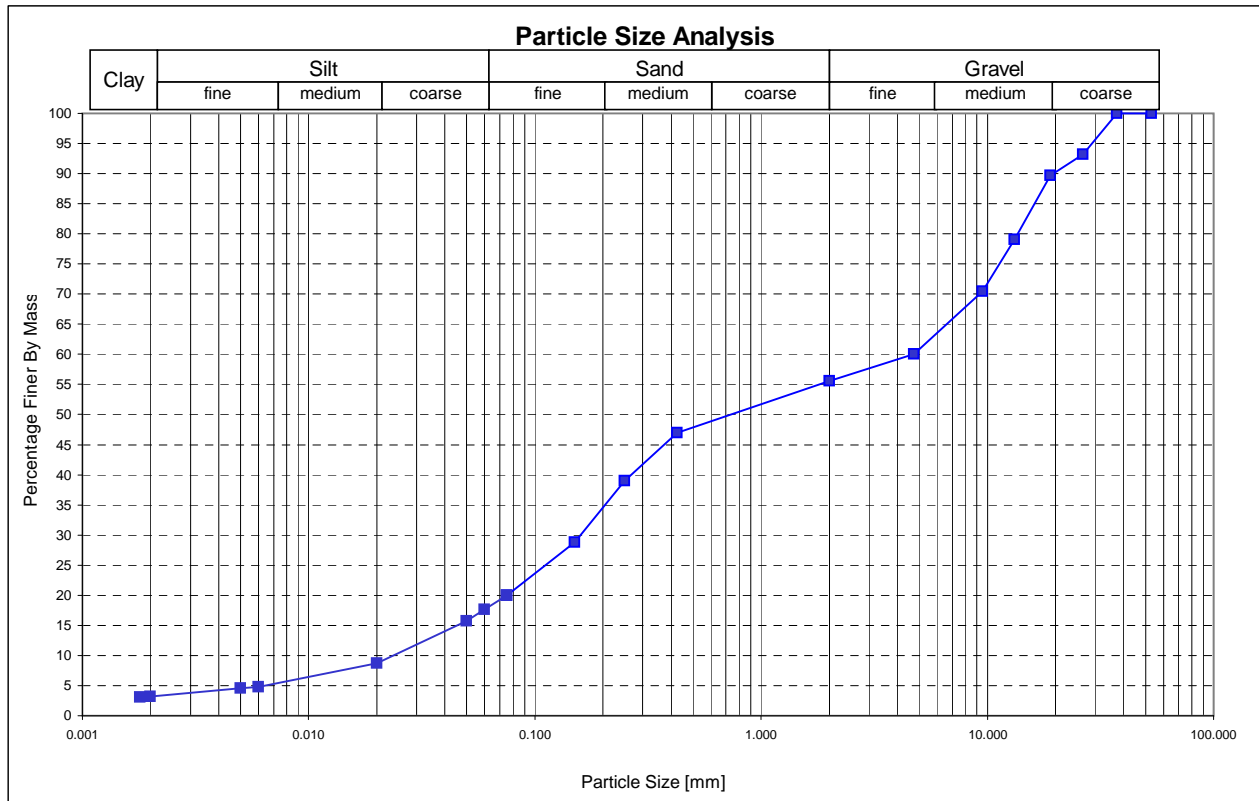
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
0	NP		0.0	1.77

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.1.b (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	3	<b>Silt :</b>	14	<b>Sand :</b>	38	<b>Gravel :</b>	44	<b>Fines :</b>	47	<b>Soil description :</b>	Dark Yellowish Orange Soil
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<b>D<sub>10</sub> :</b>	0.024	<b>D<sub>30</sub> :</b>	0.159	<b>D<sub>60</sub> :</b>	4.677	<b>Uniformity coefficient :</b>	198	<b>Curvature coefficient :</b>	0	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY : G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 9	<b>Depth [m] :</b>	1.300-2.300
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0289

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	93	85	74	66	55	47	36	26	23	20	12	6	6	4	4

**ATTERBERG LIMITS**

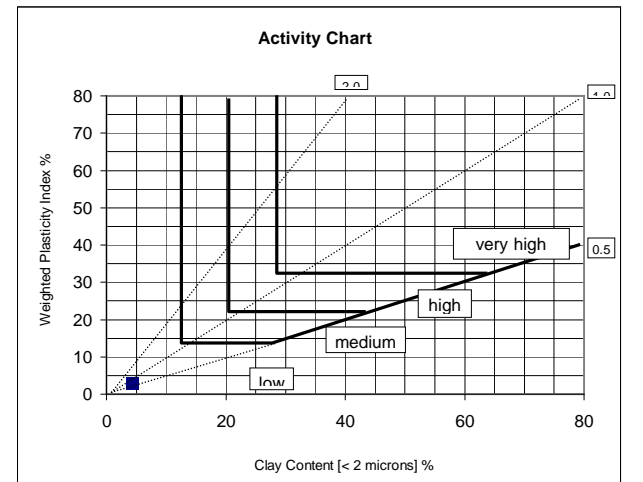
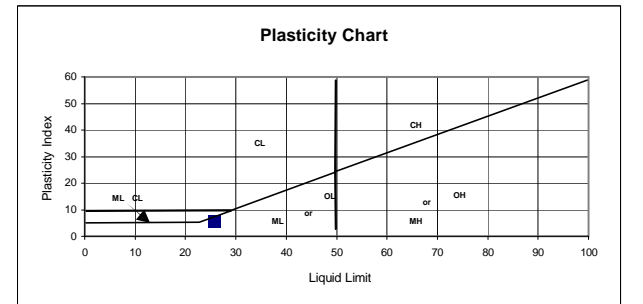
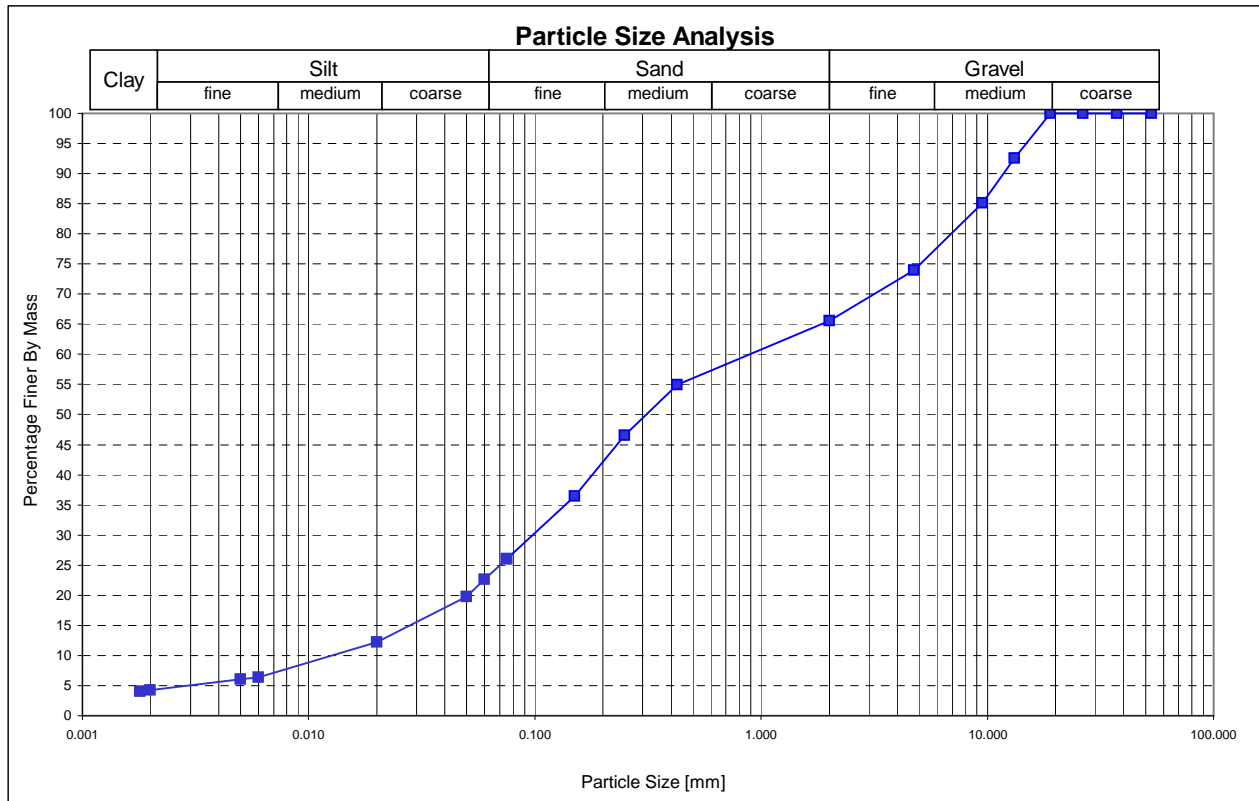
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
26	6	3	2.7	1.53

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM/SC	A.2.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	4	<b>Silt :</b>	18	<b>Sand :</b>	43	<b>Gravel :</b>	34	<b>Fines :</b>	55	<b>Soil description :</b>	Light Reddish Brown Soil
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<b>D<sub>10</sub> :</b>	0.013	<b>D<sub>30</sub> :</b>	0.098	<b>D<sub>60</sub> :</b>	0.884	<b>Uniformity coefficient :</b>	70	<b>Curvature coefficient :</b>	1	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder





**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC		<b>PROJECT :</b>	#999	
<b>Position :</b>	TP 10	<b>Depth [m] :</b>	0.300-0.650	<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0290

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	99	97	92	79	68	52	37	32	28	17	10	10	8	7

**ATTERBERG LIMITS**

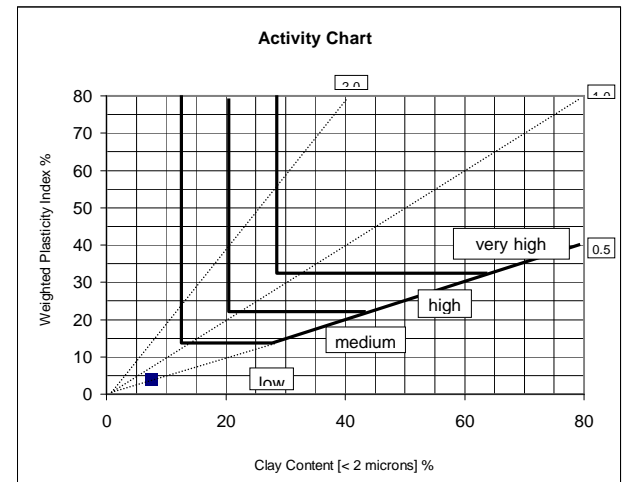
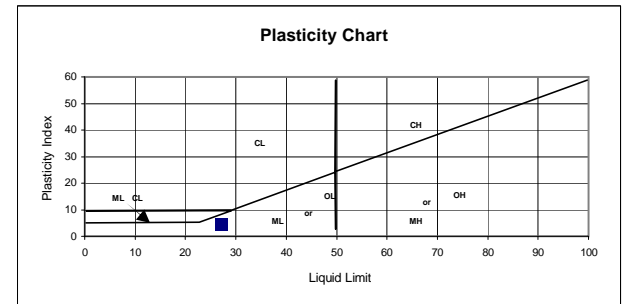
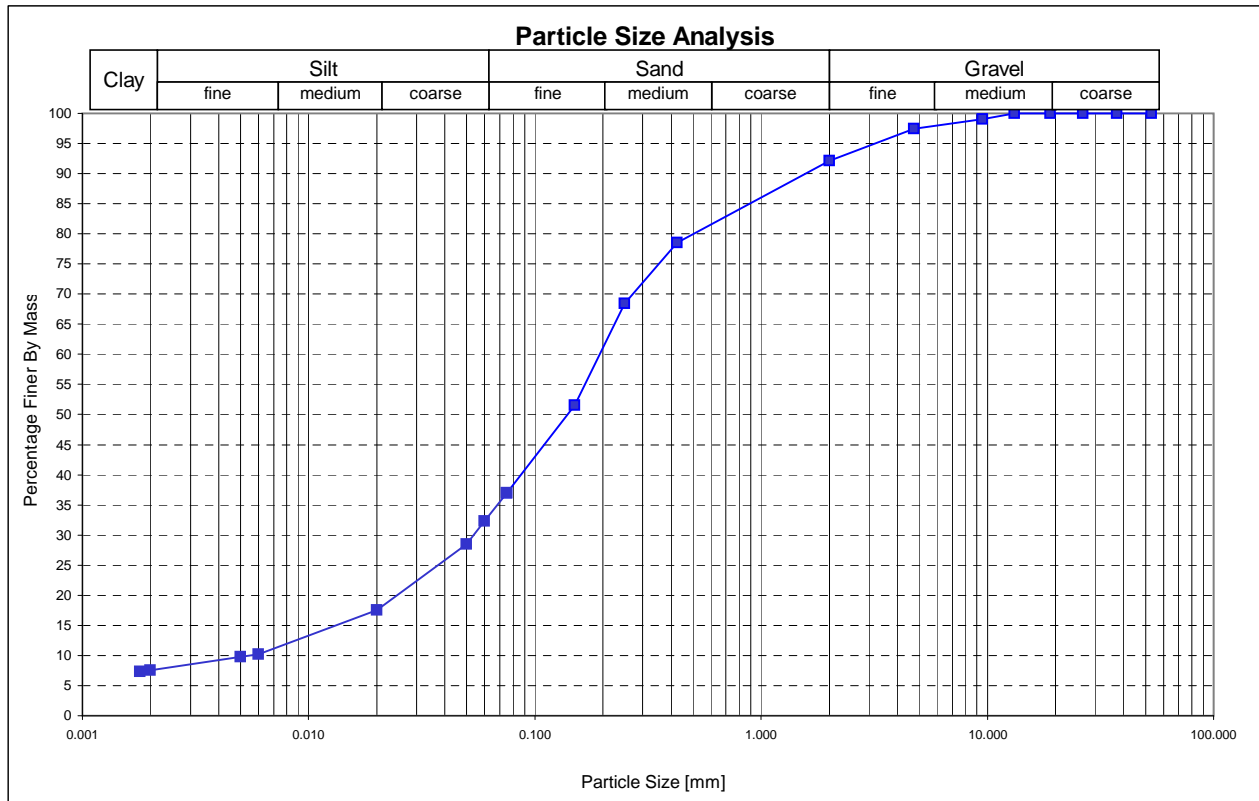
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
27	5	4	2.0	0.92

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	8	<b>Silt :</b>	25	<b>Sand :</b>	60	<b>Gravel :</b>	8	<b>Fines :</b>	79	<b>Soil description :</b>	Dark Brown Soil
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<b>D<sub>10</sub> :</b>	0.006	<b>D<sub>30</sub> :</b>	0.054	<b>D<sub>60</sub> :</b>	0.193	<b>Uniformity coefficient :</b>	35	<b>Curvature coefficient :</b>	3	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC		<b>PROJECT :</b>	#999	
<b>Position :</b>	TP 12	<b>Depth [m] :</b>	0.650-1.650	<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0291

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	92	85	70	60	50	47	42	34	29	25	18	13	12	8	8

**ATTERBERG LIMITS**

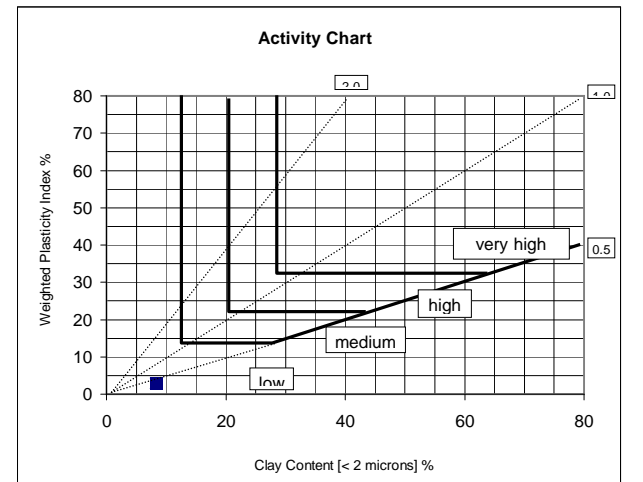
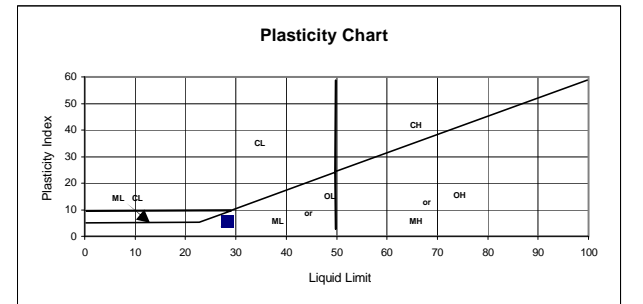
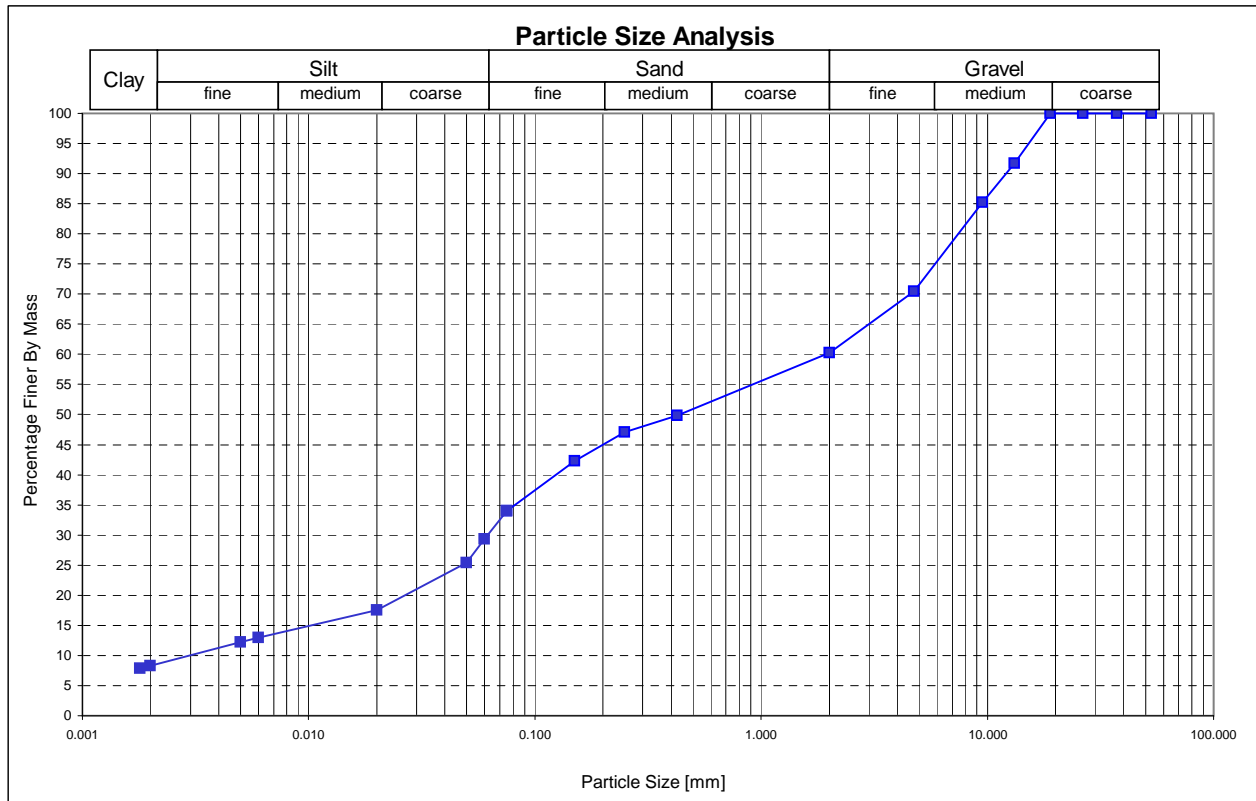
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
28	6	3	2.7	1.56

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.2.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	8	<b>Silt :</b>	21	<b>Sand :</b>	31	<b>Gravel :</b>	40	<b>Fines :</b>	50	<b>Soil description :</b>	Light Brown Soil
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<b>D<sub>10</sub> :</b>	0.003	<b>D<sub>30</sub> :</b>	0.062	<b>D<sub>60</sub> :</b>	1.913	<b>Uniformity coefficient :</b>	641	<b>Curvature coefficient :</b>	1	<b>Active program :</b>	YES
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**REMARKS:**

none

**CHECKED BY :**

G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 13	<b>Depth [m] :</b>	@ 0.80m
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
21-Feb-12	<b>Sample No.</b>	12/0292

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	100	100	92	86	78	57	47	38	27	18	17	12	12

**ATTERBERG LIMITS**

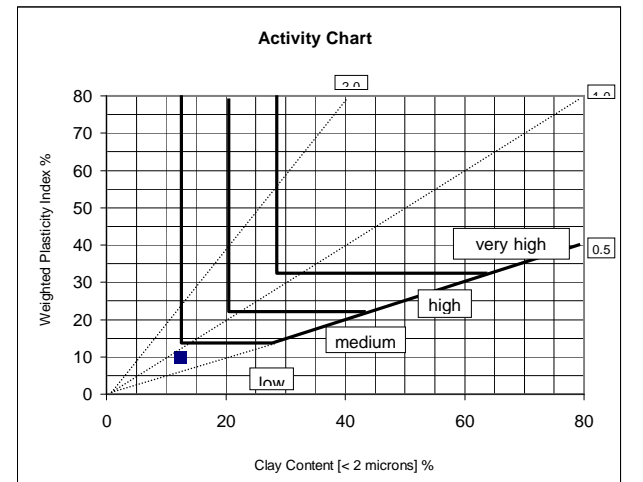
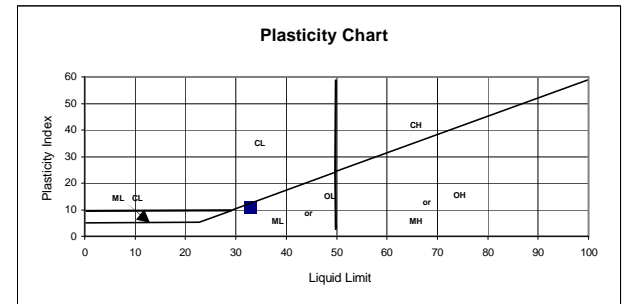
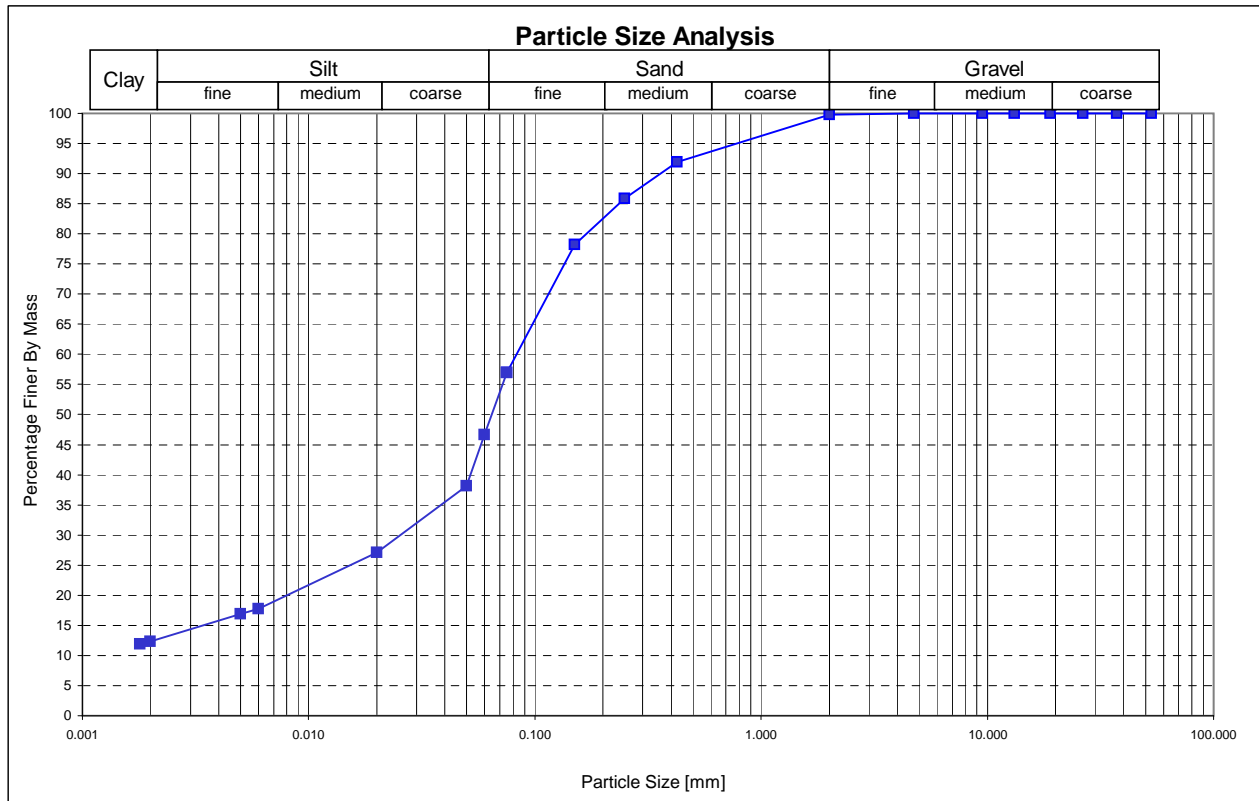
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
33	11	10	5.4	0.51

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
CL	A.6 (4)	

<b>Soil constituents % :</b>	<b>Clay :</b>	12	<b>Silt :</b>	34	<b>Sand :</b>	53	<b>Gravel :</b>	0	<b>Fines :</b>	92	<b>Soil description :</b>	Dark Reddish Brown Soil
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<b>D<sub>10</sub> :</b>	<b>D<sub>30</sub> :</b>	0.025	<b>D<sub>60</sub> :</b>	0.083	<b>Uniformity coefficient :</b>		<b>Curvature coefficient :</b>		<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder

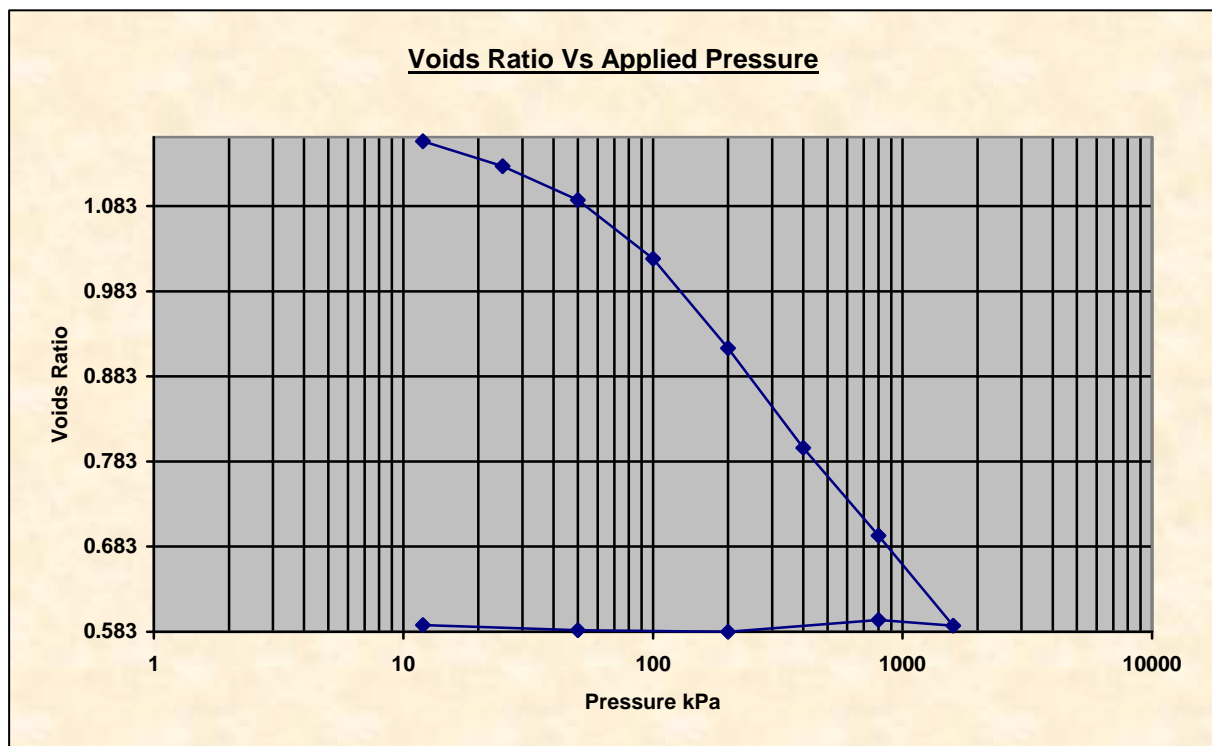
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 13	<b>Sample</b>	12-0287

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.80 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	A	<b>Description</b>	
<b>Depth within Sample</b>	50.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	138.38 g	<b>Condition</b>	Inundated
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	5	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	108.40 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	9.24 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 13	<b>Sample</b>	12-0287

<b>Initial Moisture Content*</b>	29.3 % (trimmings: 28.6 %)	<b>Final Moisture Content</b>	20.6 %
<b>Initial Bulk Density</b>	1.57 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	1.99 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.21 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.65 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	1.1635	<b>Final Void Ratio</b>	0.5907
<b>Initial Degree of Saturation</b>	66.04%	<b>Final Degree of Saturation</b>	91.19 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.19 m <sup>2</sup> /MN	-----
25.0 kPa	1.03 m <sup>2</sup> /MN	37.88 m <sup>2</sup> /yr
50.0 kPa	0.74 m <sup>2</sup> /MN	30.67 m <sup>2</sup> /yr
100.0 kPa	0.66 m <sup>2</sup> /MN	32.46 m <sup>2</sup> /yr
200.0 kPa	0.52 m <sup>2</sup> /MN	47.46 m <sup>2</sup> /yr
400.0 kPa	0.30 m <sup>2</sup> /MN	45.96 m <sup>2</sup> /yr
800.0 kPa	0.14 m <sup>2</sup> /MN	25.77 m <sup>2</sup> /yr
1600.0 kPa	0.08 m <sup>2</sup> /MN	16.14 m <sup>2</sup> /yr
800.0 kPa	0.01 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.01 m <sup>2</sup> /MN	-----
12.0 kPa	0.09 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120220
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317

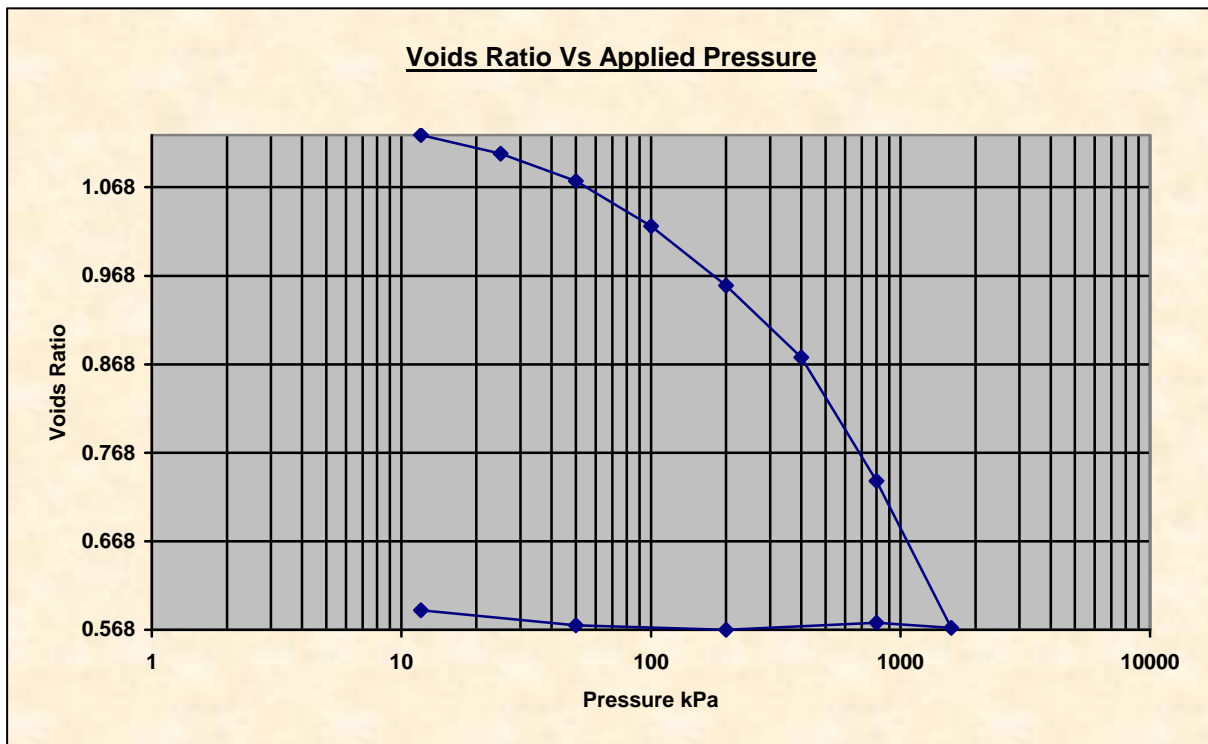
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 13	<b>Sample</b>	12-0292

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.80 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	B	<b>Description</b>	
<b>Depth within Sample</b>	75.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	140.03 g	<b>Condition</b>	Natural Moisture
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	6	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	108.50 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	9.42 mm	<b>Swelling Pressure</b>	0.0 kPa
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# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 13	<b>Sample</b>	12-0292

<b>Initial Moisture Content*</b>	28.5 % (trimmings: 28.6 %)	<b>Final Moisture Content</b>	12.8 %
<b>Initial Bulk Density</b>	1.58 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	1.86 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.23 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.65 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	1.1238	<b>Final Void Ratio</b>	0.5896
<b>Initial Degree of Saturation</b>	66.37%	<b>Final Degree of Saturation</b>	57.08 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	-0.12 m <sup>2</sup> /MN	-----
25.0 kPa	0.76 m <sup>2</sup> /MN	20.60 m <sup>2</sup> /yr
50.0 kPa	0.59 m <sup>2</sup> /MN	30.59 m <sup>2</sup> /yr
100.0 kPa	0.49 m <sup>2</sup> /MN	33.96 m <sup>2</sup> /yr
200.0 kPa	0.33 m <sup>2</sup> /MN	29.93 m <sup>2</sup> /yr
400.0 kPa	0.21 m <sup>2</sup> /MN	27.94 m <sup>2</sup> /yr
800.0 kPa	0.19 m <sup>2</sup> /MN	35.58 m <sup>2</sup> /yr
1600.0 kPa	0.12 m <sup>2</sup> /MN	48.70 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.02 m <sup>2</sup> /MN	-----
12.0 kPa	0.28 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120220
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC		<b>PROJECT :</b>	#999	
<b>Position :</b>	TP 13	<b>Depth [m] :</b>	1.200-1.900	<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
21-Feb-12	<b>Sample No.</b>	12/0293

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	97	93	84	79	74	56	45	36	24	15	15	11	11

**ATTERBERG LIMITS**

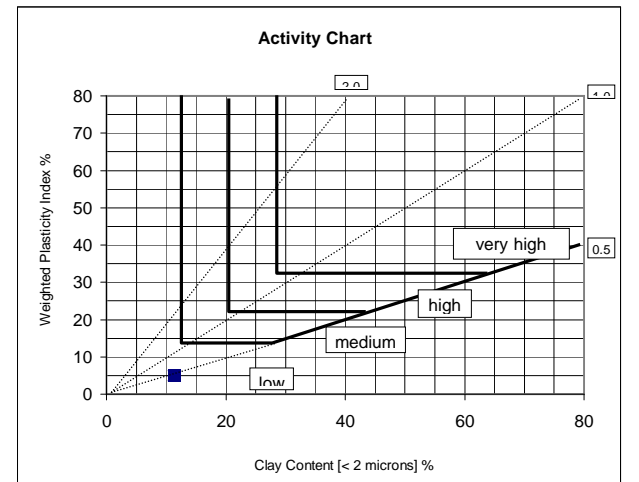
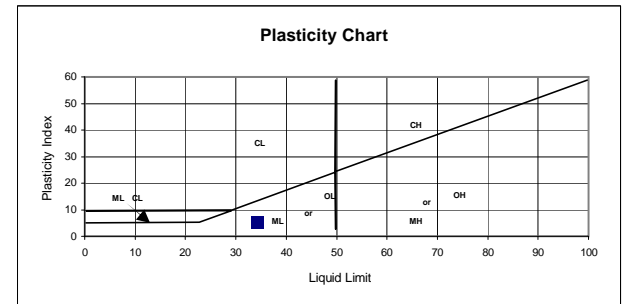
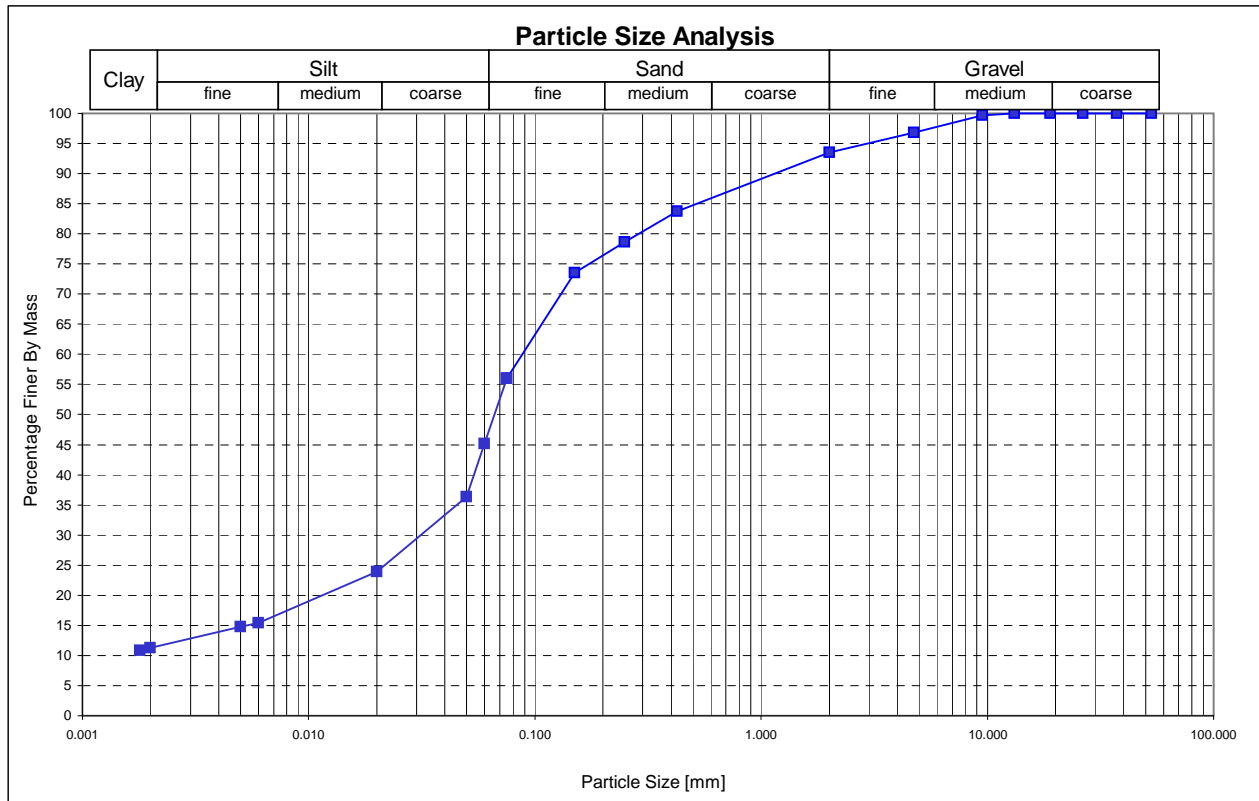
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
34	5	5	5.4	0.67

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
ML	A.4 (4)	

<b>Soil constituents % :</b>	<b>Clay :</b>	11	<b>Silt :</b>	34	<b>Sand :</b>	48	<b>Gravel :</b>	7	<b>Fines :</b>	84	<b>Soil description :</b>	Dark Reddish Brown Soil
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<b>D<sub>10</sub> :</b>	<b>D<sub>30</sub> :</b>	0.031	<b>D<sub>60</sub> :</b>	0.088	<b>Uniformity coefficient :</b>		<b>Curvature coefficient :</b>		<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder

# Engeo Lab (Pty) Ltd

## INSITU DENSITY & MOISTURE DETERMINATION

JOB NO: 1450 (#990)

DATE: 1-Mar-2012

Sample Number			0389				
Position			TP 13				
Depth			@ 1.50m				
Mass of sample in air	(g)	a	77.40				
Mass of waxed sample in air	(g)	b	81.60				
Mass of waxed sample in water @ 25°C	(g)	c	35.90				
Mass of water displaced (b - c)	(g)	d	45.70				
Mass of wax (b - a)	(g)	e	4.20				
Density of wax	(kg/m <sup>3</sup> )	f	0.93				
Volume of wax (e / f)	(ml)	g	4.52				
Volume of sample (d - g)	(ml)	h	41.18				
Wet density of sample ( a / h *100 )	(kg/m <sup>3</sup> )	i	1879				
Dry density of sample ( i / (100 + k) * 1000)	(kg/m <sup>3</sup> )	j	<b>1473</b>				
Mass Pan & Wet Mat.	(g)		78.14				
Mass Pan & Dry Mat.	(g)		73.34				
Mass Pan	(g)		55.93				
% Moisture	(%)	k	<b>27.6</b>				
Laboratory Determined Max. Dry Density	(kg/m <sup>3</sup> )	l					
Laboratory Determined O.M.C.	%	m					
Percentage of Max. Dry Density (j/l*100)	%						
Percentage Wet (-) Dry (+) of O.M.C. (m-k)	%						
Specific Gravity			<b>2.62</b>				
Void ratio			0.779				
Degree of saturation	%		92.8				



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 14	<b>Depth [m] :</b>	1.000-1.600
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0294

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	98	91	84	82	78	64	54	45	30	23	22	19	19

**ATTERBERG LIMITS**

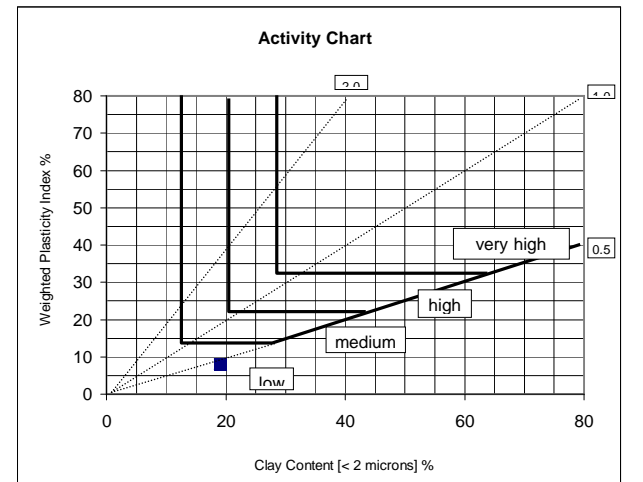
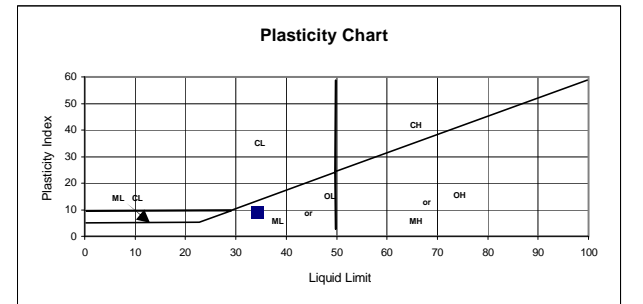
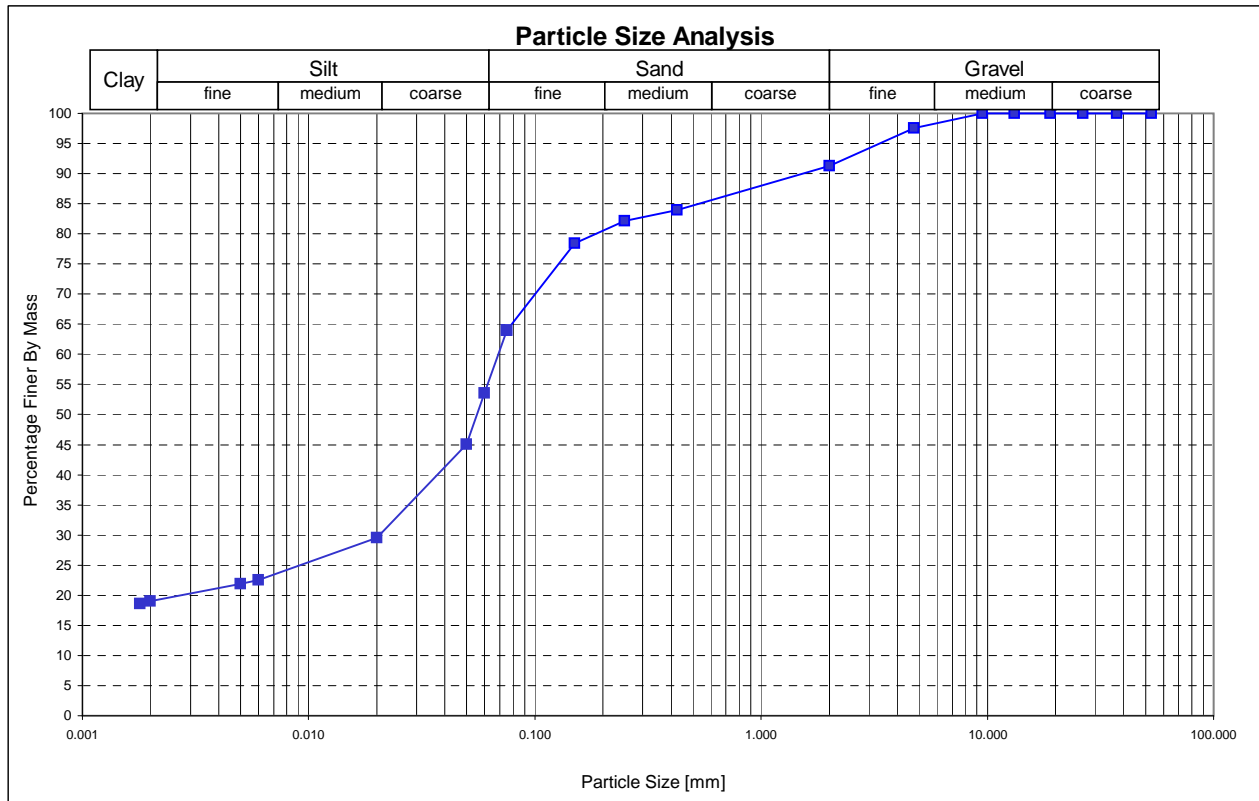
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
34	9	8	4.7	0.61

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
ML	A.4 (6)	

<b>Soil constituents % :</b>	<b>Clay :</b>	19	<b>Silt :</b>	35	<b>Sand :</b>	38	<b>Gravel :</b>	9	<b>Fines :</b>	84	<b>Soil description :</b>	Buff Soil
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<b>D<sub>10</sub> :</b>	<b>D<sub>30</sub> :</b>	0.021	<b>D<sub>60</sub> :</b>	0.069	<b>Uniformity coefficient :</b>		<b>Curvature coefficient :</b>		<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC		<b>PROJECT :</b>	#999	
<b>Position :</b>	TP 16	<b>Depth [m] :</b>	0.200-0.600	<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0295

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	99	99	97	92	87	72	45	38	33	22	15	14	9	9

**ATTERBERG LIMITS**

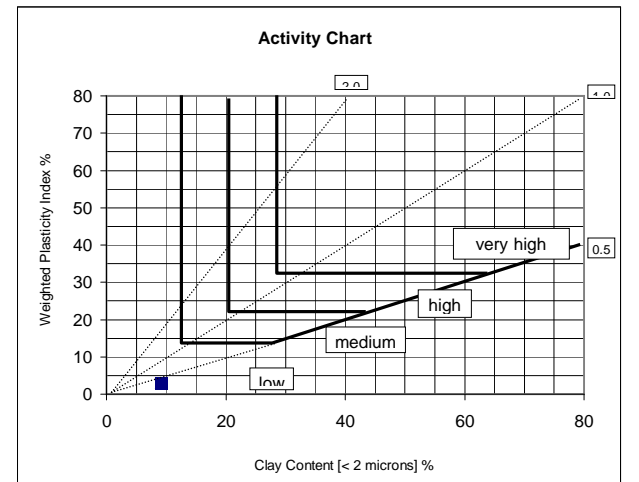
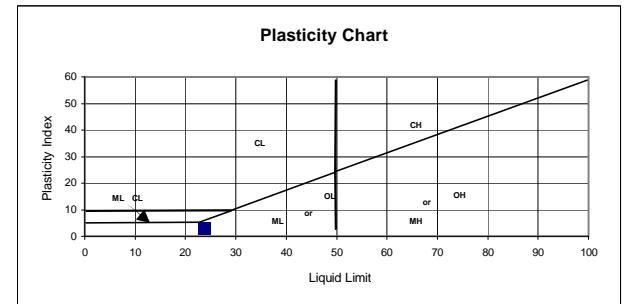
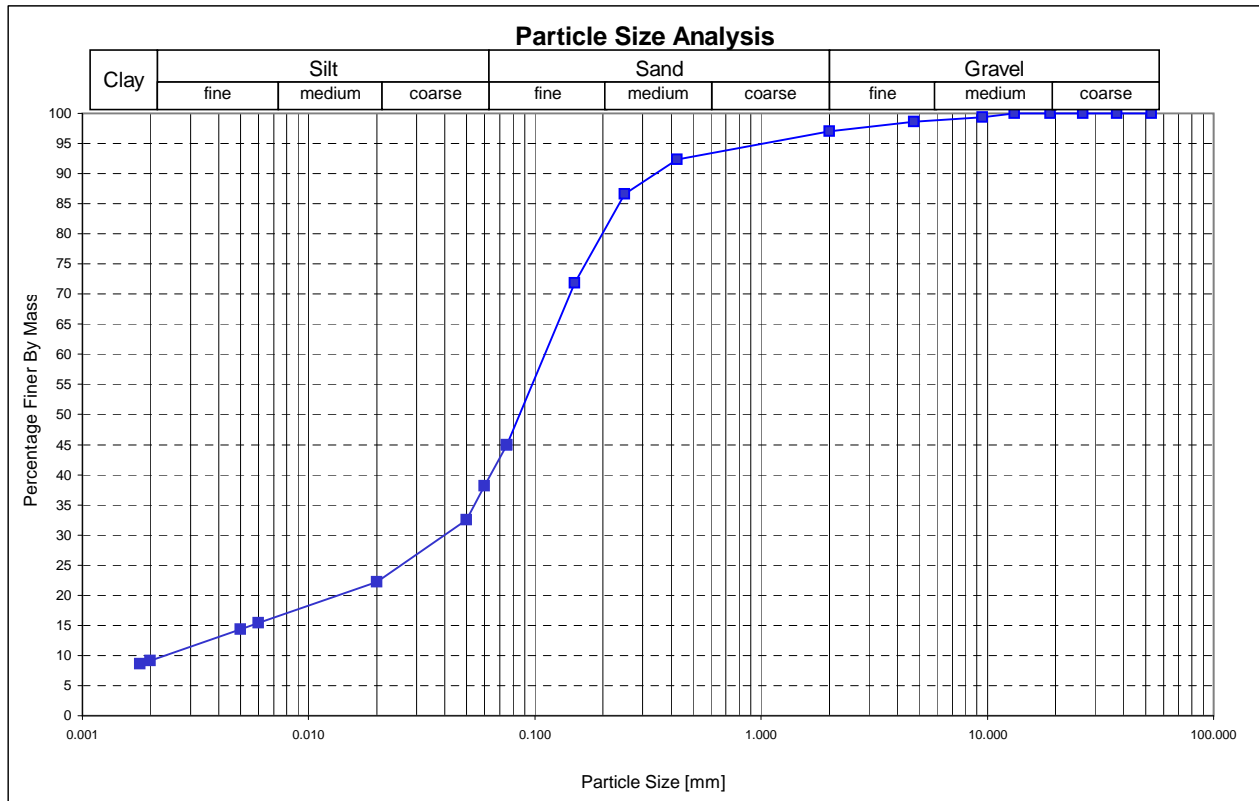
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
24	3	3	1.3	0.66

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.4 (2)	

<b>Soil constituents % :</b>	<b>Clay :</b>	9	<b>Silt :</b>	29	<b>Sand :</b>	59	<b>Gravel :</b>	3	<b>Fines :</b>	92	<b>Soil description :</b>	Dark Brown Soil
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<b>D<sub>10</sub> :</b>	0.002	<b>D<sub>30</sub> :</b>	0.040	<b>D<sub>60</sub> :</b>	0.110	<b>Uniformity coefficient :</b>	48	<b>Curvature coefficient :</b>	6	<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 16	<b>Depth [m] :</b>	0.700-1.300
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0296

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	94	75	70	63	57	49	46	42	30	25	20	12	6	6	4	4

**ATTERBERG LIMITS**

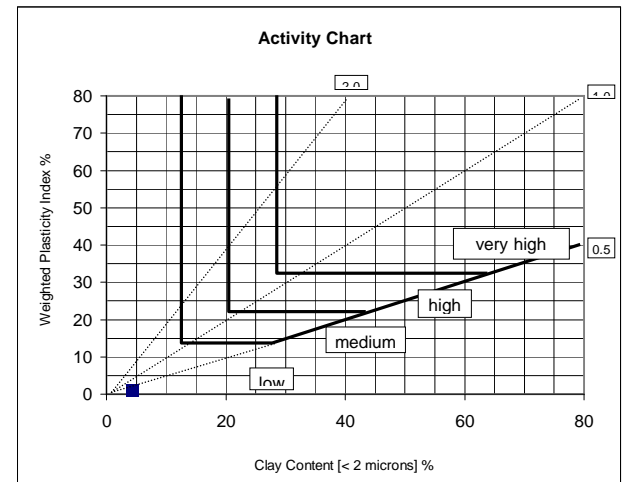
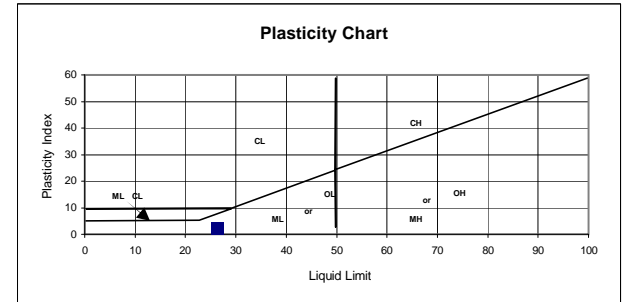
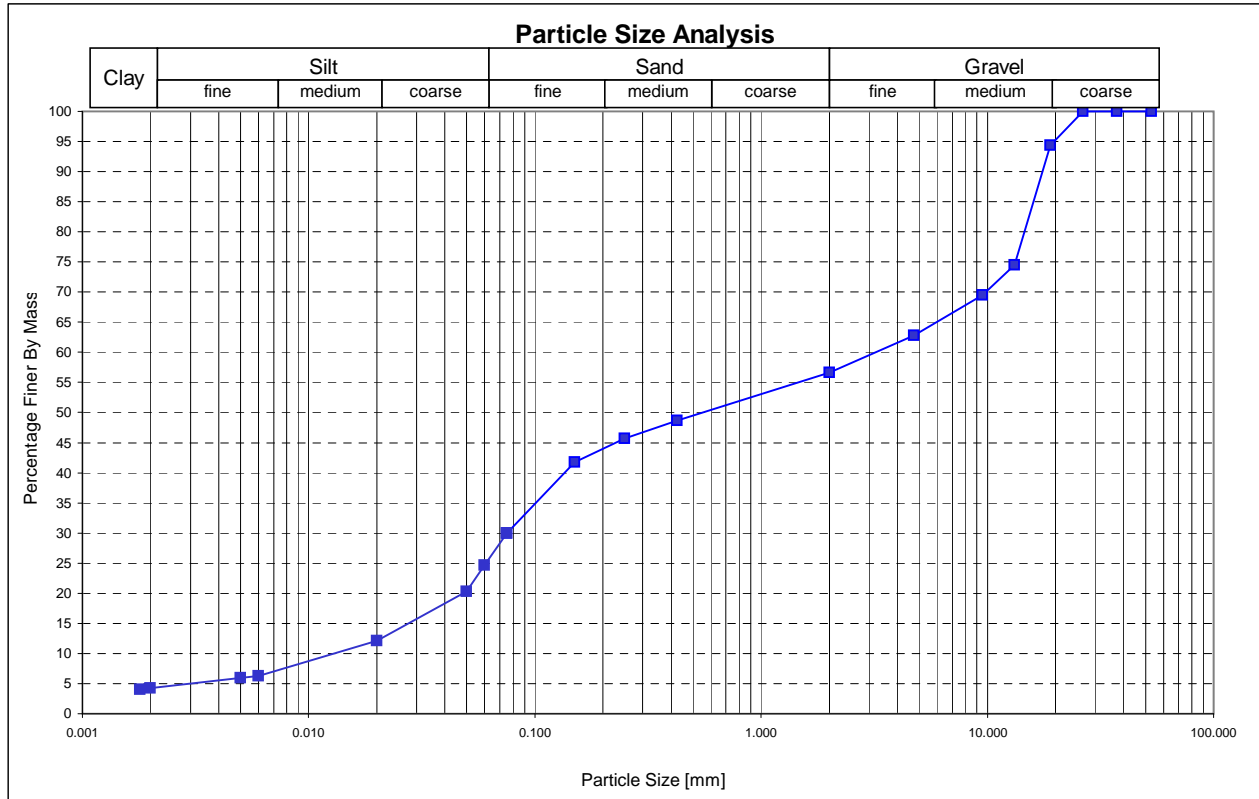
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
26	2		1.0	1.65

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.2.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	4	<b>Silt :</b>	20	<b>Sand :</b>	32	<b>Gravel :</b>	43	<b>Fines :</b>	49	<b>Soil description :</b>	Light Grey Soil
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<b>D<sub>10</sub> :</b>	0.013	<b>D<sub>30</sub> :</b>	0.075	<b>D<sub>60</sub> :</b>	3.207	<b>Uniformity coefficient :</b>	250	<b>Curvature coefficient :</b>	0	<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder





**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 18	<b>Depth [m] :</b>	0.800-1.600
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0297

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	95	89	82	76	58	47	36	26	22	19	11	6	6	5	5

**ATTERBERG LIMITS**

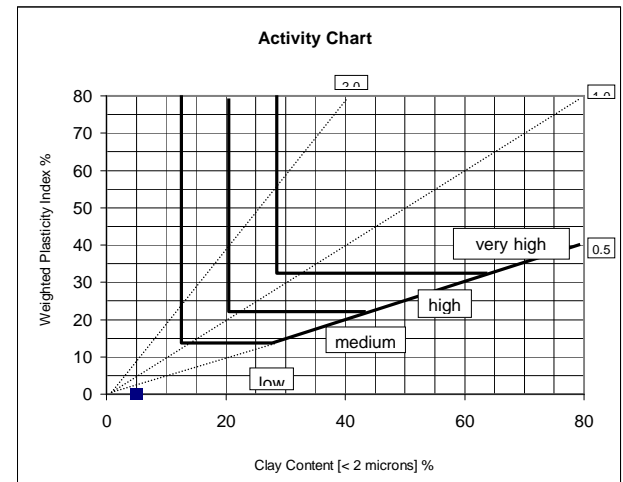
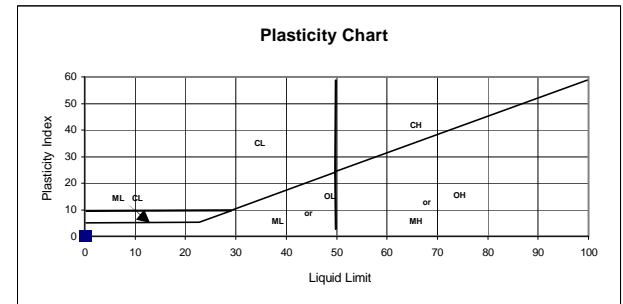
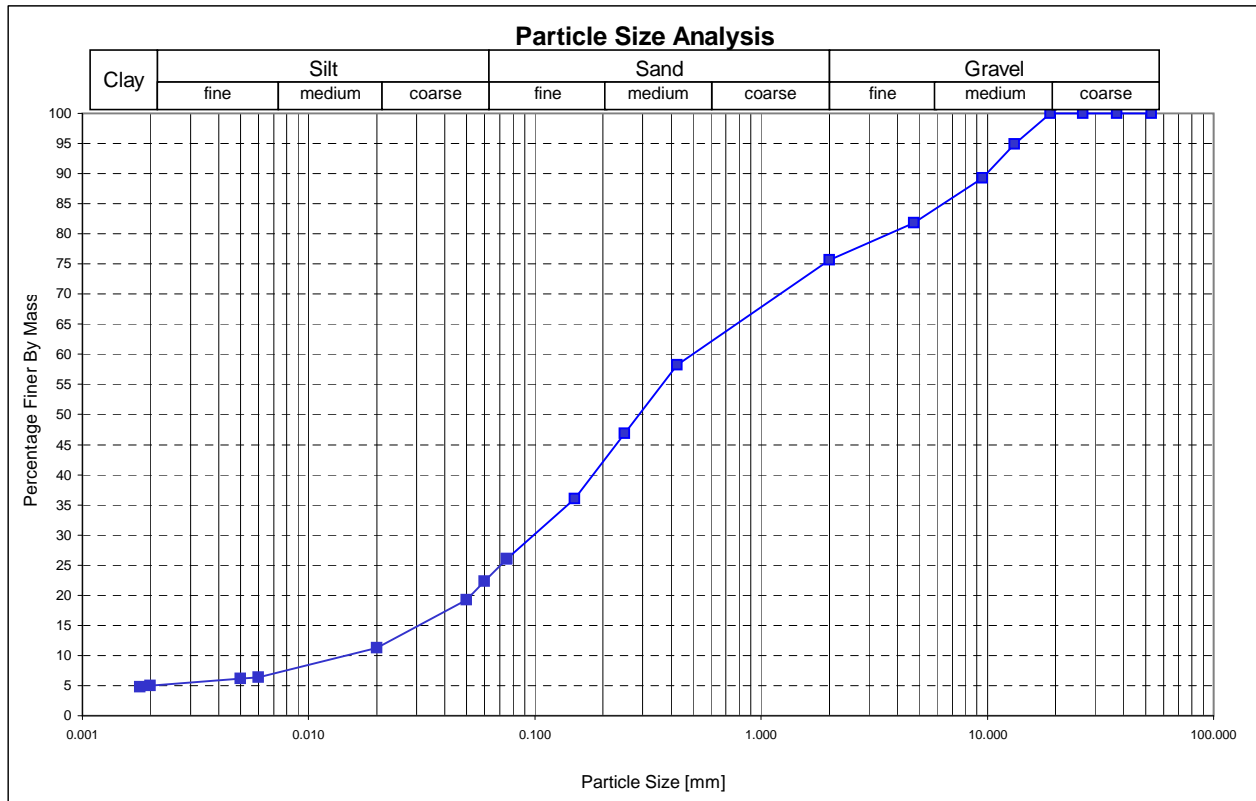
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
0	NP		0.0	1.40

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.2.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	5	<b>Silt :</b>	17	<b>Sand :</b>	53	<b>Gravel :</b>	24	<b>Fines :</b>	58	<b>Soil description :</b>	Dark Yellowish Orange Soil
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<b>D<sub>10</sub> :</b>	0.015	<b>D<sub>30</sub> :</b>	0.099	<b>D<sub>60</sub> :</b>	0.497	<b>Uniformity coefficient :</b>	34	<b>Curvature coefficient :</b>	1	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder

# Engeo Lab (Pty) Ltd

## INSITU DENSITY & MOISTURE DETERMINATION

JOB NO: 1450 (#990)  
DATE: 1-Mar-2012

Sample Number			0298				
Position			TP 18				
Depth			@ 1.00m				
Mass of sample in air	(g)	a	142.60				
Mass of waxed sample in air	(g)	b	148.80				
Mass of waxed sample in water @ 25°C	(g)	c	75.80				
Mass of water displaced (b - c)	(g)	d	73.00				
Mass of wax (b - a)	(g)	e	6.20				
Density of wax	(kg/m <sup>3</sup> )	f	0.93				
Volume of wax (e / f)	(ml)	g	6.67				
Volume of sample (d - g)	(ml)	h	66.33				
Wet density of sample ( a / h *100 )	(kg/m <sup>3</sup> )	l	2150				
Dry density of sample ( l / (100 + k) * 1000)	(kg/m <sup>3</sup> )	j	<b>1949</b>				
Mass Pan & Wet Mat.	(g)		83 91				
Mass Pan & Dry Mat.	(g)		81 32				
Mass Pan	(g)		56 07				
% Moisture	(%)	k	<b>10.3</b>				
Laboratory Determined Max. Dry Density	(kg/m <sup>3</sup> )	l					
Laboratory Determined O.M.C.	%	m					
Percentage of Max. Dry Density (j/l*100)	%						
Percentage Wet (-) Dry (+) of O.M.C. (m-k)	%						
Specific Gravity			<b>2.61</b>				
Void ratio			0.339				
Degree of saturation	%		79.3				



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC		<b>PROJECT :</b>	#999	
<b>Position :</b>	TP 21	<b>Depth [m] :</b>	0.300-0.600	<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0299

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	99	96	81	62	52	37	22	18	16	9	3	3	2	2

**ATTERBERG LIMITS**

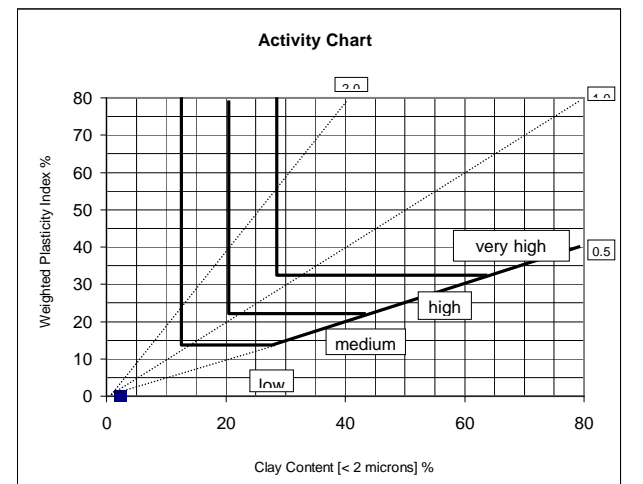
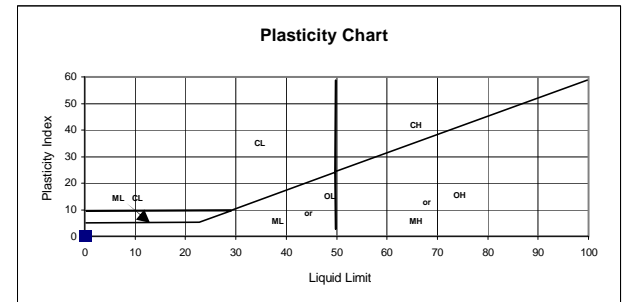
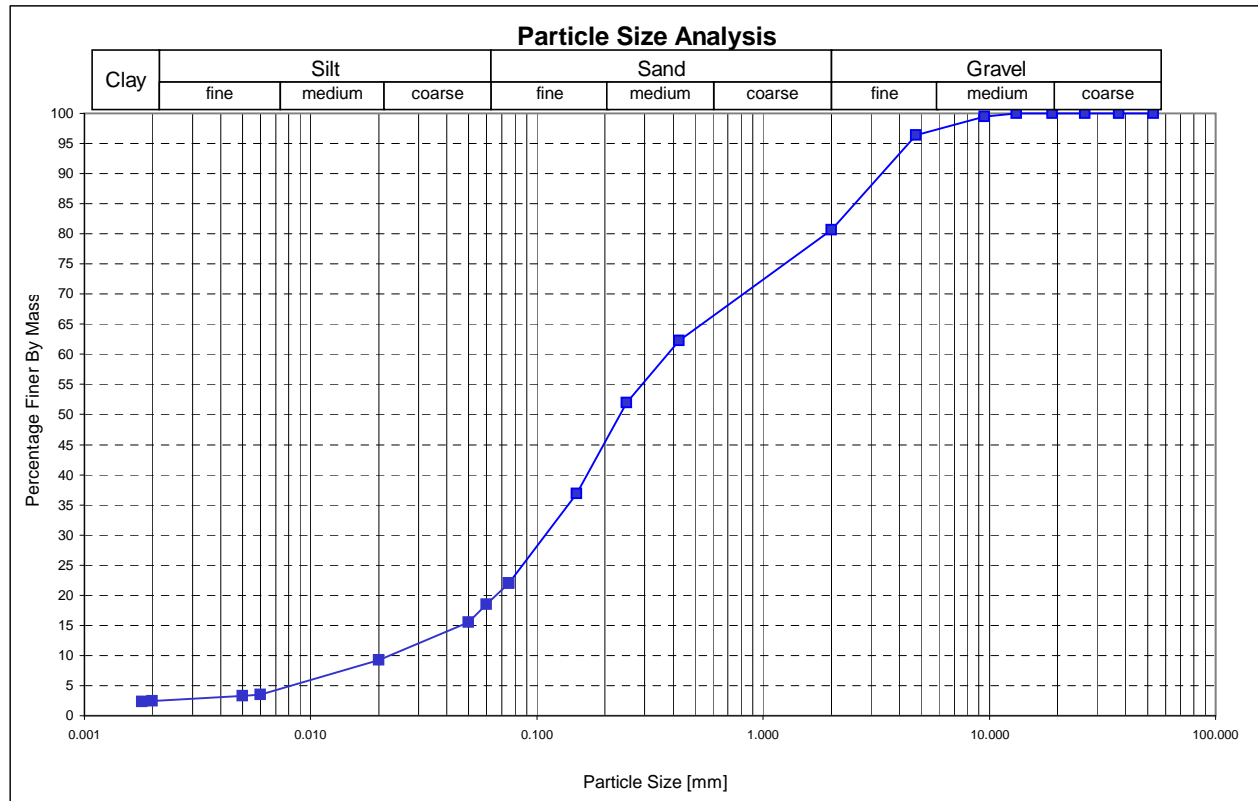
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
0	NP		0.0	1.35

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.2.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	2	<b>Silt :</b>	16	<b>Sand :</b>	62	<b>Gravel :</b>	19	<b>Fines :</b>	62	<b>Soil description :</b>	Dark Brown Soil
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<b>D<sub>10</sub> :</b>	0.022	<b>D<sub>30</sub> :</b>	0.109	<b>D<sub>60</sub> :</b>	0.378	<b>Uniformity coefficient :</b>	17	<b>Curvature coefficient :</b>	1	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY : G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 21	<b>Depth [m] :</b>	0.600-0.850
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0300

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	86	80	66	52	36	23	15	12	9	5	4	4	2	1	1	1	1

**ATTERBERG LIMITS**

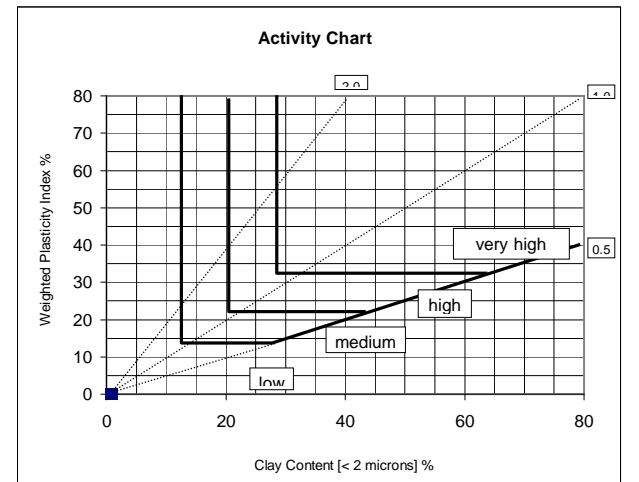
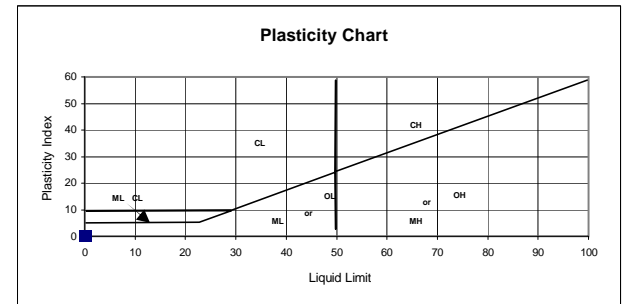
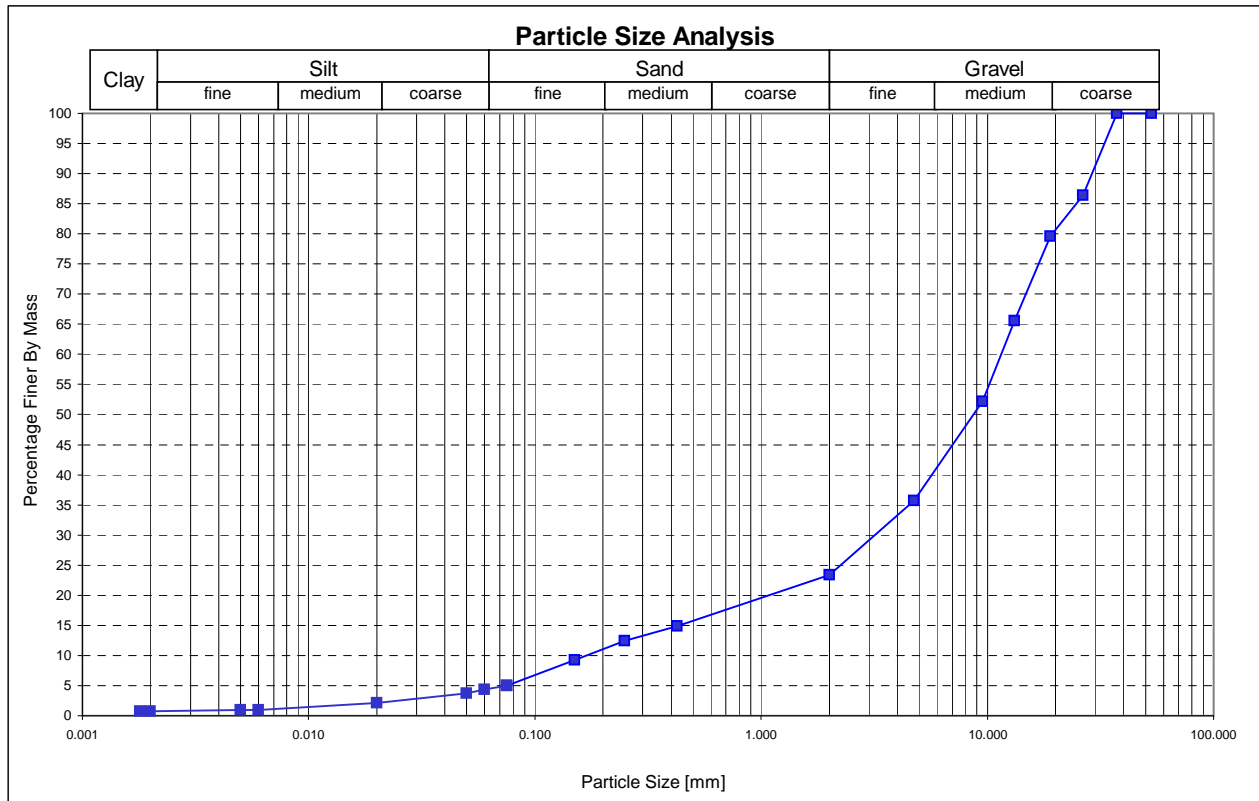
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
0	NP		0.0	2.57

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
GP	A.1.a (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	1	<b>Silt :</b>	4	<b>Sand :</b>	19	<b>Gravel :</b>	77	<b>Fines :</b>	15	<b>Soil description :</b>	Dark Brown Soil
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<b>D<sub>10</sub> :</b>	0.170	<b>D<sub>30</sub> :</b>	3.186	<b>D<sub>60</sub> :</b>	11.517	<b>Uniformity coefficient :</b>	68	<b>Curvature coefficient :</b>	5	<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC		<b>PROJECT :</b>	#999	
<b>Position :</b>	TP 21	<b>Depth [m] :</b>	0.850-1.500	<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0301

**SIEVE ANALYSIS (% PASSING)**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	98	96	80	65	44	37	31	22	19	17	9	4	4	3	2

**ATTERBERG LIMITS**

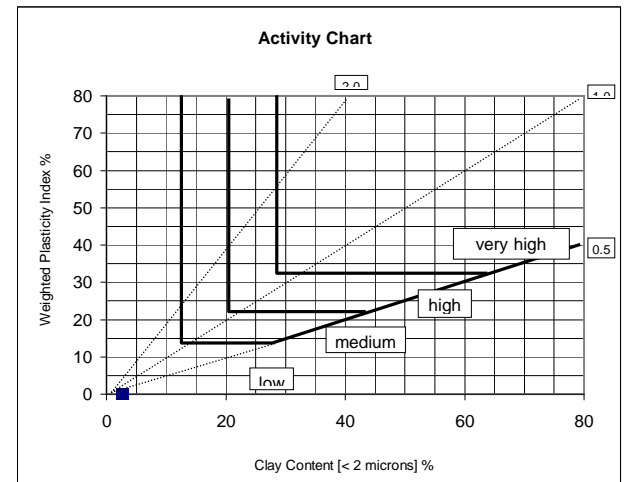
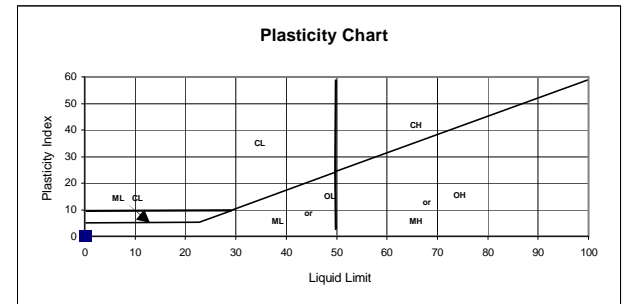
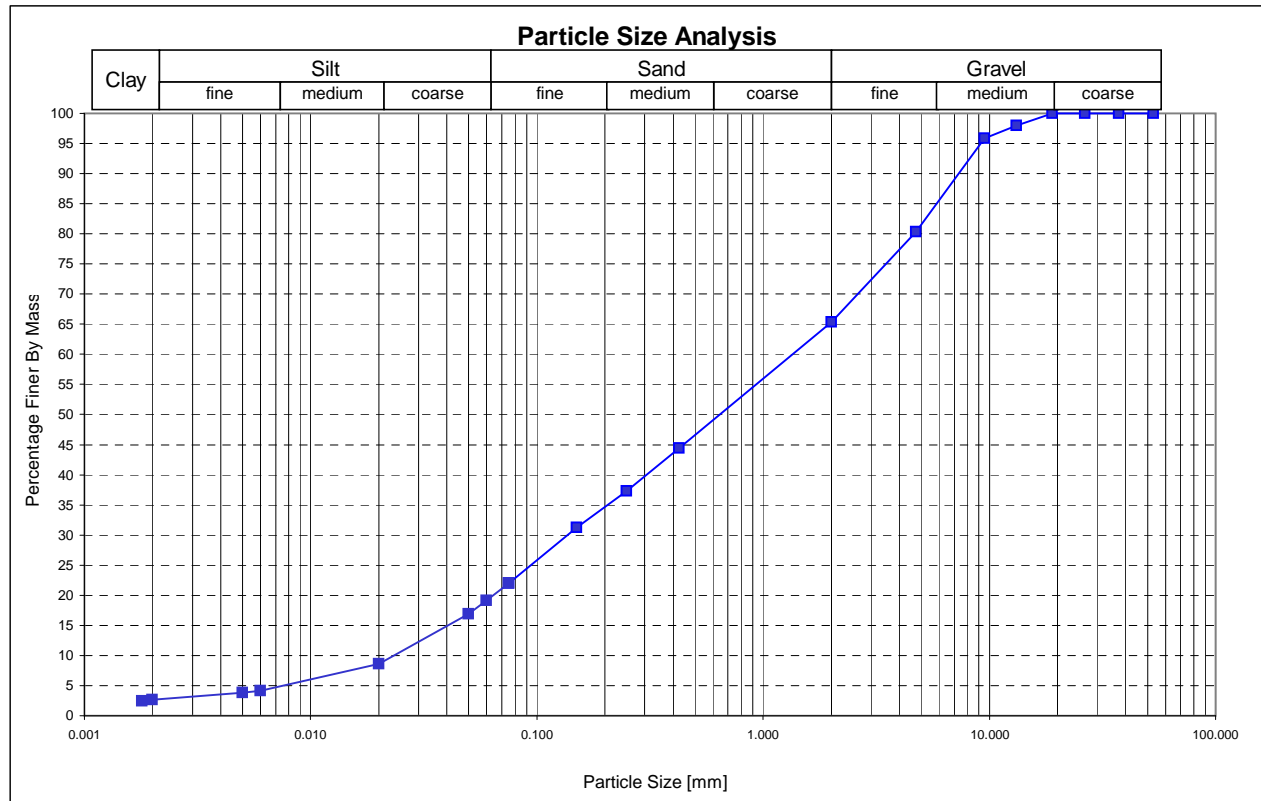
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
0	NP		0.0	1.68

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.1.b (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	3	<b>Silt :</b>	17	<b>Sand :</b>	46	<b>Gravel :</b>	35	<b>Fines :</b>	44	<b>Soil description :</b>	Pale Red Soil
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<b>D<sub>10</sub> :</b>	0.023	<b>D<sub>30</sub> :</b>	0.136	<b>D<sub>60</sub> :</b>	1.345	<b>Uniformity coefficient :</b>	58	<b>Curvature coefficient :</b>	1	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder

# Engeo Lab (Pty) Ltd

## INSITU DENSITY & MOISTURE DETERMINATION

JOB NO: 1450 (#990)

DATE: 1-Mar-2012

Sample Number			0302				
Position			TP 21				
Depth			@ 1.00m				
Mass of sample in air	(g)	a	145.50				
Mass of waxed sample in air	(g)	b	153.30				
Mass of waxed sample in water @ 25°C	(g)	c	76.50				
Mass of water displaced (b - c)	(g)	d	76.80				
Mass of wax (b - a)	(g)	e	7.80				
Density of wax	(kg/m <sup>3</sup> )	f	0.93				
Volume of wax (e / f)	(ml)	g	8.39				
Volume of sample (d - g)	(ml)	h	68.41				
Wet density of sample ( a / h *100 )	(kg/m <sup>3</sup> )	i	2127				
Dry density of sample ( i / (100 + k) * 1000)	(kg/m <sup>3</sup> )	j	<b>1890</b>				
Mass Pan & Wet Mat.	(g)		88.33				
Mass Pan & Dry Mat.	(g)		84.72				
Mass Pan	(g)		55.83				
% Moisture	(%)	k	<b>12.5</b>				
Laboratory Determined Max. Dry Density	(kg/m <sup>3</sup> )	l					
Laboratory Determined O.M.C.	%	m					
Percentage of Max. Dry Density (j/l*100)	%						
Percentage Wet (-) Dry (+) of O.M.C. (m-k)	%						
Specific Gravity			<b>2.63</b>				
Void ratio			0.392				
Degree of saturation	%		83.9				





**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 22	<b>Depth [m] :</b>	0.300-0.800
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0303

**SIEVE ANALYSIS (% PASSING)**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	95	92	88	78	68	53	36	30	25	14	8	8	5	5

**ATTERBERG LIMITS**

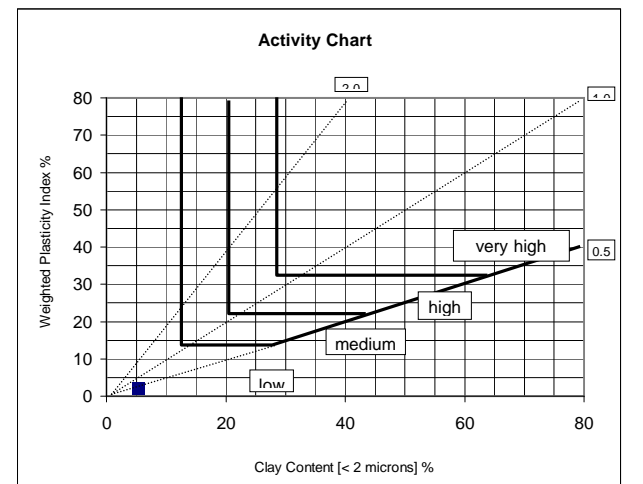
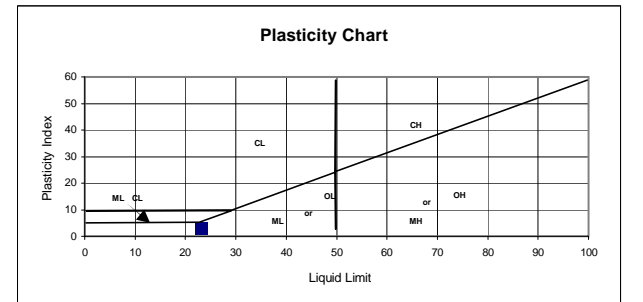
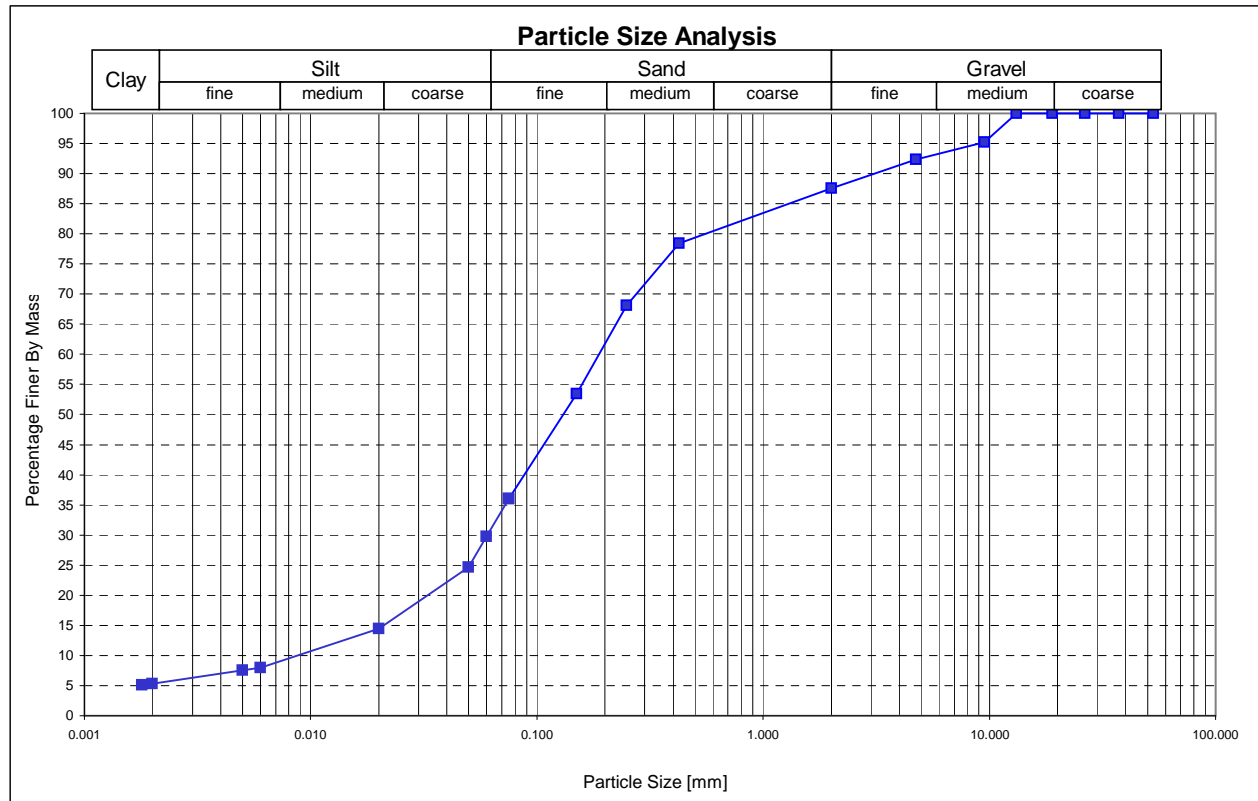
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
23	3	2	1.7	0.98

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	5	<b>Silt :</b>	24	<b>Sand :</b>	58	<b>Gravel :</b>	12	<b>Fines :</b>	78	<b>Soil description :</b>	Dark Yellowish Orange Soil
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<b>D<sub>10</sub> :</b>	0.009	<b>D<sub>30</sub> :</b>	0.061	<b>D<sub>60</sub> :</b>	0.188	<b>Uniformity coefficient :</b>	22	<b>Curvature coefficient :</b>	2	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY :

G van Gelder

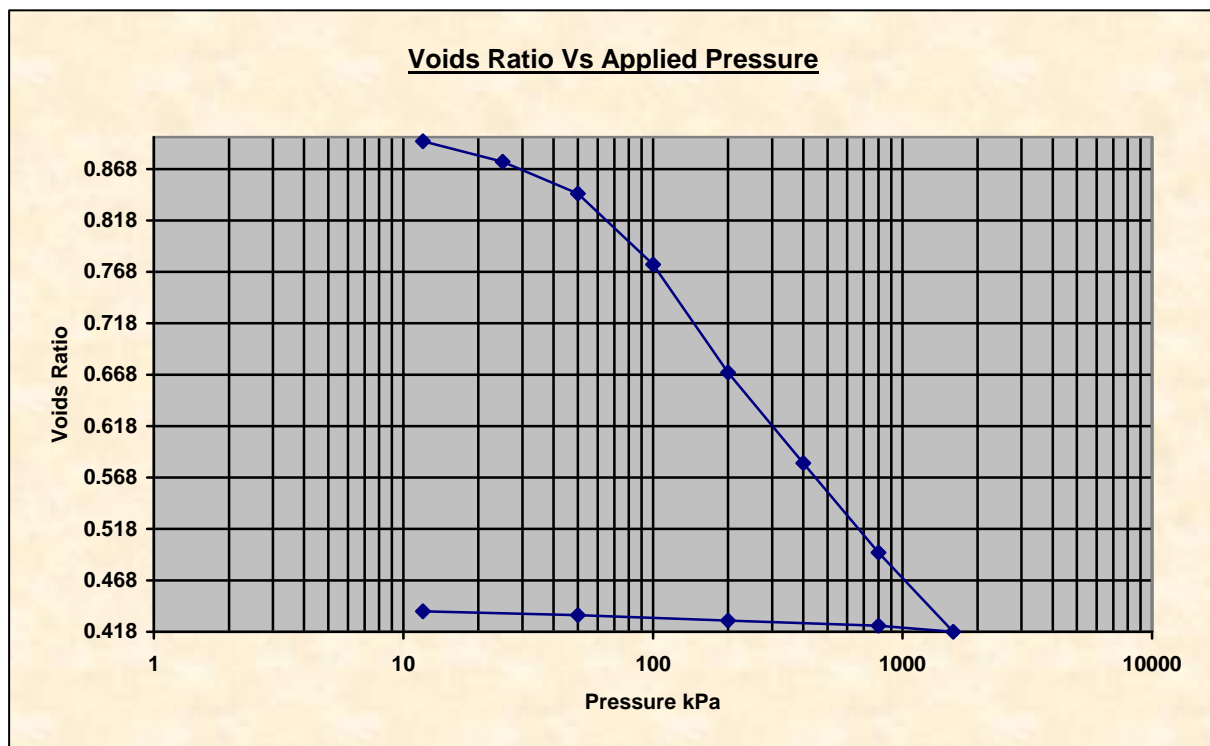
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 22	<b>Sample</b>	12-0304

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.60 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.60 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	A	<b>Description</b>	
<b>Depth within Sample</b>	50.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	149.16 g	<b>Condition</b>	Inundated
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	1	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	116.00 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.53 mm	<b>Swelling Pressure</b>	0.0 kPa
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# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 22	<b>Sample</b>	12-0304

<b>Initial Moisture Content*</b>	23.3 % (trimmings: 22.7 %)	<b>Final Moisture Content</b>	16.5 %
<b>Initial Bulk Density</b>	1.69 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.11 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.37 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.81 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8986	<b>Final Void Ratio</b>	0.4385
<b>Initial Degree of Saturation</b>	67.34%	<b>Final Degree of Saturation</b>	98.01 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.18 m <sup>2</sup> /MN	5.79 m <sup>2</sup> /yr
25.0 kPa	0.80 m <sup>2</sup> /MN	21.53 m <sup>2</sup> /yr
50.0 kPa	0.65 m <sup>2</sup> /MN	29.13 m <sup>2</sup> /yr
100.0 kPa	0.75 m <sup>2</sup> /MN	50.09 m <sup>2</sup> /yr
200.0 kPa	0.59 m <sup>2</sup> /MN	51.53 m <sup>2</sup> /yr
400.0 kPa	0.26 m <sup>2</sup> /MN	52.05 m <sup>2</sup> /yr
800.0 kPa	0.14 m <sup>2</sup> /MN	34.97 m <sup>2</sup> /yr
1600.0 kPa	0.06 m <sup>2</sup> /MN	25.50 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.02 m <sup>2</sup> /MN	-----
12.0 kPa	0.09 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120302
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317

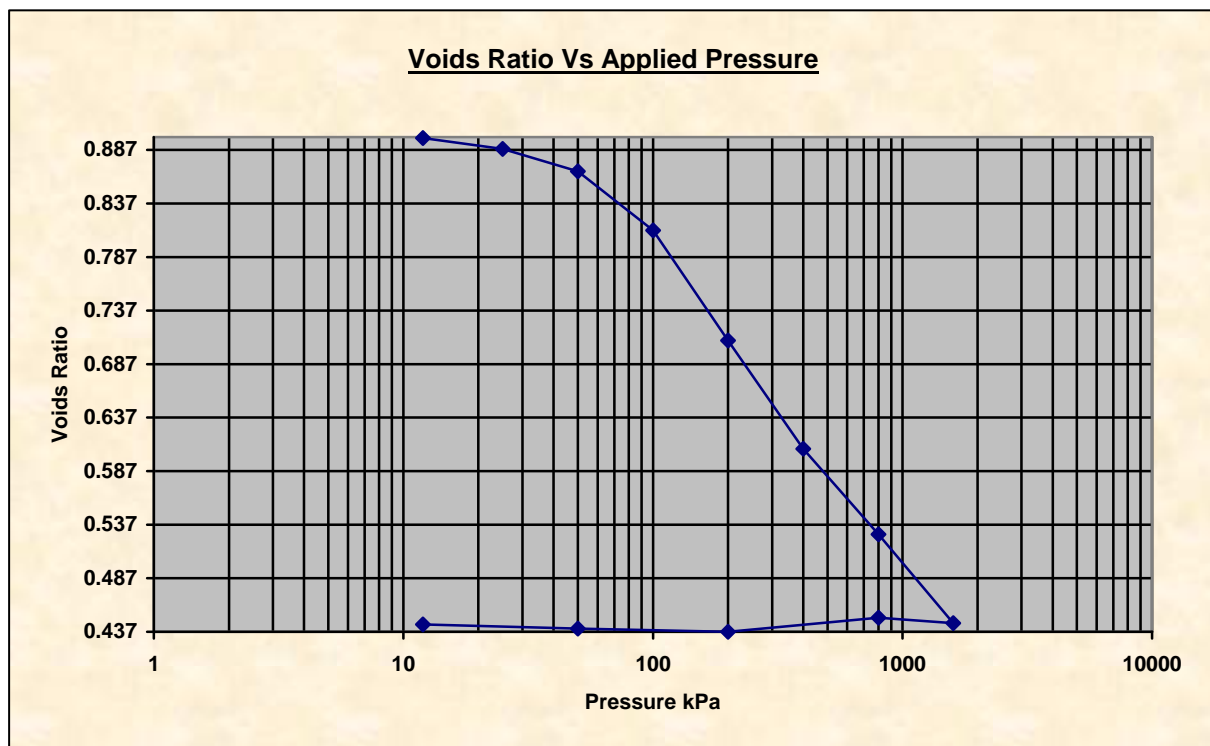
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 22	<b>Sample</b>	12-0304

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.60 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.60 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	B	<b>Description</b>	
<b>Depth within Sample</b>	100.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	149.24 g	<b>Condition</b>	Natural Moisture
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	3	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	116.74 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.53 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 22	<b>Sample</b>	12-0304

<b>Initial Moisture Content*</b>	23.3 % (trimmings: 22.7 %)	<b>Final Moisture Content</b>	17.4 %
<b>Initial Bulk Density</b>	1.69 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.11 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.37 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.80 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8986	<b>Final Void Ratio</b>	0.4445
<b>Initial Degree of Saturation</b>	67.53%	<b>Final Degree of Saturation</b>	101.52 %

- Calculated from initial and dry weights of whole specimen

<b>Pressure (Loading Stages)</b>	<b>Coefficient of Volume Compressibility (m<sub>v</sub>)</b>	<b>Coefficient of Consolidation (c<sub>v</sub>)</b>
<b>0.00</b>		
12.0 kPa	0.05 m <sup>2</sup> /MN	-----
25.0 kPa	0.37 m <sup>2</sup> /MN	10.97 m <sup>2</sup> /yr
50.0 kPa	0.46 m <sup>2</sup> /MN	7.31 m <sup>2</sup> /yr
100.0 kPa	0.59 m <sup>2</sup> /MN	21.06 m <sup>2</sup> /yr
200.0 kPa	0.57 m <sup>2</sup> /MN	33.14 m <sup>2</sup> /yr
400.0 kPa	0.30 m <sup>2</sup> /MN	32.20 m <sup>2</sup> /yr
800.0 kPa	0.12 m <sup>2</sup> /MN	20.86 m <sup>2</sup> /yr
1600.0 kPa	0.07 m <sup>2</sup> /MN	26.15 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.02 m <sup>2</sup> /MN	-----
50.0 kPa	0.01 m <sup>2</sup> /MN	-----
12.0 kPa	0.08 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120302
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 25	<b>Depth [m] :</b>	0.200-1.600
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0305

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	99	97	90	81	68	50	44	39	26	16	15	9	8

**ATTERBERG LIMITS**

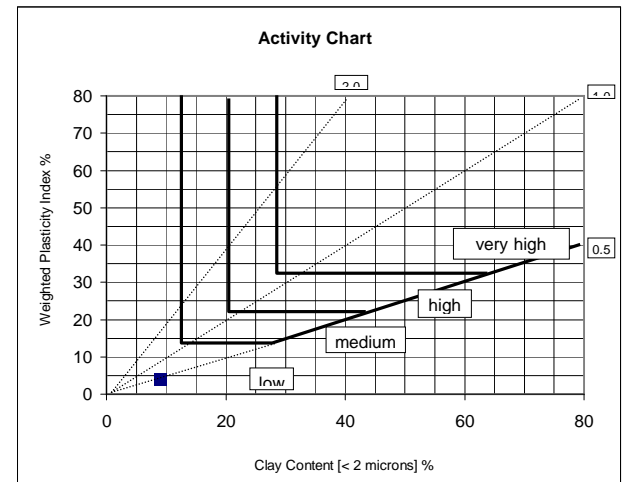
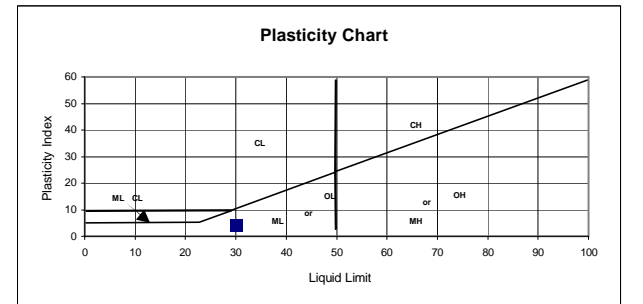
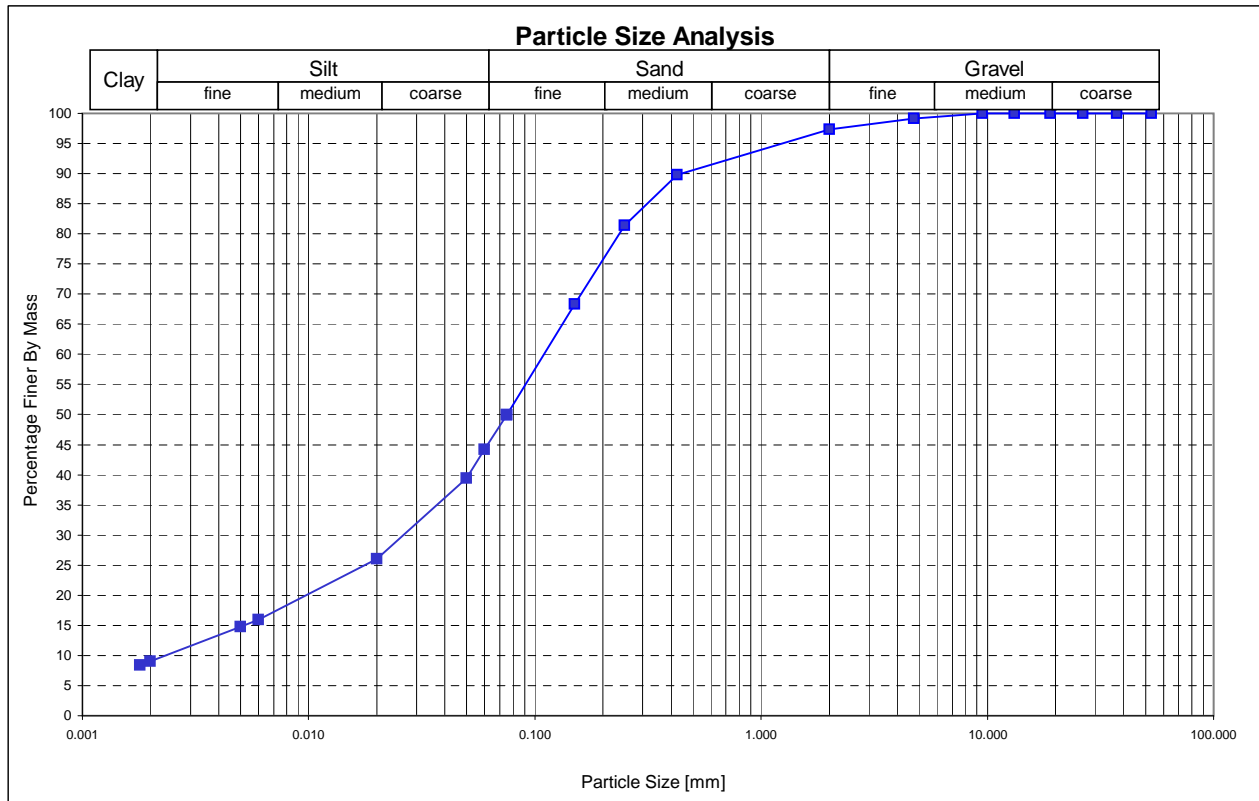
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
30	4	4	2.0	0.63

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.4 (3)	

<b>Soil constituents % :</b>	<b>Clay :</b>	9	<b>Silt :</b>	35	<b>Sand :</b>	53	<b>Gravel :</b>	3	<b>Fines :</b>	90	<b>Soil description :</b>	Dark Reddish Brown Soil
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<b>D<sub>10</sub> :</b>	0.002	<b>D<sub>30</sub> :</b>	0.026	<b>D<sub>60</sub> :</b>	0.109	<b>Uniformity coefficient :</b>	47	<b>Curvature coefficient :</b>	3	<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder



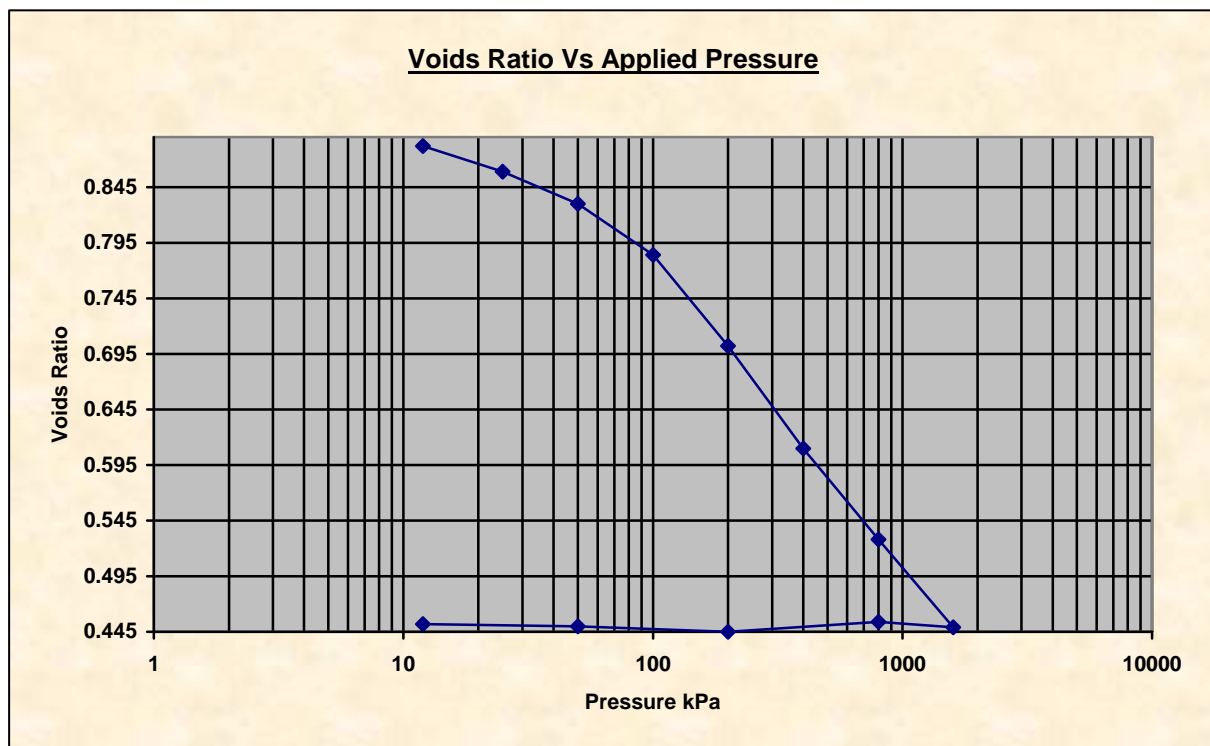
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 25	<b>Sample</b>	12-0306

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.61 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	A	<b>Description</b>	
<b>Depth within Sample</b>	40.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	142.89 g	<b>Condition</b>	Inundated
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	5	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	108.41 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.58 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 25	<b>Sample</b>	12-0306

<b>Initial Moisture Content*</b>	17.1 % (trimmings: 16.2 %)	<b>Final Moisture Content</b>	17.7 %
<b>Initial Bulk Density</b>	1.62 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.12 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.38 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.80 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8903	<b>Final Void Ratio</b>	0.4522
<b>Initial Degree of Saturation</b>	50.20%	<b>Final Degree of Saturation</b>	102.19 %

- Calculated from initial and dry weights of whole specimen

<b>Pressure (Loading Stages)</b>	<b>Coefficient of Volume Compressibility (m<sub>v</sub>)</b>	<b>Coefficient of Consolidation (c<sub>v</sub>)</b>
<b>0.00</b>		
12.0 kPa	0.35 m <sup>2</sup> /MN	17.00 m <sup>2</sup> /yr
25.0 kPa	0.96 m <sup>2</sup> /MN	25.56 m <sup>2</sup> /yr
50.0 kPa	0.63 m <sup>2</sup> /MN	43.66 m <sup>2</sup> /yr
100.0 kPa	0.50 m <sup>2</sup> /MN	32.08 m <sup>2</sup> /yr
200.0 kPa	0.46 m <sup>2</sup> /MN	42.16 m <sup>2</sup> /yr
400.0 kPa	0.27 m <sup>2</sup> /MN	36.61 m <sup>2</sup> /yr
800.0 kPa	0.13 m <sup>2</sup> /MN	29.58 m <sup>2</sup> /yr
1600.0 kPa	0.06 m <sup>2</sup> /MN	21.57 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.03 m <sup>2</sup> /MN	-----
12.0 kPa	0.04 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120302
Checked By and Date:	hjs20120318
Approved By and Date:	hjs20120318

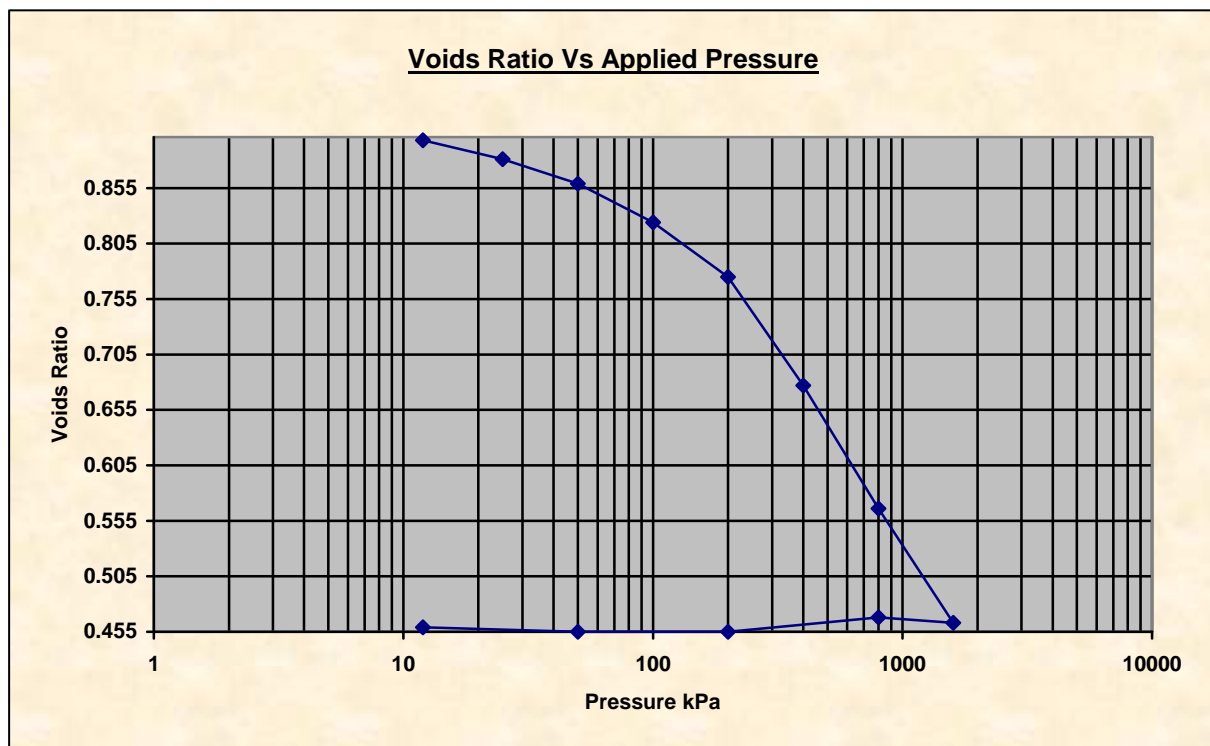
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 25	<b>Sample</b>	12-0306

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.61 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	<b>B</b>	<b>Description</b>	
<b>Depth within Sample</b>	140.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	141.34 g	<b>Condition</b>	Natural Moisture
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	3	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	116.70 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.52 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 25	<b>Sample</b>	12-0306

<b>Initial Moisture Content*</b>	16.5 % (trimmings: 16.2 %)	<b>Final Moisture Content</b>	14.8 %
<b>Initial Bulk Density</b>	1.60 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.05 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.37 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.79 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.9012	<b>Final Void Ratio</b>	0.4595
<b>Initial Degree of Saturation</b>	47.85%	<b>Final Degree of Saturation</b>	84.29 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.13 m <sup>2</sup> /MN	0.31 m <sup>2</sup> /yr
25.0 kPa	0.68 m <sup>2</sup> /MN	46.51 m <sup>2</sup> /yr
50.0 kPa	0.48 m <sup>2</sup> /MN	45.68 m <sup>2</sup> /yr
100.0 kPa	0.38 m <sup>2</sup> /MN	35.82 m <sup>2</sup> /yr
200.0 kPa	0.27 m <sup>2</sup> /MN	34.62 m <sup>2</sup> /yr
400.0 kPa	0.28 m <sup>2</sup> /MN	34.47 m <sup>2</sup> /yr
800.0 kPa	0.17 m <sup>2</sup> /MN	37.02 m <sup>2</sup> /yr
1600.0 kPa	0.08 m <sup>2</sup> /MN	31.49 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.00 m <sup>2</sup> /MN	-----
12.0 kPa	0.08 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120312
Checked By and Date:	hjs20120318
Approved By and Date:	hjs20120318



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 28	<b>Depth [m] :</b>	0.300-0.750
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0307

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	99	98	88	74	56	41	37	33	22	15	14	9	9

**ATTERBERG LIMITS**

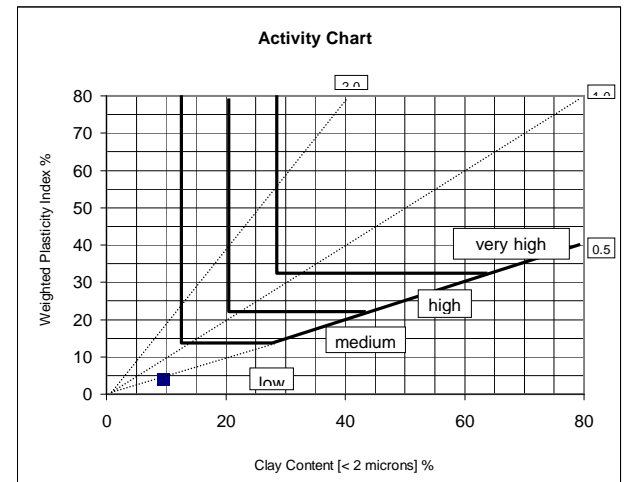
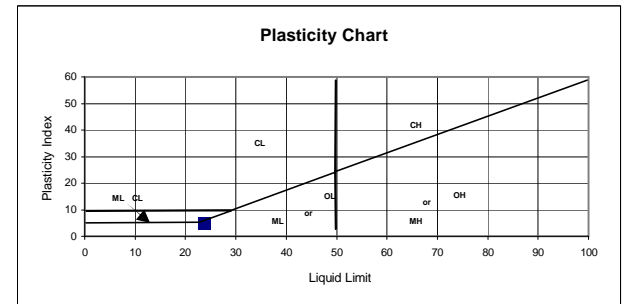
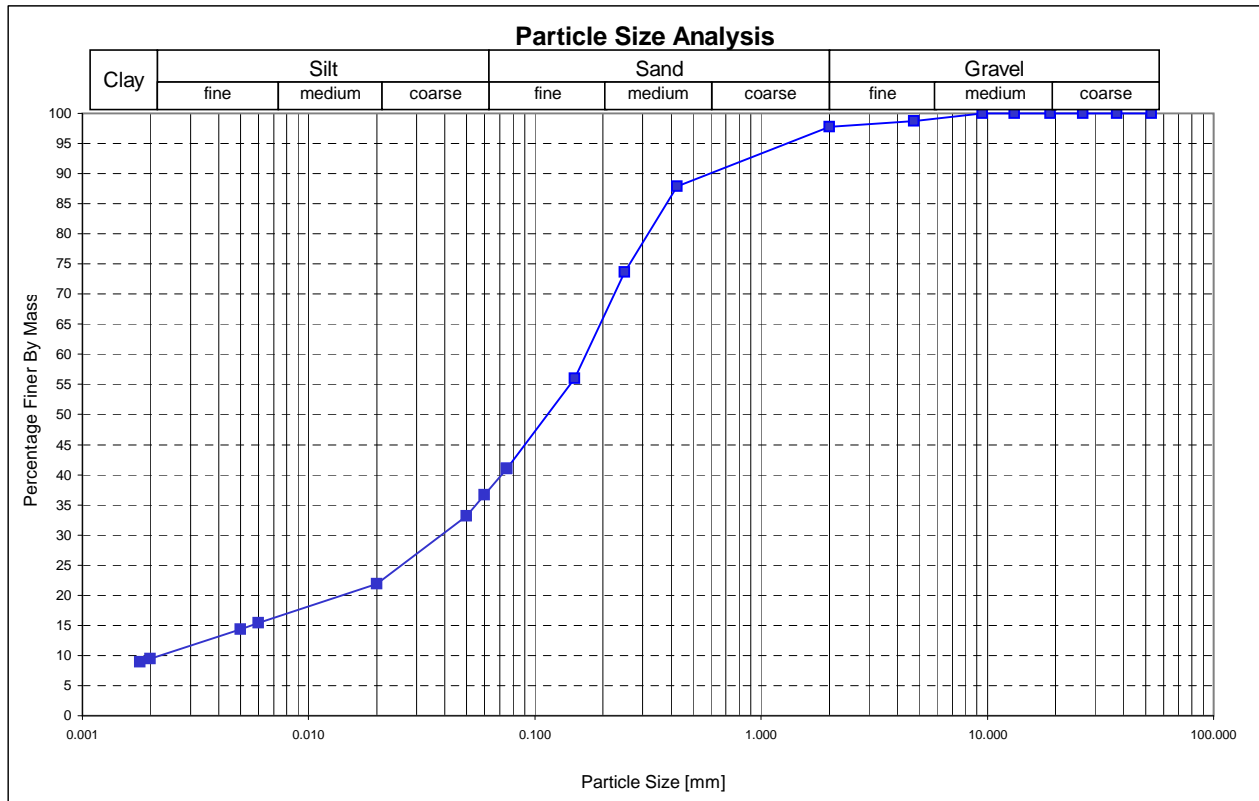
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
24	5	4	2.0	0.73

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM/SC	A.4 (1)	

<b>Soil constituents % :</b>	<b>Clay :</b>	9	<b>Silt :</b>	27	<b>Sand :</b>	61	<b>Gravel :</b>	2	<b>Fines :</b>	88	<b>Soil description :</b>	Dark Yellowish Orange Soil
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<b>D<sub>10</sub> :</b>	0.002	<b>D<sub>30</sub> :</b>	0.039	<b>D<sub>60</sub> :</b>	0.168	<b>Uniformity coefficient :</b>	76	<b>Curvature coefficient :</b>	4	<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC		<b>PROJECT :</b>	#999	
<b>Position :</b>	TP 28	<b>Depth [m] :</b>	@ 1.000	<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0308

**SIEVE ANALYSIS (% PASSING)**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	100	85	68	63	55	43	38	34	24	15	14	9	8

**ATTERBERG LIMITS**

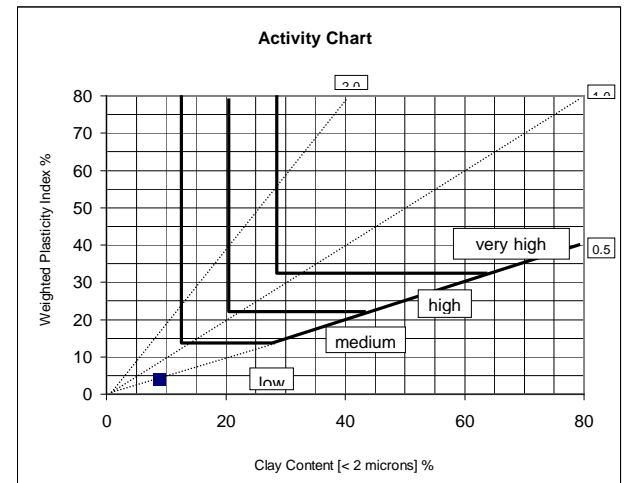
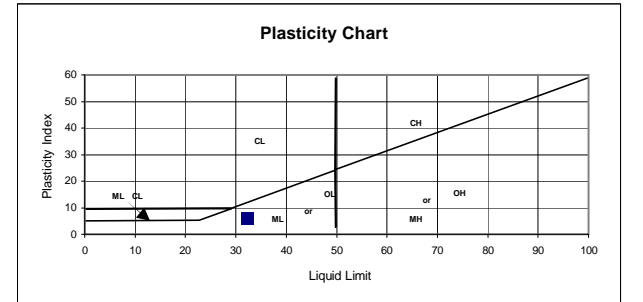
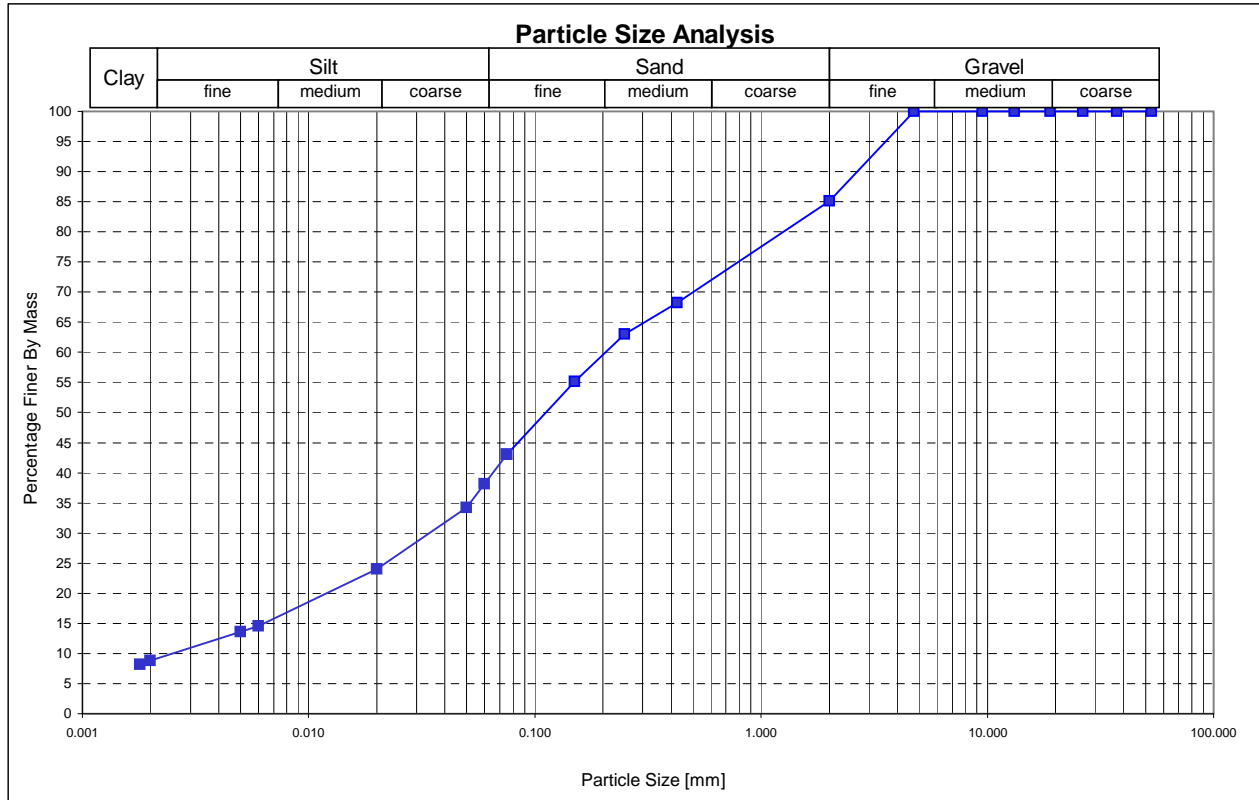
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
32	6	4	3.0	1.04

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.4 (2)	

<b>Soil constituents % :</b>	<b>Clay :</b>	9	<b>Silt :</b>	29	<b>Sand :</b>	47	<b>Gravel :</b>	15	<b>Fines :</b>	68	<b>Soil description :</b>	Light Brown Soil
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<b>D<sub>10</sub> :</b>	0.003	<b>D<sub>30</sub> :</b>	0.034	<b>D<sub>60</sub> :</b>	0.205	<b>Uniformity coefficient :</b>	81	<b>Curvature coefficient :</b>	2	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY : G van Gelder



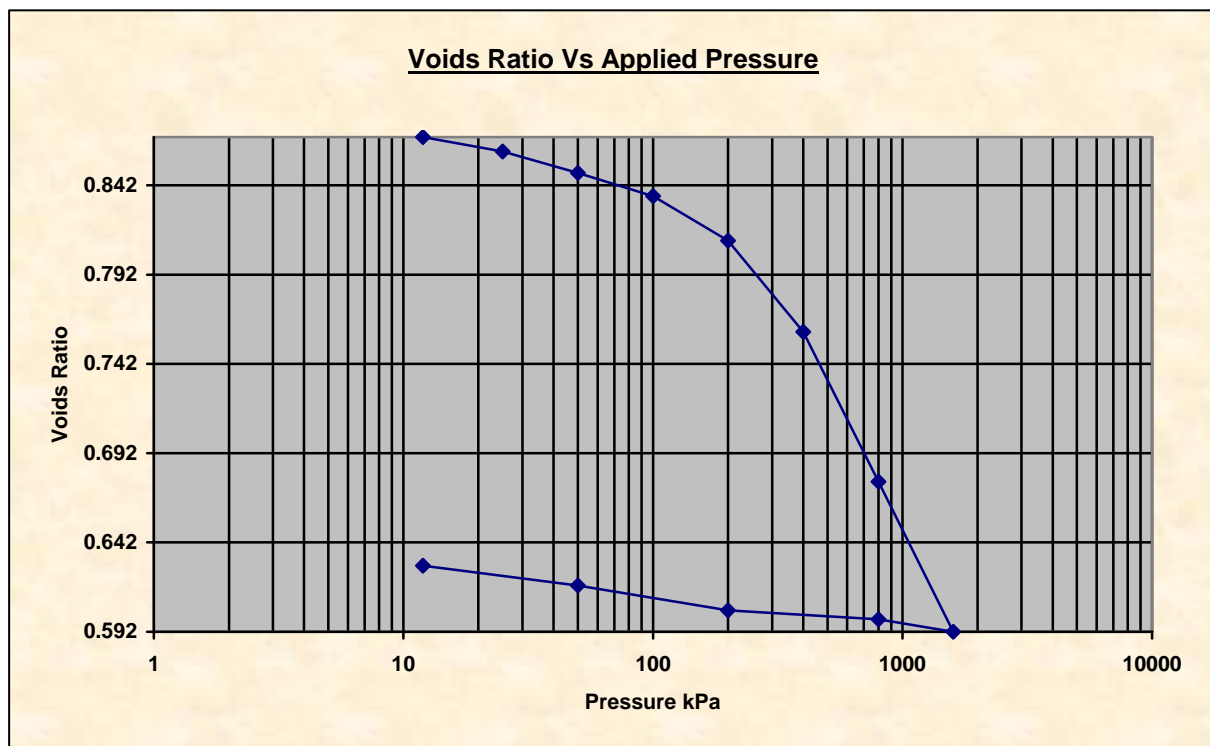
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 28	<b>Sample</b>	12-0308

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	1.00 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	A	<b>Description</b>	
<b>Depth within Sample</b>	60.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	152.00 g	<b>Condition</b>	Inundated
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	6	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	108.47 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.71 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 28	<b>Sample</b>	12-0308

<b>Initial Moisture Content*</b>	22.6 % (trimmings: 22.1 %)	<b>Final Moisture Content</b>	25.4 %
<b>Initial Bulk Density</b>	1.72 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.02 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.40 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.61 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8669	<b>Final Void Ratio</b>	0.6293
<b>Initial Degree of Saturation</b>	68.24%	<b>Final Degree of Saturation</b>	105.76 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	-0.11 m <sup>2</sup> /MN	57.10 m <sup>2</sup> /yr
25.0 kPa	0.33 m <sup>2</sup> /MN	35.28 m <sup>2</sup> /yr
50.0 kPa	0.27 m <sup>2</sup> /MN	25.94 m <sup>2</sup> /yr
100.0 kPa	0.14 m <sup>2</sup> /MN	30.35 m <sup>2</sup> /yr
200.0 kPa	0.13 m <sup>2</sup> /MN	20.80 m <sup>2</sup> /yr
400.0 kPa	0.14 m <sup>2</sup> /MN	29.43 m <sup>2</sup> /yr
800.0 kPa	0.12 m <sup>2</sup> /MN	37.13 m <sup>2</sup> /yr
1600.0 kPa	0.06 m <sup>2</sup> /MN	41.24 m <sup>2</sup> /yr
800.0 kPa	0.01 m <sup>2</sup> /MN	-----
200.0 kPa	0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.06 m <sup>2</sup> /MN	-----
12.0 kPa	0.19 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120307
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317

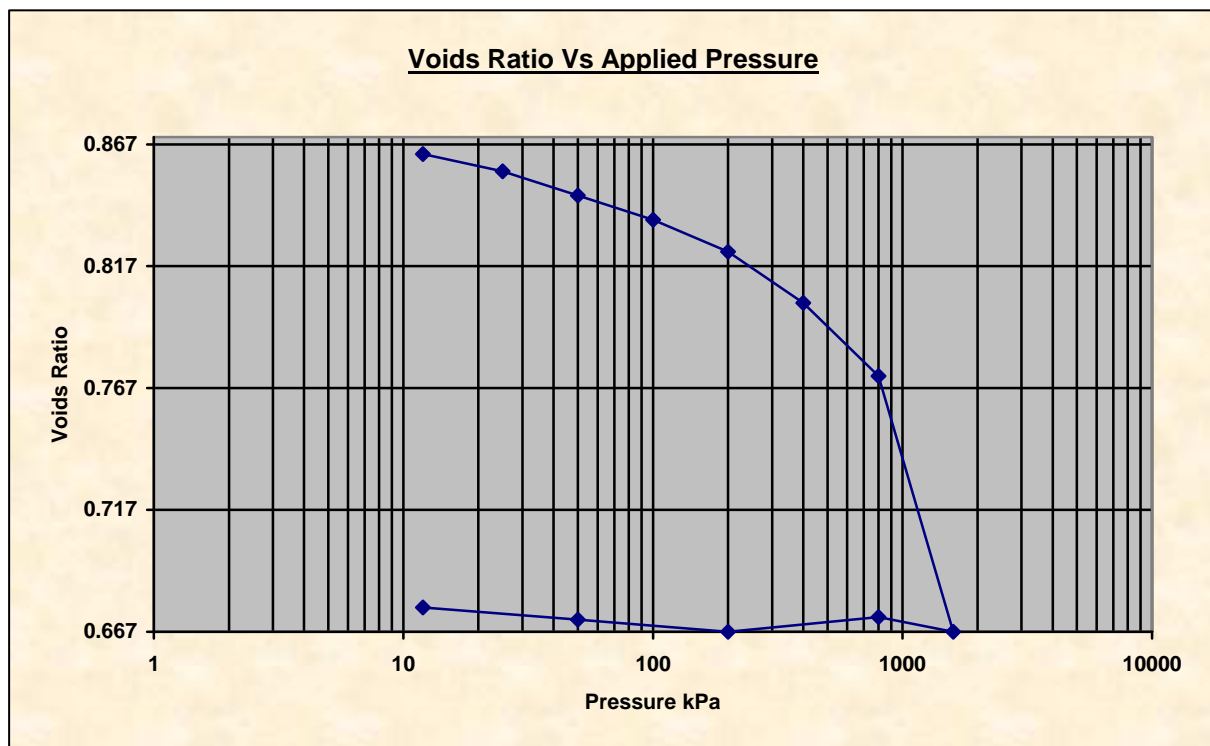
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 28	<b>Sample</b>	12-0308

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.62 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	1.00 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	B	<b>Description</b>	
<b>Depth within Sample</b>	130.00mm	<b>Orientation within Sample</b>	horizontal
<b>Specimen Mass</b>	153.00 g	<b>Condition</b>	Natural Moisture
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	2	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	114.18 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.70 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 28	<b>Sample</b>	12-0308

<b>Initial Moisture Content*</b>	23.6 % (trimmings: 22.1 %)	<b>Final Moisture Content</b>	19.4 %
<b>Initial Bulk Density</b>	1.73 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	1.87 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.40 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.56 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8699	<b>Final Void Ratio</b>	0.6769
<b>Initial Degree of Saturation</b>	71.04%	<b>Final Degree of Saturation</b>	75.04 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.32 m <sup>2</sup> /MN	-----
25.0 kPa	0.27 m <sup>2</sup> /MN	-----
50.0 kPa	0.22 m <sup>2</sup> /MN	-----
100.0 kPa	0.11 m <sup>2</sup> /MN	-----
200.0 kPa	0.07 m <sup>2</sup> /MN	-----
400.0 kPa	0.06 m <sup>2</sup> /MN	-----
800.0 kPa	0.04 m <sup>2</sup> /MN	-----
1600.0 kPa	0.07 m <sup>2</sup> /MN	41.56 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.02 m <sup>2</sup> /MN	-----
12.0 kPa	0.08 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120312
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 29	<b>Depth [m] :</b>	0.700-1.000
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0309

**SIEVE ANALYSIS (% PASSING)**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	97	94	87	77	63	57	49	40	36	33	23	15	14	9	9

**ATTERBERG LIMITS**

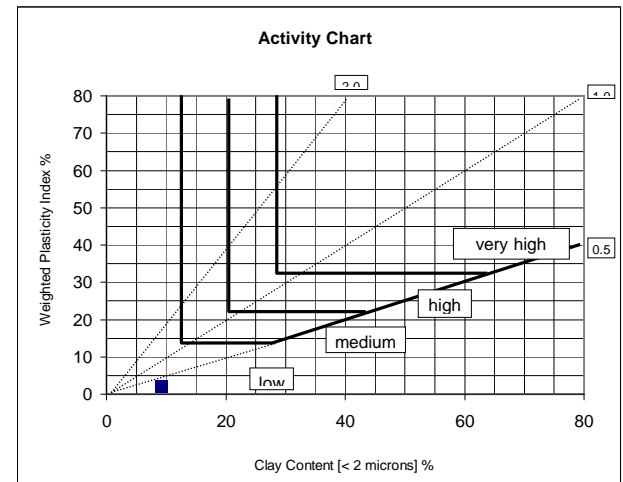
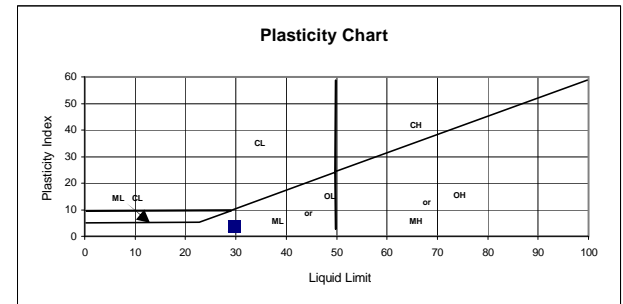
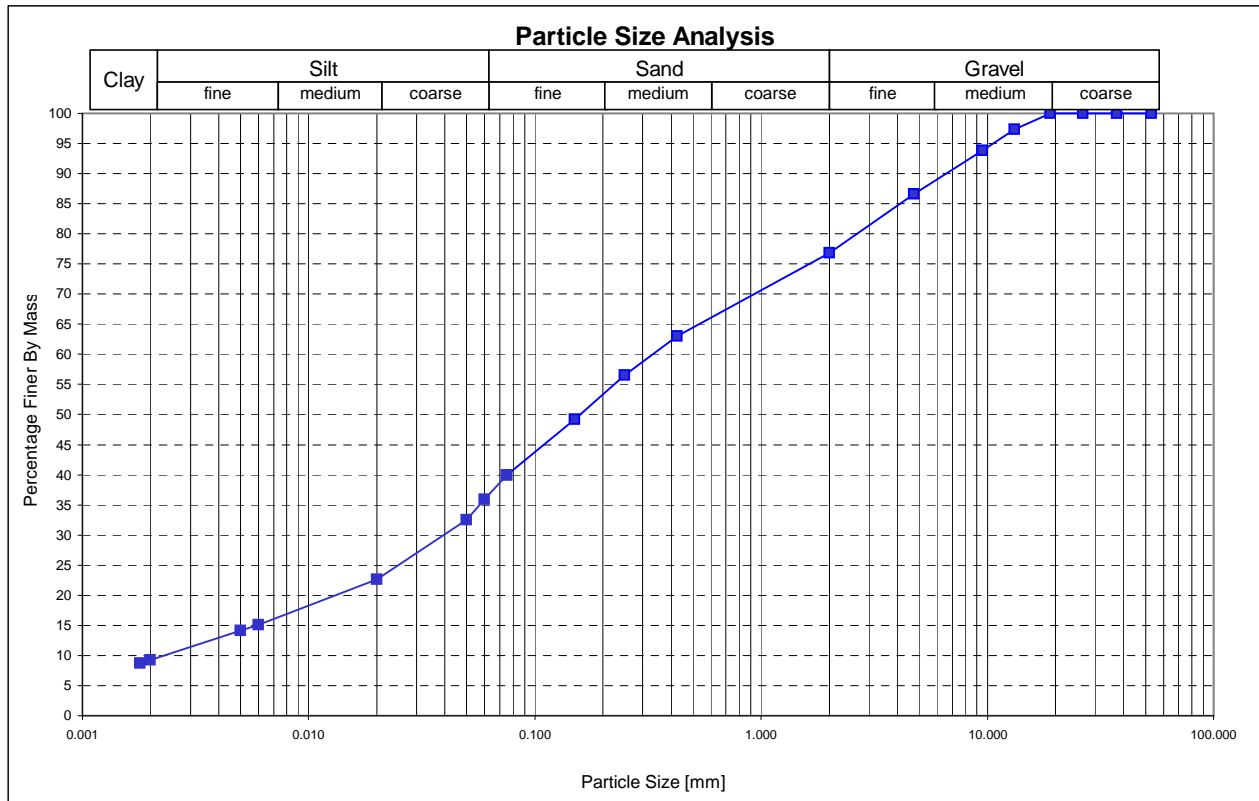
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
30	4	2	2.0	1.20

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.4 (1)	

<b>Soil constituents % :</b>	<b>Clay :</b>	9	<b>Silt :</b>	27	<b>Sand :</b>	41	<b>Gravel :</b>	23	<b>Fines :</b>	63	<b>Soil description :</b>	Light Reddish Brown Soil
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<b>D<sub>10</sub> :</b>	0.002	<b>D<sub>30</sub> :</b>	0.040	<b>D<sub>60</sub> :</b>	0.333	<b>Uniformity coefficient :</b>	145	<b>Curvature coefficient :</b>	2	<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY : G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 29	<b>Depth [m] :</b>	1.000-2.100
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0310

**SIEVE ANALYSIS (% PASSING)**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	99	97	94	87	73	66	58	48	41	36	25	16	15	11	10

**ATTERBERG LIMITS**

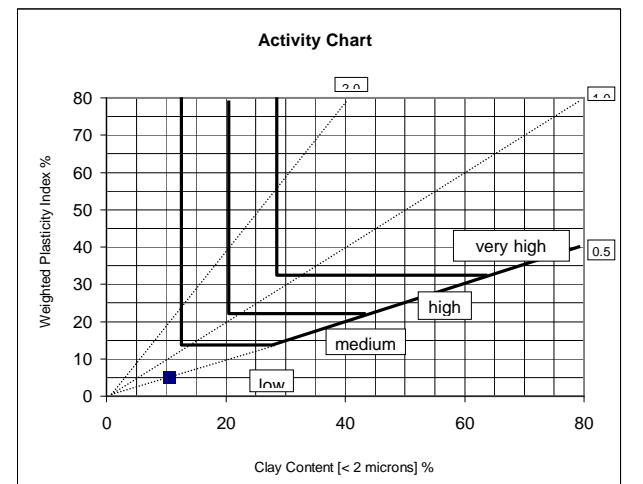
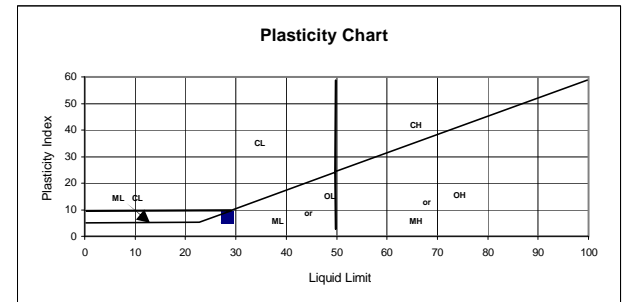
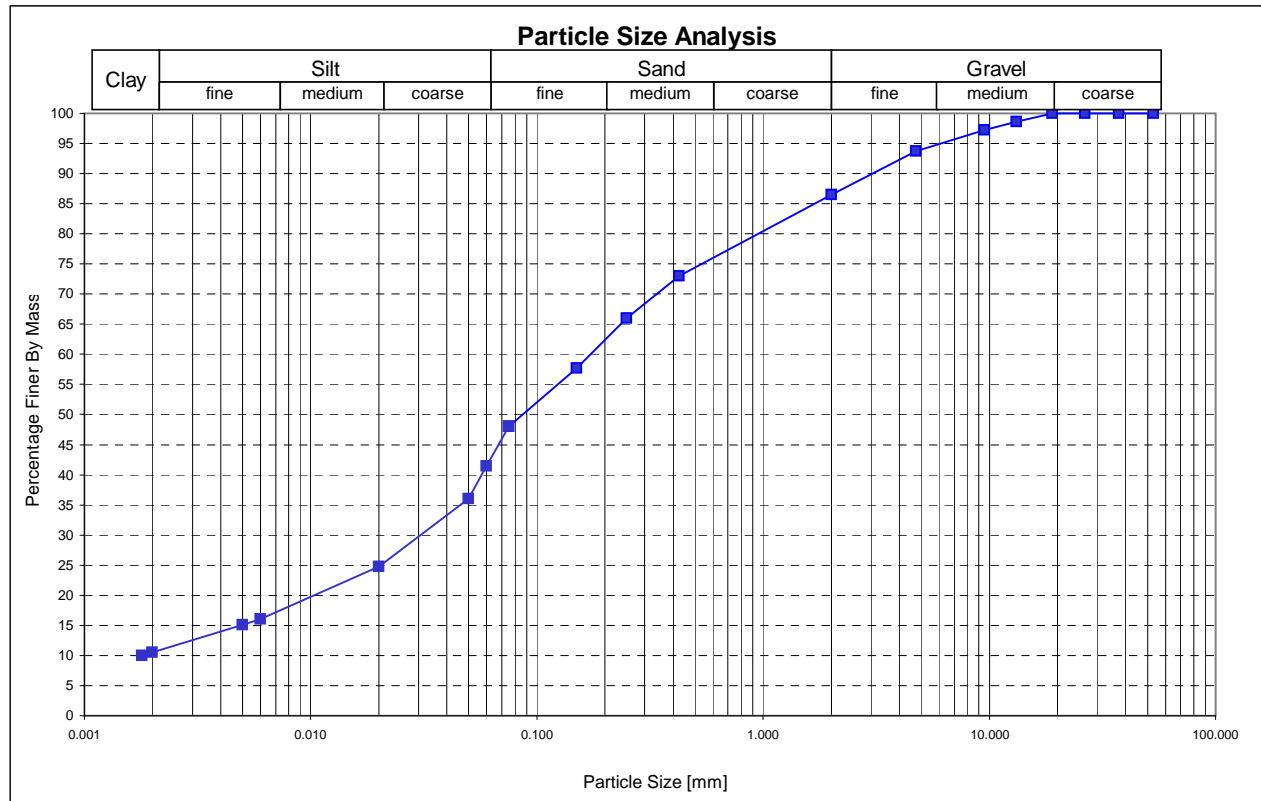
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
28	7	5	3.4	0.93

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SC	A.4 (3)	

<b>Soil constituents % :</b>	<b>Clay :</b>	11	<b>Silt :</b>	31	<b>Sand :</b>	45	<b>Gravel :</b>	13	<b>Fines :</b>	73	<b>Soil description :</b>	Light Brown Soil
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<b>D<sub>10</sub> :</b>	<b>D<sub>30</sub> :</b>	0.031	<b>D<sub>60</sub> :</b>	0.172	<b>Uniformity coefficient :</b>		<b>Curvature coefficient :</b>		<b>Active program :</b>	YES
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**REMARKS:**

none

**CHECKED BY :**

G van Gelder



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 31	<b>Depth [m] :</b>	0.500-1.000
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0311

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	84	79	73	66	57	48	38	34	27	18	15	13	9	7	6	4	4

**ATTERBERG LIMITS**

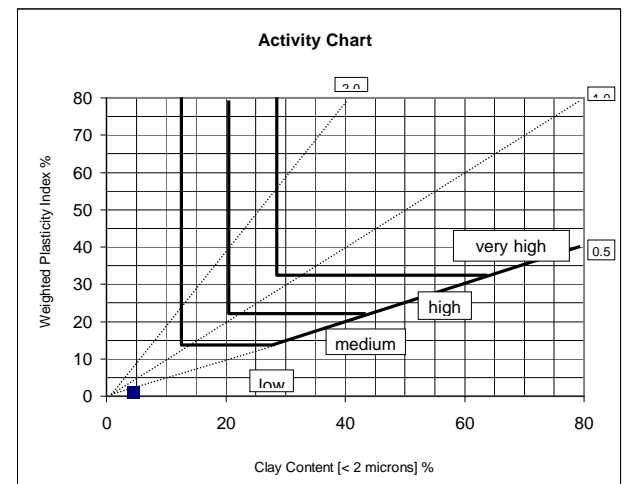
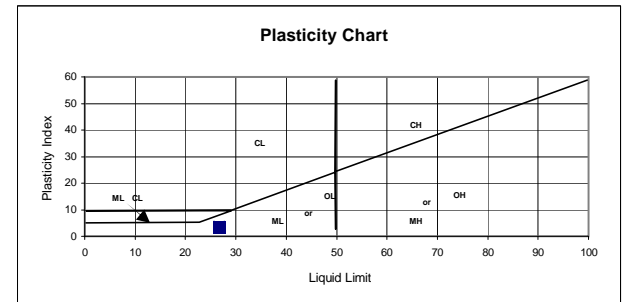
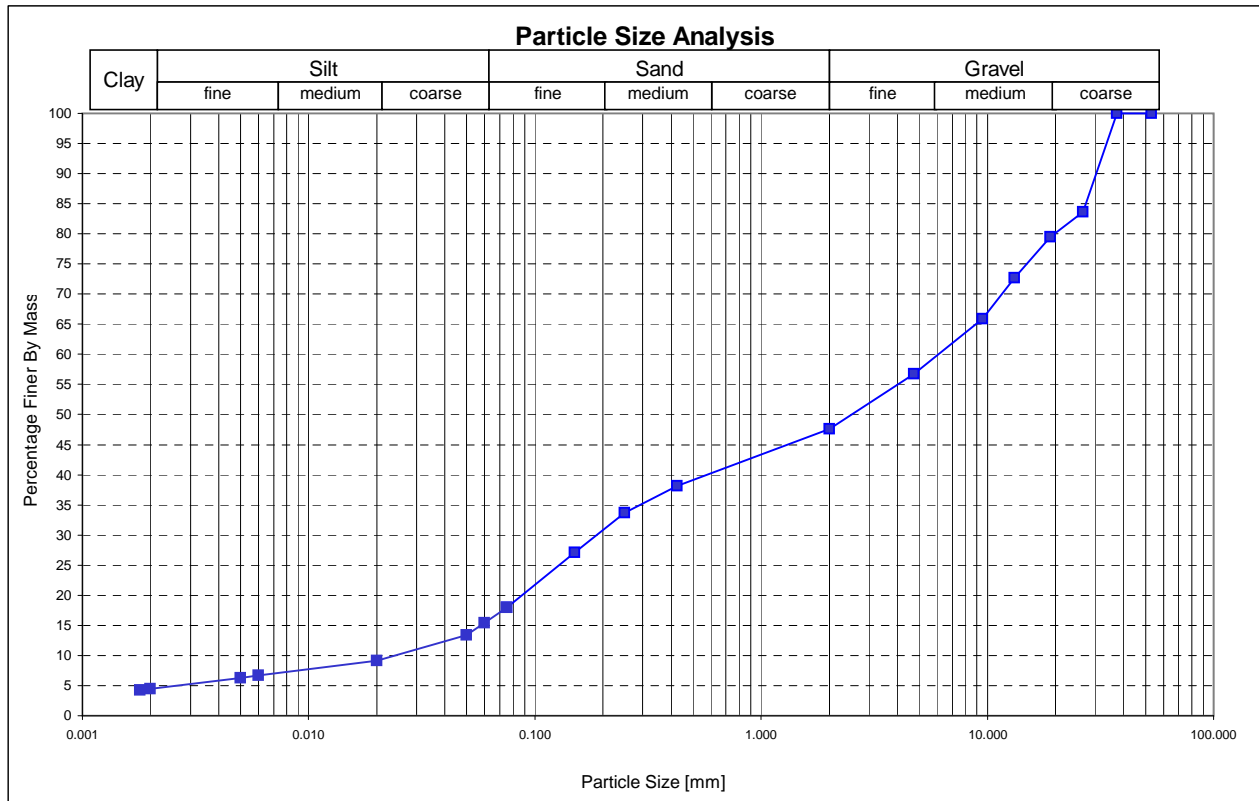
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
27	4		2.0	1.96

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM	A.1.b (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	4	<b>Silt :</b>	11	<b>Sand :</b>	32	<b>Gravel :</b>	52	<b>Fines :</b>	38	<b>Soil description :</b>	Light Brown Soil
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<b>D<sub>10</sub> :</b>	0.024	<b>D<sub>30</sub> :</b>	0.187	<b>D<sub>60</sub> :</b>	6.094	<b>Uniformity coefficient :</b>	254	<b>Curvature coefficient :</b>	0	<b>Active program :</b>	YES
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**REMARKS:**

none

**CHECKED BY :**

G van Gelder



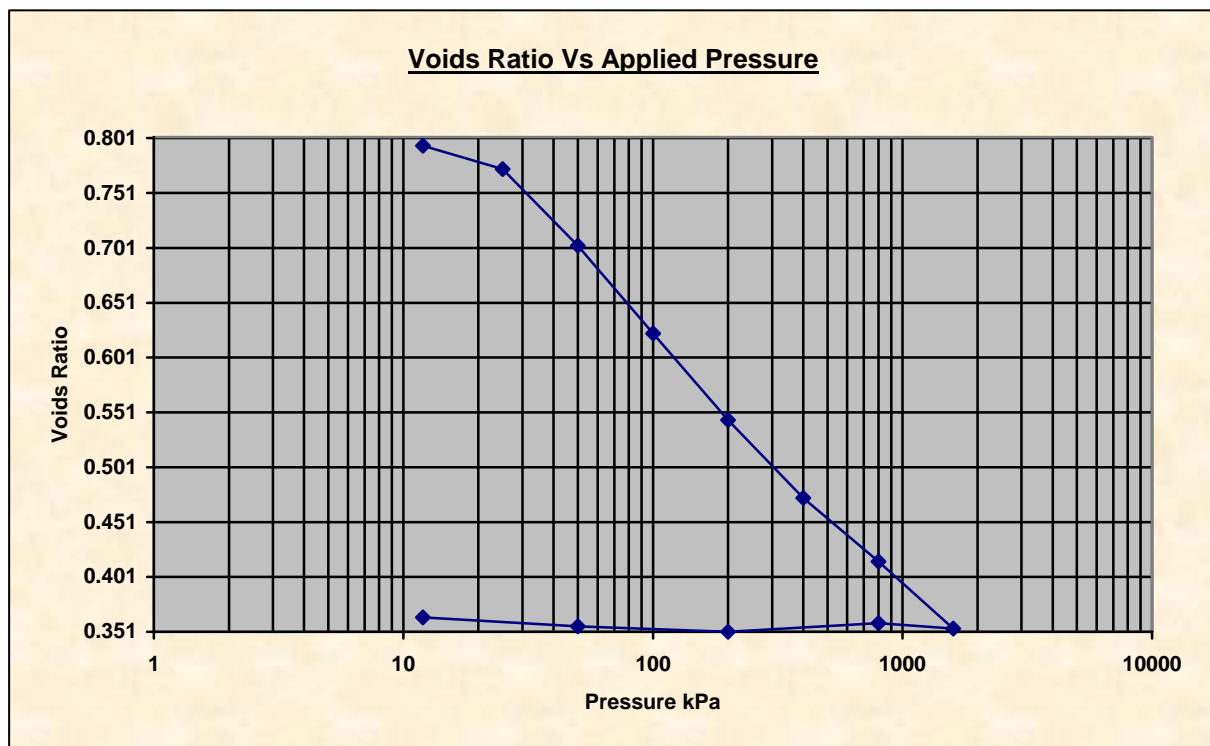
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 31	<b>Sample</b>	12-0312

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.61 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	A	<b>Description</b>	
<b>Depth within Sample</b>	50.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	142.48 g	<b>Condition</b>	Inundated
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	4	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	108.76 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	11.10 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 31	<b>Sample</b>	12-0312

<b>Initial Moisture Content*</b>	11.3 % (trimmings: 8.1 %)	<b>Final Moisture Content</b>	14.2 %
<b>Initial Bulk Density</b>	1.61 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.19 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.45 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.91 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8017	<b>Final Void Ratio</b>	0.3641
<b>Initial Degree of Saturation</b>	36.83%	<b>Final Degree of Saturation</b>	101.92 %

- Calculated from initial and dry weights of whole specimen

<b>Pressure (Loading Stages)</b>	<b>Coefficient of Volume Compressibility (m<sub>v</sub>)</b>	<b>Coefficient of Consolidation (c<sub>v</sub>)</b>
<b>0.00</b>		
12.0 kPa	0.33 m <sup>2</sup> /MN	-----
25.0 kPa	0.93 m <sup>2</sup> /MN	32.48 m <sup>2</sup> /yr
50.0 kPa	1.58 m <sup>2</sup> /MN	21.07 m <sup>2</sup> /yr
100.0 kPa	0.93 m <sup>2</sup> /MN	28.96 m <sup>2</sup> /yr
200.0 kPa	0.49 m <sup>2</sup> /MN	34.29 m <sup>2</sup> /yr
400.0 kPa	0.23 m <sup>2</sup> /MN	39.11 m <sup>2</sup> /yr
800.0 kPa	0.10 m <sup>2</sup> /MN	31.93 m <sup>2</sup> /yr
1600.0 kPa	0.05 m <sup>2</sup> /MN	26.22 m <sup>2</sup> /yr
800.0 kPa	0.00 m <sup>2</sup> /MN	-----
200.0 kPa	-0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.03 m <sup>2</sup> /MN	-----
12.0 kPa	0.16 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120307
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317

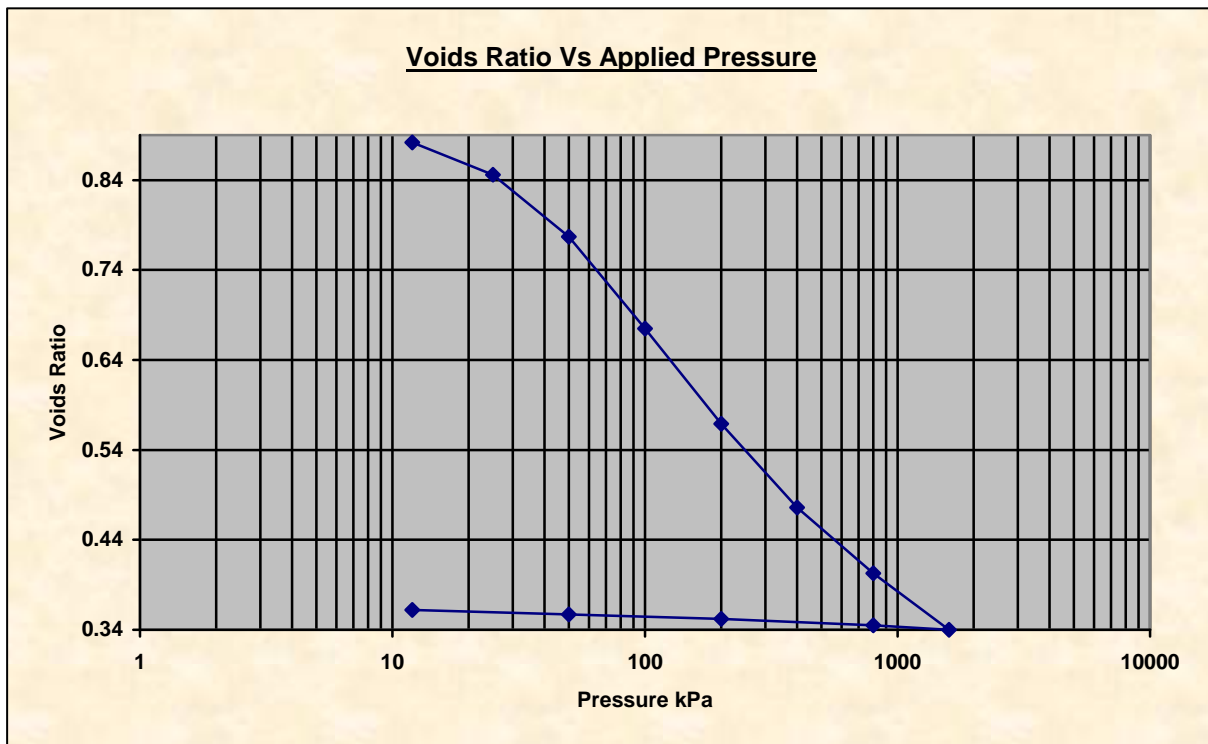
# One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 31	<b>Sample</b>	12-0312

Test Details			
<b>Standard</b>	BS 1377: Part 5 : 1990 : Clause 3	<b>Particle Density</b>	2.61 Mg/m <sup>3</sup>
<b>Sample Type</b>	Block sample	<b>Lab Temperature</b>	20.0 deg.C
<b>Sample Depth</b>	0.70 m		
<b>Sample Description</b>			
<b>Variations from Procedure</b>	None		

Specimen Details			
<b>Specimen Reference</b>	B	<b>Description</b>	
<b>Depth within Sample</b>	120.00mm	<b>Orientation within Sample</b>	vertical
<b>Specimen Mass</b>	136.44 g	<b>Condition</b>	Natural Moisture
<b>Specimen Height</b>	20.00 mm	<b>Preparation</b>	cut from undisturbed sample
<b>Comments</b>			

Test Apparatus			
<b>Ring Number</b>	1	<b>Ring Diameter</b>	75.00 mm
<b>Ring Height</b>	20.00 mm	<b>Ring Weight</b>	116.00 g
<b>Lever Ratio</b>	9.00 : 1		



<b>Height of Solid Particles</b>	10.58 mm	<b>Swelling Pressure</b>	0.0 kPa
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## One Dimensional Consolidation Properties (Oedometer)

<b>Client</b>	geo 3 cc	<b>Lab Ref</b>	
<b>Project</b>	#999	<b>Job</b>	1450
<b>Borehole</b>	TP 31	<b>Sample</b>	12-0312

<b>Initial Moisture Content*</b>	11.8 % (trimmings: 16.2 %)	<b>Final Moisture Content</b>	17.7 %
<b>Initial Bulk Density</b>	1.54 Mg/m <sup>3</sup>	<b>Final Bulk Density</b>	2.25 Mg/m <sup>3</sup>
<b>Initial Dry Density</b>	1.38 Mg/m <sup>3</sup>	<b>Final Dry Density</b>	1.92 Mg/m <sup>3</sup>
<b>Initial Void Ratio</b>	0.8903	<b>Final Void Ratio</b>	0.3625
<b>Initial Degree of Saturation</b>	34.70%	<b>Final Degree of Saturation</b>	127.48 %

- Calculated from initial and dry weights of whole specimen

Pressure (Loading Stages)	Coefficient of Volume Compressibility (m <sub>v</sub> )	Coefficient of Consolidation (c <sub>v</sub> )
<b>0.00</b>		
12.0 kPa	0.37 m <sup>2</sup> /MN	0.25 m <sup>2</sup> /yr
25.0 kPa	1.45 m <sup>2</sup> /MN	22.08 m <sup>2</sup> /yr
50.0 kPa	1.50 m <sup>2</sup> /MN	26.13 m <sup>2</sup> /yr
100.0 kPa	1.15 m <sup>2</sup> /MN	29.62 m <sup>2</sup> /yr
200.0 kPa	0.63 m <sup>2</sup> /MN	34.76 m <sup>2</sup> /yr
400.0 kPa	0.29 m <sup>2</sup> /MN	29.35 m <sup>2</sup> /yr
800.0 kPa	0.12 m <sup>2</sup> /MN	25.18 m <sup>2</sup> /yr
1600.0 kPa	0.06 m <sup>2</sup> /MN	24.84 m <sup>2</sup> /yr
800.0 kPa	0.01 m <sup>2</sup> /MN	-----
200.0 kPa	0.01 m <sup>2</sup> /MN	-----
50.0 kPa	0.02 m <sup>2</sup> /MN	-----
12.0 kPa	0.10 m <sup>2</sup> /MN	-----

<b>Method of Time Fitting Used</b>	Log Time
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Tested By and Date:	gvg20120312
Checked By and Date:	hjs20120317
Approved By and Date:	hjs20120317



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 31	<b>Depth [m] :</b>	1.000-2.200
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0313

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	93	90	82	78	70	61	47	42	36	27	23	20	12	8	7	5	5

**ATTERBERG LIMITS**

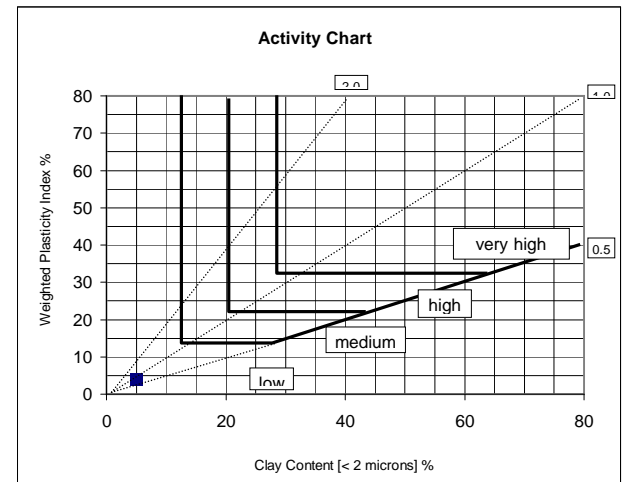
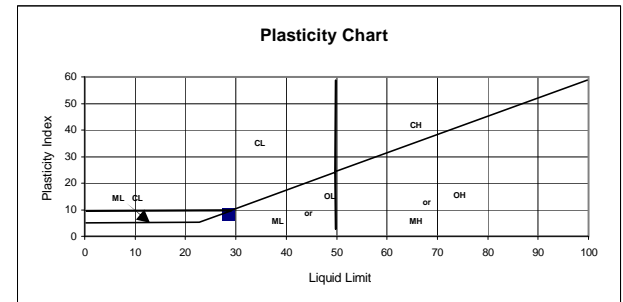
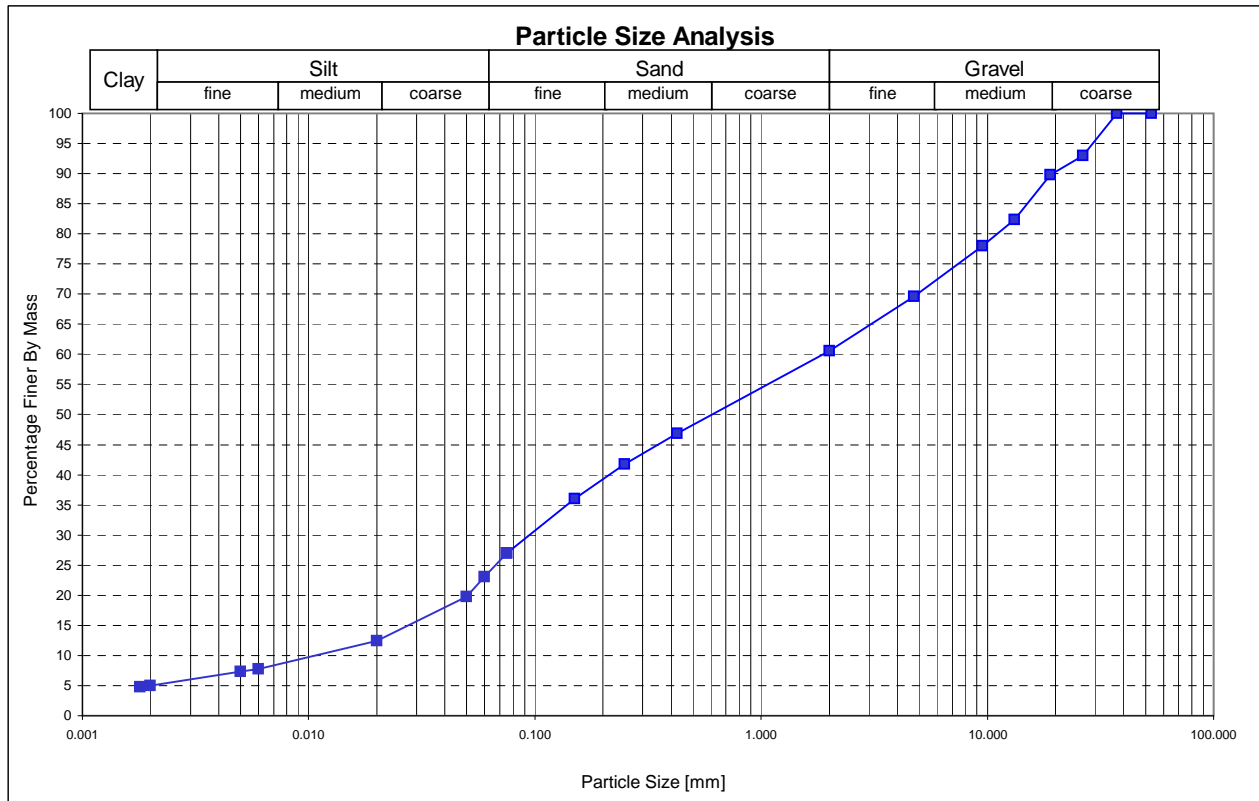
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
28	8	4	3.4	1.66

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SC	A.2.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	5	<b>Silt :</b>	18	<b>Sand :</b>	37	<b>Gravel :</b>	39	<b>Fines :</b>	47	<b>Soil description :</b>	Buff Soil
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<b>D<sub>10</sub> :</b>	0.011	<b>D<sub>30</sub> :</b>	0.094	<b>D<sub>60</sub> :</b>	1.883	<b>Uniformity coefficient :</b>	177	<b>Curvature coefficient :</b>	0	<b>Active program :</b>	YES
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**REMARKS:**

none

**CHECKED BY :**

G van Gelder

# Engeo Lab (Pty) Ltd

## INSITU DENSITY & MOISTURE DETERMINATION

JOB NO: 1450 (#990)  
 DATE: 1-Mar-2012

Sample Number			0314				
Position			TP 31				
Depth			@ 1.20m				
Mass of sample in air	(g)	a	122.90				
Mass of waxed sample in air	(g)	b	128.30				
Mass of waxed sample in water @ 25°C	(g)	c	63.90				
Mass of water displaced (b - c)	(g)	d	64.40				
Mass of wax (b - a)	(g)	e	5.40				
Density of wax	(kg/m <sup>3</sup> )	f	0.93				
Volume of wax (e / f)	(ml)	g	5.81				
Volume of sample (d - g)	(ml)	h	58.59				
Wet density of sample ( a / h *100 )	(kg/m <sup>3</sup> )	l	2098				
Dry density of sample ( l / (100 + k) * 1000)	(kg/m <sup>3</sup> )	j	<b>1845</b>				
Mass Pan & Wet Mat.	(g)		83 24				
Mass Pan & Dry Mat.	(g)		79 94				
Mass Pan	(g)		55 81				
% Moisture	(%)	k	<b>13.7</b>				
Laboratory Determined Max. Dry Density	(kg/m <sup>3</sup> )	l					
Laboratory Determined O.M.C.	%	m					
Percentage of Max. Dry Density (j/l*100)	%						
Percentage Wet (-) Dry (+) of O.M.C. (m-k)	%						
Specific Gravity			<b>2.62</b>				
Void ratio			0.420				
Degree of saturation	%		85.5				



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 33	<b>Depth [m] :</b>	@0.70m
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
21-Feb-12	<b>Sample No.</b>	12/0315

**SIEVE ANALYSIS ( % PASSING )**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	100	99	84	71	53	36	31	26	15	11	10	7	7

**ATTERBERG LIMITS**

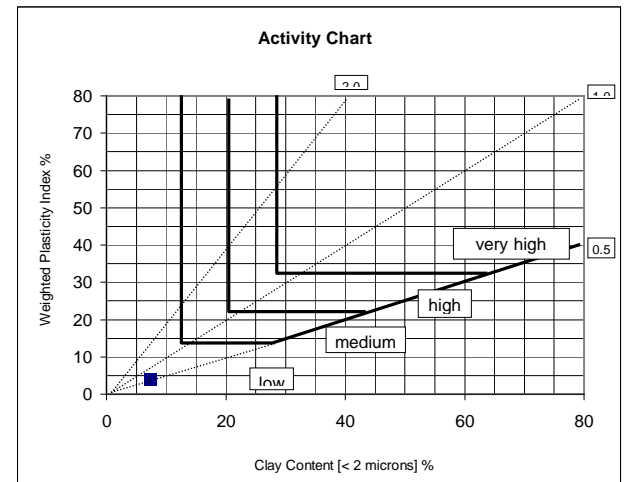
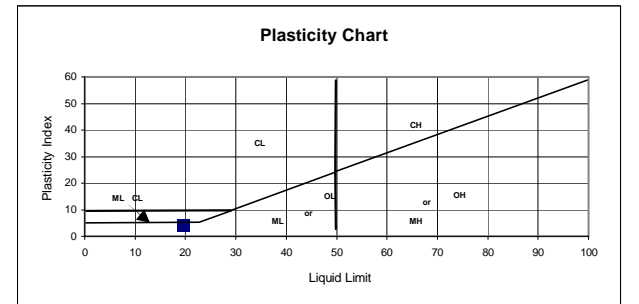
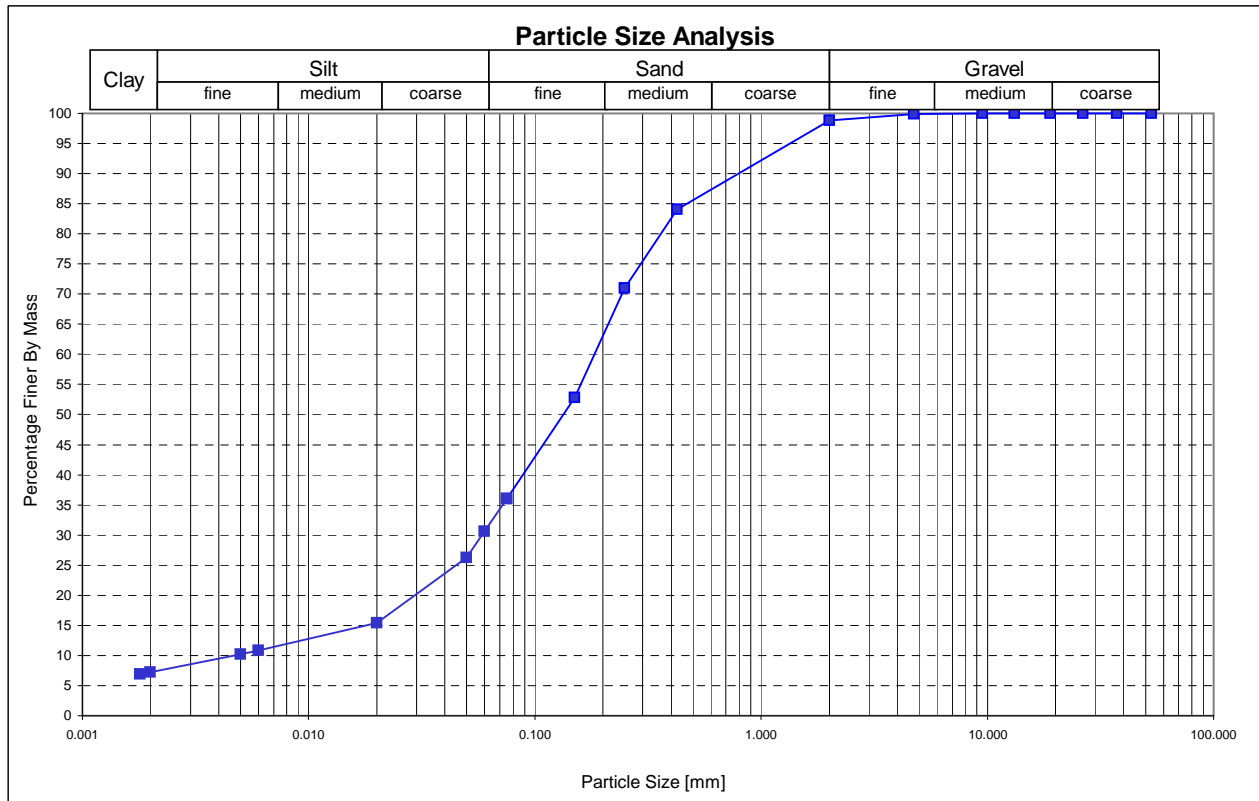
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
20	4	4	2.0	0.81

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
SM/SC	A.4 (0)	

<b>Soil constituents % :</b>	<b>Clay :</b>	7	<b>Silt :</b>	23	<b>Sand :</b>	68	<b>Gravel :</b>	1	<b>Fines :</b>	84	<b>Soil description :</b>	Dark Yellowish Orange Soil
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<b>D<sub>10</sub> :</b>	0.005	<b>D<sub>30</sub> :</b>	0.058	<b>D<sub>60</sub> :</b>	0.184	<b>Uniformity coefficient :</b>	39	<b>Curvature coefficient :</b>	4	<b>Active program :</b>	YES
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REMARKS: none

CHECKED BY : G van Gelder



# Engeo Lab (Pty) Ltd

## INSITU DENSITY & MOISTURE DETERMINATION

JOB NO: 1450 (#990)  
DATE: 1-Mar-2012

Sample Number			0315				
Position			TP 33				
Depth			@ 0.7m				
Mass of sample in air	(g)	a	124.70				
Mass of waxed sample in air	(g)	b	130.10				
Mass of waxed sample in water @ 25°C	(g)	c	55.10				
Mass of water displaced (b - c)	(g)	d	75.00				
Mass of wax (b - a)	(g)	e	5.40				
Density of wax	(kg/m <sup>3</sup> )	f	0.93				
Volume of wax (e / f)	(ml)	g	5.81				
Volume of sample (d - g)	(ml)	h	69.19				
Wet density of sample ( a / h *100 )	(kg/m <sup>3</sup> )	l	1802				
Dry density of sample ( l / (100 + k) * 1000)	(kg/m <sup>3</sup> )	j	<b>1560</b>				
Mass Pan & Wet Mat.	(g)		78 32				
Mass Pan & Dry Mat.	(g)		75 33				
Mass Pan	(g)		55 98				
% Moisture	(%)	k	<b>15.5</b>				
Laboratory Determined Max. Dry Density	(kg/m <sup>3</sup> )	l					
Laboratory Determined O.M.C.	%	m					
Percentage of Max. Dry Density (j/l*100)	%						
Percentage Wet (-) Dry (+) of O.M.C. (m-k)	%						
Specific Gravity			<b>2.61</b>				
Void ratio			0.673				
Degree of saturation	%		60.1				



**FOUNDATION INDICATOR TEST RESULT**

Tests undertaken in terms of TMH 1 Methods: A1a, A2, A3, A4, A5

<b>CLIENT:</b>	GEO 3 CC	<b>PROJECT :</b>	#999
<b>Position :</b>	TP 34	<b>Depth [m] :</b>	0.500-2.100
		<b>Source :</b>	INSITU

<b>Date</b>	<b>Job No.</b>	1450
10-Feb-12	<b>Sample No.</b>	12/0316

**SIEVE ANALYSIS (% PASSING)**

53.0mm	37.5mm	26.5mm	19.0mm	13.2mm	9.5mm	4.75mm	2.0mm	0.425mm	0.250mm	0.150mm	0.075mm	0.060mm	0.050mm	0.020mm	0.006mm	0.005mm	0.002mm	0.0018mm
100	100	100	100	100	100	99	96	87	84	78	65	59	54	40	29	27	17	16

**ATTERBERG LIMITS**

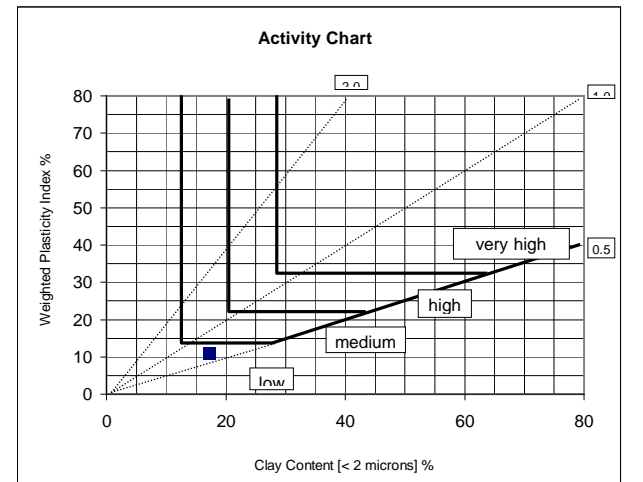
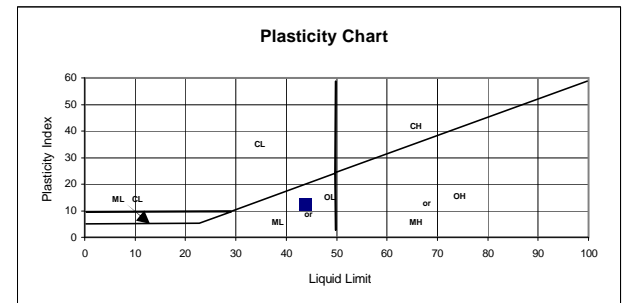
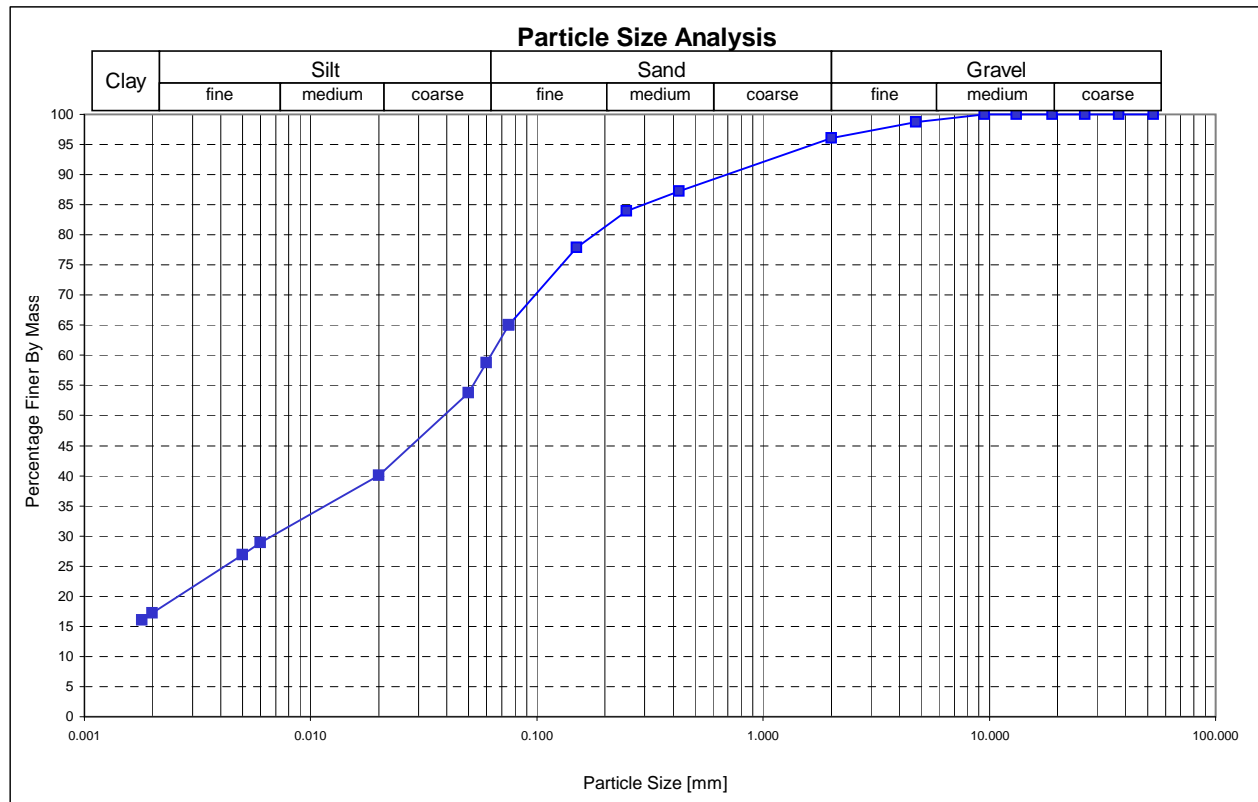
<b>Liquid Limit</b>	<b>Plasticity Index</b>	<b>PI (weighted)</b>	<b>Linear Shrinkage</b>	<b>Grading modulus</b>
44	12	11	5.4	0.52

**CLASSIFICATION**

<b>UNIFIED</b>	<b>PRA</b>	<b>TRH</b>
ML	A.7.5 (8)	

<b>Soil constituents % :</b>	<b>Clay :</b>	17	<b>Silt :</b>	42	<b>Sand :</b>	37	<b>Gravel :</b>	4	<b>Fines :</b>	87	<b>Soil description :</b>	Light Reddish Brown Soil
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<b>D<sub>10</sub> :</b>	<b>D<sub>30</sub> :</b>	0.007	<b>D<sub>60</sub> :</b>	0.063	<b>Uniformity coefficient :</b>		<b>Curvature coefficient :</b>		<b>Active program :</b>	YES
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REMARKS:

none

CHECKED BY : G van Gelder

# Engeo Lab (Pty) Ltd

## INSITU DENSITY & MOISTURE DETERMINATION

JOB NO: 1450 (#990)  
DATE: 1-Mar-2012

Sample Number			0317				
Position			TP 34				
Depth			@ 0.7m				
Mass of sample in air	(g)	a	98.80				
Mass of waxed sample in air	(g)	b	103.00				
Mass of waxed sample in water @ 25°C	(g)	c	45.30				
Mass of water displaced (b - c)	(g)	d	57.70				
Mass of wax (b - a)	(g)	e	4.20				
Density of wax	(kg/m <sup>3</sup> )	f	0.93				
Volume of wax (e / f)	(ml)	g	4.52				
Volume of sample (d - g)	(ml)	h	53.18				
Wet density of sample ( a / h *100 )	(kg/m <sup>3</sup> )	l	1858				
Dry density of sample ( l / (100 + k) * 1000)	(kg/m <sup>3</sup> )	j	<b>1586</b>				
Mass Pan & Wet Mat.	(g)		79 21				
Mass Pan & Dry Mat.	(g)		75 80				
Mass Pan	(g)		55 90				
% Moisture	(%)	k	<b>17.1</b>				
Laboratory Determined Max. Dry Density	(kg/m <sup>3</sup> )	l					
Laboratory Determined O.M.C.	%	m					
Percentage of Max. Dry Density (j/l*100)	%						
Percentage Wet (-) Dry (+) of O.M.C. (m-k)	%						
Specific Gravity			<b>2.62</b>				
Void ratio			0.652				
Degree of saturation	%		68.7				